ABSTRACT

The TPS65233 and TPS65235 are designed for analog and digital satellite receivers. They are monolithic voltage regulator with I²C interface. This application report mainly introduces some design considerations in application which including soft start design consideration, I²C address and tone mode setup, DiSEqc2.x tone design consideration and surge protection design consideration.

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1 Introduction
TPS65233 and TPS65235 are LNB (Low Noise Block) voltage regulators for digital and analog satellite receivers. It offers a complete solution with low component count, low power dissipation, together with simple design and I²C standard interface.

2 Soft Start Design Consideration

2.1 Soft Start
Usually LNB regulator needs to support different types of LNB, some LNBs have smaller capacitive load, some have larger capacitive load up to serval hundreds of micro farad.

With this higher capacitive load on VLNBo output, the startup current is higher and reaches the current limit set for the devices, this triggers the hiccup timer. If this over current situation keeps longer than hiccup ON time (8 ms maximum for TPS65235 and 4 ms for TPS65233), the device is in hiccup state which means off and startup again, this is not expected in application.

Equation 1 can be used to do the estimation for startup current.

\[ I_{\text{startup}} (mA) = \frac{C_{\text{load}} (\mu F) \times V_{\text{VLNB}} (V)}{T_{\text{SS}} (ms)} \]

where
- \( I_{\text{startup}} \rightarrow \) Startup current
- \( T_{\text{SS}} \rightarrow \) Soft start time
- \( V_{\text{VLNB}} \rightarrow \) VLNBo output voltage when startup
- \( C_{\text{load}} \rightarrow \) Capacitive load on VLNBo output

In TPS65233 or TPS65235 design, an external capacitor is added on TCAP pin to implement the soft start time control, Equation 2 is used to do the estimation for soft start time

\[ T_{\text{SS}} (ms) = \frac{C_{\text{SS}} (nF) \times V_{\text{VLNB}} (V)}{I_{\text{SS}} (\mu A) \times K} \]

where
- \( I_{\text{SS}} \rightarrow \) Internal charging current for TCAP pin, about 10 µA
- \( C_{\text{SS}} \rightarrow \) External capacitor on TCAP pin
- \( K \rightarrow \) Internal ratio, 10 for TPS65233, 6 for TPS65235

Combine Equation 1 and Equation 2, Equation 3 to provide a startup current estimation.

\[ I_{\text{startup}} (mA) = \frac{C_{\text{load}} (\mu F) \times I_{\text{SS}} (\mu A) \times K}{C_{\text{SS}} (nF)} \]

Based on this equation, for TPS65233 or TPS65235, since the \( I_{\text{SS}} \) and \( K \) is fixed, given \( C_{\text{load}} \) (capacitive load on VLNBo output), the conclusions are as follows:
- The startup current is not related to VLNBo startup voltage.
- The larger \( C_{\text{SS}} \) (capacitor on TCAP pin), the smaller startup current.

For TPS65233 and TPS65235, the \( I_{\text{SS}} \) is nearly same about 10 µA, while for \( K \), it is different. For TPS6233, the \( K \) is 10, and for TPS65235, the \( K \) is 6.
2.2 TPS65235 Soft Start Test Result

2.2.1 Normal Startup

The startup current for TPS65235 is in Figure 1 and Figure 2. With 100 µF ±20% capacitive load on VLN output, the $C_{SS}$ is 22 nF. Based on Equation 3, the startup current is not related to VLN startup voltage, either with 13.4-V VLN output or 18.2-V VLN output, the startup current is same with 232 mA.

\[
C_{SS} = 22 \text{ nF} \\
C_{load} = 100 \text{ µF}
\]

Figure 1. Startup with 13.4-V VLN Output

\[
C_{SS} = 22 \text{ nF} \\
C_{load} = 100 \text{ µF}
\]

Figure 2. Startup with 18.2-V VLN Output
2.2.2 Startup with Different HICCUP_ON Time

Keep the same \( C_{SS} \) with 22 nF, enlarge the capacitive load on VLN output to 560 \( \mu \)F ±20%. With 13.4-V VLN output startup, the waveform is in Figure 3.

