**Design Guide: TIDA-01041**

**Battery Tester Reference Design for Multiphase High-Precision 0.5- to 100-A Battery Formation**

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### Description

This reference design provides a multiphase solution for a wide range of current battery test applications. Leveraging the dual phase buck-boost controller daisy chain configuration of the LM5170 gives the design the ability to achieve 100-A charging and discharging rates. Utilizing high accuracy constant current (CC) and constant voltage (CV) calibration loops, the design can achieve up to 0.01% voltage control accuracy. All key design theories are described guiding users through the part selection process and optimization.

### Features

- High precision calibration control achieving 0.02% full scale current control accuracy and 0.01% full scale voltage control accuracy
- Supports from 0.5-A to 100-A charge and discharge
- Input voltage (bus) from 8 V–16 V and output load (battery) from 0 V–4.2 V (5 V max)
- Two LM5170 multiphase bidirectional buck, boost integrated controllers and drivers for charging and discharging

### Resources

- **TIDA-01041** Design Folder
- **LM5170-Q1** Product Folder
- **INA828** Product Folder
- **DAC80004** Product Folder
- **ADS131A04** Product Folder

### Applications

- Battery test equipment

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1 System Description

Battery testers include high performing battery manufacturing equipment and laboratory test instruments, circuit control and data acquisition tools, battery simulation and manufacturing automation tools, appropriate to all battery applications and chemistries.

![Figure 1. Battery Tester Block Diagram](image-url)
1.1 **Li-Ion Formation**

Figure 2 shows the manufacturing process for the Li-Ion battery, a popular, rechargeable battery chemistry. A battery test is involved in the final part of the manufacturing process: Formation.

**Figure 2. Simplified Li-Ion Battery Manufacturing Process**

- Electrode Coating
- Mixing
- Coating
- Compressing
- Drying
- Slitting
- Cell Assembly
- Stacking/Wingding
- Insert Electrode Stack
- Connect Electrodes
- Sub Assembly
- Heat Seal/Weld
- Formation
- Labelling
- Acceptance Testing
- Packing Shipping

1.2 **Li-Ion Battery Formation Profile**

Figure 3 shows the typical Li-Ion battery formation profile, detailing the phases of the initial charging and formation of a battery which directly affects its quality and capacity for the entirety of the life span of the battery. In the first phase, labeled “Initial,” a small initial charge of around 10% of the full-charge current is applied. This is done to prevent the cell from overheating and is done until the battery is able to accept the full current of the constant-current phase. During the constant-current, or “CC” phase, the battery is typically charged at 1 A or less until the battery voltage reaches 4.1 V or 4.2 V (depending on electrochemistry) where it then transitions to the constant voltage, or “CV” phase. For detailed test results on the transformation between CC and CV, see Section 3.1.4.3.

**Figure 3. Regular Li-Ion Battery Formation Profile**

For more information on Li-Ion battery formation, see the TIDA-01040 Battery Tester Reference Design for High Current Applications design guide.
2 System Overview

This design encompasses the Battery Test Cell Unit and analog front end subsystems as Figure 1 shows. In the following subsections, the system and its design theory are detailed.

2.1 Block Diagram

In this reference design, the LM5170 device is a multiphase, buck-boost bidirectional controller that is able to charge or discharge the load at up to 50 A each depending on the “DIR” setting. The DAC80004 device is a 16-bit DAC that sets the reference current and reference voltage for either CC or CV mode using the USB2ANY interface. The high-precision INA188 current sense amplifier measures the current charging or discharging the load. That measurement is compared with the reference control signal using the TLV07 op amp. The load voltage is compared with the reference control signal using the LM6142 op amp. The system is using two OPA827 devices to buffer the current measurement and voltage measurement signals before the data acquisition phase and the THS4561 differential amplifier converts the single-ended measurement signals to differential signals. The ADS131A04 device is a 24-bit delta-sigma ADC used to monitor the current and voltage of the load. An onboard TIVA processor is used to communicate between the ADS131A04 device and the PC for this reference design. When the system is set to CC or CV mode, the multiphase controller will output the signified voltage or current to the load. The system monitors and controls the output at the load to ensure precision while the user can monitor the results through the acquired data.
Figure 4. TIDA-01041 Block Diagram
### 2.2 Key System Specifications

