







TPS563201, TPS563208 SLVSD90A - DECEMBER 2015 - REVISED APRIL 2024

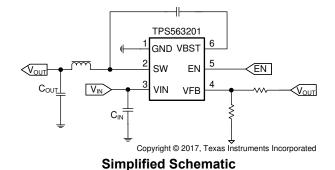
# TPS56320x 4.5V to 17V Input, 3A Synchronous Step-Down Voltage Regulator in **SOT-23**

#### 1 Features

- TPS563201 and TPS563208 3A converter integrated  $95m\Omega$  and  $57m\Omega$  FETs
- D-CAP2<sup>™</sup> control scheme with fast transient response
- Input voltage range: 4.5V to 17V
- Output voltage range: 0.76V to 7V
- Pulse-skip mode (TPS563201) or continuous current mode (TPS563208)
- 580kHz switching frequency
- Low shutdown current less than 20µA
- 2% feedback voltage accuracy (25°C)
- Startup from prebiased output voltage
- Cycle-by-cycle overcurrent limit
- Hiccup-mode overcurrent protection
- Non-latch UVP and TSD protections
- Fixed soft start: 1.0ms
- Create a custom design using the TPS56320x with the WEBENCH® Power Designer

### 2 Applications

- Digital TV power supply
- High definition Blu-ray<sup>™</sup> disc players
- Networking home terminal
- Digital Set Top Box (STB)
- Surveillance



# 3 Description

The TPS563201 and TPS563208 are simple, easy-touse, 3A synchronous step-down converters in SOT-23 package.

The devices are designed to operate with minimum external component counts and also designed to achieve low standby current.

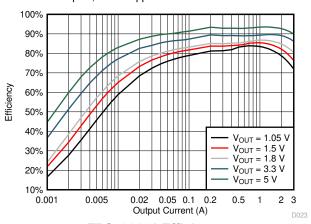
These switch mode power supply (SMPS) devices employ D-CAP2 control scheme providing a fast transient response and supporting both low equivalent series resistance (ESR) output capacitors such as specialty polymer and ultra-low ESR ceramic capacitors with no external compensation components.

The TPS563201 operates in pulse skip mode, which maintains high efficiency during light load operation. The TPS563201 and TPS563208 are available in a 6-pin 1.6mm × 2.9mm SOT (DDC) package, and specified from a –40°C to 125°C junction temperature.

#### **Device Information**

PART NUMBER	MODE	PACKAGE <sup>(1)</sup>	PACKAGE SIZE <sup>(2)</sup>
TPS563201	ECO	DDC (SOT, 6)	1.6mm × 2.9mm
TPS563208	FCCM	000 (301, 0)	1.0111111 ^ 2.9111111

- For more information, see Section 10.
- The package size (length × width) is a nominal value and includes pins, where applicable.



TPS563201 Efficiency



# **Table of Contents**

1 Features	1	7 Application and Implementation	13
2 Applications		7.1 Application Information	
3 Description		7.2 Typical Application	
4 Pin Configuration and Functions		7.3 Power Supply Recommendations	
5 Specifications	4	7.4 Layout	19
5.1 Absolute Maximum Ratings		8 Device and Documentation Support	
5.2 ESD Ratings		8.1 Device Support	
5.3 Recommended Operating Conditions	4	8.2 Receiving Notification of Documentation Updates	21
5.4 Thermal Information	<mark>5</mark>	8.3 Support Resources	21
5.5 Electrical Characteristics	6	8.4 Trademarks	21
5.6 Typical Characteristics	7	8.5 Electrostatic Discharge Caution	21
6 Detailed Description	10	8.6 Glossary	21
6.1 Overview		9 Revision History	22
6.2 Functional Block Diagram	10	10 Mechanical, Packaging, and Orderable	
6.3 Feature Description		Information	22
6.4 Device Functional Modes	12		



# 4 Pin Configuration and Functions

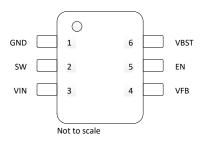


Figure 4-1. DDC Package 6-Pin SOT Top View

**Table 4-1. Pin Functions** 

PIN		TYPE <sup>(1)</sup>	DESCRIPTION		
NAME	NO.	1115 = 1	DESCRIPTION		
GND	1	_	Ground pin Source terminal of low-side power NFET as well as the ground terminal for controller circuit. Connect sensitive VFB to this GND at a single point.		
SW 2 O Switch node connection b		0	Switch node connection between high-side NFET and low-side NFET.		
VIN	3	I	Input voltage supply pin. The drain terminal of high-side power NFET.		
VFB	4	I	Converter feedback input. Connect to output voltage with feedback resistor divider.		
EN	5	I	Enable input control. Active high and must be pulled up to enable the device.		
VBST 6		0	Supply input for the high-side NFET gate drive circuit. Connect 0.1 µF capacitor between VBST and SW pins.		

