

# OPA207 低消費電力、高精度、低ノイズ、 レール・ツー・レール出力のオペアンプ

## 1 特長

- 非常に低いオフセット電圧：150 $\mu$ V (最大値)
- 非常に低いドリフト係数： $\pm 1\mu$ V/ $^{\circ}$ C (最大値)
- ゲイン帯域幅：1MHz (標準値)
- スルー・レート：3.6V/ $\mu$ s (標準値)
- 高いオープン・ループ・ゲイン：130dB (最小値)
- 高い同相除去：115dB (最小値)
- 高い電源除去：5 $\mu$ V/V (最大値)
- 低いバイアス電流：2.8nA (最大値)
- 広い電源電圧範囲： $\pm 2.25$ V $\sim$  $\pm 18$ V
- 低い静止電流：375 $\mu$ A (最大値)
- OP-07、OP-77、OP-177の代替

## 2 アプリケーション

- アナログ入力モジュール
- バッテリー試験装置
- データ・アキュイジション (DAQ)
- 圧カトランスミッタ
- 温度トランスミッタ

## 3 概要

OPA207高精度オペアンプは、業界標準のOP-07、OP-77、OP-177アンプに置き換わる製品です。OPA207は業界標準の同等製品と比較してノイズが低く、出力電圧スイングが広く、2倍の速度で、静止電流は半分です。非常に低い入力オフセット電圧およびドリフト係数、低い入力バイアス電流、高い同相除去比、高い電源除去比といった特長があります。

OPA207オペアンプは $\pm 2.25$ V $\sim$  $\pm 18$ Vの広い電源電圧範囲で動作し、優れた性能を実現します。アンプが規定された制限までスイングしても、高い性能が維持されます。

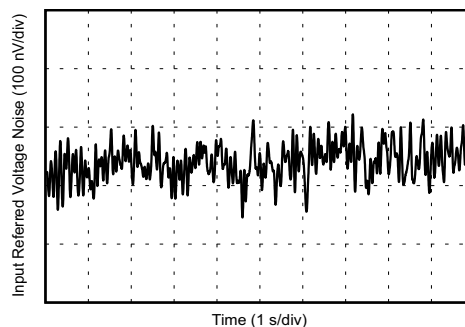
OPA207オペアンプは簡単に使用でき、一部のオペアンプに見られる位相反転や過負荷の問題は発生しません。OPA207はユニティ・ゲイン安定で、広い範囲の負荷状況にわたって優れた動的動作を実現します。

### 製品情報(1)

型番	パッケージ	本体サイズ(公称)
OPA207	SOIC (8)	4.90mm $\times$ 3.91mm
	VSSOP (8)	3.00mm $\times$ 3.00mm
	SOT-23 (5)	2.90mm $\times$ 1.60mm

(1) 利用可能なすべてのパッケージについては、このデータシートの末尾にあるパッケージ・オプションについての付録を参照してください。

### 非常に低い0.1Hz $\sim$ 10Hzのノイズ



## 目次

1	特長 .....	1	7.4	Device Functional Modes .....	19
2	アプリケーション .....	1	<b>8</b>	<b>Application and Implementation</b> .....	<b>20</b>
3	概要 .....	1	8.1	Application Information .....	20
4	改訂履歴 .....	2	8.2	Typical Applications .....	20
5	<b>Pin Configuration and Functions</b> .....	<b>3</b>	<b>9</b>	<b>Power Supply Recommendations</b> .....	<b>23</b>
6	<b>Specifications</b> .....	<b>4</b>	<b>10</b>	<b>Layout</b> .....	<b>23</b>
6.1	Absolute Maximum Ratings .....	4	10.1	Layout Guidelines .....	23
6.2	ESD Ratings .....	4	10.2	Layout Example .....	24
6.3	Recommended Operating Conditions .....	4	<b>11</b>	<b>デバイスおよびドキュメントのサポート</b> .....	<b>25</b>
6.4	Thermal Information .....	4	11.1	デバイス・サポート .....	25
6.5	Electrical Characteristics .....	5	11.2	ドキュメントのサポート .....	25
6.6	Typical Characteristics .....	7	11.3	ドキュメントの更新通知を受け取る方法 .....	25
<b>7</b>	<b>Detailed Description</b> .....	<b>13</b>	11.4	サポート・リソース .....	25
7.1	Overview .....	13	11.5	商標 .....	26
7.2	Functional Block Diagram .....	13	11.6	静電気放電に関する注意事項 .....	26
7.3	Feature Description .....	13	<b>12</b>	<b>メカニカル、パッケージ、および注文情報</b> .....	<b>26</b>

## 4 改訂履歴

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

<b>Revision C (March 2019) から Revision D に変更</b>	<b>Page</b>
• SOT-23 (DBV) パッケージをプレビューから量産データ (アクティブ) に変更 .....	1
• Added specifications for new DBV package .....	4

<b>Revision B (March 2019) から Revision C に変更</b>	<b>Page</b>
• Added input offset voltage specification for OPA207DGK .....	5
• Added input offset voltage drift specification for OPA207DGK .....	5

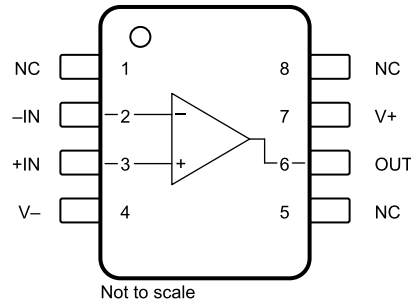
<b>Revision A (December 2018) から Revision B に変更</b>	<b>Page</b>
• 量産データ・データシートの初回リリースで VSSOP (DGK) パッケージに関する情報を追加 .....	1

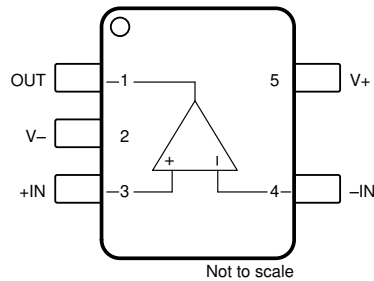
<b>2017年12月発行のものから更新</b>	<b>Page</b>
• 事前情報で 5 ピン SOT-23 パッケージに関する情報を追加 .....	1

## 5 Pin Configuration and Functions

**D and DGK Packages  
8-Pin SOIC and 8-Pin VSSOP  
Top View**



**DBV Package  
5-Pin SOT-23  
Top View**



### Pin Functions

NAME	PIN NO.		I/O	DESCRIPTION
	NO.			
	D (SOIC), DGK(VSSOP)	DBV (SOT-23)		
-IN	2	4	I	Inverting input
+IN	3	3	I	Non-inverting input
NC	1, 5, 8	—	—	No internal connection (can be left floating or connected to ground)
OUT	6	1	O	Output
V-	4	2	—	Negative (lowest) power supply
V+	7	5	—	Positive (highest) power supply

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) <sup>(1)</sup>

	MIN	MAX	UNIT
Supply voltage, $V_s = (V+) - (V-)$		36	V
Input voltage - Common-mode <sup>(2)</sup>	(V-) -0.7	(V+) +0.7	V
Input voltage - Differential	-1	1	V
Output short-circuit <sup>(3)</sup>	Continuous		
Operating temperature	-55	125	°C
Junction temperature		150	°C
Storage temperature, $T_{stg}$	-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Input current must be limited to 10 mA.
- (3) Short circuit to ground, one amplifier per package.

### 6.2 ESD Ratings

		VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	2000
		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	1000

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
Supply voltage, $V_s = (V+) - (V-)$	Single Supply	4.5	30	36	V
	Dual Supply	±2.25	±15	±18	V
Specified temperature		-40		125	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		OPA207			UNIT
		DGK (VSSOP)	D (SOIC)	DBV (SOT-23)	
		8 PINS	8 PINS	8 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	176.7	121.5	166.3	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	63.9	64.3	116.9	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	99.4	65.0	63.2	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	8.8	18.2	45	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	97.6	64.3	62.9	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package ThermalMetrics](#) application report.

## 6.5 Electrical Characteristics

at  $V_S = \pm 15\text{ V}$ ,  $T_A = 25^\circ\text{C}$ ,  $R_L = 2\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>						
$V_{OS}$	Input offset voltage OPA207D			15	$\pm 100$	$\mu\text{V}$
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			$\pm 150$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 200$	
	Input offset voltage OPA207DGK			15	$\pm 125$	
		$T_A = 0^\circ\text{C}$ to $85^\circ\text{C}$			$\pm 170$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 225$	
Input offset voltage OPA207DBV			15	$\pm 130$		
	$T_A = 0^\circ\text{C}$ to $85^\circ\text{C}$			$\pm 170$		
	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 225$		
$dV_{OS}/dT$	Input offset voltage drift OPA207D	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$		$\pm 0.2$	$\pm 8$	$\mu\text{V}/^\circ\text{C}$
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 0.2$	$\pm 8$	
	Input offset voltage drift OPA207DGK and OPA207DBV	$T_A = 0^\circ\text{C}$ to $85^\circ\text{C}$		$\pm 0.2$	$\pm 1.1$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 0.2$	$\pm 1.1$	
PSRR	Input offset voltage versus power supply	$V_S = \pm 2.25\text{ V}$ to $\pm 18\text{ V}$		$\pm 0.5$	$\pm 3$	$\mu\text{V}/\text{V}$
		$V_S = \pm 2.25\text{ V}$ to $\pm 18\text{ V}$ , $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			$\pm 4.2$	
		$V_S = \pm 2.25\text{ V}$ to $\pm 18\text{ V}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 5$	
<b>INPUT BIAS CURRENT</b>						
$I_B$	Input bias current			$\pm 0.2$	$\pm 1.5$	nA
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			$\pm 2$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 7$	
$I_{OS}$	Input offset current			$\pm 0.13$	$\pm 1.5$	nA
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$			$\pm 2$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 7$	
<b>NOISE</b>						
	Input voltage noise	$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		0.16		$\mu\text{V}_{PP}$
				0.024		$\mu\text{V}_{RMS}$
$e_N$	Input voltage noise density	$f = 1\text{ Hz}$		9.5		$\text{nV}/\sqrt{\text{Hz}}$
		$f = 10\text{ Hz}$		7.5		
		$f = 100\text{ Hz}$		7.5		
		$f = 1\text{ kHz}$		7.5		
$i_N$	Input current noise	$f = 1\text{ kHz}$		0.18		$\text{pA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>						
$V_{CM}$	Common-mode voltage range		$(V-) + 1.25$	$(V+) - 1.25$		V
CMRR	Common-mode rejection ratio	$(V-) + 1.25\text{ V} < V_{CM} < (V+) - 1.25\text{ V}$	120	140		dB
		$(V-) + 1.25\text{ V} < V_{CM} < (V+) - 1.25\text{ V}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	115	140		
<b>INPUT CAPACITANCE</b>						
$Z_{ID}$	Differential			3    14		$\text{M}\Omega$    $\text{pF}$
$Z_{ICM}$	Common-mode			1    1		$\text{G}\Omega$    $\text{pF}$
<b>OPEN-LOOP GAIN</b>						
$A_{OL}$	Open-loop voltage gain	$(V-) + 200\text{ mV} < V_O < (V+) - 200\text{ mV}$ , $R_L = 10\text{ k}\Omega$		130	140	dB
			$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	126		
		$(V-) + 200\text{ mV} < V_O < (V+) - 200\text{ mV}$ , $R_L = 2\text{ k}\Omega$	OPA207D, OPA207DGK	120	140	
		$(V-) + 300\text{ mV} < V_O < (V+) - 300\text{ mV}$ , $R_L = 2\text{ k}\Omega$	OPA207DBV	130	140	
		$(V-) + 200\text{ mV} < V_O < (V+) - 200\text{ mV}$ , $R_L = 2\text{ k}\Omega$	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ , OPA207D, OPA207DGK	114		
	$(V-) + 300\text{ mV} < V_O < (V+) - 300\text{ mV}$ , $R_L = 2\text{ k}\Omega$	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ , OPA207DBV	120			