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>SPECIFICATIONS</th>
<th>DETAILS</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{\text{battery_min}}$</td>
<td>0 V</td>
<td>Battery-port minimum operating voltage</td>
</tr>
<tr>
<td>$V_{\text{battery_nominal}}$</td>
<td>4.2 V</td>
<td>Battery-port normal operating voltage</td>
</tr>
<tr>
<td>$V_{\text{battery_max}}$</td>
<td>5 V</td>
<td>Battery-port maximum operating voltage</td>
</tr>
<tr>
<td>$V_{\text{bus_min}}$</td>
<td>8 V</td>
<td>Bus-port minimum operating voltage</td>
</tr>
<tr>
<td>$V_{\text{bus_nominal}}$</td>
<td>12 V</td>
<td>Bus-port normal operating voltage</td>
</tr>
<tr>
<td>$V_{\text{bus_max}}$</td>
<td>16 V</td>
<td>Bus-port normal operating voltage</td>
</tr>
<tr>
<td>$F_{\text{SW}}$</td>
<td>100 kHz</td>
<td>Switching frequency</td>
</tr>
<tr>
<td>$I_{\text{ph_max}}$</td>
<td>25 A</td>
<td>Maximum DC current per phase, bidirectional</td>
</tr>
<tr>
<td>$I_{\text{Total_max}}$</td>
<td>100 A</td>
<td>Total maximum DC current at battery-port</td>
</tr>
<tr>
<td>Current control accuracy</td>
<td>0.02%</td>
<td>Full-scale current control accuracy for charge and discharge</td>
</tr>
<tr>
<td>Voltage control accuracy</td>
<td>0.01%</td>
<td>Full-scale current control accuracy for charge and discharge</td>
</tr>
</tbody>
</table>

For detailed test results on current control accuracy, refer to Section 3.1.4.1
For detailed test results on voltage control accuracy, refer to Section 3.1.4.2
2.3 Design Considerations

This reference design must test at charge and discharge rates of up to 100-A continuous for larger capacity batteries. The following makes this possible:

- Multiphase design, eliminating the need for larger, more expensive power stage inductors needed to draw the same amount of current with a single phase.
- To maximize battery performance however, the constant current and voltage control systems must be designed to an accuracy range within ±0.05%. The next section takes a deeper dive into the need for multiphase in this design.

Inductor currents for each conductor are charging and discharging the output capacitor of the design concurrently depending on whether or not a given phase is active. This produces one overall current whose AC portion is absorbed by the output capacitor, resulting in a lower overall voltage ripple. As the number of phases increase, the current and voltage output ripple decreases.

2.3.1 MultiPhase Design

Multiphase converters use multiple inductors operating in parallel to operate beyond the saturation current rating of a single inductor and require less RMS current from the input capacitor; thereby, reducing the solution size and cost. See the *Multiphase buck design from start to finish (part 1)* application report for more details.

TI recommends selecting an inductor such that its peak-to-peak ripple current is less than 80% of the channel inductor full load DC current. Therefore, the inductor should satisfy:

\[
L_m \geq \frac{V_{ramp} \times (1 - D_{PC, min})}{80\% \times I_{in} \times F_s} = \frac{4\times V \times (1 - 0.2)}{0.8 \times 25\times 100kHz} = 1.6\mu H
\]

This design uses 4.7-µH inductors to further decrease current ripple. Multiphase converters parallel multiple inductors to draw currents that would be problematic for a single-phase converter due to current saturation limitations. Multiphase reduces input RMS current and output ripple current, allowing the design to employ smaller value inductors and reduce the size of the design. The ability to have inductors rated for lower current also decreases the system cost.

![Figure 5. Normalized Input Capacitance RMS Current](image-url)
Inductor currents at each of the four power stages of the design sum to charge and discharge its output capacitor concurrently, depending on whether or not a given phase is active. This produces one overall current, $I_{\text{sum}}$, whose AC portion is absorbed by the output capacitor, resulting in a lower overall voltage ripple.