(1) I = input, O = output



### **5 Specifications**

## 5.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)(1)

		MIN	MAX	UNIT
	VIN, EN	-0.3	19	V
	VBST	-0.3	25	V
	VBST (10 ns transient)	-0.3	27	V
Input voltage	VBST (vs SW)	-0.3	6	V
	VFB	-0.3	6	V
	SW	-2	19	V
	SW (10 ns transient)	-3.5	21	V
Operating junction tempera	ature, T <sub>J</sub>	-40	150	°C
Storage temperature, T <sub>stg</sub>		<b>-</b> 55	150	°C

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 5.2 ESD Ratings

			VALUE	UNIT
		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	
V <sub>(ESD)</sub>	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1500	V

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

#### 5.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

			MIN	NOM	MAX	UNIT	
V <sub>IN</sub>	Supply input voltage range		4.5		17	V	
		VBST	-0.1		23		
		VBST (10 ns transient)	-0.1	-	26		
		VBST (vs SW)	-0.1		5.5		
VI	Input voltage range	EN	-0.1		17	_	
		VFB	-0.1	,	5.5		
		SW	-1.8		17		
		SW (10 ns transient)	-3.5		20		
TJ	Operating junction temperature	,	-40		125	°C	

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### **5.4 Thermal Information**

		TPS56320x	
	THERMAL METRIC <sup>(1)</sup>	DDC (SOT)	UNIT
		6 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	92.6	°C/W
R <sub>0JC(top)</sub>	Junction-to-case (top) thermal resistance	48.5	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	15.5	°C/W
ΨЈТ	Junction-to-top characterization parameter	2.5	°C/W
ΨЈВ	Junction-to-board characterization parameter	15.5	°C/W

<sup>(1)</sup> For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application



### **5.5 Electrical Characteristics**

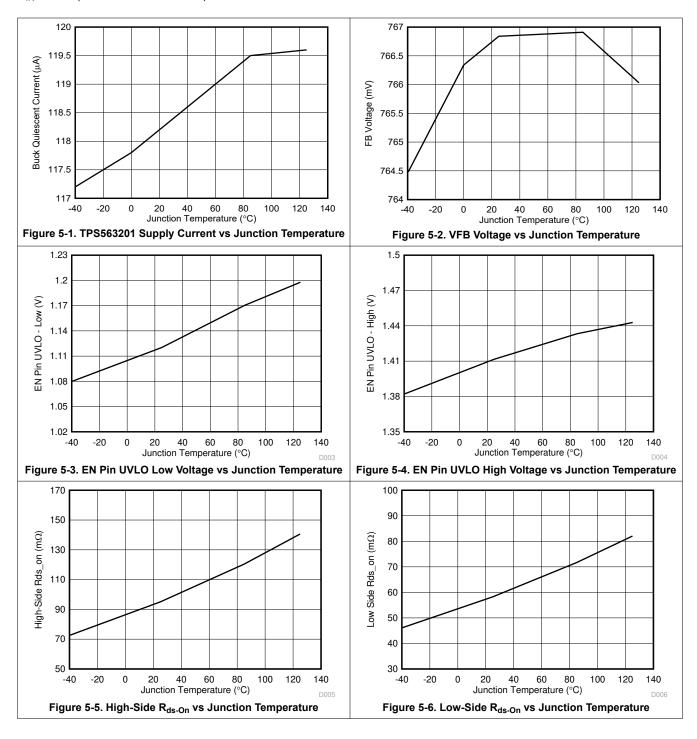
 $T_J = -40$ °C to 125°C,  $V_{IN} = 12$  V (unless otherwise noted)

