

# Selecting Electrolytic Bus Capacitor for Universal input (85-V to 265-V RMS) Low Power Adapters ( $P_{in} < 75\text{-W}$ )

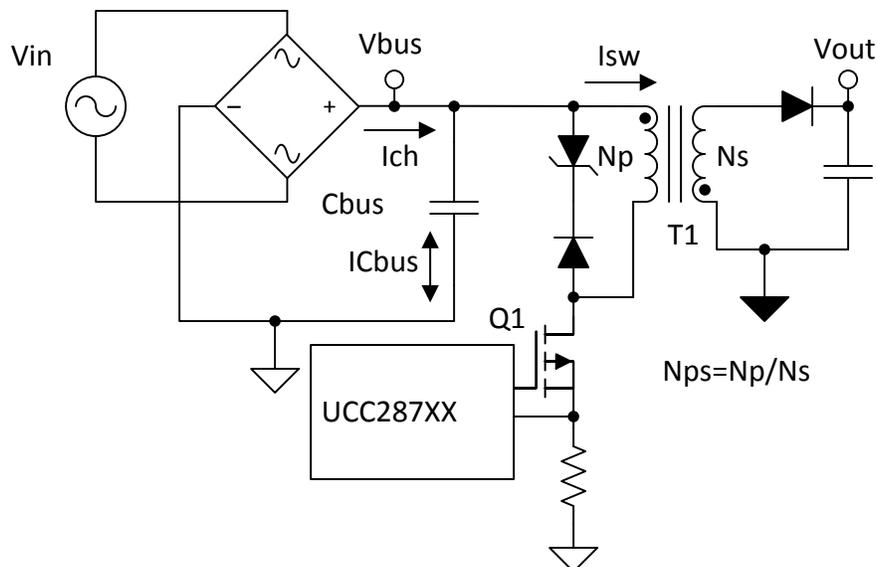
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## 1 Introduction

In the past designers would have selected the converter's bus capacitor ( $C_{bus}$ ) using various approximations and "rules of thumb" which are not particularly accurate.

This application note presents a quick and reliable method for selecting the smallest electrolytic input bus capacitors that will provide the desired service life in ac-to-dc converters with capacitive input filters.

We will consider a quasi resonant flyback converter (Figure 1). Since most inexpensive simulator tools do not allow use of subscripts, so subscripts were intentionally left out of this application note.



**Figure 1. Simplified Low Power AC-to-DC Adapter Flyback Schematic**

The bus capacitor  $C_{bus}$ , sometime referred to as the bulk capacitor, stores and delivers energy ( $w$ ) to the power system.

$$w = \frac{1}{2} C_{bus} \times V_{bus}^2 \quad (1)$$

Capacitor  $C_{bus}$  is charged every half line cycle by low frequency current and discharged continuously by the high-frequency current pulses drawn by the converter. This action results in a low frequency ac current ( $I_{lf}$ ) and a high frequency ac current ( $I_{hf}$ ) passing through  $C_{bus}$ . This application brief will use circuit simulation to obtain the RMS current of  $I_{lf}$  and calculate  $I_{hf}$  going through  $C_{bus}$ .

$$I_{Cbus} = I_{lf} + I_{hf} \quad (2)$$

The bus capacitor ( $C_{bus}$ ) selection algorithm consists of few simulation iterations of a circuit model based on the output power requirements ( $P_{out}$ ), assumed efficiency ( $\eta$ ), and the duty cycle of the converter ( $D$ ) this algorithm enables selection of capacitors that will provide the service life required by the application.

The algorithm will be illustrated for the converter with the following specifications:

- $P_{out} = 45\text{-W}$  output power
- $V_{out} = 20\text{-V}$ , output voltage
- $V_{in} = 85\text{-}265\text{-V}$  RMS, input voltage
- $\eta = 90\%$
- $V_{bus(\min)} = 75\text{ v}$ , lowest allowable dc bus voltage
- Service life: 2000 hours @full load, 100v 50hz input, 80°C internal ambient temperature.
- $f_{sw} = 100\text{ khz}$ , converter switching frequency @ highest  $I_{lf}$  and  $I_{hf}$
- $D_{\max} = 50\%$ , maximum duty cycle

Selecting the bus capacitor ( $C_{bus}$ ):