**Electrical Characteristics (continued)**

 at  $V_S = \pm 15\text{ V}$ ,  $T_A = 25^\circ\text{C}$ ,  $R_L = 2\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S/2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>FREQUENCY RESPONSE</b>						
GBW	Gain-bandwidth product			1.3		MHz
SR	Slew rate	10-V step, $G = 1$		2.7		V/ $\mu\text{s}$
$t_s$	Settling time	To 0.1%, 10-V step, $G = 1$		4.8		$\mu\text{s}$
		To 0.01%, 10-V step, $G = 1$		5.4		
		To 0.001%, 10-V step, $G = 1$		8.1		
	Overload recovery time	$V_{IN} \times \text{gain} > V_S$		1.1		$\mu\text{s}$
	Total harmonic distortion + noise (THD+N)	$V_O = 3 V_{RMS}$ , $G = 1$ , $f = 1\text{ kHz}$ , $R_L = 10\text{ k}\Omega$		-114		dB
<b>OUTPUT</b>						
	Voltage output swing from rail	$T_A = 25^\circ\text{C}$ , no load, OPA207DBV		15	40	mV
		$T_A = 25^\circ\text{C}$ , $R_L = 10\text{ k}\Omega$ , OPA207DBV		40	60	
		$T_A = 25^\circ\text{C}$ , $R_L = 2\text{ k}\Omega$ , OPA207DBV		80	140	
		$T_A = 25^\circ\text{C}$ , no load, OPA207D, OPA207DGK		15	30	
		$T_A = 25^\circ\text{C}$ , $R_L = 10\text{ k}\Omega$ , OPA207D, OPA207DGK		40	50	
		$T_A = 25^\circ\text{C}$ , $R_L = 2\text{ k}\Omega$ , OPA207D, OPA207DGK		80	125	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ , $R_L = 10\text{ k}\Omega$		75	200	
$I_{SC}$	Short-circuit current	Sinking		-40		mA
		Sourcing		40		
$C_{LOAD}$	Capacitive load drive			200		pf
$R_O$	Open-loop output impedance	$f = 1\text{ MHz}$		45		$\Omega$
<b>POWER SUPPLY</b>						
$I_Q$	Quiescent current per amplifier	$I_O = 0\text{ A}$		350	375	$\mu\text{A}$
		$I_O = 0\text{ A}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			450	
	Turnon time	At $T_A = 25^\circ\text{C}$ , $V_S = 36\text{ V}$ , $V_S$ ramp rate $> 0.3\text{ V}/\mu\text{s}$		27		$\mu\text{s}$

## 6.6 Typical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ , and  $R_L = 2\text{ k}\Omega$  (unless otherwise noted)