	PARAMETER	TEST CONDITION	NS	MIN	TYP	MAX	UNIT
SUPPLY CUF	RRENT						
	Operating – non-switching		TPS563201		120	200	
$I_{VIN}$	supply current	$V_{IN}$ current, EN = 5 V, $V_{FB}$ = 0.9 V	TPS563208		350	500	μA
I <sub>VINSDN</sub>	Shutdown supply current	V <sub>IN</sub> current, EN = 0 V			8	20	μA
LOGIC THRE	SHOLD					I	
V <sub>ENH</sub>	EN high-level input voltage			1.6			V
V <sub>ENL</sub>	EN low-level input voltage					8.0	V
R <sub>EN</sub>	EN pin resistance to GND	V <sub>EN</sub> = 1.5 V		600	1500	2400	kΩ
I <sub>EN</sub>	EN pulldown current	V <sub>EN</sub> = 1.5 V			1		μΑ
V <sub>FB</sub> VOLTAG	E AND DISCHARGE RESISTA	NCE					
	V <sub>FB</sub> threshold voltage <sup>(1)</sup>	V <sub>O</sub> = 1.05 V, I <sub>O</sub> = 10 mA, Eco-mode	operation		774		mV
$V_{FBTH}$	V <sub>FB</sub> threshold voltage	V <sub>O</sub> = 1.05 V, continuous mode oper	ation	749	768	787	mV
I <sub>VFB</sub>	V <sub>FB</sub> input current	V <sub>FB</sub> = 0.8 V			0	±0.1	μΑ
MOSFET				•			
R <sub>DS(on)h</sub>	High-side switch resistance	T <sub>A</sub> = 25°C, V <sub>BST</sub> – SW = 5 V			95		mΩ
R <sub>DS(on)I</sub>	Low-side switch resistance	T <sub>A</sub> = 25°C			57		mΩ
CURRENT LI	MIT			•		1	
I <sub>ocl</sub>	Current limit	DC current, V <sub>OUT</sub> = 1.05 V, L <sub>1</sub> = 1.5 μH		3.3	4.2	5.1	Α
THERMAL SI	HUTDOWN						
т	Thermal shutdown threshold	Shutdown temperature		172		°C	
T <sub>SDN</sub>	(1) Hysteresis				37		C
ON-TIME TIM	ER CONTROL			•		1	
t <sub>OFF(MIN)</sub>	Minimum off time	V <sub>FB</sub> = 0.5 V			220	310	ns
SOFT START	•						
Tss	Soft-start time	Internal soft-start time			1.0		ms
FREQUENCY	•			•		•	
F <sub>sw</sub>	Switching frequency	V <sub>IN</sub> = 12 V, V <sub>O</sub> = 1.05 V, FCCM mod	le		580		kHz
OUTPUT UNI	DERVOLTAGE AND OVERVO	LTAGE PROTECTION		•		,	
V <sub>UVP</sub>	Output UVP threshold	Hiccup detect (H > L)			65%		
T <sub>HICCUP_WAIT</sub>	Hiccup on time				1.2		ms
T <sub>HICCUP_RE</sub>	Hiccup time before restart				10		ms
UVLO						'	
		Wake up VIN voltage			3.8	4.3	
UVLO	UVLO threshold	Shutdown VIN voltage	3.3	3.4		V	
		Hysteresis VIN voltage			0.4		

(1) Not production tested.

### **5.6 Typical Characteristics**

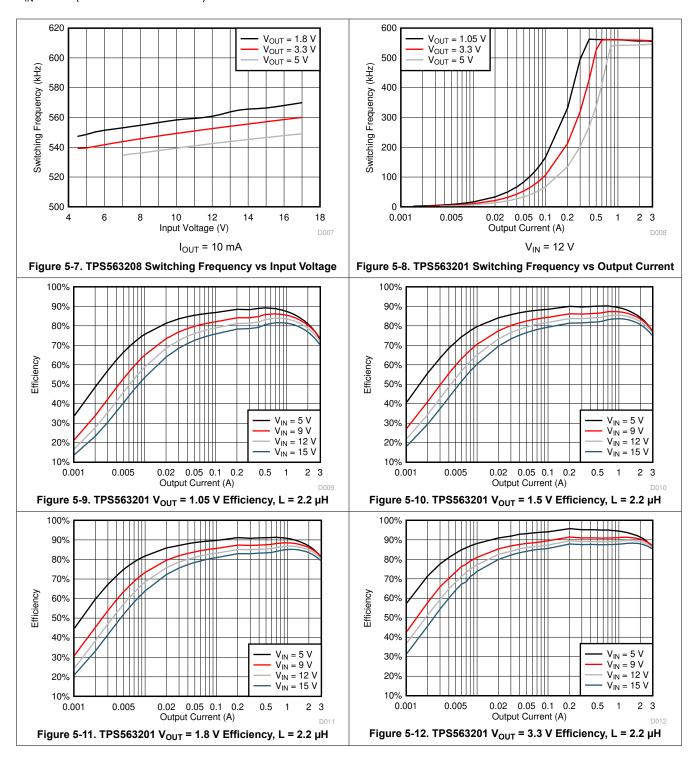
V<sub>IN</sub> = 12 V (unless otherwise noted)