1. Select a bus capacitor voltage rating greater than the maximum bus voltage ( $V_{bus(\max)}$ ).

$V_{bus(\max)}$  can be calculated on the maximum RMS input voltage ( $V_{in(\max)}$ ) using equation 3. For this design the maximum bus voltage would be 375-V the voltage rating of  $C_{bus}$  needs to be rated for higher voltage than calculated, so 400-V is appropriate for this design.

$$V_{bus(\max)} = V_{in(\max)} \times \sqrt{2} = 265V \times \sqrt{2} = 375V \quad (3)$$

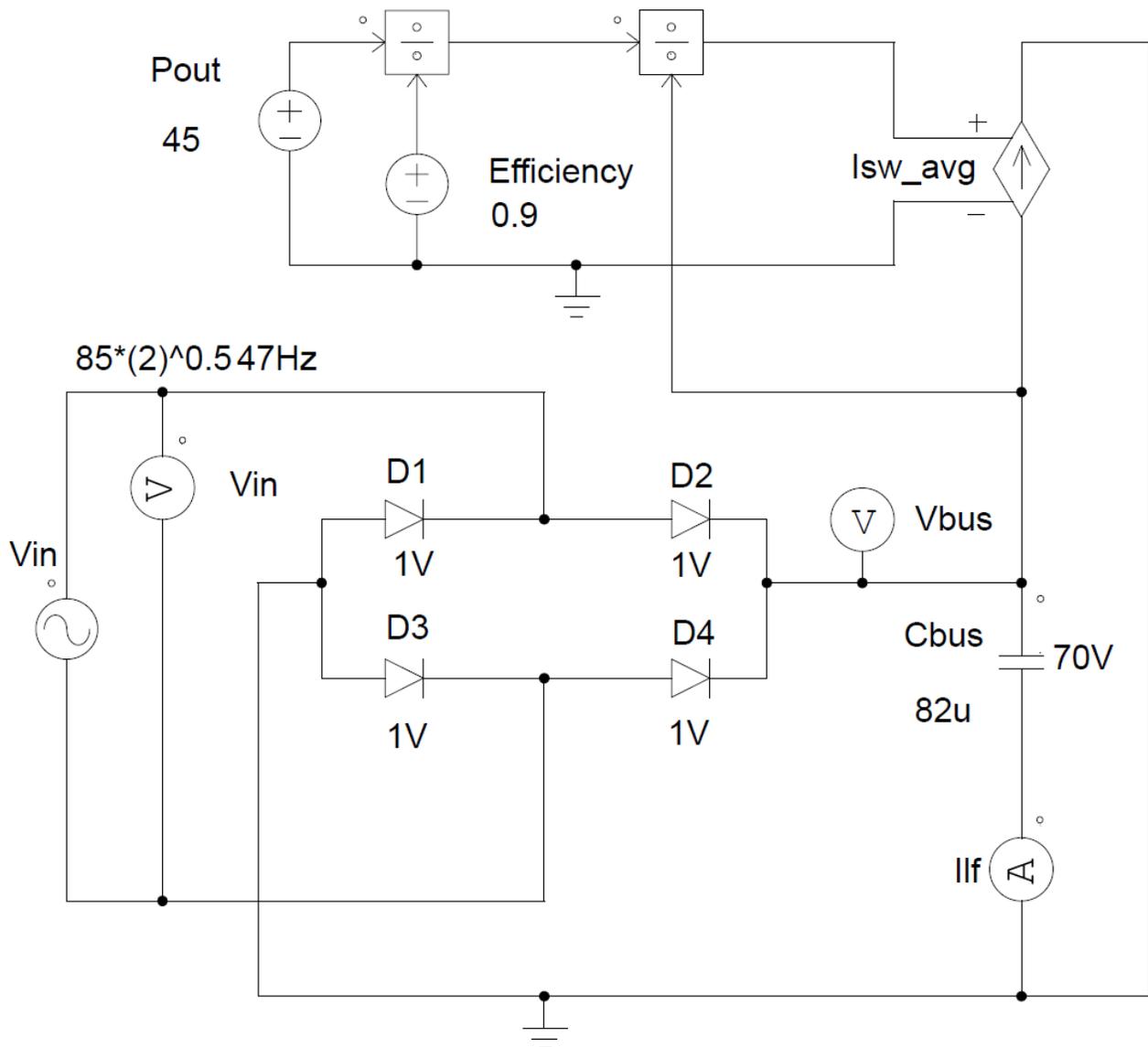
2. Assuming a minimum dc bus voltage of 75-V, calculate the average input current of the converter and select an initial bus capacitor ( $C_{bus(\text{init})}$ ) value based on 120uF/ampere dc:

$$C_{bus(\text{init})} = \frac{120\mu F}{1A} \times \frac{P_{out}}{V_{bus(\min)} \times \eta} = \frac{120\mu F}{1A} \times \frac{45W}{75V \times 0.9} \approx 80\mu F \quad (4)$$