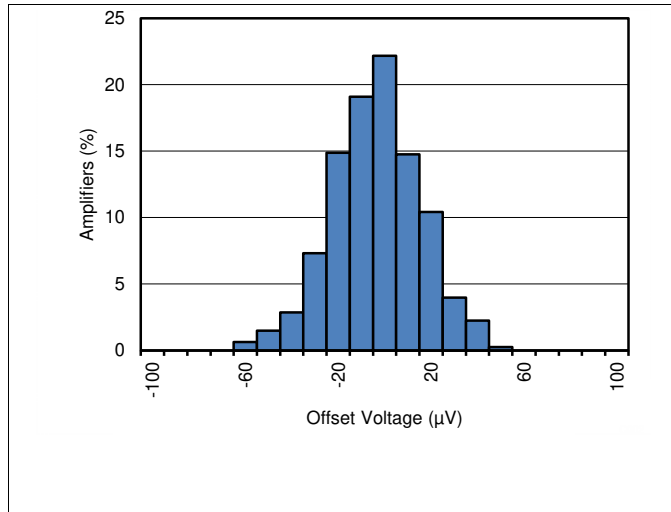


Fig 1. Input Referred Offset Voltage Distribution

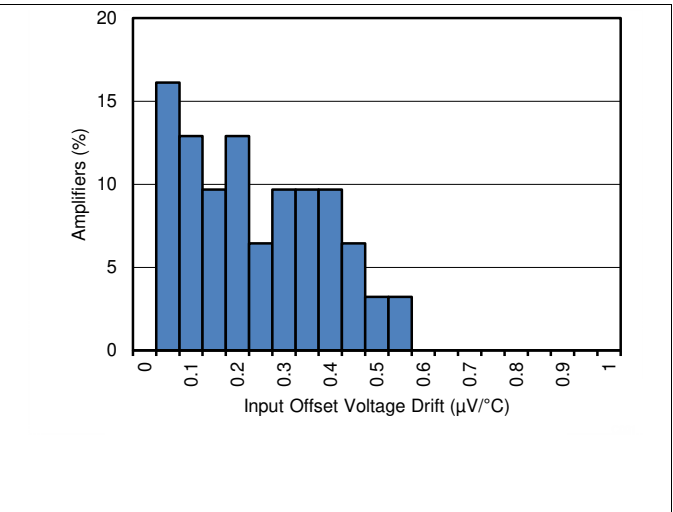


Fig 2. Input Referred Offset Voltage Drift Distribution

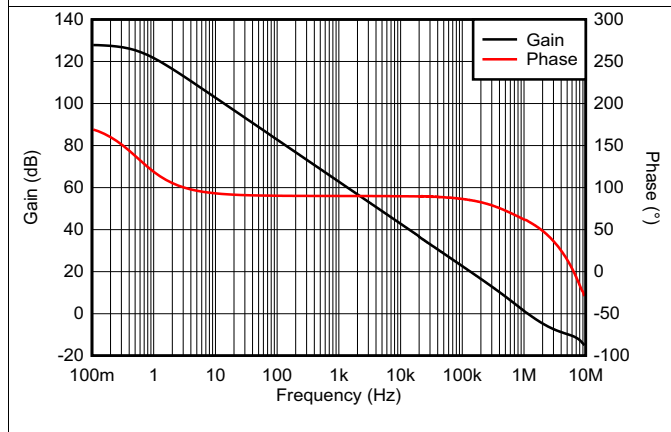


Fig 3. Open-Loop Gain and Phase vs Frequency

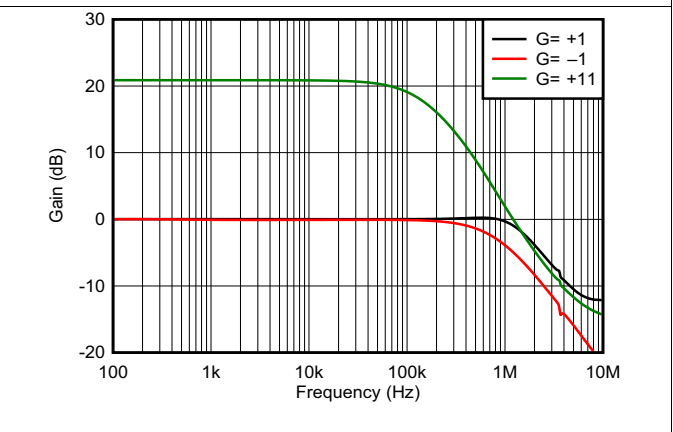


Fig 4. Closed Loop Gain vs Frequency

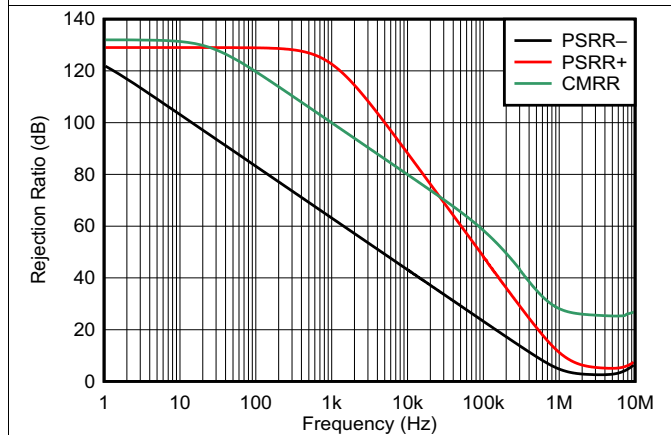


Fig 5. Power Supply Rejection Ratio and Common-Mode Rejection Ratio vs Frequency

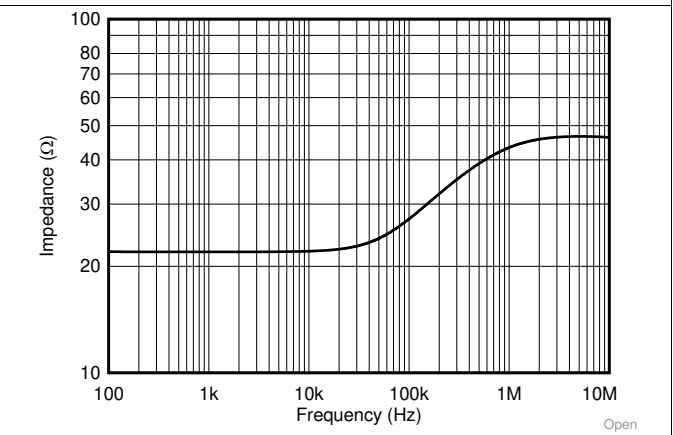
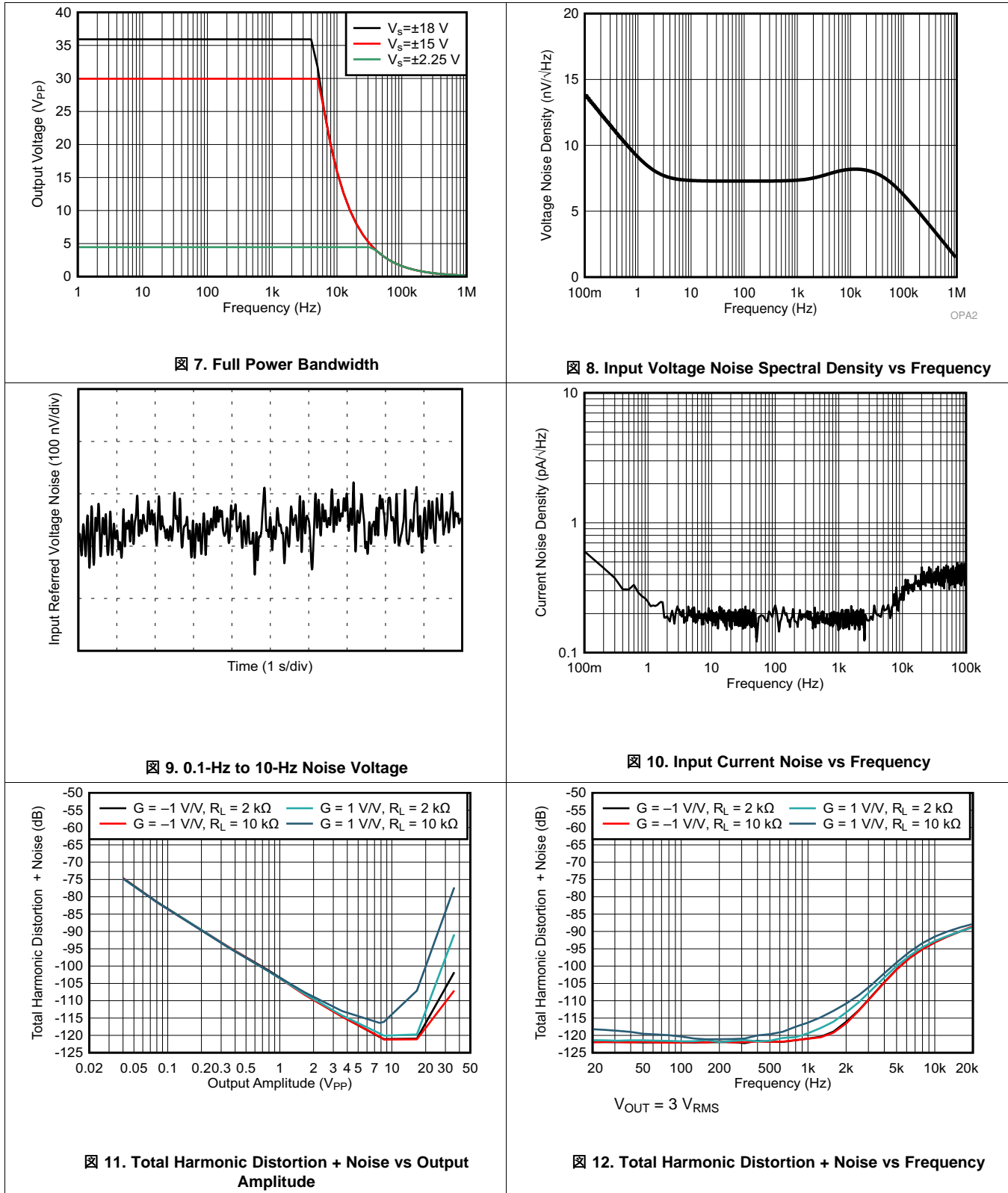


Fig 6. Open-Loop Output Impedance vs Frequency

**Typical Characteristics (continued)**

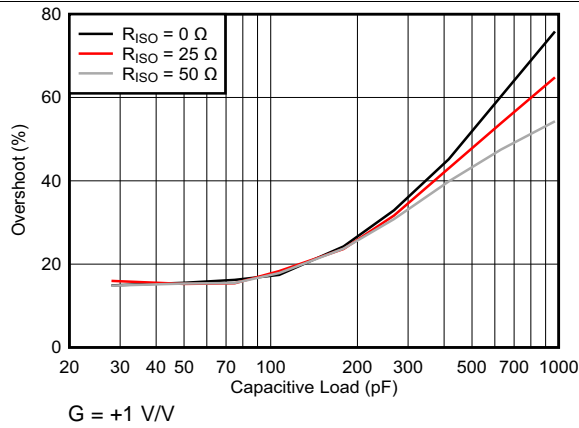
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ , and  $R_L = 2\text{ k}\Omega$  (unless otherwise noted)



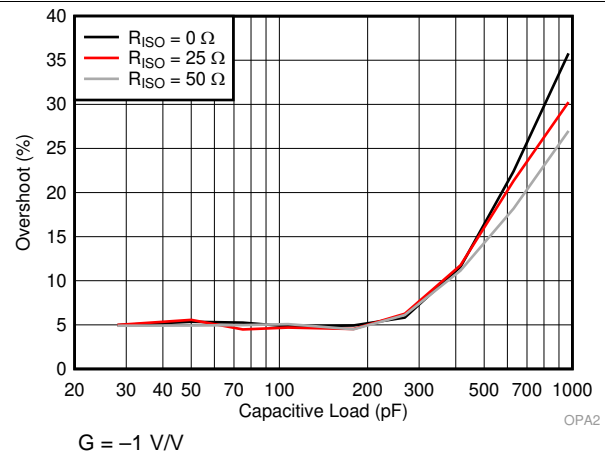


Typical Characteristics (continued)

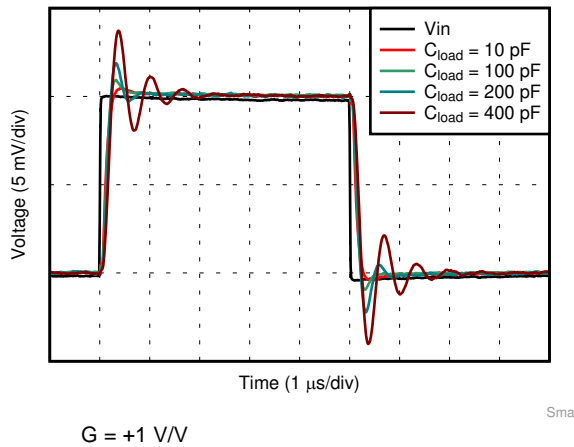
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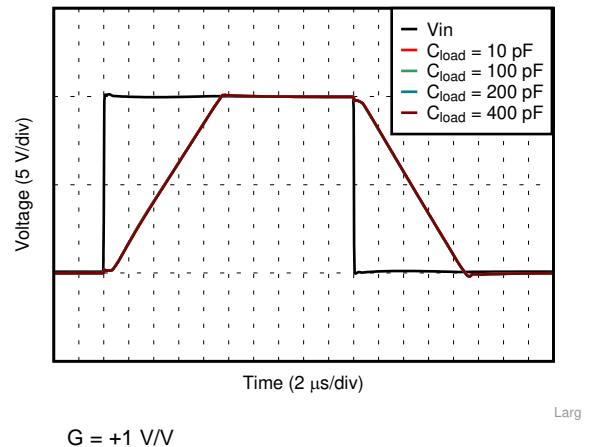
13. Overshoot vs Capacitive Load