### 5.6 Typical Characteristics (continued)

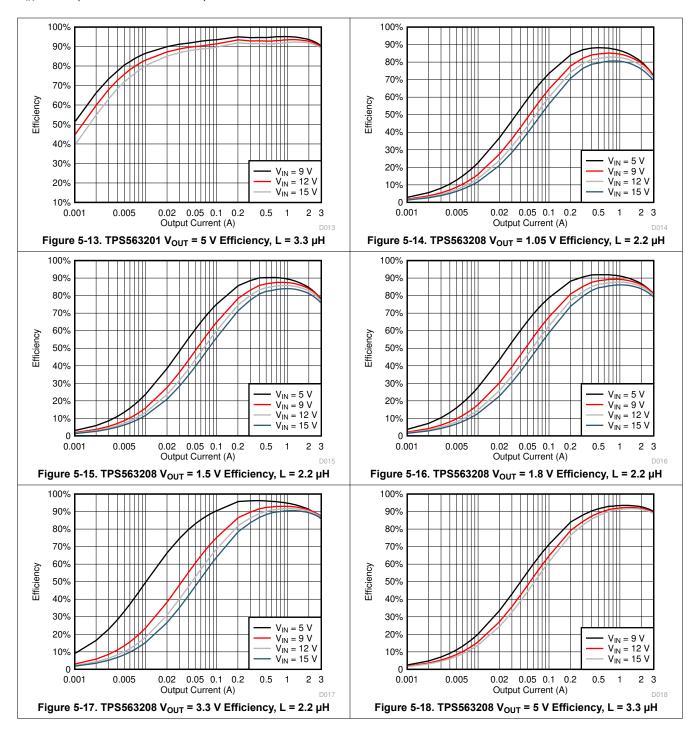
V<sub>IN</sub> = 12 V (unless otherwise noted)





### 5.6 Typical Characteristics (continued)

V<sub>IN</sub> = 12 V (unless otherwise noted)

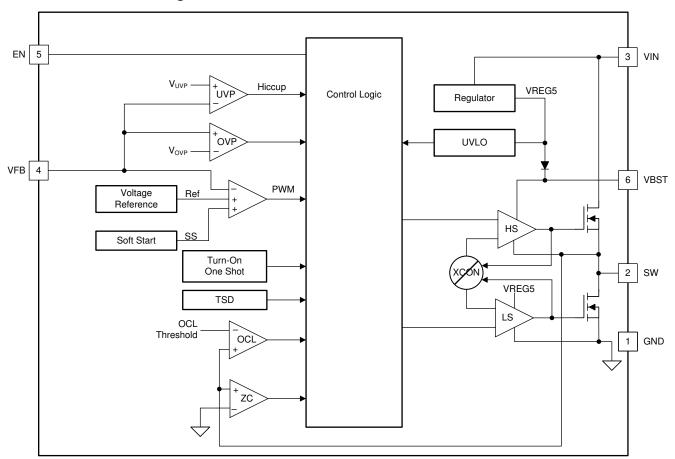


### **6 Detailed Description**

#### 6.1 Overview

The TPS563201 and TPS563208 are 3-A synchronous step-down converters. The proprietary D-CAP2 control scheme supports low ESR output capacitors such as specialty polymer capacitors and multi-layer ceramic capacitors without complex external compensation circuits. The fast transient response of D-CAP2 control scheme can reduce the output capacitance required to meet a specific level of performance.

### 6.2 Functional Block Diagram



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#### **6.3 Feature Description**

#### 6.3.1 Adaptive On-Time Control and PWM Operation

The main control loop of the TPS563201 and TPS563208 is adaptive on-time pulse width modulation (PWM) controller that supports a proprietary D-CAP2 control scheme. The D-CAP2 control scheme combines adaptive on-time control with an internal compensation circuit for pseudo-fixed frequency and low external component count configuration with both low-ESR and ceramic output capacitors. It is stable even with virtually no ripple at the output.

At the beginning of each cycle, the high-side MOSFET is turned on. This MOSFET is turned off after internal one shot timer expires. This one shot duration is set proportional to the converter input voltage, VIN, and inversely proportional to the output voltage, V<sub>O</sub>, to maintain a pseudo-fixed frequency over the input voltage range, hence it is called adaptive on-time control. The one-shot timer is reset and the high-side MOSFET is turned on again when the feedback voltage falls below the reference voltage. An internal ramp is added to reference voltage to simulate output ripple, eliminating the need for ESR induced output ripple from D-CAP2 control scheme.