Based on the Equation 3, the startup current is 1.4 A, it is larger than the OCL setting 1 A in TPS65235. Triggering the OCL leads the hiccup timer starts to count and limits the VLN output charging the capacitive load with 1 A current only.

For TPS65235, the hiccup ON/OFF time is about 4 ms / 128 ms and 8 ms / 256 ms selectable by \( \text{i}^2\text{C} \) register. As default, it is 4 ms / 128 ms setting.

\[
\begin{align*}
C_{SS} &= 22 \text{ nF} \\
C_{load} &= 560 \text{ \( \mu \)F} \\
\text{Hiccup\_ON} &= 4\text{ms}
\end{align*}
\]

*Figure 3. Startup with 13.4-V VLN and Hiccup Triggered*

\[
\begin{align*}
C_{SS} &= 22 \text{ nF} \\
C_{load} &= 560 \text{ \( \mu \)F} \\
\text{Hiccup\_ON} &= 8\text{ms}
\end{align*}
\]

*Figure 4. Startup with 13.4-V VLN and non Hiccup Triggered*

With 1-A charging on 560 \( \mu \)F \( C_{load} \). It takes about 7.2 ms for 13.4-V VLN output to startup, which is less than hiccup ON time 8 ms, the startup can be finished without hiccup trigger in Figure 4.

Due to the current is limited to be 1 A for charging the capacitive load on VLN, the VLN output voltage ramping is lower than TCAP voltage ramping in Figure 4.

Setting the hiccup ON/OFF time to be 8 ms / 256 ms, it can be implemented by pull EN to low when power up, then control the VLN output through the \( \text{i}^2\text{C} \) register. For the detail, refer to 7.3.10 in SLVSD80.
2.2.3 Startup with Different $C_{SS}$ on TCAP Pin

With same setting, when startup with 18.2-V VLN1 output voltage, OCL 1-A charging on about 560-µF capacitive load, it takes about 10 ms for 18.2-V VLN1 output startup. Which means even put the hiccup ON time to be 8 ms, it still cannot startup without hiccup trigger in Figure 5.

Based on Equation 3, the $C_{SS}$ on TCAP pin should be enlarged to make sure the startup current to be less than OCL value. Replace $C_{SS}$ with 47-nF capacitor, and the startup waveform is in Figure 6. The startup current is 630 mA, since the OCL is not triggered, the hiccup timer is not started, and the startup waveform is not related to the hiccup ON time.

$$C_{SS} = 22 \text{nF}$$
$$C_{load} = 560 \text{µF}$$
$$\text{Hiccup\_ON} = 8 \text{ms}$$

Figure 5. Startup with 18.2-V VLN1 and Hiccup Triggered

$$C_{SS} = 22 \text{nF}$$
$$C_{load} = 560 \text{µF}$$
$$\text{Hiccup\_ON} = 4 \text{or 8 ms}$$

Figure 6. Startup with 18.2-V VLN1 and non Hiccup Triggered
2.2.4 Startup with Different OCL Setting

With same setting, and the OCL lowered from 1 A to 560 mA with a 630 mA startup current, the over current and hiccup timer are triggered. Figure 7 shows a hiccup when started up with 13.4-V VLNB output and OCL 560 mA setting. To fix this, the 68 nF C\text{SS} is used for to get a lower startup current of 450 mA in Figure 8 and Figure 9.

**Figure 7. Startup with 13.4-V VLNB and Hiccup Triggered**

\[
\begin{align*}
C_{\text{SS}} &= 47 \text{nF} \\
C_{\text{load}} &= 560 \mu\text{F} \\
\text{OCL} &= 560 \text{mA} \\
\text{Hiccup_ON} &= 8 \text{ms}
\end{align*}
\]

**Figure 8. Startup with 13.4-V VLNB and non Hiccup Triggered**

\[
\begin{align*}
C_{\text{SS}} &= 68 \text{nF} \\
C_{\text{load}} &= 560 \mu\text{F} \\
\text{OCL} &= 560 \text{mA} \\
\text{Hiccup_ON} &= 4 \text{ or } 8 \text{ms}
\end{align*}
\]