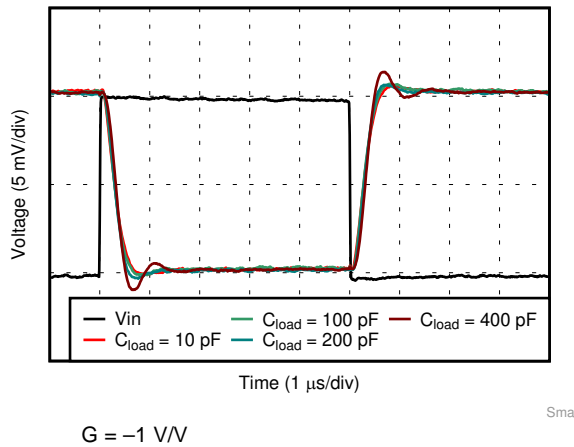
14. Overshoot vs Capacitive Load



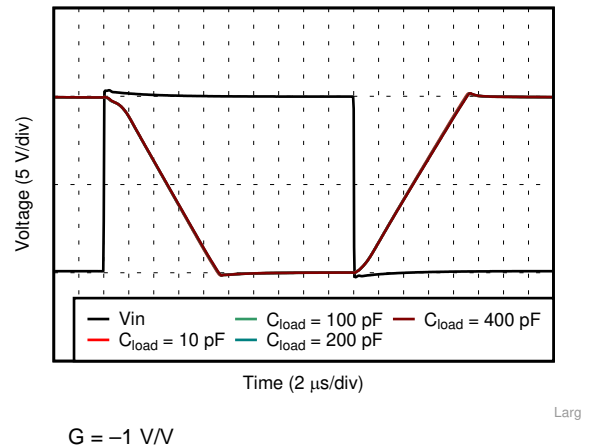
15. Small-Signal Step Response



16. Large-Signal Step Response



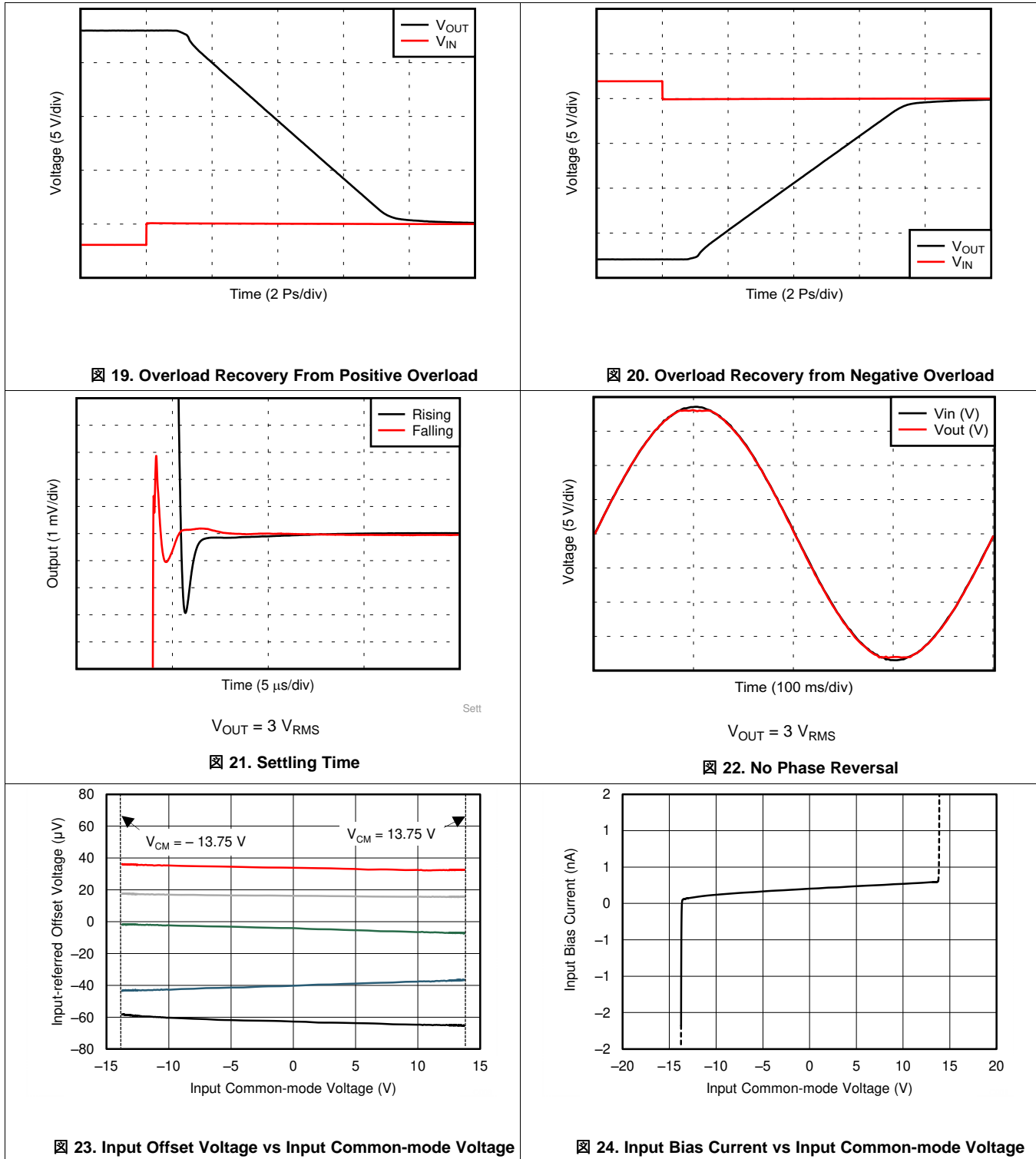
17. Small-Signal Step Response



18. Large-Signal Step Response

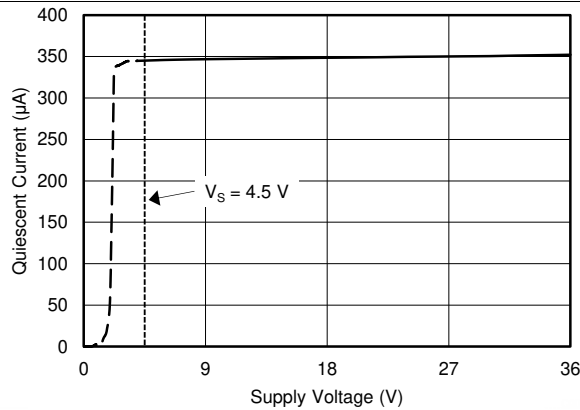
Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ , and  $R_L = 2\text{ k}\Omega$  (unless otherwise noted)

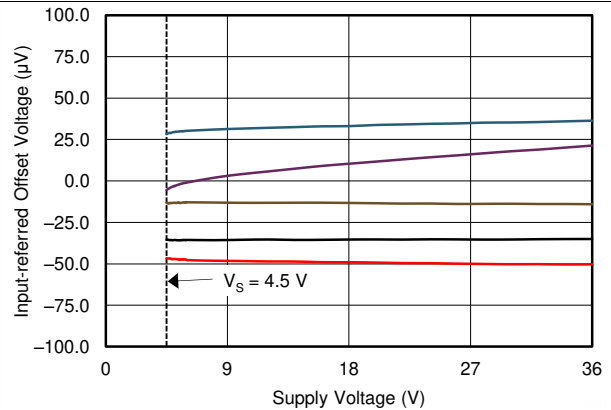


Typical Characteristics (continued)

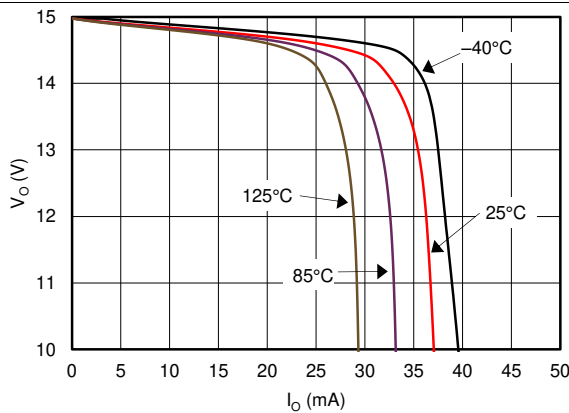
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ , and  $R_L = 2\text{ k}\Omega$  (unless otherwise noted)



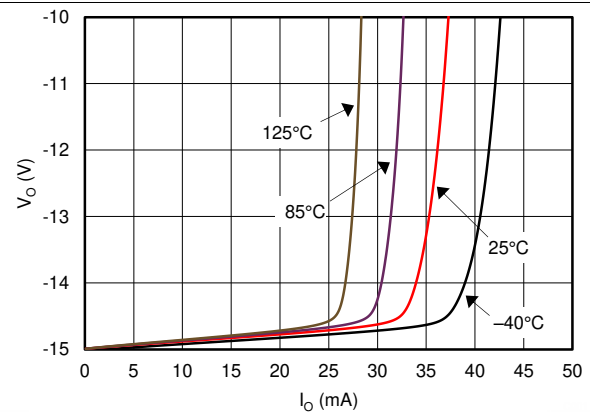
25. Quiescent Current vs Power Supply Voltage



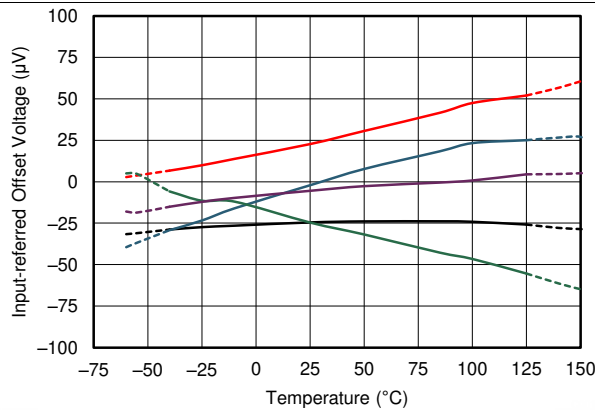
26. Input Offset Voltage vs Power Supply Voltage



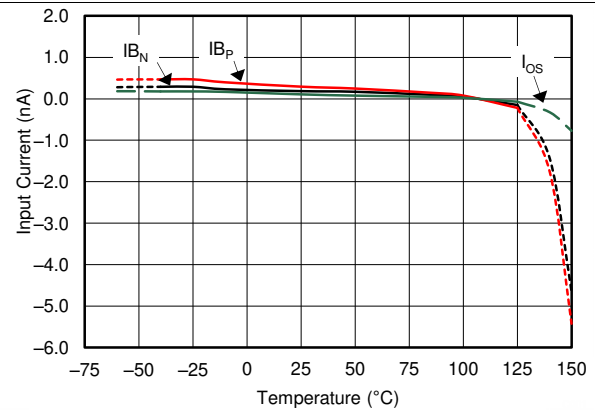
27. Output Voltage vs Output Current (Sourcing)



