

# PMP15037 Test Results

### **System Description**

Figure 1 is a basic LED driver circuit where the LED is connected between the Vout pin and the FB pin of the converter. The LED current is determined by  $V_{FB}$  and  $R_S$ . So the higher the FB pin voltage, the higher the loss across the  $R_S$ . Therefore, if we can make  $V_{FB}$  both contributes by the output voltage and the LED current, then the conversion efficiency can be greatly improved.

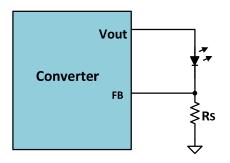


Figure 1. Basic LED driver circuit

TPS61021A is a high efficiency synchronous boost converter. It isolates the output from the input side when shutdown. So it can help to reduce the battery loss when the LED is turned off.

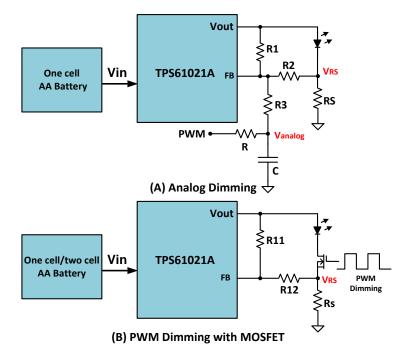


Figure 2. Block Diagram of the PMP15037



The block diagram of reference design PMP15037 is shown in Figure 2. This reference design delivers a high efficiency LED driver circuit with dimming function with the boost converter TPS61021A. The PWM dimming method (Figure 1. (A)) can be used in the one cell or two cell AA battery input application. The analog dimming method (Figure 1. (B)) can be used in the one cell AA battery input application. The TI design PMP15037 is very simple, it realizes the dimming function by just adding several resistors and one MOSFET into the circuit. So this is a low cost and high efficiency solution for the LED driver application.

Table 1 gives out the performance specification of the TI design PMP15037 under PWM dimming. It has 0.5A output current capability at one cell AA battery input application and has 1A output current capability at two cell AA battery input applications.

Input Voltage Range(V)	Maximum LED Current(A)	Dimming Frequency(HZ)
One cell AA Battery	0.5 (R1=383k)	200-1k
Two cell AA Battery	<b>1</b> (R1=523k)	200-1k

#### Table 1 Performance Specification under the PWM Dimming

Table 2 gives out the performance specification of the TI design PMP15037 under analog dimming. It has 0.5A output current capability at one cell AA battery input application. It has no limit on the dimming frequency since the dimming depth is only determined by the analog voltage level V<sub>ANALOG</sub> added to the FB pin. Two cell AA battery input is not supported under the analog dimming method.

Table 2 Performance Specification under the Analog Dimming

Input Voltage Range(V)	Maximum LED Current(A)	Dimming Frequency(HZ)
One cell AA Battery	0.5	Not limited

## **Design Theory**

Figure 2.1 shows the schematic of the TI design PMP15037 under analog dimming. R5 and C6 forms a RC filter, it converts the PWM signal PWM1 to the analog signal  $V_{ANALOG}$ . The voltage level of  $V_{ANALOG}$  changes in accordance with the duty cycle of PWM1. The high voltage level of PWM1 set at 3V, the low voltage level of PWM1 set at GND in this TI design.

When the duty cycle of PWM1 is 0%,  $V_{ANALOG}$  is 0 V. The LED is always on. The current flowing through the LED is a DC current, which is set at 0.5A in this TI design. The FB pin voltage is determined by the output voltage  $V_{OUT1}$  and the voltage  $V_{RS}$  across the sense resistor.

$$V_{OUT1} \times \frac{R_{p1}}{R_{p1} + R1} + V_{RS} \times \frac{R_{p2}}{R_{p2} + R2} = V_{FB}$$
(1)

Where

- $V_{OUT1}$  is the TPS61021's output voltage when LED current is 0.5A,  $V_{OUT1}$ =3.2V.
- V<sub>FB</sub> is the TPS61021's feedback regulation voltage (V<sub>FB</sub>=0.795V).