**Figure 9. Startup with 18.2-V VLNB Output**

\[
\begin{align*}
C_{\text{SS}} &= 68 \text{nF} \\
C_{\text{load}} &= 560 \mu\text{F} \\
\text{OCL} &= 560 \text{mA} \\
\text{Hiccup_ON} &= 4 \text{ or } 8 \text{ms}
\end{align*}
\]
2.3 **TPS65233 Soft Start Test Results**

The startup current for TPS65233 is in Figure 10 and Figure 11, with 100 µF ±20% capacitive load on VLNB output, the $C_{SS}$ is 22 nF. Either with 13.4-V VLNB output or 18.6-V VLNB output, the startup current is same with 470 mA. Based on the Equation 3, the $K$ in the TPS65233 is 10 which is larger than TPS65235, with the same setting, the startup current is larger than TPS65235.

For TPS65233, all the behaviors are same with the TPS65235, while the hiccup ON time is fixed about 4 ms. To support lower OCL setting or higher capacitive load on VLNB output, if hiccup happens when startup, the larger TCAP capacitor $C_{SS}$ should be used to decrease the startup current lower than OCL value.
2.4 **VLNB Output Voltage Transition**

To support the vertical polarization and horizontal polarization control for LNB, the voltage transition frequently happens in the application.

Larger $C_{SS}$ on the TCAP pin can avoid the hiccup happens when startup, while the VLNB output voltage transition time is also enlarged. Equation 4 can be used for estimation.

$$T_{ts}(ms) = \frac{Abs(V_{VLNB1}(V) - V_{VLNB2}(V))}{K} \times \frac{C_{SS}(nF)}{I_{SS}(uA)}$$

where

- $T_{ts}$ → Transition time between $V_{VLNB1}$ and $V_{VLNB2}$
- For TPS65233, from 13.4 V to 18.6 V transition, the transition time is about 1.1 ms with 22 nF $C_{SS}$.
- For TPS65235, from 13.4 V to 18.2 V transition, the transition time is about 2 ms with 22 nF $C_{SS}$.  \(\text{(4)}\)

---

**Figure 14. Voltage Transition for TPS65233**

**Figure 15. Voltage Transition for TPS65235**
3 I2C Address and Tone Mode Setup

3.1 I2C Address Setup

The TPS65233 has two I2C address, which is 0x60H and 0x61H.

If 0x60H is used, the EN pin should be always pulled low and the VLN output is controlled by I2C bit 3 in control register 1. Which means before the I2C configuration done, there is no VLN output as the default bit 7 in control register 1 is “0” to disable the I2C control.

If 0x61H is used, the EN pin should always be pulled high, and the VLN output is not controlled by I2C bit 3 in control register 1 when powered up. The VLN output is enabled once VIN power up and the initial VLN output voltage may not be what the application needs. So the VCTRL pin should be set to make sure the VLN output voltage is expected by application.

If two TPS65233 are used with I2C interface in one application, one EN pin should be always kept low and the other should be always kept high for correct I2C access.

For TPS65235 I2C address setup, refer to SLVSD80.
3.2 Tone Mode Setup

3.2.1 TPS65233 Tone Mode Setup

There are totally 5 kinds of tone control mode in TPS65233, two modes are for non-I\(^2\)C application mode 1 and mode 2, three modes are for I\(^2\)C application mode 3, mode 4 and mode 5.

<table>
<thead>
<tr>
<th>Mode</th>
<th>Control Register 1</th>
<th>Note For EXTM Pin</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>bit 7 (I2C_CON)</td>
<td>bit 6 (RSV)</td>
</tr>
<tr>
<td>Mode 1</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Mode 2</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Mode 3</td>
<td>1</td>
<td>0</td>
</tr>
<tr>
<td>Mode 4</td>
<td>1</td>
<td>0</td>
</tr>
<tr>
<td>Mode 5</td>
<td>1</td>
<td>0</td>
</tr>
</tbody>
</table>

**NOTE:** For mode 3 and mode 4, bit5 = 1 tone on; bit5 = 0 tone off

For mode 5, as the note in Table 1, when the tone stops, the EXTM signal should be kept “High", then the bit3 and bit4 in control register 2 can be used to control the tone level of the VLN output. Otherwise, if it is kept as “Low", bit3 and bit4 in control register 2 are useless, the tone level is always above the DC output in Figure 18, and this is usually not expected in this design. In Figure 19, EXTM stops the tone and stays in “High", the tone level can be set in the middle of VLN output.