3. We select the next standard value capacitor equal to or greater than  $C_{bus(\text{init})}$

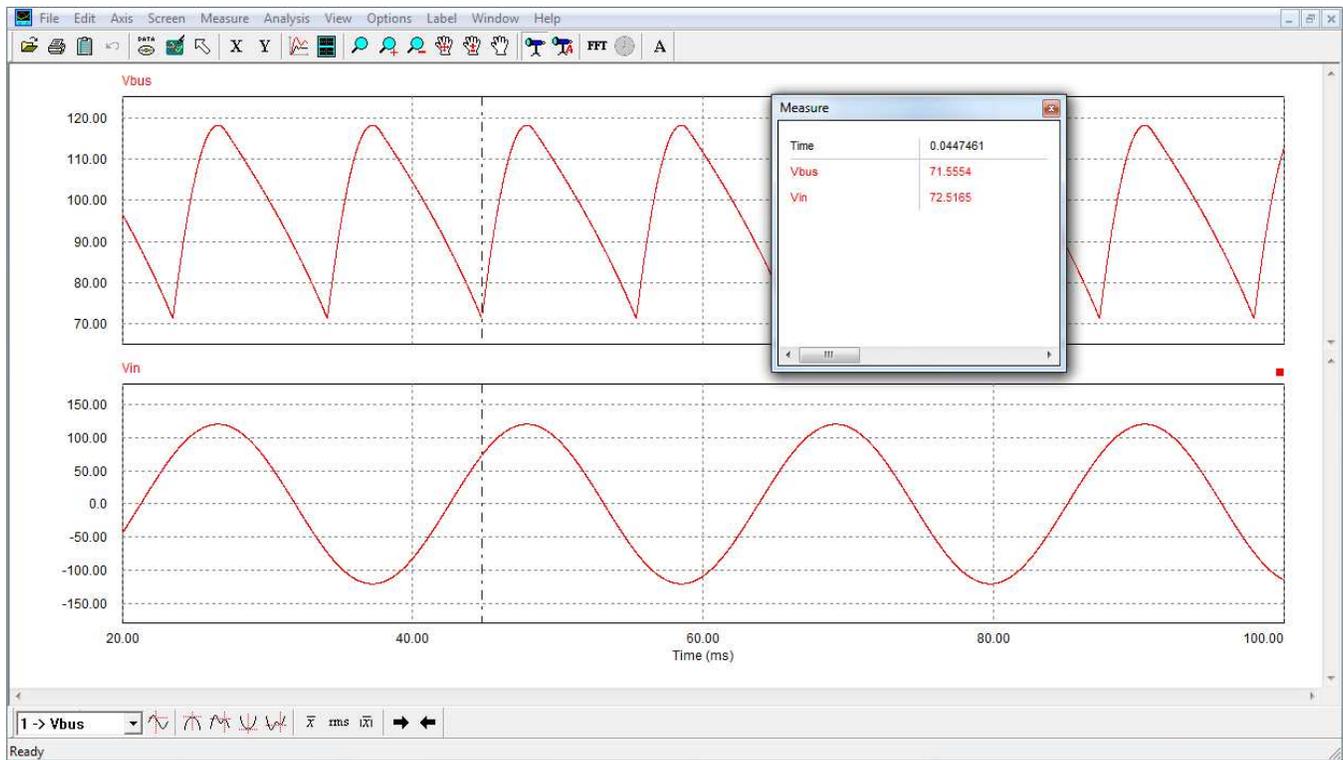
$$C_{bus} = 82\mu F \quad (5)$$

4. Use your favorite circuit simulator and the model presented in figure 2 to extract the maximum  $C_{bus}$  low frequency current ( $I_{lf}$ ), which occurs at the maximum output power and minimum input voltage. In order to avoid division by zero at divider on  $C_{bus}$  should be set to a positive voltage (say 70-V) and the simulation run until the circuit reaches steady-state.