28. Output Voltage vs Output Current (Sinking)



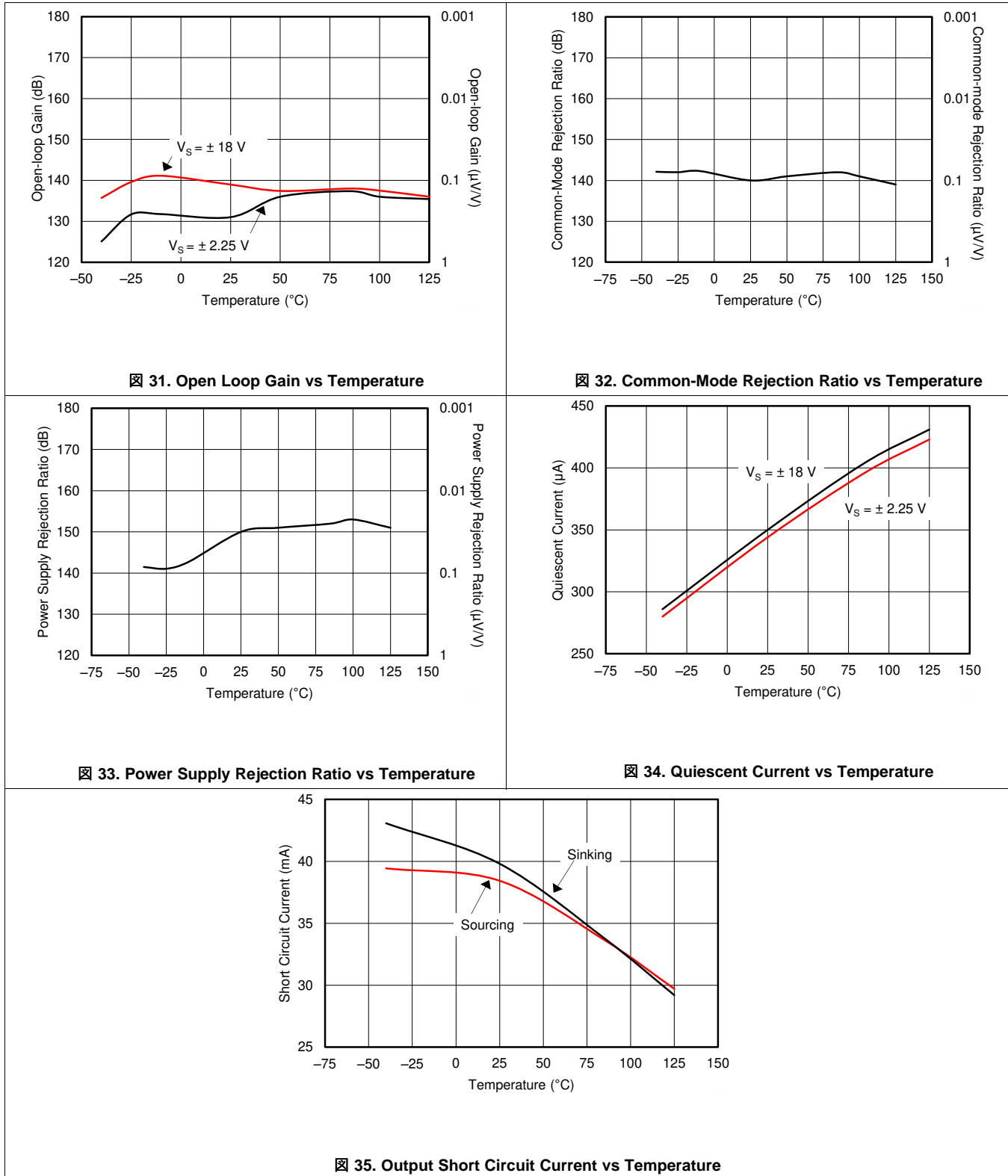
29. Input Offset Voltage vs Temperature



30. Input Bias Current vs Temperature

Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ , and  $R_L = 2\text{ k}\Omega$  (unless otherwise noted)

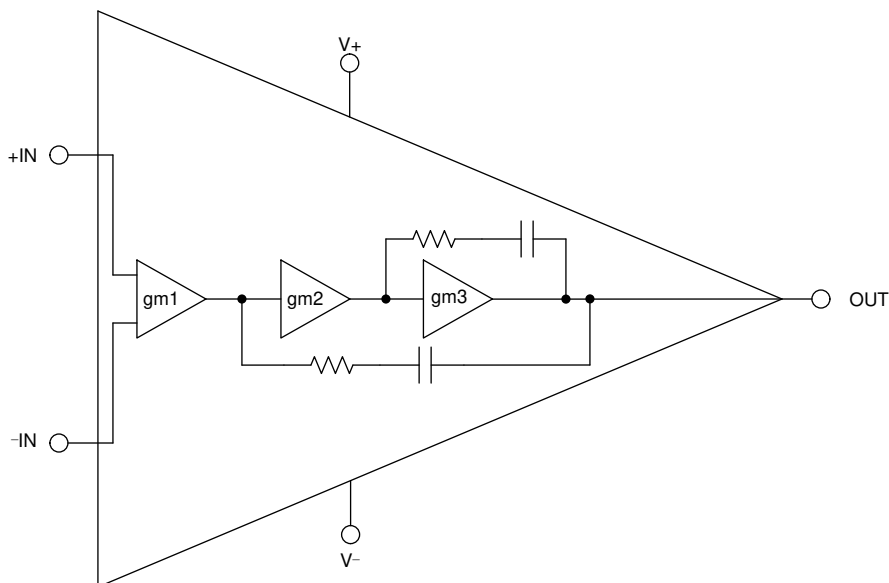


## 7 Detailed Description

### 7.1 Overview

The OPA207 precision operational amplifier replaces the industry standard OP-177. The OPA207 offers improved noise, wider output voltage swing, has twice the bandwidth, ten times the slew rate and consumes only half the quiescent current as the OP-177. Additional features include ultralow offset voltage and drift, low bias current, high common-mode rejection, and high power supply rejection.

### 7.2 Functional Block Diagram



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### 7.3 Feature Description

The OPA207 is unity-gain stable and free from unexpected output phase reversal, making it easy to use in a wide range of applications. Applications with noisy or high-impedance power supplies may require decoupling capacitors close to the device pins. In most cases 0.1- $\mu$ F capacitors are adequate.

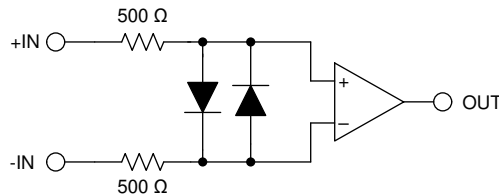
#### 7.3.1 Operating Voltage

The OPA207 operates from  $\pm 2.25$  V to  $\pm 18$  V supplies with excellent performance. Key parameters are assured over the specified temperature range,  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ . Most behavior remains unchanged through the full operating voltage range ( $\pm 2.25$  V to  $\pm 18$  V). Parameters which vary significantly with operating voltage or temperature are shown in [Typical Characteristics](#).

## Feature Description (continued)

### 7.3.2 Input Protection

The input stage of the OPA207 is internally protected with resistors in series with diode clamps as shown in [Figure 36](#). The inputs can withstand  $\pm 10$  V differential inputs without damage and the maximum input current should be limited to 10 mA or less. The protection diodes conduct current when the inputs are over-driven such as when the opamp output is slewing. This may disturb the slewing behavior of unity-gain follower applications, but will not damage the operational amplifier.

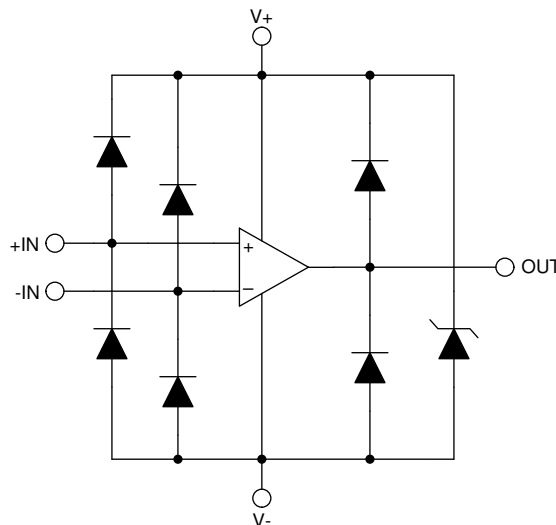


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**Figure 36. Simplified OPA207 Input Protection Circuit**

### 7.3.3 ESD Protection

The OPA207 is internally protected against ESD events that can occur during manufacturing, handling, or printed-circuit-board assembly. The internal ESD protection diodes are not intended to protect the OPA207 during normal operation when the device is operating under power. In cases where the inputs or output can be driven above the positive power supply or below the negative power supply care must be taken to limit the current through the internal diodes to 10 mA or less. In harsh electrical environments external protection circuitry may be required and is dependant upon the application requirements and environmental conditions.



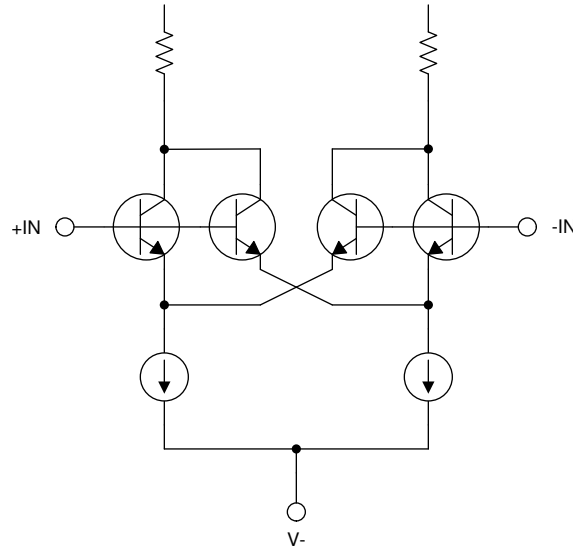
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**Figure 37. Simplified OPA207 ESD Protection Circuit**

## Feature Description (continued)

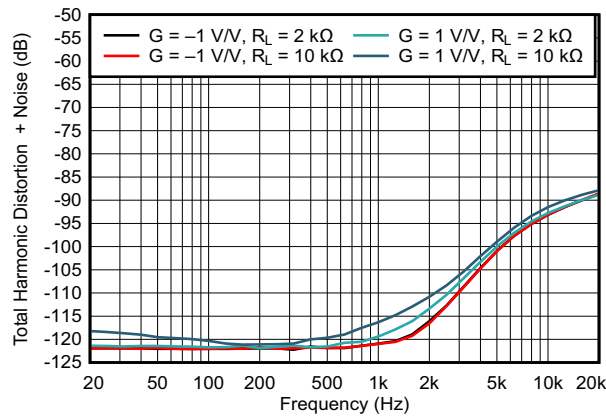
### 7.3.4 Input Stage Linearization

The OPA207 uses linearization techniques to reduce the total harmonic distortion. [Figure 38](#) illustrates the linearization concept, and [Figure 39](#) illustrates the total harmonic distortion performance of the OPA207.