#### 6.3.2 Pulse Skip Control (TPS563201)

The TPS563201 is designed with advanced Eco-mode to maintain high light load efficiency. As the output current decreases from heavy load condition, the inductor current is also reduced and eventually comes to point that its rippled valley touches zero level, which is the boundary between continuous conduction and discontinuous conduction modes. The rectifying MOSFET is turned off when the zero inductor current is detected. As the load current further decreases the converter runs into discontinuous conduction mode. The on-time is kept almost the same as it was in the continuous conduction mode so that it takes longer time to discharge the output capacitor with smaller load current to the level of the reference voltage. This makes the switching frequency lower, proportional to the load current, and keeps the light load efficiency high. The transition point to the light load operation  $I_{OUT(LL)}$  current can be calculated in Equation 1.

$$I_{OUT(LL)} = \frac{1}{2 \times L \times f_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}}$$
(1)

#### 6.3.3 Soft Start and Pre-Biased Soft Start

The TPS563201 and TPS563208 have an internal 1-ms soft-start. When the EN pin becomes high, the internal soft-start function begins ramping up the reference voltage to the PWM comparator.

If the output capacitor is pre-biased at startup, the devices initiate switching and start ramping up only after the internal reference voltage becomes greater than the feedback voltage  $V_{FB}$ . This scheme ensures that the converters ramp up smoothly into regulation point.

#### 6.3.4 Current Protection

The output over-current limit (OCL) is implemented using a cycle-by-cycle valley detect control circuit. The switch current is monitored during the OFF state by measuring the low-side FET drain to source voltage. This voltage is proportional to the switch current. To improve accuracy, the voltage sensing is temperature compensated.

During the on time of the high-side FET switch, the switch current increases at a linear rate determined by Vin, Vout, the on-time and the output inductor value. During the on time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current I<sub>out</sub>. If the monitored current is above the OCL level, the converter maintains low-side FET on and delays the creation of a new set pulse, even the voltage feedback loop requires one, until the current level becomes OCL level or lower. In subsequent switching cycles, the on-time is set to a fixed value and the current is monitored in the same manner.

There are some important considerations for this type of over-current protection. The load current is higher than the over-current threshold by one half of the peak-to-peak inductor ripple current. Also, when the current is being limited, the output voltage tends to fall as the demanded load current may be higher than the current available from the converter. This may cause the output voltage to fall. When the VFB voltage falls below the UVP threshold voltage, the UVP comparator detects it. And then, the device will shut down after the UVP delay time (typically 256 µs) and re-start after the hiccup time (typically 10 ms).

When the over current condition is removed, the output voltage returns to the regulated value.

### 6.3.5 Undervoltage Lockout (UVLO) Protection

UVLO protection monitors the internal regulator voltage. When the voltage is lower than UVLO threshold voltage, the device is shut off. This protection is non-latching.

#### 6.3.6 Thermal Shutdown

The device monitors the temperature of itself. If the temperature exceeds the threshold value (typically 172°C), the device is shut off. This is a non-latch protection.



#### 6.4 Device Functional Modes

### 6.4.1 Normal Operation

When the input voltage is above the UVLO threshold and the EN voltage is above the enable threshold, the TPS563201 and TPS563208 can operate in their normal switching modes. Normal continuous conduction mode (CCM) occurs when the minimum switch current is above 0 A. In CCM, the TPS563201 and TPS563208 operate at a quasi-fixed frequency of 580 kHz.

#### 6.4.2 Eco-mode Operation

When the TPS563201 and TPS563208 are in the normal CCM operating mode and the switch current falls to 0 A, the TPS563201 and TPS563208 begin operating in pulse skipping Eco-mode. Each switching cycle is followed by a period of energy saving sleep time. The sleep time ends when the VFB voltage falls below the Eco-mode threshold voltage. As the output current decreases, the perceived time between switching pulses increases.

#### 6.4.3 Standby Operation

When the TPS563201 and TPS563208 are operating in either normal CCM or Eco-mode, they may be placed in standby by asserting the EN pin low.

Product Folder Links: TPS563201 TPS563208

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### 7 Application and Implementation

#### **Note**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 7.1 Application Information

The devices are typical step-down DC-DC converters. It typically uses to convert a higher dc voltage to a lower dc voltage with a maximum available output current of 3 A. The following design procedure can be used to select component values for the TPS563201 and TPS563208. Alternately, the WEBENCH® software may be used to generate a complete design. The WEBENCH software uses an iterative design procedure and accesses a comprehensive database of components when generating a design. This section presents a simplified discussion of the design process.

### 7.2 Typical Application

The application schematic in Figure 7-1 was developed to meet the previous requirements. This circuit is available as the evaluation module (EVM). The sections provide the design procedure.

Figure 7-1 shows the TPS563201 and TPS563208 4.5-V to 17-V input, 1.05-V output converter schematics.