• 
$$R_{p1} = \frac{R2 \times R3}{R2 + R3}$$
,  $R_{p2} = \frac{R1 \times R3}{R1 + R3}$ 

•  $V_{RS} = I_{LED} \times R_S = 0.5 \times 0.3 = 0.15V$ 

When the duty cycle of PWM1 is 100%,  $V_{ANALOG}$  is 3V. The LED is off. The FB pin voltage is contributed by the output voltage  $V_{OUT2}$  and  $V_{ANALOG}$  at this time.

$$V_{OUT2} \times \frac{R_{p1}}{R_{p1} + R1} + V_{ANALOG} \times \frac{R_{p3}}{R_{p3} + R3} = V_{FB}$$
(2)

Where

•  $V_{OUT2}$  is the TPS61021's output voltage when LED off,  $V_{OUT2}$ =2.7V.

• 
$$R_{p3} = \frac{R1 \times R2}{R1 + R2}$$

From equation (1) and (2), equation (3) and equation (4) can be deduced:

$$V_{OUT1} \times \frac{R_{p1}}{R_{p1} + R1} + V_{RS} \times \frac{R_{p2}}{R_{p2} + R2} = V_{OUT2} \times \frac{R_{p1}}{R_{p1} + R1} + V_{ANALOG} \times \frac{R_{p3}}{R_{p3} + R3}$$
(3)

$$(V_{OUT1} - V_{OUT2}) \times \frac{R_{p1}}{R_{p1} + R1} + V_{RS} \times \frac{R_{p2}}{R_{p2} + R2} = V_{ANALOG} \times \frac{R_{p3}}{R_{p3} + R3}$$
(4)

In equation (4), set R2=200k, R3=2M, thus Rp1=181.8k. So only R1 is an unknown number. We can get equation (5) and (6):

$$(V_{OUT1} - V_{OUT2}) \times \frac{181.8}{181.8 + R1} + V_{RS} \times \frac{\frac{R1 \times 2000}{R1 + 2000}}{\frac{R1 \times 2000}{R1 + 2000} + 200} = V_{ANALOG} \times \frac{\frac{R1 \times 200}{R1 + 200}}{\frac{R1 \times 200}{R1 + 200} + 2000}$$
(5)  
$$0.5 \times \frac{181.8}{181.8 + R1} + 0.15 \times \frac{\frac{R1 \times 2000}{R1 + 2000}}{\frac{R1 \times 2000}{R1 + 2000} + 200} = 3 \times \frac{\frac{R1 \times 200}{R1 + 200}}{\frac{R1 \times 200}{R1 + 200} + 2000}$$
(6)

Solving equation (6), we can get R1≈ 665k ohm.



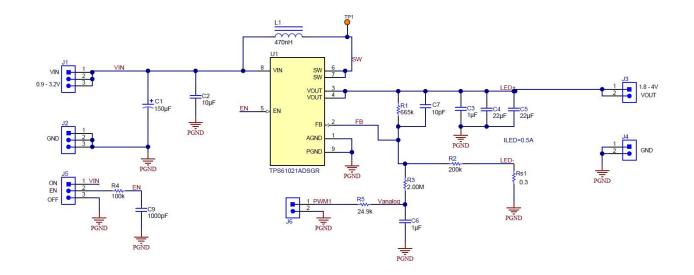
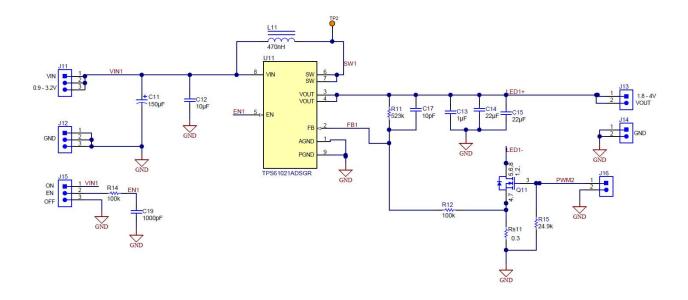


