

Thermistor Coefficient Calculator for TI Advanced Fuel Gauges

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Battery Management

ABSTRACT

TI advanced fuel-gauge battery-management ICs use a polynomial model to translate the voltage measured across the thermistor terminals into a temperature value. While the recommended Semitec AT103 is readily available, some customers prefer to use an alternate device. This report describes the use of a companion Excel® spreadsheet that automates coefficient calculation for a given thermistor. Project collateral discussed in this application report can be downloaded from the following URL: www.ti.com/lit/zip/SLUA398.

1 Introduction

The firmware algorithm in TI advanced fuel gauge battery management ICs uses a polynomial model to translate voltage measured across the thermistor terminals into temperature. While the recommended Semitec AT103 is readily available in various shapes, some customers prefer to use an alternate device. This report describes the use of a companion Excel spreadsheet that automates the calculation of coefficients for a given thermistor.

The Thermistor Coefficient Calculator is a Microsoft[®] Excel spreadsheet, which is available as a zip file in the same location as this report. It can be used for various advanced fuel gauge ICs such as the bq2084, bq20z70, bq20z80, bq20z90, etc.

2 Theory of Operation

Solver, an add-in tool for Excel, which is part of the standard installation, is used in this case to find a solution to a set of 3rd order polynomials. Given a few points on an unknown curve, it finds the coefficients of a cubic polynomial equation that best fits the available data. The fuel-gauge device firmware uses the cubic polynomial along with the dataflash-based coefficients at 1-s intervals when converting the A/D reading from the thermistor into a temperature value.

Solver's job is to minimize the value in cell B33 (see Figure 1), which is the sum of the norms for each known data point. The norms are simply the square of the difference between what you want and what you get. Solver updates the polynomial coefficients in E25 ~ E28 for the best overall fit. You can, of course, change the coefficients manually to see what happens. The values in E31 ~ E36 should be programmed into the respective fuel gauge dataflash locations.

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Thermistor Tables

				atarfflash Thermistor Consta	nts E	F	G	HI	J	K L	
		Calculation of best-fit									
			Calculation of	(using 3rd order					Partial Result Bounds		
1 T	Temperature	Resistance	A/D Count	polynomial)	Norm	Instructions		c	Check		
2	-20	67770	25982	-19.55338015	0.199469	1. Insert Temperature and Res	sistance values in colums A&B	1	10248.5197	-3774.69	
3	-15	53410	25309	-15.13893104	0.019302	2. Verify A/D count value in ce	II C2 does not exceed 27000	1	10557.1208	-3760.757	
4	-10	42470	24537	-10.40258881	0.162078	If necessary, raise value	e of R1 in cell B24 to a higher standard	1	10911.1179	-3752.579	
5	-5	33900	23646	-5.334192226		resistor value so that C2			11319.6818		
6	0	27280	22657	-0.155141665			enu. Use Add-Ins menu if not available.		11773.1833		
7	5	22050	21562	5.103094832		4. Set Target Cell to \$B\$33			12275.2905		
8	10	17960	20391	10.26512627		5. Choose Equal to: Value Of 0 (choose "Value Of", enter 0			12812.2472		
9	15	14690	19143	15.35518484		6. Set "By Changing Cells" to \$E\$25:\$E\$28			13384.5119		
10	20	12090	17853	20.30002249		7. Press Solve button - Accept the solution, even though not "feasible"			13976.0355		
11	25	10000	16537	25.1540882		8. Compare columns A and D to evaluate the accuracy			14579.4813		
12	30	8313	15220	29.96452929		A lower number in B33 indicates a better fit			15183.3856		
13	35	6940	13920	34.80931675		9. Linearity may be improved by changing R2 in some cases			15779.4947		
14 15	40 45	5827	12668	39.69777558		10. Insure none of the values in columns J or K exceed +/- 32767			16353.5936		
16	45	4911 4160	11469 10344	44.70168577 49.78340483					16903.3895		
17	55	3536	9293	49.78340483 54.9514734					17419.2531 17901.1844		
18	60	3020	8328	60.11969589					18343.6807		
19	65	2588	7445	65.25409511			— Tout (pulsed Vref)		18748.5763		
20	70	2228	6648	70.25884332	0.004304	R1 <	2		19114.0371		
21	75	1924	5927	75.11718798		9	>		19444.6483		
22	80	1668	5283	79.74269257		8.45k (typ)			19739.9516		
23	00	TS (measurement)				02101010					
	R1	8450	1	Polynomial coefficients	Value	1	– i S (measurement)				
	R2	61900		A0	4032.48						
	Vref	3.3		A0 A1	-7837.818						
	Vadref	3.3		A2	22162.45		Thermistor				
	ADres	0.000100708		A3	-30050.77						
	Vadmax	2.64				R2 <	10K@25°C				
	Rs	7435.03909		Data Flash Thermistor Co	netante	61.9K (typ)	> \$\				
	Vs	2.903624733		A0 (** Coefficient 4)	4032	• (.) ()					
32	¥5	2.000024100	1	A1 (** Coefficient 3)	-7838		and the second				
	Sum of Norms:	1.330484661		A2 (** Coefficient 2)	22162	ſ					
34	com or Norms.	1.550404001		A3 (** Coefficient 1)	-30051	_	-				
35				Min A/D							
36				Max Temp (K)	4032						
37		** The polynomial coefficients have alternate names in some fuel gauges									

Figure 1. Thermistor Coefficient Calculator Spreadsheet

3 Thermistor Tables

Enter the data for the desired thermistor into cells B2 ~ B22 which correspond to the temperatures in column A. Some vendors include resistance tables in their catalog; others provide a calculator for you to generate them. If a given vendor only supplies a small table with multiples of 10°C, then use it as-is in the spreadsheet, but include some of the degree-resistance pairs twice to fill up the table of 21 pairs.

4 Circuit Modifications

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For maximum accuracy, the voltage input voltage to the A/D converter in the fuel gauge should be limited to around 82% of the reference voltage, which is the same as V_{CC} in this case. Looking at it another way, the A/D count should not exceed 27000 (82% of full scale 32767) counts for low temperature readings that must be accurate. Column C displays the expected A/D count for a given temperature. Measurements between 27000 and 32767 will be degraded somewhat, but still useful.

The recommended thermistor circuit, where R1 = 8.45 k Ω , R2 = 61.9 k Ω and Thermistor = 10 k Ω at 25°C, should satisfy the above requirement in most cases. However, if a 10-k Ω thermistor cannot be used, the fixed resistors should be modified in cells B24 and B25 to optimize the measurement. B25 is used to linearize the thermistor curve somewhat, enhancing the polynomial curve-fitting accuracy.

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