**Figure 2. Cbus Low Frequency Current (Ilf) Simulation Model**

The 82uf capacitor yields a minimum bus voltage of 71.6 v, which is below the minimum 75v bus voltage requirement, so a larger capacitance value must be selected.

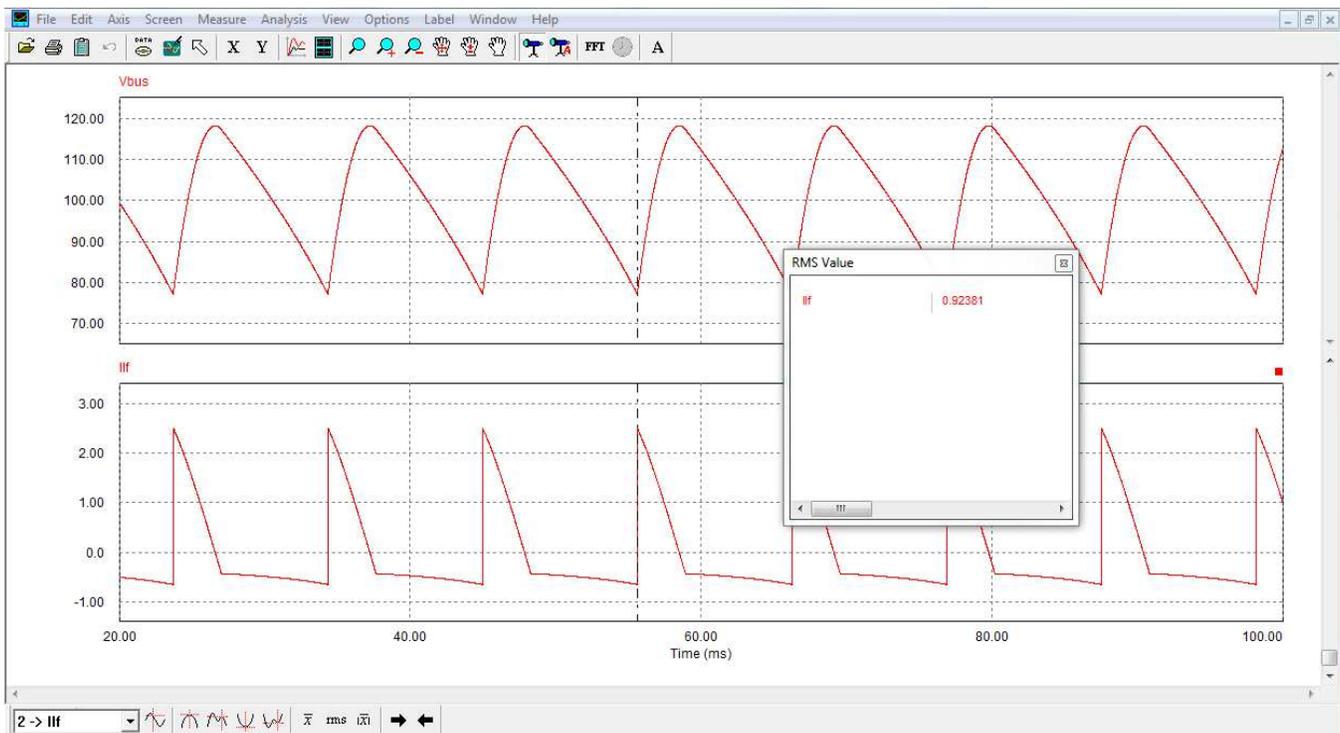


**Figure 3. first Vbus Ripple Voltage Simulation**

5. Selecting two 47uf capacitors in parallel for a total of 94 uf yields a minimum bus voltage of 78-V and a total (I<sub>lft</sub>) of 924 mA, 100-Hz RMS low frequency current , (462 mA of low frequency current (I<sub>lf</sub>) through each C<sub>bus</sub> capacitor).