Figure 7 shows the effect of a dual-phase system on voltage ripple. As the number of phases increase, the current and output ripple decrease.

Four phases of current allow the TIDA-01041 design to charge and discharge at up to 100 A. This is achieved by daisy chaining two LMS170 devices, each with two phases, into a multiphase configuration. Figure 10 shows a block diagram of this configuration.
The LM5170 devices are connected from the SYNCOUT of one device to the SYNCIN of another, and can be synchronized using either an internal or external clock reference. The OPT pin of the LM5170 allows the user to adjust the phase delay of the SYNCOUT pin. A high value on the pin provides a 90 degree phase shift needed for this four-phase design. See Table 5 for proper jumper setup for multiphase configuration.
This reference design can also be operated in a two-phase, 50-A configuration using a single LM5170 device. This is done by disconnecting jumper 3, the SYNC connection between both LM5170 devices.

This reference design requires simultaneous control of both current and voltage within an accuracy of ±0.05% to properly perform the battery test. The next two sections detail the design of the current and voltage control systems.

### 2.3.2 Constant Current Control Design

This section details the process for designing the control system that handles constant current flow for battery charging and discharging. See Section 3.1.4.1 for more information on accuracy test results for this system. For information on part selection and the simulation tool used for this design, see the [TIDA-01040 battery tester reference design for high current applications reference design](#).

The INA828 device, a precision instrumentation amplifier, provides a low-noise differential signal that dictates current regulation. The TIDA-01040 design uses the INA188 device as its instrumentation amplifier. There are two gain settings for the instrumentation amplifier: low current (0–50 A) and high current (50–100 A) as Figure 11 shows.

![Figure 11. INA828 Gain Settings](#)
Figure 12 highlights the calculation results of the INA828 input and output ranges for this reference design. In this case, the maximum common-mode voltage is the same as the maximum voltage on the battery side, so its maximum value is 5 V. For low current gain at 44.48, the input range for an INA828 device with power rails at 10 V and –5 V is –60.701 mV to 89.926 mV. For high current gain at 88.96, the calculation results show the input range from –30.351 mV to 44.96 mV. These ranges both fit within the current signal range (±100 A × 0.5 mΩ = ±50 mV).

Due to the high precision of the INA828 device, the CC control amplifier it provides feedback to needs to meet certain accuracy requirements or it will bottleneck the design. In the 100-A high-current application, worst-case, the input offset voltage causes an error of 112.5 µV / (100 A × 0.001 × 21.57) × 100% = 0.005216% on the control loop. The error is less than the 0.01% demanded accuracy, making the TLV07 device a suitable amplifier.

Further information on the TLV07 device and its control stability is found in the TIDA-01040 battery tester reference design for high current applications reference design.

Figure 13 shows the CC control simulation schematic. To keep the system working in CC control mode, ISETA provides a DC voltage for D4 to conduct continuously. ISET1 and ISET2 capture the differential voltage across the current sense resistor, E1 is an ideal differential amplifier to output a single-ended signal, R16 and C19 create a low-pass filter, and X6 is the error amplifier used to calibrate the current signal to the reference signal.
Figure 13. Constant Current Control Simulation Schematic

Figure 14 shows the small signal performance of this CC control subsystem. The gain crossover frequency is 22.15 kHz, and the phase margin is 69.57° which means this control circuit is stable and can provide enough bandwidth.

Figure 14. CC Small Signal Simulation Results

To generate a reference signal for current (DAC Channel D) control, commands are written to the 32-bit wide SPI shift register.
The bits that are altered for this design are the ‘Channel Address bits’ and the ‘Data bits’. For example, inputting '03 31 C7 70' generates a reference voltage that causes the CC amplifier to regulate the charge and discharge rate of the battery to 25 A. D23–D20 is set to ‘03 3’, selecting DAC output channel D and D19–D04 is set to ‘1 C7 7’, which generates a decimal value that is converted into an analog signal based off the bit rate of the DAC and its voltage reference, calculated with Equation 2 and Equation 3.

\[
D_{IN} = \frac{INAGIN}{REFIN} \times R_{CS} \times \text{Ideal Current} \times 65536
\]

(2)

\[
V_{OUT} = D_{IN} \times \text{REFIN}
\]

(3)

More information on DAC80004 commands are found in the DACx0004, quad 16-,14-,12-bit, 1 LSB INL, buffered, voltage-output digital-to-analog converters data sheet.