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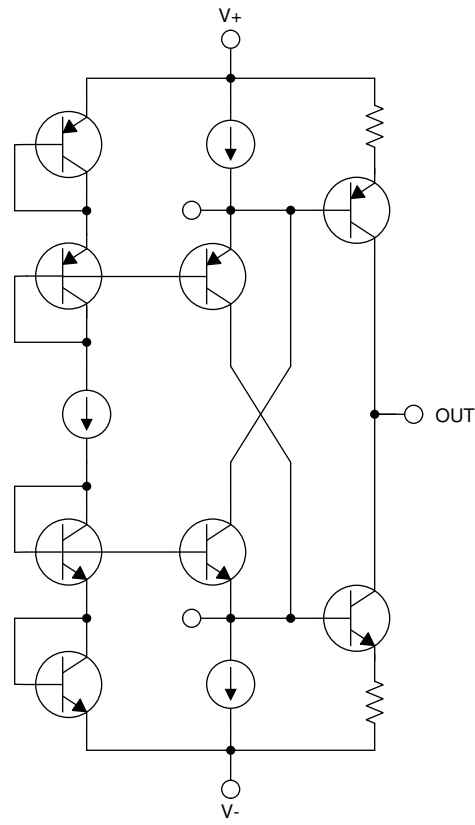
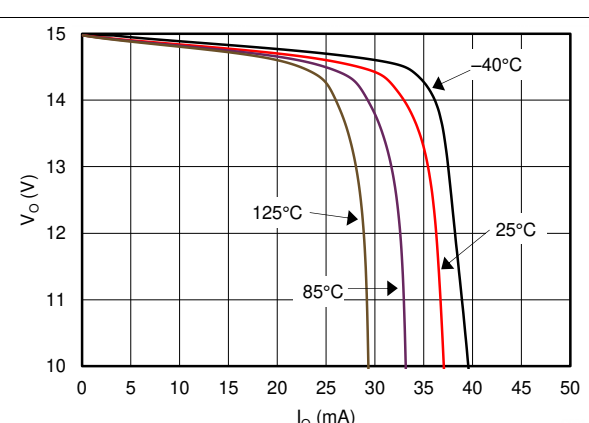
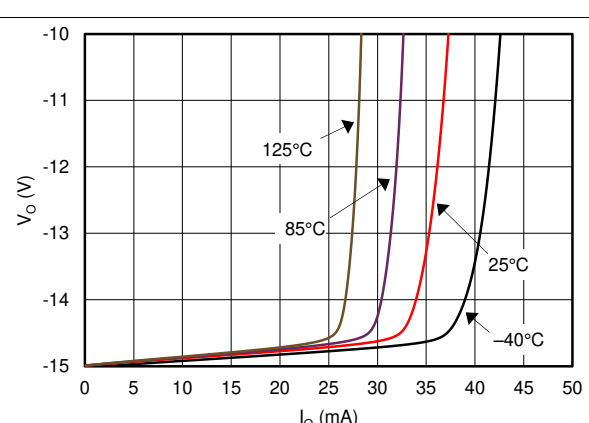
**Figure 38. Simplified Input Stage Linearization Circuit**

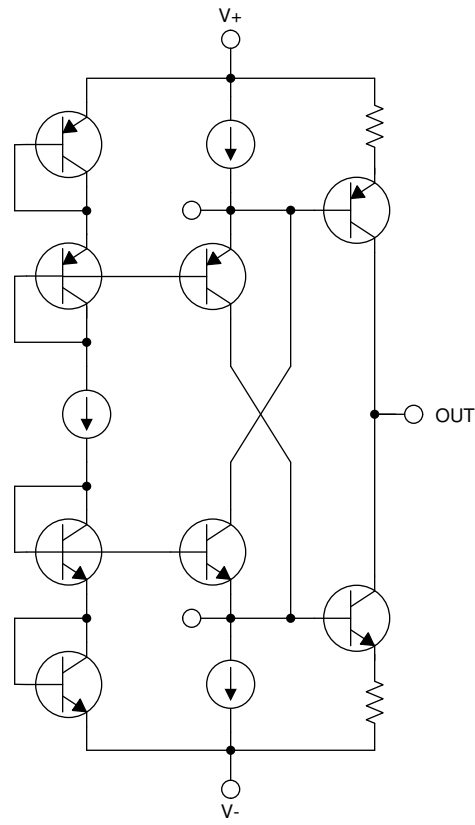


**Figure 39. Total Harmonic Distortion**

**Feature Description (continued)**

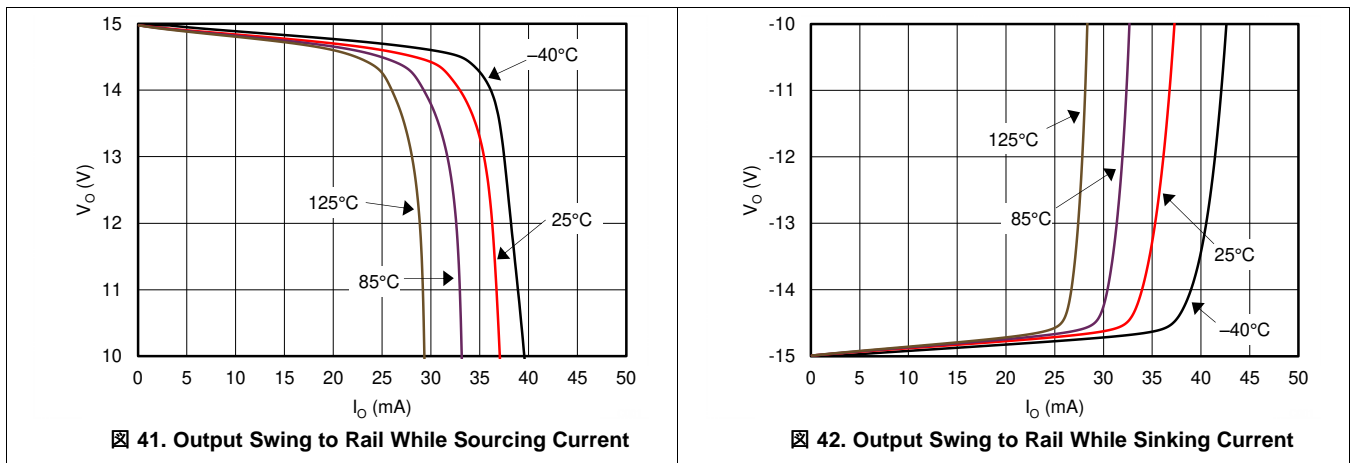
**7.3.5 Rail-to-Rail Output**

The OPA207 uses a rail-to-rail output stage capable of swinging within a few millivolts from either power supply rail while maintaining high open-loop gain.  shows a simplified drawing of the output stage circuit. Resistors connected in series with each output transistor ensure a consistent output current limit. Limiting the output current in this way ensures reliable operation of the OPA207 under short circuited conditions and protects sensitive loads from being damaged by excessive current.  and  illustrate the maximum output current available from the OPA207 at various temperatures.



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**Figure 40. Simplified Rail-to-Rail Output Stage Circuit**

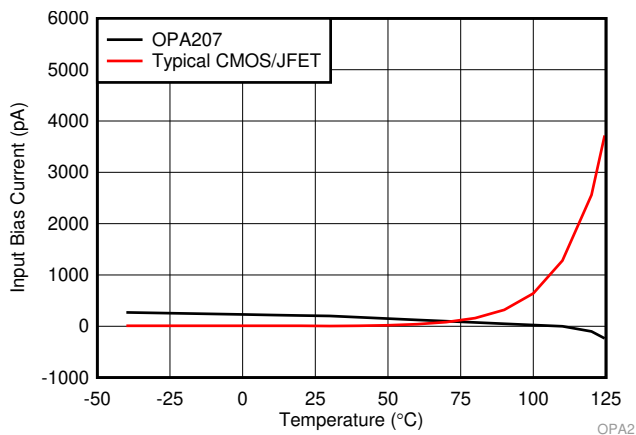




## Feature Description (continued)

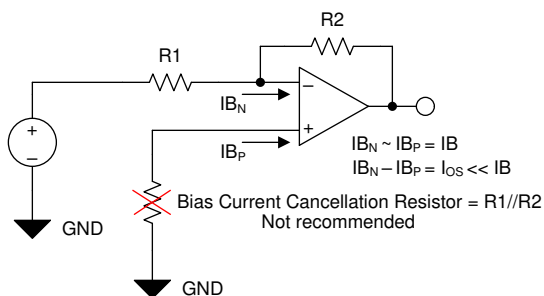
### 7.3.6 Low Input Bias Current

The OPA207 uses super-beta bipolar transistors and employs an input bias current cancellation technique. This combination results in very low input bias currents that remain low over the full specified temperature range from  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$  unlike CMOS or JFET amplifiers whose input bias currents typically double every  $10^{\circ}\text{C}$  and can be extremely high at  $125^{\circ}\text{C}$ . [Figure 43](#) illustrates the comparison between the OPA207 and typical CMOS or JFET amplifiers.



**Figure 43. Input Bias Current vs Temperature**

It is common practice to place a bias current cancellation resistor as illustrated in [Figure 42](#). This approach works well with amplifiers that do not employ an internal input bias current cancellation technique. Because the OPA207 uses an internal bias current cancellation technique, TI does not recommend the bias cancellation resistor.



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**Figure 44. Bias Current Cancellation Resistor — Not Recommended**

## Feature Description (continued)

### 7.3.7 Slew Boost

The OPA207 uses a novel internal slew-boost technique. This method allows the OPA207 to consume very low power yet still achieve a high slew rate of 3.6 V/ $\mu$ s. This makes the OPA207 ideal for applications that require low noise and high out voltage swings where the high slew rate is necessary to achieve fast settling times.

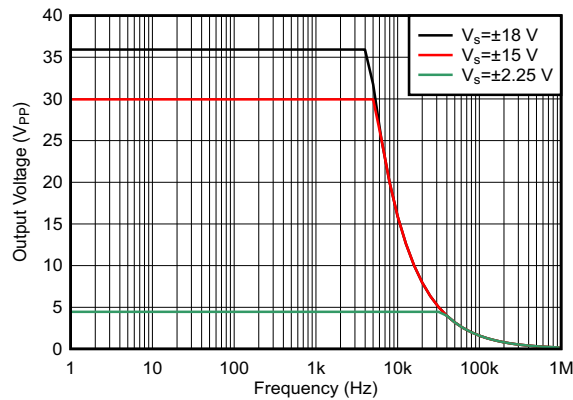


Figure 45. Full Power Bandwidth

### 7.3.8 EMI Rejection Ratio (EMIRR)

The electromagnetic interference (EMI) rejection ratio, or EMIRR, describes the EMI immunity of operational amplifiers. An adverse effect that is common to many operational amplifiers is a change in the offset voltage as a result of RF signal rectification. An operational amplifier that is more efficient at rejecting this change in offset as a result of EMI has a higher EMIRR and is quantified by a decibel value. Measuring EMIRR can be performed in many ways, but this report provides the EMIRR IN+, which specifically describes the EMIRR performance when the RF signal is applied to the noninverting input pin of the operational amplifier. In general, only the noninverting input is tested for EMIRR for the following three reasons:

1. Operational amplifier input pins are known to be the most sensitive to EMI, and typically rectify RF signals better than the supply or output pins.
2. The noninverting and inverting operational amplifier inputs have symmetrical physical layouts and exhibit nearly matching EMIRR performance.
3. EMIRR is easier to measure on noninverting pins than on other pins because the noninverting input terminal can be isolated on a printed circuit board (PCB). This isolation allows the RF signal to be applied directly to the noninverting input terminal with no complex interactions from other components or connecting PCB traces.

