# Low-side, bidirectional current sensing circuit

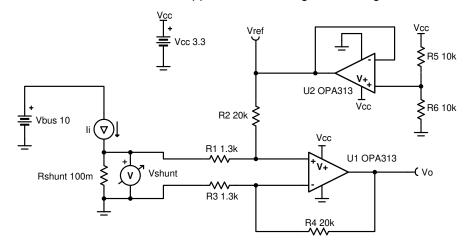


# **Design Goals**

Input		Output		Supply		
l <sub>iMin</sub>	I <sub>iMax</sub>	V <sub>oMin</sub>	$V_{oMax}$	V <sub>cc</sub>	V <sub>ee</sub>	V <sub>ref</sub>
-1A	1A	110mV	3.19V	3.3V	0V	1.65V

#### **Design Description**

This single-supply low-side, bidirectional current sensing solution can accurately detect load currents from –1A to 1A. The linear range of the output is from 110mV to 3.19V. Low-side current sensing keeps the common-mode voltage near ground, and is thus most useful in applications with large bus voltages.



#### **Design Notes**

- 1. To minimize errors, set  $R_3 = R_1$  and  $R_4 = R_2$ .
- 2. Use precision resistors for higher accuracy.
- 3. Set output range based on linear output swing (see A<sub>ol</sub> specification).
- 4. Low-side sensing should not be used in applications where the system load cannot withstand small ground disturbances or in applications that need to detect load shorts.



# **Design Steps**

1. Determine the transfer equation given  $R_4 = R_2$  and  $R_1 = R_3$ .

$$V_{o} = \left(I_{i} \times R_{shunt} \times \frac{R_{4}}{R_{3}}\right) + V_{ref}$$

$$V_{ref} = V_{cc} \times \left(\frac{R_6}{R_5 + R_6}\right)$$

2. Determine the maximum shunt resistance.

$$R_{shunt} = \frac{V_{shunt}}{I_{imax}} = \frac{100mV}{1 A} = 100m\Omega$$

- 3. Set reference voltage.
  - a. Since the input current range is symmetric, the reference should be set to mid supply. Therefore, make  $R_5$  and  $R_6$  equal.

$$R_5 = R_6 = 10k\Omega$$

4. Set the difference amplifier gain based on the op amp output swing. The op amp output can swing from 100mV to 3.2V, given a 3.3-V supply.

$$Gain = \frac{V_{0Max} - V_{0Min}}{R_{Shunt} \times (I_{iMax} - I_{iMin})} = \frac{3.2 \text{ V} - 100 \text{mV}}{100 \text{m}\Omega \times (1 \text{ A} - (-1 \text{ A}))} = 15.5 \text{ } \frac{\text{V}}{\text{V}}$$

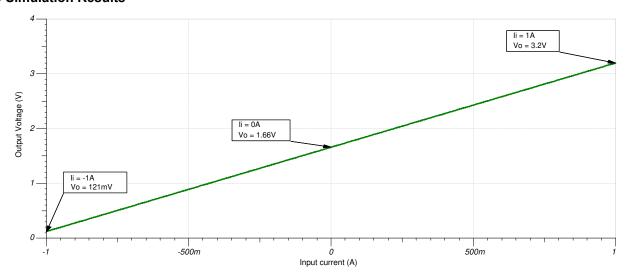
Gain = 
$$\frac{R_4}{R_3}$$
 = 15 .5  $\frac{V}{V}$ 

Choose  $R_1 = R_3 = 1.3k\Omega$  (Standard Value)

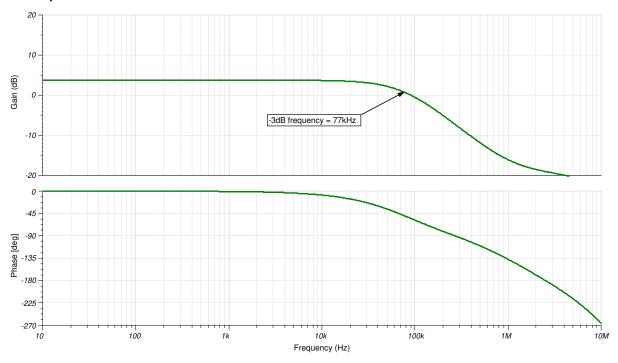
$$R_2=R_4=15.5\frac{V}{V}\times 1.3 k\Omega=20.15~k\Omega\approx 20 k\Omega$$
 (Standard Value)

# **Design Simulations**

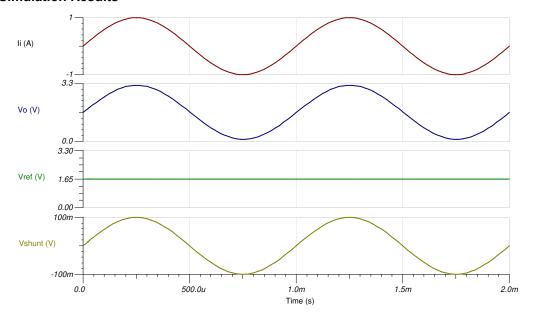
# **DC Simulation Results**



# **Closed Loop AC Simulation Results**



# **Transient Simulation Results**



#### **Design References**

See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.

See circuit SPICE simulation file SBOC500.

See TIPD175, www.ti.com/tipd175.

# **Design Featured Op Amp**

OPA313				
V <sub>cc</sub>	1.8V to 5.5V			
V <sub>inCM</sub>	Rail-to-rail			
V <sub>out</sub>	Rail-to-rail			
V <sub>os</sub>	500μV			
Iq	50μA/Ch			
l <sub>b</sub>	0.2pA			
UGBW	1MHz			
SR	0.5V/µs			
#Channels	1, 2, 4			
www.ti.com/p	roduct/opa313			

# **Design Alternate Op Amp**

	TLV9062	OPA376
V <sub>cc</sub>	1.8V to 5.5V	2.2V to 5.5V
V <sub>inCM</sub>	Rail-to-rail	Rail-to-rail
V <sub>out</sub>	Rail-to-rail	Rail-to-rail
V <sub>os</sub>	300µV	5µV
Iq	538μA/Ch	760μA/Ch
I <sub>b</sub>	0.5pA	0.2pA
UGBW	10MHz	5.5MHz
SR	6.5V/µs	2V/μs
#Channels	1, 2, 4	1, 2, 4
	www.ti.com/product/tlv9062	www.ti.com/product/opa376

For battery-operated or power-conscious designs, outside of the original design goals described earlier, where lowering total system power is desired.

LPV821				
V <sub>cc</sub>	1.7V to 3.6V			
V <sub>inCM</sub>	Rail-to-rail			
V <sub>out</sub>	Rail-to-rail			
V <sub>os</sub>	1.5µV			
Iq	650nA/Ch			
I <sub>b</sub>	7pA			
UGBW	8KHz			
SR	3.3V/ms			
#Channels	1			
www.ti.com/product/lpv821				



# **Revision History**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision A (May 2018) to Revision B (January 2019)  - Brotherstiale tthreititleit.cookbook landing page		
C	hanges from Revision * (February 2018) to Revision A (May 2018)	Page
•	Changed title role to 'Amplifiers'	1
•	Added SPICE simulation file link	1
•	Added LPV821 as a Design Alternate Op Amp for battery-operated or power-conscious designs	1

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