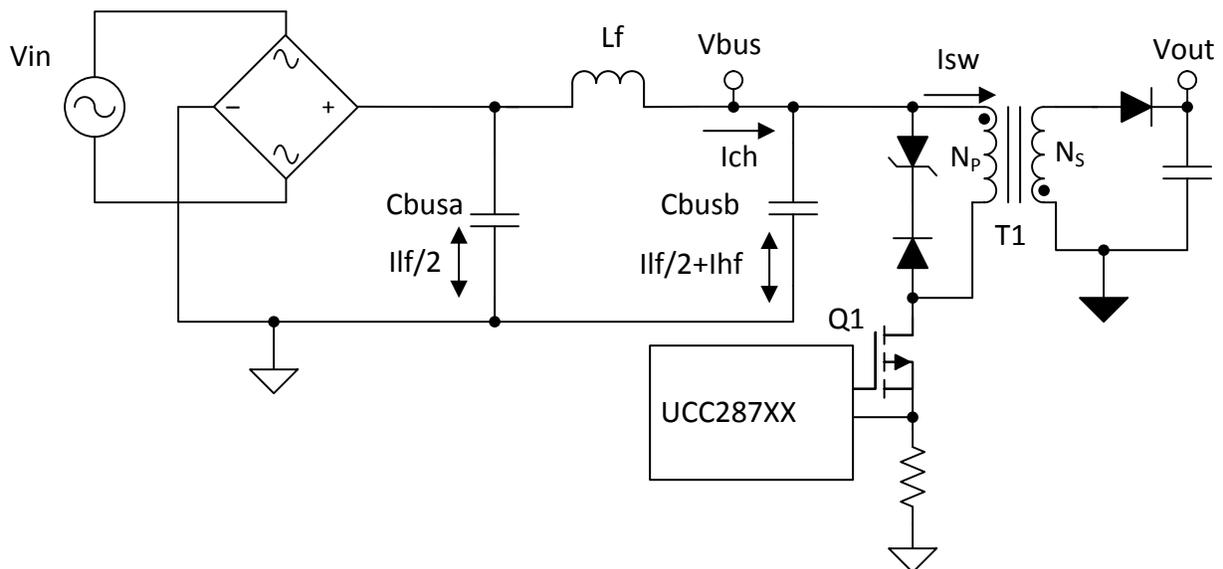
$$I_{lft} \approx 924mA \tag{6}$$

$$I_{lf} \approx \frac{924}{2}mA = 462mA \tag{7}$$



**Figure 4. Ripple Voltage Simulation, Cbus = 2x47uf**

Having two capacitors in parallel provides the opportunity to create a differential mode EMI  $\pi$  filter by inserting an RF filter inductor ( $L_f$ ) in between the two caps (figure 5), which will force the high-frequency current to flow into  $C_{busb}$ , but have little impact on the sharing of low frequency current between the two capacitors.



**Figure 5. low power offline power adaptor.**

The maximum high frequency RMS current ( $I_{hf}$ ) going through the bus capacitor ( $C_{busb}$ ) in this example can be calculated based on  $p_{out}$ ,  $V_{bus(min)}$ , estimated efficiency ( $\eta$ ), and knowing the converters maximum duty cycle. for this design example the maximum duty cycle was limited to 50%.

$$D_{max} = 0.5 \quad (8)$$

First calculate the peak switch current ( $I_{swpk}$ ):

$$I_{swpk} = \frac{P_{out} \times 2}{V_{bus(min)} \times Efficiency \times D_{max}} = \frac{45W \times 2}{78V \times 0.9 \times 0.5} \approx 2.56 \quad (9)$$

With  $I_{swpk}$  the  $I_{hf}$  RMS current can be calculated:

$$I_{hf} = \sqrt{\left( I_{swpk} \times \sqrt{\frac{D_{max}}{3}} \right)^2 - \left( I_{swpk} \times \frac{D_{max}}{2} \right)^2} \quad (10)$$

$$I_{hf} = \sqrt{\left( 2.56A \times \sqrt{\frac{0.5}{3}} \right)^2 - \left( 2.56 \times \frac{0.5}{2} \right)^2} = 826mA \quad (11)$$

6. Once the simulation is complete and you have the simulated value of  $I_{lf}$  and calculated  $I_{hf}$  for the bus capacitor/s used in your design, extract from the datasheet of your favorite electrolytic capacitors family the rated 120 Hz ripple current ( $I_{lf}$ ), the frequency ripple current coefficient (K) and the rated load life (L) of 47- $\mu$ f, 400-V at the current  $I_{lf}$  and rated ambient temperature. For our example, we select an 47- $\mu$ f capacitor with a 100-kHz ripple current rating ( $I_{lf}$ ) of 1.2-A @85° C, a frequency ripple current ripple coefficient K of 2 and load life L of 2000 hours @85°C.
7. Calculate the effective RMS current ( $I_{eff}$ ) in the bus capacitor using equation 4 (see appendix for derivation):

$$I_{eff} = \sqrt{I_{lf}^2 + \frac{I_{hf}^2}{K^2}} = \sqrt{(462mA)^2 + \left(\frac{826mA}{2}\right)^2} \approx 620mA \quad (12)$$