**Figure 18. Mode 5 with EXTM Stop at “Low”**

**Figure 19. Mode 5 with EXTM Stop at “High”**

If the application cannot put the EXTM stops at “High", then use TPS65235.

For other tone mode introduction, refer to the TPS65233-1 datasheet **SLVSD66** for detail clarification.
3.2.2 TPS65235 44-KHz Tone Mode Setup
The TPS65235 also supports the 44-KHz tone output. Compared with 22-KHz tone output mode, the 44-KHz tone output only has an external tone mode. To support the 44-KHz external tone mode, the bit0 (EXTM TONE) in control register 1 should be “1”.

Table 2. TPS65235 Tone Mode

<table>
<thead>
<tr>
<th>Output Tone Frequency</th>
<th>External Tone Mode</th>
<th>Internal Tone Mode</th>
<th>EXTM TONE</th>
</tr>
</thead>
<tbody>
<tr>
<td>22 KHz</td>
<td>✓</td>
<td>✓</td>
<td>“0”</td>
</tr>
<tr>
<td>44 KHz</td>
<td>✓</td>
<td>x</td>
<td>“1”</td>
</tr>
</tbody>
</table>

Figure 20. 44-KHz Tone Output

4 DisEqc2.x Tone Design Consideration
The TPS65235 supports DisEqc2.x tone signal detection. There are two I2C bits in Control Register 2 TONE_AUTO and TONE_TRANS for tone detection mode selection. When the tone transmits from the TPS65235, the Bypass FET should be turn on and pass the tone signal output. When receiving the tone signal from satellite, the Bypass FET should be turn off for DisEqc 2.x tone receiving. Turning on or off the Bypass FET is controlled by the GDR pin from the TPS65235.

Table 3. 22-KHz Tone Receive Mode Selection

<table>
<thead>
<tr>
<th>TONE_AUTO</th>
<th>TONE_TRANS</th>
<th>Bypass FET</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>0</td>
<td>OFF</td>
</tr>
<tr>
<td>0</td>
<td>1</td>
<td>ON</td>
</tr>
<tr>
<td>1</td>
<td>X</td>
<td>Auto Detect</td>
</tr>
</tbody>
</table>

When TONE_AUTO is set to “0”, the MCU software should control the TONE_TRANS bit through I2C interface. For example, when it needs to send the tone output, the MCU software puts the TONE_TRANS to be “1”; otherwise, the MCU software keeps TONE_TRANS as “0” for receiving the tone from satellite.

When TONE_AUTO is set to “1”, the TPS65235 does the same thing as MCU software. When the EXTM is high or has the 22-KHz tone input, which means TPS65235 outputs the 22-KHz tone, then TPS65235 controls the GDR output with VCP voltage value (higher than VLN output about 5.4-V) to close the external Bypass FET for tone transmit. Otherwise, the TPS65235 controls the GDR output with VLN voltage value to open the Bypass FET for tone receiving from satellite.

Figure 21 shows the DisEqc 2.x application for TPS65235. The RC Network is for tone detection input, and the recommended value should be followed.
Figure 21. Application for DiSEqc2.x Support on TPS65235

V_{VLNB} = 13.4 V  \quad \text{TONE\_AUTO} = 1

Figure 22. GDR = 18.8 V for Transmit Data “0”,
GDR = 13.4 V for Tone Receive

V_{VLNB} = 13.4 V  \quad \text{TONE\_AUTO} = 1

Figure 23. GDR = 18.8 V for Transmit Data “1”,
GDR = 13.4 V for Tone Receive
As the default status of TONE_AUTO is “0”, the TPS65235 cannot implement the tone detection function in non-I²C working condition.

To be noted, the TPS65235 does not do anything related to DisEqC protocol.