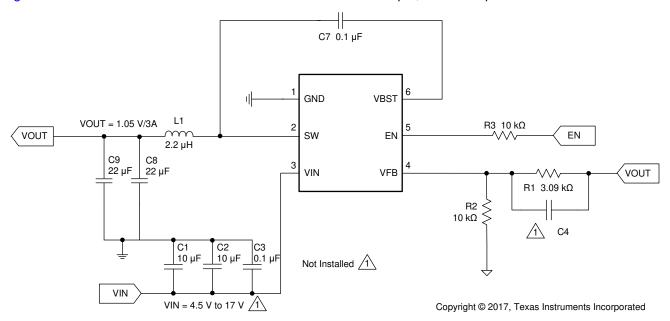


Figure 7-1. TPS563201 and TPS563208 1.05-V/3-A Reference Design

#### 7.2.1 Design Requirements

Table 7-1 shows the design parameters for this application.

Table 7-1. Design Parameters

PARAMETER	EXAMPLE VALUE
Input voltage range	4.5 to 17 V
Output voltage	1.05 V
Transient response, 1.5-A load step	ΔVout = ±5%
Input ripple voltage	400 mV
Output ripple voltage	30 mV
Output current rating	3 A
Operating frequency	580 kHz

#### 7.2.2 Detailed Design Procedure

### 7.2.2.1 Custom Design with WEBENCH® Tools

Click here to create a custom design using the TPS56320x device with the WEBENCH® Power Designer.

- 1. Start by entering the input voltage  $(V_{IN})$ , output voltage  $(V_{OUT})$ , and output current  $(I_{OUT})$  requirements.
- 2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
- 3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- · Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at www.ti.com/WEBENCH.

#### 7.2.2.2 Output Voltage Resistors Selection

The output voltage is set with a resistor divider from the output node to the VFB pin. TI recommends to use 1% tolerance or better divider resistors. Start by using Equation 2 to calculate V<sub>OUT</sub>.

To improve efficiency at very light loads consider using larger value resistors, too high of resistance will be more susceptible to noise and voltage errors from the VFB input current will be more noticeable.

$$V_{OUT} = 0.768 \times \left(1 + \frac{R1}{R2}\right) \tag{2}$$

#### 7.2.2.3 Output Filter Selection

The LC filter used as the output filter has double pole at:

$$f_{P} = \frac{1}{2\pi\sqrt{L_{OUT} \times C_{OUT}}}$$
 (3)

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the device. The low frequency phase is 180°. At the output filter pole frequency, the gain rolls off at a –40 dB per decade rate and the phase drops rapidly. D-CAP2 control scheme introduces a high frequency zero that reduces the gain roll off to –20 dB per decade and increases the phase to 90° one decade above the zero frequency. The inductor and capacitor for the output filter must be selected so that the double pole of Equation 3



is located below the high frequency zero but close enough that the phase boost provided be the high frequency zero provides adequate phase margin for a stable circuit. To meet this requirement use the values recommended in Table 7-2.

Table 7-2. Neconiniended Component Values							
OUTPUT VOLTAGE	R1 (kΩ)	R2 (kΩ)	L1 (µH)	C8 + C9 (µF)			
(V)	K1 (K12)	K2 (K12)	MIN	TYP	MAX	C6 + C9 (μΓ)	
1	3.09	10.0	1.5	2.2	4.7	20 to 68	
1.05	3.74	10.0	1.5	2.2	4.7	20 to 68	
1.2	5.76	10.0	1.5	2.2	4.7	20 to 68	
1.5	9.53	10.0	1.5	2.2	4.7	20 to 68	
1.8	13.7	10.0	1.5	2.2	4.7	20 to 68	
2.5	22.6	10.0	2.2	2.2	4.7	20 to 68	
3.3	33.2	10.0	2.2	2.2	4.7	20 to 68	
5	54.9	10.0	3.3	3.3	4.7	20 to 68	
6.5	75	10.0	3.3	3.3	4.7	20 to 68	

Table 7-2. Recommended Component Values

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using Equation 4, Equation 5, and Equation 6. The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current.

$$II_{P-P} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}}$$
(4)

$$II_{PEAK} = I_O + \frac{II_{P-P}}{2} \tag{5}$$

$$I_{LO(RMS)} = \sqrt{I_O^2 + \frac{1}{12}II_{P-P}^2}$$
 (6)

For this design example, the calculated peak current is 3.5 A and the calculated RMS current is 3.01 A. The inductor used is a WE 74431122 with a peak current rating of 13 A and an RMS current rating of 9 A.