Figure 2.1 Schematic of the PMP15037 (Analog Dimming)



#### Figure 2.2 Schematic of the PMP15037 (PWM Dimming)

Figure 2.2 shows the schematic of the TI design PMP15037 under PWM dimming. When MOSFET Q11 is fully on, the FB pin voltage is contributed by the output voltage VOUT and the voltage  $V_{RS}$  across the sense resistor.

$$V_{OUT} \times \frac{R12}{R11 + R12} + V_{RS} \times \frac{R11}{R11 + R12} = V_{FB}$$
(7)

Where



- V<sub>OUT</sub> is the TPS61021's output voltage when LED current is 1A, V<sub>OUT</sub>=3.4V.
- $V_{RS} = I_{LED} \times R_{S11} = 1 \times 0.3 = 0.3V$

Set R12=100k ohm. Then R11 is the only unknown value in the above equation.

$$R11 = \frac{(V_{OUT} - V_{FB}) \times R12}{(V_{FB} - V_{RS})}$$
(8)

Solving equation (8), we can get R11≈523k ohm in this TI design.

## **Test Result**

Figure 3 shows the LED current versus the PWM duty cycle under analog dimming. The LED current changes in accordance with the PWM duty cycle, which is the voltage level of  $V_{ANALOG}$  under analog dimming.

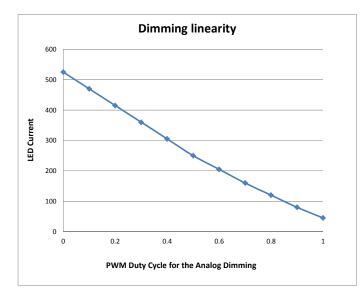


Figure 3. LED Current VS. PWM Duty Cycle under Analog Dimming



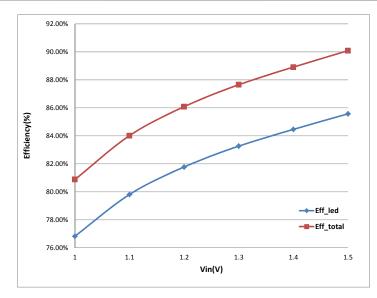


Figure 4. Conversion Efficiency under Analog Dimming (Io=0.5A)

Figure 4 shows the conversion efficiency under analog dimming when the sense resistor is 0.3 ohm. Reducing the sense resistor from 0.3 ohm to 0.15 ohm can increase the conversion efficiency by 2%.

Figure 5 shows the conversion efficiency under PWM dimming at different dimming frequency. When MOSFET Q11 is fully on, the LED current is 1A. So the average current flowing through the LED is 0.5A at 50% duty cycle and 0.95A at 95% duty cycle.

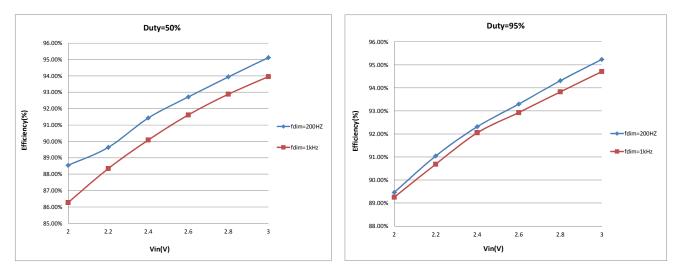


Figure 5. Conversion Efficiency under PWM Dimming

#### IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATASHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, or other requirements. These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to TI's Terms of Sale (https://www.ti.com/legal/termsofsale.html) or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2021, Texas Instruments Incorporated