8. The load life  $L_x$  of the capacitor can be calculated using equation 13. Please note there is a derivation of the formula in the appendix at the end of the application note. in our design example we are calculating  $L_x$  based on:
  - $T_{max}$  is the rated ambient temperature from the datasheet (85° C for our case)
  - $\Delta T_{max}$  is the maximum allowed hotspot temperature rise above the ambient  $T_{max}$  (typically 5° C for 105° C rated capacitors, 15° C for 85° C rated capacitors - contact the manufacturer for more specific information)
  - L is the rated load life at @ the rated ambient temperature  $T_{max}$  (2000 hrs. for our case)
  - $T_x$  is the operating ambient temperature (80°C for our case)
  - In our example the life of the capacitor is calculated to be 2144 hours
  - If this service life is not acceptable, the next larger value or higher ambient temperature (105oc instead of 85oc) can be selected – the change will have size and/or cost consequences.

$$L_x = L \times 2^{\left[ \frac{T_{max} - T_x + \Delta T_{max} \times \left( 1 - \frac{I_{eff}^2}{I_{lf}^2} \right)}{10} \right]} = 2000hr \times 2^{\left[ \frac{85^\circ C - 80^\circ C + 5^\circ C \times \left( 1 - \frac{(620mA)^2}{(462mA)^2} \right)}{10} \right]} = 2144hrs \quad (13)$$

This application note demonstrated with the use of proper simulation and modeling a bus capacitor or capacitors can be more accurately selected to meet your design requirements in low power offline flyback converters. This technique gives a more accurate prediction of the low and high frequency bus capacitor RMS current that can be used to select a better bus capacitor for the design with a longer life.

## 2 Appendix: Formulas Derivation.

### 1. Effective RMS current ( $I_{eff}$ ):

Since the capacitor's maximum internal temperature rise above the ambient is the same for low and high-frequency ripple current power dissipation must be equal for both:

$$ESR_{LF} \times I_{LF}^2 = ESR_{HF} \times I_{HF}^2 \quad (14)$$

$$\frac{I_{HF}}{I_{LF}} = K \quad (15)$$

(Where k is the frequency ripple current coefficient provided by the datasheet)

Therefore, the high frequency ESR is:

$$ESR_{HF} = \frac{I_{LF}}{K^2} \quad (16)$$

The equivalent RMS current for the mix of low and high-frequency currents will be:

$$I_{eff}^2 \times ESR_{LF} = I_{LFx}^2 \times ESR_{LF} + I_{HFx}^2 \times \frac{ESR_{LF}}{K^2} \quad (17)$$

$$I_{eff}^2 = \sqrt{\frac{I_{HFx}^2}{K^2} + I_{LFx}^2} \quad (18)$$

### 2. Life Expectancy Calculation:

The life expectancy vs. temperature of electrolytic capacitors follows arrhenius' law, i.e. it decreases by a factor of 2 for every 10°C increase in temperature. most caps manufacturers specify the internal hot spot  $\Delta T$  of 5° c and 15° c respectively for capacitors rated 105° C and 85° C ambient temperature.

Defining:

- $T_{max}$  Rated ambient temperature
- $\Delta T_{max}$  Maximum allowed internal hotspot temperature rise above Tmax
- $T_x$  Operating ambient temperature
- $\Delta T_x$  Operating hotspot temperature rise above  $T_x$
- L Rated load life at  $T_{max}$
- $L_x$  Load life at  $T_x$

$$\Delta T_x = \Delta T_{max} \times \left( \frac{I_{eff}}{I_{LF}} \right)^2 \quad (19)$$

$$L_x = L \times 2 \frac{[T_{max} + \Delta T_{max} - (T_x + \Delta T_x)]}{10} \quad (20)$$

$$L_x = L \times 2 \frac{[T_{max} + \Delta T_{max} \times \left(1 - \frac{I_{eff}^2}{I_{LF}^2}\right)]}{10} \quad (21)$$

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