The capacitor value and ESR determines the amount of output voltage ripple. The TPS563201 and TPS563208 are intended for use with ceramic or other low ESR capacitors. Recommended values range from 20  $\mu$ F to 68  $\mu$ F. Use Equation 7 to determine the required RMS current rating for the output capacitor.

$$I_{CO(RMS)} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{\sqrt{12} \times V_{IN} \times L_O \times f_{SW}}$$
(7)

For this design two TDK C3216X5R0J226M 22- $\mu$ F output capacitors are used. The typical ESR is 2 m $\Omega$  each. The calculated RMS current is 0.286 A and each output capacitor is rated for 4 A.

#### 7.2.2.4 Input Capacitor Selection

The TPS563201 and TPS563208 require an input decoupling capacitor and a bulk capacitor is needed depending on the application. TI recommends a ceramic capacitor over 10 µF for the decoupling capacitor. An additional 0.1-µF capacitor (C3) from pin 3 to ground is optional to provide additional high frequency filtering. The capacitor voltage rating needs to be greater than the maximum input voltage.

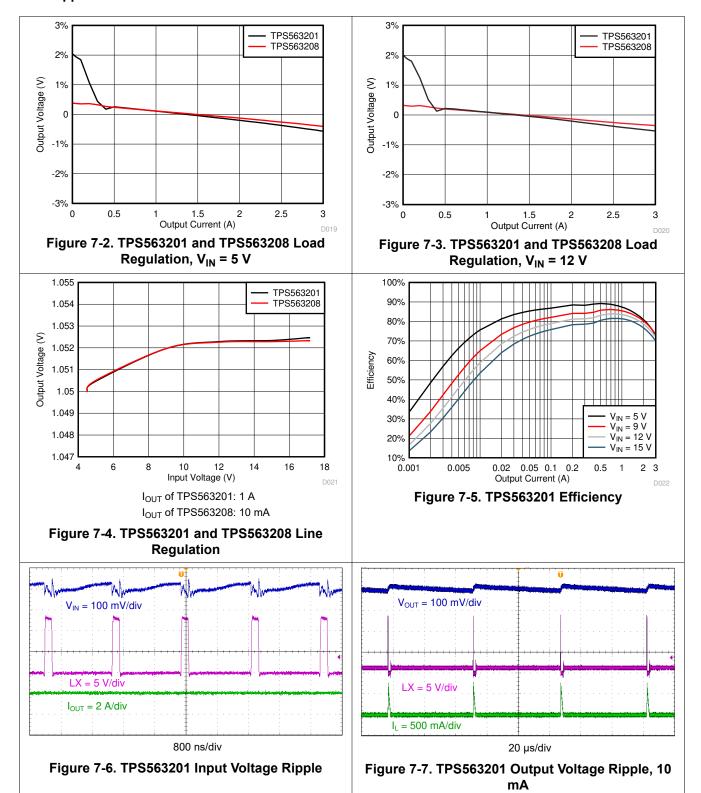


### 7.2.2.5 Bootstrap Capacitor Selection

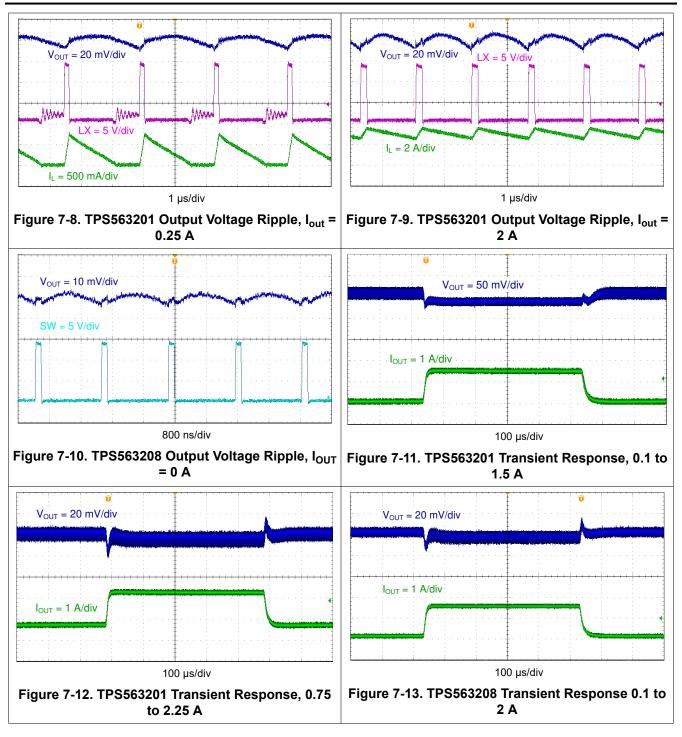
A 0.1- $\mu F$  ceramic capacitor must be connected between the VBST to SW pin for proper operation. TI recommends to use a ceramic capacitor.