A more formal discussion of the EMIRR IN+ definition and test method is provided in TI Application Report [EMI Rejection Ratio of Operational Amplifiers](#), available for download at [www.ti.com](http://www.ti.com). The EMIRR IN+ of the OPA207 is plotted versus frequency as shown in Figure 46.

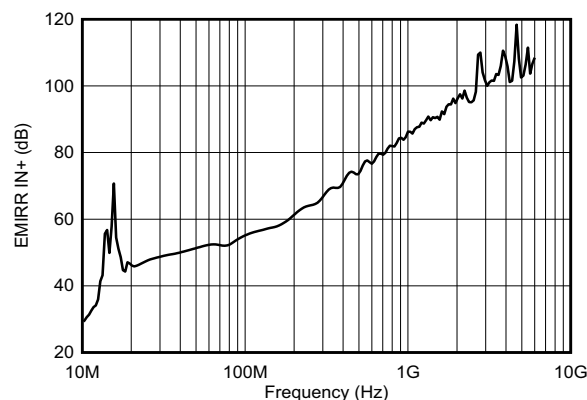


Figure 46. OPA207 EMIRR IN+ vs Frequency

## Feature Description (continued)

If available, any dual and quad operational amplifier device versions have nearly similar EMIRR IN+ performance. The OPA207 unity-gain bandwidth is 1 MHz. EMIRR performance below this frequency denotes interfering signals that fall within the operational amplifier bandwidth.

表 1 shows the EMIRR IN+ values for the OPA207 at particular frequencies commonly encountered in real-world applications. Applications listed in 表 1 may be centered on or operated near the particular frequency shown. This information may be of special interest to designers working with these types of applications, or working in other fields likely to encounter RF interference from broad sources, such as the industrial, scientific, and medical (ISM) radio band.

**表 1. OPA207 EMIRR IN+ for Frequencies of Interest**

FREQUENCY	APPLICATION/ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite/space operation, weather, radar, UHF	72 dB
900 MHz	GSM, radio com./nav./GPS (to 1.6 GHz), ISM, aeronautical mobile, UHF	83 dB
1.8 GHz	GSM, mobile personal comm. broadband, satellite, L-band	95 dB
2.4 GHz	802.11b/g/n, Bluetooth <sup>®</sup> , mobile personal comm., ISM, amateur radio/satellite, S-band	94 dB
3.6 GHz	Radiolocation, aero comm./nav., satellite, mobile, S-band	103 dB
5 GHz	802.11a/n, aero comm./nav., mobile comm., space/satellite operation, C-band	102 dB

## 7.4 Device Functional Modes

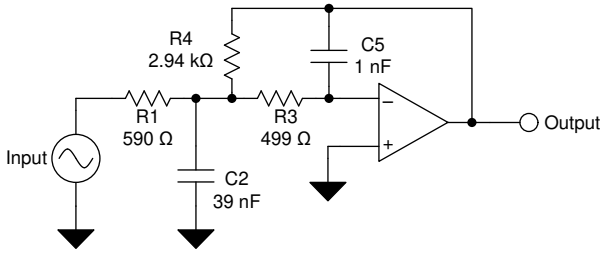
The OPA207 has a single functional mode and is operational when the power-supply voltage is greater than 4.5 V ( $\pm 2.25$  V). The maximum power supply voltage for the OPA207 is 36 V ( $\pm 18$  V).

## 8 Application and Implementation

### 注

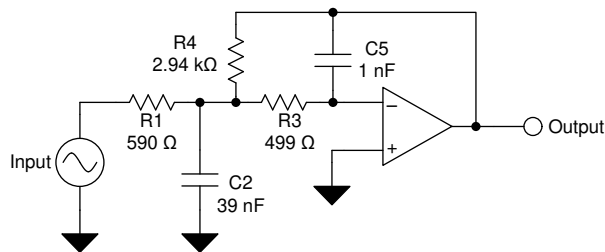
Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

Low-pass filters are commonly employed in signal processing applications to reduce noise and prevent aliasing. The OPA207 is designed to construct high-precision active filters.  shows a second-order, low-pass filter commonly encountered in signal processing applications.

### 8.2 Typical Applications

#### 8.2.1 Typical OPA207 Application



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**图 47. Typical OPA207 Application Schematic**

##### 8.2.1.1 Design Requirements

Use the following parameters for this design example:

- Gain = 5 V/V (inverting gain)
- Low-pass cutoff frequency = 25 kHz
- Second-order Chebyshev filter response with 3-dB gain peaking in the passband

##### 8.2.1.2 Detailed Design Procedure

The infinite-gain multiple-feedback circuit for a low-pass network function is shown in . Use [式 1](#) to calculate the voltage transfer function.

$$\frac{\text{Output}}{\text{Input}}(s) = \frac{-1/R_1 R_3 C_2 C_5}{s^2 + (s/C_2)(1/R_1 + 1/R_3 + 1/R_4) + 1/R_3 R_4 C_2 C_5} \quad (1)$$

This circuit produces a signal inversion. For this circuit, the gain at dc and the low-pass cutoff frequency are calculated by [式 2](#):

$$\text{Gain} = \frac{R_4}{R_1}$$

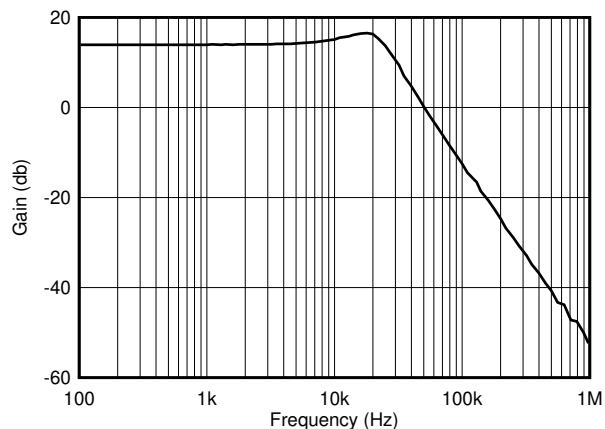
$$f_c = \frac{1}{2\pi} \sqrt{1/R_3 R_4 C_2 C_5} \quad (2)$$

Software tools are readily available to simplify filter design. [WEBENCH® Filter Designer](#) is a simple, powerful, and easy-to-use active filter design program. The WEBENCH Filter Designer lets designers create optimized filter designs using a selection of TI operational amplifiers and passive components from TI's vendor partners.

Available as a web-based tool from the WEBENCH® Design Center, [WEBENCH® Filter Designer](#) allows to design, optimize, and simulate complete multi-stage active filter solutions within minutes.

**Typical Applications (continued)**

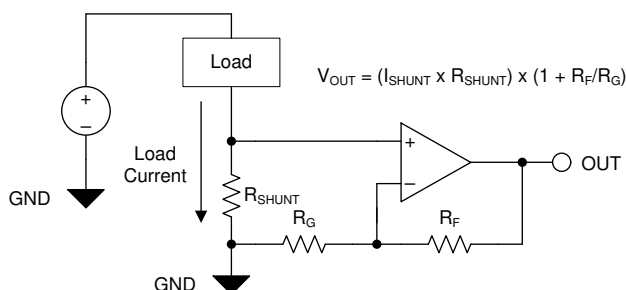
**8.2.1.3 Application Curve**



**48. Low-Pass Filter Transfer Function**

**8.2.2 Precision Low-Side Current Sensing**

With low offset voltage and low offset voltage drift over time and temperature the OPA207 works well for precision low-side current sensing applications as shown in 49



$$V_{OUT} = (I_{SHUNT} \times R_{SHUNT}) \times (1 + R_F/R_G)$$

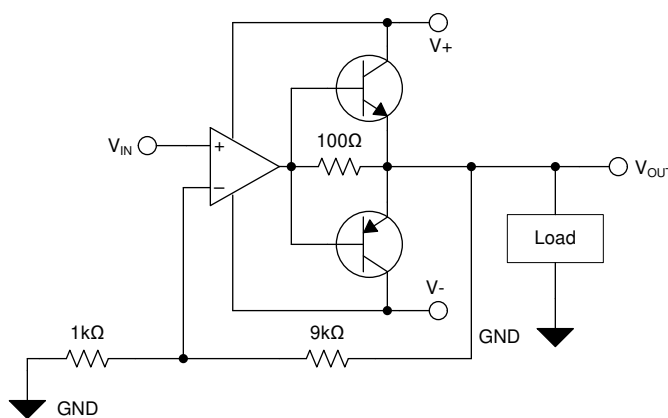
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**49. Precision Low-Side Current Sensing**

## Typical Applications (continued)

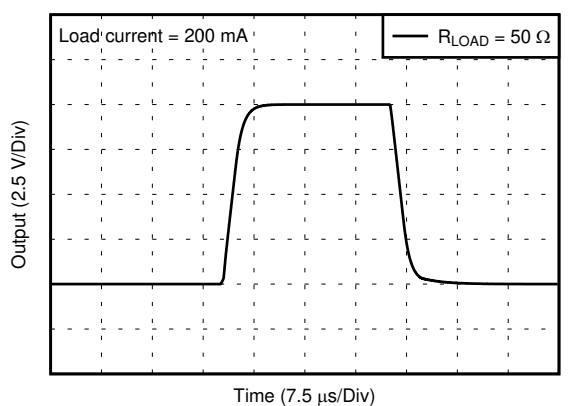
### 8.2.3 Precision Buffer With Increased Output Current

The OPA207 can be configured as illustrated in [Figure 50](#) to drive low impedance loads. In [Figure 50](#), the OPA207 is configured in a gain of +10 V/V, and the output current is boosted by the NPN (2N2904) and PNP (2N2906) bipolar transistors. For low output voltages the OPA207 supplies the load current directly through the 100-Ω resistor. The bipolar transistors begin to supply current when the voltage drop across the 100-Ω resistor exceeds approximately 500 mV. [Figure 50](#) illustrates the results for a 50-Ω load resistor driven with a 10-V step at the output. This results in a 200-mA current supplied by the circuit.



