

# LMH6642

*Photo-Diode Current-To-Voltage Converters*



Literature Number: SNOA806

# Application Brief

## Photo-Diode Current-To-Voltage Converters

Application Brief 104

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Converting the small output current of a photo-diode transducer to a fast responding voltage is often challenging. Here are some ways to use high-speed current feedback and voltage feedback op amps to do the job.

### Current Feedback Amplifier Solution

Current feedback amplifiers (CFA) are especially suited to implement this function, as shown in *Figure 1*. With an effective internal buffer on the inverting node of the op amp, the output impedance  $R_O$  (internal to U1, not shown) and the photo-diode's output capacitance  $C_{IN}$  (typically 10-200 pF) introduce a zero in the noise gain at approximately  $1/2\pi(R_O C_{IN})$ . In comparison, the zero produced by a voltage feedback op amp in a similar configuration  $[1/2\pi(R_{IN}||R_i||R_{BIAS})C_{IN}]$  tends to be much lower in frequency and more troublesome. This being the case,  $C_{IN}$  has less of an effect on reduction of the converter bandwidth, and achieving stability is easier when using a CFA.

If  $C_{IN}$  is sufficiently large, the closed loop phase shift will approach  $-180^\circ$  at the cross-over frequency (where open loop transimpedance gain crosses the noise gain function). As with voltage feedback amplifiers, the closed loop amplifier can be compensated by adding a small capacitor ( $C_f$ ) across  $R_f$ .

In the case of *Figure 1*, using the CLC450 CFA,  $C_f$  was experimentally determined to be around 2 pF for about 10% overshoot in the step response.  $C_f$  improves stability by counteracting the effect of the zero discussed in the paragraph above by introducing a low frequency pole ( $1/2\pi R_f C_f$ ) and an inconsequential zero ( $1/2\pi R_O C_f$ ).

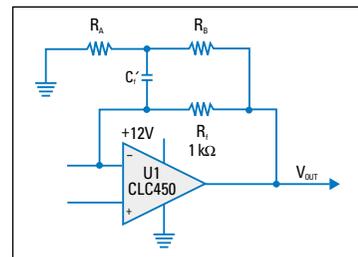


Figure 2.  $R_A$ - $R_B$  Resistor Divider Allows Use Of Practical Value for  $C_f$

It is possible to change the required 2 pF compensation capacitor to a more practical value, by adding  $R_A$  and  $R_B$  in a voltage divider, as shown in *Figure 2*. The new value of  $C_f$  is  $(1+R_B/R_A) \times C_f$ . This relationship holds true as long as  $R_B \ll R_f$ .

For this example, select  $R_A=50\Omega$ , and  $R_B=500\Omega$ . Therefore,  $C_f=(1+500/50) \times 2 \text{ pF}=22 \text{ pF}$ , which is a much more practical component value. This value needs to be "fine tuned" in the real application for proper step response.

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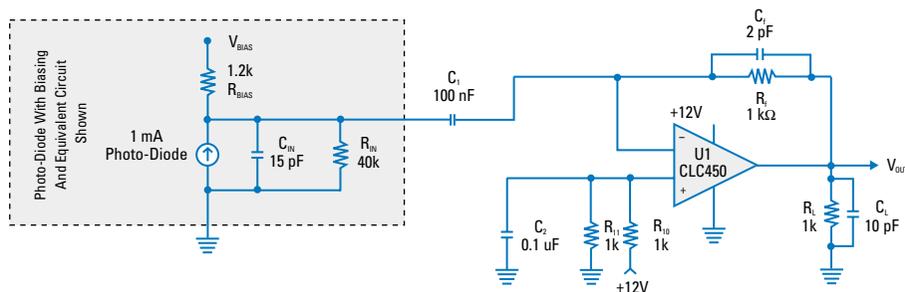


Figure 1. Single-Supply Photo-Diode Amplifier Using CLC450 Current-Feedback Amplifier

### Voltage Feedback Amplifier Solution

It's more difficult to design a good current-to-voltage converter using a voltage feedback amplifier (VFA). As discussed above, phase shift caused by photo-diode capacitance is often a source of instability. Furthermore, wide bandwidth usually comes at the expense of supply current and higher supply voltage. However, the new LMH6642 high-speed low-voltage VFA has excellent performance in a transimpedance gain block, as shown in Figure 3. This device can operate down to 2.7V single supply and its -3 dB BW ( $A_v = +1$ ) is more than 100 MHz (with a supply current of only 2.7 mA)! Because of the "Dielectric Isolation" process this device is based on, the traditional supply voltage vs. speed trade-off has been alleviated to a great extent allowing low-power consumption and operation at lower supply voltages. In addition, the device has rail-to-rail output swing capability to maximize the output swing, and is capable of driving  $\pm 50$  mA into the load.

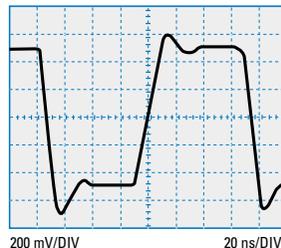


Figure 4. Output Step Response 20 ns/DIV, 0.2V/DIV.

The diode on the base of  $Q_1$  is for temperature compensation of its bias point.  $Q_1$  bias current is set to be large enough to handle the peak-to-peak photo-diode excitation, yet not too large as to shift the  $U_1$  output too far from mid-supply. The overall circuit draws about 4.5 mA from the +5V power supply and achieves about 35 MHz of closed loop bandwidth @1  $V_{pp}$ . Figure 4 shows the output large signal step response.  $C_f$  can be increased to reduce the overshoot, at the expense of bandwidth.

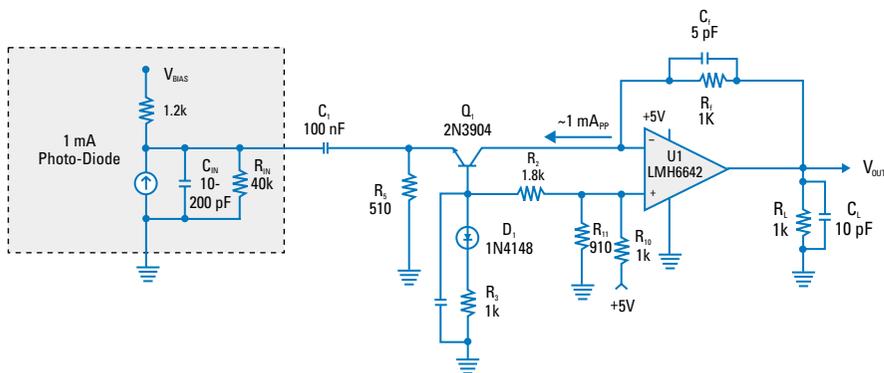


Figure 3. 5V Single-Supply Photo-Diode Amplifier Using LMH6642 Voltage-Feedback Op Amp

With 5V single supply, the device common mode voltage is shifted to near half-supply using  $R_{10}$ - $R_{11}$  as a voltage divider from  $V_{CC}$ . The common-base transistor stage ( $Q_1$ ) isolates the photo-diode's capacitance from the inverting terminal, allowing wider bandwidth and easing the compensation required. Note that the collector of  $Q_1$  does not have any voltage swing, so the Miller effect is minimized.

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