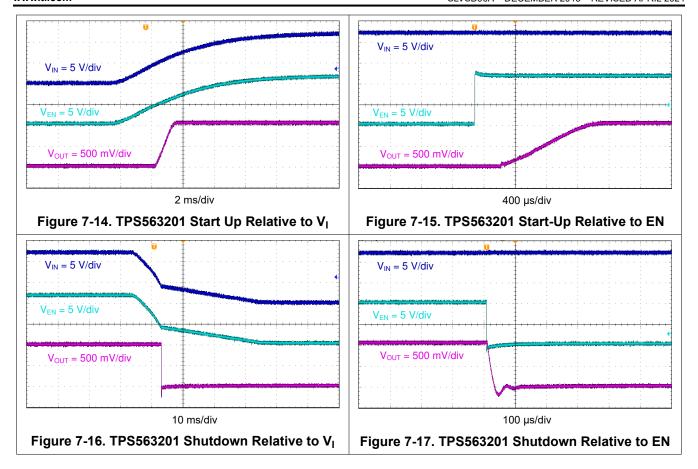


### 7.2.3 Application Curves









### 7.3 Power Supply Recommendations

TPS563201 and TPS563208 are designed to operate from input supply voltage in the range of 4.5 V to 17 V. Buck converters require the input voltage to be higher than the output voltage for proper operation. The maximum recommended operating duty cycle is 75%. Using that criteria, the minimum recommended input voltage is  $V_{\rm O}$  / 0.75.

### 7.4 Layout

### 7.4.1 Layout Guidelines

- VIN and GND traces should be as wide as possible to reduce trace impedance. The wide areas are also of advantage from the view point of heat dissipation.
- 2. The input capacitor and output capacitor should be placed as close to the device as possible to minimize trace impedance.
- 3. Provide sufficient vias for the input capacitor and output capacitor.
- 4. Keep the SW trace as physically short and wide as practical to minimize radiated emissions.
- 5. Do not allow switching current to flow under the device.
- 6. A separate VOUT path should be connected to the upper feedback resistor.
- 7. Make a Kelvin connection to the GND pin for the feedback path.
- 8. Voltage feedback loop should be placed away from the high-voltage switching trace, and preferably has ground shield.
- 9. The trace of the VFB node should be as small as possible to avoid noise coupling.
- 10. The GND trace between the output capacitor and the GND pin should be as wide as possible to minimize its trace impedance.



### 7.4.2 Layout Example

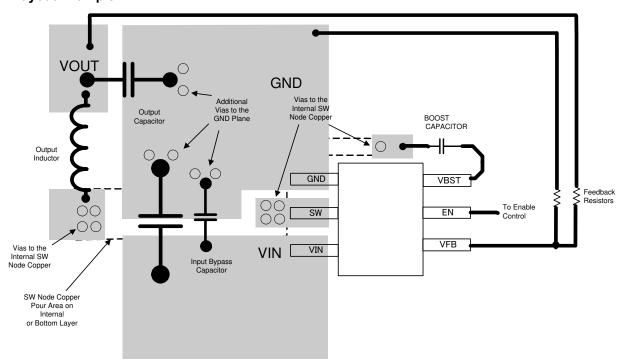


Figure 7-18. TPS563201 and TPS563208 Layout



## 8 Device and Documentation Support

### 8.1 Device Support

### 8.1.1 Development Support

#### 8.1.1.1 Custom Design with WEBENCH® Tools

Click here to create a custom design using the TPS56320x device with the WEBENCH® Power Designer.

- 1. Start by entering the input voltage  $(V_{IN})$ , output voltage  $(V_{OUT})$ , and output current  $(I_{OUT})$  requirements.
- 2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
- 3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- · Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at www.ti.com/WEBENCH.

#### 8.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 8.3 Support Resources

TI E2E<sup>™</sup> support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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#### 8.4 Trademarks

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### 8.5 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### 8.6 Glossary

TI Glossary

This glossary lists and explains terms, acronyms, and definitions.



# 9 Revision History

Changes from Revision * (December 2015) to Revision A (April 2024)	Page
• Updated the numbering format for tables, figures, and cross-references througho	ut the document1
• Changed low shutdown current from less than 10µA to 20µA	
Added WEBENCH information throughout the document	1
Updated trademark information	1
Updated Device Information table format	
Changed VBST (vs SW) and VFB MAX from 6.5 to 6	4
Changed Human-body model (HBM) value from 3000 to 2000	4
Changed VBST (vs SW) MAX from 6.0 to 5.5	4
Updated Specifications in the Electrical Characteristics table	6
Updated Figure 5-1 and Figure 5-2	7
Updated the Current Protection section	11

# 10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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