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**Figure 50. Precision Buffer ( $G = 10$  V/V) With High Output Drive Capability**



Prec

**Figure 51. 50-Ω Load Driven With a 10-V Step**

## 9 Power Supply Recommendations

The OPA207 is specified for operation from 4.5 V to 36 V ( $\pm 2.25$  V to  $\pm 18$  V); many specifications apply from  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ . Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the [Typical Characteristics](#).

### 注意

Supply voltages larger than 36 V can permanently damage the device; see the [Absolute Maximum Ratings](#).

Place 0.1- $\mu\text{F}$  bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or high-impedance power supplies. For more detailed information on bypass capacitor placement, refer to the [Layout Guidelines](#).

## 10 Layout

### 10.1 Layout Guidelines

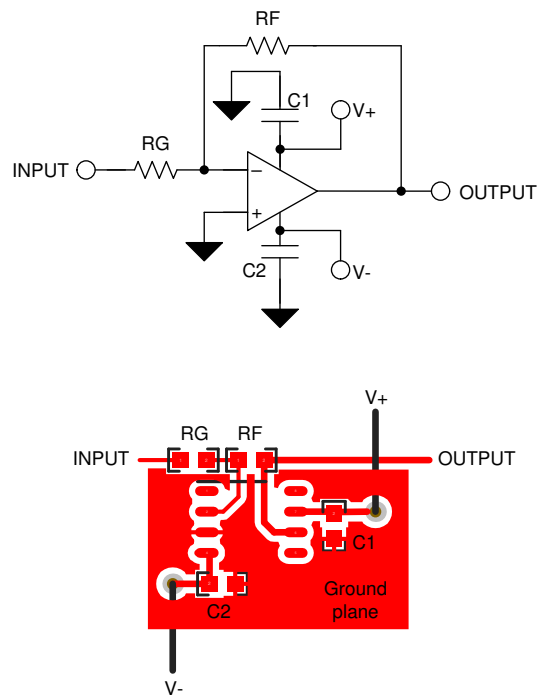
The OPA207 series has low offset voltage and drift. To achieve highest performance, optimize the circuit layout and mechanical conditions. Offset voltage and drift can be degraded by small thermoelectric potentials at the op amp inputs. Connections of dissimilar metals generate thermal potential, which can degrade the ultimate performance of the OPA207. These thermal potentials can be made to cancel by assuring that they are equal in both input terminals.

- Keep the thermal mass of the connections to the two input terminals similar.
- Locate heat sources as far as possible from the critical input circuitry.
- Shield operational amplifier and input circuitry from air currents, such as cooling fans.

For best operational performance of the device, use good PCB layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and op amp itself. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1- $\mu\text{F}$  ceramic bypass capacitors between each supply pin and ground, placed as close as possible to the device. A single bypass capacitor from  $V+$  to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds paying attention to the flow of the ground current.
- In order to reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better as opposed to in parallel with the noisy trace.
- Place the external components as close as possible to the device. As shown in [Layout Example](#), keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.
- For best performance, TI recommends cleaning the PCB following board assembly.
- Any precision integrated circuit may experience performance shifts due to moisture ingress into the plastic package. Following any aqueous PCB cleaning process, TI recommends baking the PCB assembly to remove moisture introduced into the device packaging during the cleaning process. A low temperature, post-cleaning bake at  $85^{\circ}\text{C}$  for 30 minutes is sufficient for most circumstances.

## 10.2 Layout Example



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☒ 52. OPA207 Layout Example for the Inverting Configuration



## 11 デバイスおよびドキュメントのサポート

### 11.1 デバイス・サポート

#### 11.1.1 開発サポート

##### 11.1.1.1 WEBENCH Filter Designer ツール

WEBENCH® Filter Designer は単純で強力な、使いやすいアクティブ・フィルタ設計プログラムです。WEBENCH Filter Designer を使用すると、TI のベンダ・パートナーからの TI 製オペアンプやパッシブ・コンポーネントを使用して、最適なフィルタ設計を作成できます。

##### 11.1.1.2 TINA-TI™ (無料のダウンロード・ソフトウェア)

TINA™ は、SPICE エンジンに基づいた単純かつ強力な、使いやすい回路シミュレーション・プログラムです。また、TINA-TI は、TINA ソフトウェアの完全な機能を持つ無償バージョンで、パッシブ・モデルとアクティブ・モデルに加えて、マクロ・モデルのライブラリがプリロードされています。TINA-TI には、SPICE の標準的な DC 解析、過渡解析、周波数ドメイン解析などの全機能に加え、追加の設計機能が搭載されています。

TINA-TI は Analog eLab Design Center から無料でダウンロードでき、ユーザーが結果をさまざまな方法でフォーマットできる、広範な後処理機能を備えています。仮想計測器により、入力波形を選択し、回路ノード、電圧、および波形をプローブして、動的なクイック・スタート・ツールを作成できます。

#### 注

これらのファイルを使用するには、TINA ソフトウェア ( DesignSoft™ 製) または TINA-TI ソフトウェアがインストールされている必要があります。TINA-TI フォルダから、無料の TINA-TI ソフトウェアをダウンロードしてください。

##### 11.1.1.3 TI Precision Designs

OPA207 はいくつかの TI Precision Designs に使用されており、これらは <http://www.ti.com/ww/en/analog/precision-designs> からオンラインで入手できます。TI Precision Designs は、TI の高精度アナログ・アプリケーションの専門家により作成されたアナログ・ソリューションで、多くの有用な回路に関して、動作理論、コンポーネント選択、シミュレーション、完全な PCB 回路図とレイアウト、部品表、性能測定結果を提供します。

## 11.2 ドキュメントのサポート

### 11.2.1 関連資料

関連資料については、以下を参照してください。

- テキサス・インスツルメンツ、『オペアンプの EMI 除去率』
- テキサス・インスツルメンツ、『回路基板のレイアウト技法』

### 11.3 ドキュメントの更新通知を受け取る方法

ドキュメントの更新についての通知を受け取るには、[ti.com](http://ti.com) のデバイス製品フォルダを開いてください。右上の「アラートを受け取る」をクリックして登録すると、変更されたすべての製品情報に関するダイジェストを毎週受け取れます。変更の詳細については、修正されたドキュメントに含まれている改訂履歴をご覧ください。

### 11.4 サポート・リソース

TI E2E™ support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

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TINA, DesignSoft are trademarks of DesignSoft, Inc.  
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## 11.6 静電気放電に関する注意事項



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## 12 メカニカル、パッケージ、および注文情報

以降のページには、メカニカル、パッケージ、および注文に関する情報が記載されています。この情報は、そのデバイスについて利用可能な最新のデータです。このデータは予告なく変更されることがあり、ドキュメントが改訂される場合もあります。本データシートのブラウザ版を使用されている場合は、画面左側の説明をご覧ください。

## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
OPA207ID	ACTIVE	SOIC	D	8	75	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA207	<a href="#">Samples</a>
OPA207IDBVR	ACTIVE	SOT-23	DBV	5	3000	RoHS & Green	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	1NBW	<a href="#">Samples</a>
OPA207IDBVT	ACTIVE	SOT-23	DBV	5	250	RoHS & Green	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	1NBW	<a href="#">Samples</a>
OPA207IDGKR	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	NIPDAUAG   SN	Level-2-260C-1 YEAR	-40 to 125	117Q	<a href="#">Samples</a>
OPA207IDGKT	ACTIVE	VSSOP	DGK	8	250	RoHS & Green	NIPDAUAG   SN	Level-2-260C-1 YEAR	-40 to 125	117Q	<a href="#">Samples</a>
OPA207IDR	ACTIVE	SOIC	D	8	2500	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	OPA207	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA207IDBVR	SOT-23	DBV	5	3000	180.0	8.4	3.23	3.17	1.37	4.0	8.0	Q3
OPA207IDBVT	SOT-23	DBV	5	250	180.0	8.4	3.23	3.17	1.37	4.0	8.0	Q3
OPA207IDGKR	VSSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA207IDGKT	VSSOP	DGK	8	250	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA207IDR	SOIC	D	8	2500	330.0	12.5	6.4	5.2	2.1	8.0	12.0	Q1

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA207IDBVR	SOT-23	DBV	5	3000	213.0	191.0	35.0
OPA207IDBVT	SOT-23	DBV	5	250	213.0	191.0	35.0
OPA207IDGKR	VSSOP	DGK	8	2500	366.0	364.0	50.0
OPA207IDGKT	VSSOP	DGK	8	250	366.0	364.0	50.0
OPA207IDR	SOIC	D	8	2500	340.5	336.1	25.0

**TUBE**


\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (μm)	B (mm)
OPA2071D	D	SOIC	8	75	507	8	3940	4.32



D0008A

# PACKAGE OUTLINE

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



4214825/C 02/2019

## NOTES:

- Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- This drawing is subject to change without notice.
- This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed  $.006$  [0.15] per side.
- This dimension does not include interlead flash.
- Reference JEDEC registration MS-012, variation AA.



# EXAMPLE BOARD LAYOUT

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
 EXPOSED METAL SHOWN  
 SCALE:8X



SOLDER MASK DETAILS

4214825/C 02/2019

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON .005 INCH [0.125 MM] THICK STENCIL  
SCALE:8X

4214825/C 02/2019

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.



# EXAMPLE BOARD LAYOUT

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214839/K 08/2024

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214839/K 08/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

# DGK0008A



# PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



**NOTES:**

PowerPAD is a trademark of Texas Instruments.

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

# EXAMPLE BOARD LAYOUT

DGK0008A

<sup>TM</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 15X



SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

# EXAMPLE STENCIL DESIGN

DGK0008A

<sup>TM</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
SCALE: 15X

4214862/A 04/2023

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.



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