For TPS65233, it also can support the DisEqC2.x application by adding the external circuit for tone receiving detection and to control Bypass FET. This application report does not clarify the detail due to it is more related to the customer design.
For surge design consideration, except D0 and D2, usually a schottky diode is serialized in the path of VLNBO output, refer to D4 in Figure 28. This external schottky diode D4 is to block the surge current into the device, and the external dummy load R1 is to provide the discharge path for C1 to make sure the correct tone output.

Without the D4, the C1 discharge through internal M1 to implement the tone falling edge. With D4 added, the new discharge path will be C1 to R1. The value of C1 and R1 will influence the falling edge of the tone output.

Figure 28. Block for Surge Protection Design
The smaller $R_1$, the more power loss, but the larger $R_1$ cannot provide enough discharge current for $C_1$ to discharge in time, to meet the tone spec requirement for falling edge. To choose the suitable $R_1$, use Equation 5.

$$R_1 (k\Omega) < \frac{V_{VLNB\_min} (V) \times T_{\text{tone\_falling}} (\mu s)}{C_1 (nF) \times T_{\text{tone\_amp}} (V)}$$

where

- $V_{VLNB\_min}$ → Minimum VLN B DC output in application
- $T_{\text{tone\_falling}}$ → Tone falling edge requirement, about 10 $\mu$s
- $T_{\text{tone\_amp}}$ → Tone amplitude in application, 650 mV for TPS65233, 650 mV / 750 mV for TPS65235  

(5)
6 Summary

This application report introduces some design considerations on the TPS65233 and TPS65235. TI has more LNB regulator products. The TPS65233-1 has higher switching frequency up to 1-MHz compared with TPS65233. The TPS65235-1 has the anti-audible noise feature. The TPS65235-2 is based on TPS65235-1 which has the highest VLNB voltage output up to 20.3-V typical.

Table 4. TI LNB Regulators

<table>
<thead>
<tr>
<th>Features / Part Number</th>
<th>TPS65233</th>
<th>TPS65233-1</th>
<th>TPS65235</th>
<th>TPS65235-1</th>
<th>TPS65235-2</th>
</tr>
</thead>
<tbody>
<tr>
<td>Switching frequency</td>
<td>500 KHz</td>
<td>1 MHz</td>
<td>500 KHz / 1 MHz</td>
<td>500 KHz / 1 MHz</td>
<td>500 KHz / 1 MHz</td>
</tr>
<tr>
<td>22-KHz tone output support?</td>
<td>Y</td>
<td>Y</td>
<td>Y</td>
<td>Y</td>
<td>Y</td>
</tr>
<tr>
<td>44-KHz tone output support?</td>
<td>N</td>
<td>N</td>
<td>Y</td>
<td>Y</td>
<td>Y</td>
</tr>
<tr>
<td>Tone detection for DiSEqC2.x?</td>
<td>N</td>
<td>N</td>
<td>Y</td>
<td>Y</td>
<td>Y</td>
</tr>
<tr>
<td>Tone amplitude 650 mV / 750 mV selectable?</td>
<td>N</td>
<td>N</td>
<td>Y</td>
<td>Y</td>
<td>Y</td>
</tr>
<tr>
<td>Anti-audible noise feature?</td>
<td>N</td>
<td>N</td>
<td>N</td>
<td>Y</td>
<td>Y</td>
</tr>
<tr>
<td>VLNB output range</td>
<td>13 V - 19.8 V</td>
<td>13 V - 19.8 V</td>
<td>11 V - 20 V</td>
<td>11 V - 20 V</td>
<td>11 V - 20 V</td>
</tr>
</tbody>
</table>

7 References

- Datasheet: TPS65233 LNB Voltage Regulator With fC Interface, SLVSC22
- Datasheet: TPS65233-1 LNB Voltage Regulator With fC Interface, SLVSD66
- Datasheet: TPS65235 LNB Voltage Regulator With fC Interface, SLVSD80
- Datasheet: TPS65235-1 LNB Voltage Regulator With fC Interface, SLVSDP1
- User Guide: Evaluation Module for the TPS65235 LNB Voltage Regulator With fC Interface for DiSEqC2.x Application, SLVUAO1
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