### 2.3.3 Constant Voltage Control Design

For information on part selection and the simulation tool used for this design, see the TIDA-01040 battery tester reference design for high current applications reference design. There is no difference in constant voltage control design between the TIDA-01041 and the TIDA-01040 designs. This is because the output voltage at the battery is still regulated to the same range (0 V to 4.2 V).

See Section 3.1.4.2 for more information on accuracy test results for this system.

To generate a reference signal for voltage (DAC Channel A) control, commands are written to the 32-bit wide SPI shift register.

The bits that are altered for this design are the ‘Channel Address bits’ and the ‘Data bits’. For example, inputting '03 0B 87 F0' generates a reference voltage that causes the CV amplifier to regulate the voltage of the battery to 4.2 V. D23–D20 is set to ‘03 0’, selecting DAC output channel A and D19–D04 is set to ‘B 87 F’ which generates a decimal value that is converted into an analog signal based off the bit rate of the DAC and its voltage reference.

\[
V_{OUT} = D_{IN} \times \text{REFIN}
\]

(4)

\[
D_{IN} = \frac{INAGIN}{REFIN} \times \text{Ideal Voltage} \times 65536
\]

(5)

More information on DAC80004 commands is found in the DACx0004, quad 16-,14-,12-bit, 1 LSB INL, buffered, voltage-output digital-to-analog converters data sheet.

### 2.3.4 System Transient Response

Figure 13 is the simulation schematic of the CC control, CV control, and multiphase design steps connected to create the complete TIDA-01041 system, giving an indication of the expected transient results for both control subsystems and the system as a whole. The CC and CV control designs are connected to one another by R20, R15, D4, and R30. This connection simulates the startup of the control systems: the CV amplifier produces a high voltage to bias the diode, turning on the CC amp and starting the control loop for the system. The output of these amplifiers is connected to the ISETA pin on both LM5170 devices that sets current regulation for each power stage being used to charge and discharge the battery, which is then simulated with the R12!~ !~L!~load and C14.

Figure 16 shows the results of the system transient simulation and measurements. The voltage in the loop at startup is low, causing the CV loop to output a high voltage to compensate. This voltage causes the diode, D4, to conduct and the CC control loop starts taking control of the system. When the CC control loop takes over, the current going to the battery, IBAT, keeps constant at 100 A and the battery voltage increases over time. Once the battery reaches 4.5 V, the CV control loop takes back control of the system and decreases the output voltage. The battery current then decreases and voltage is kept steady.
Figure 16. Transient Response
2.4 **Highlighted Products**

This section provides more detail on some of the core products that make up this design, explaining why they were selected and their potential alternatives.

2.4.1 **LM5170-Q1 Multiphase Bidirectional Current Controller**

The LM5170-Q1 is a dual-channel, bidirectional, multiphase controller that can support high current battery test applications up to 200 A using eight phases. It can regulate the average current flowing between the high and low voltage ports in the direction designated by the DIR input signal.

Other important features include:

- 5-A peak half-bridge gate drivers which enables the ability to drive high currents
- Programmable oscillator frequency which allows the user to choose the FET switching frequency
- MOSFET failure detect at start-up and circuit breaker control which provides security to the system

![Figure 17. LM5170-Q1 Simplified Application Circuit](image)

For more on multiphase design, its benefits and the daisy chain configuration used for this design, see Section 2.3.1.
2.4.2 INA828 Precision Instrumentation Amplifier

The INA828 is a precision instrumentation amplifier with integrated resistor networks for sensing and data acquisition systems. This device measures and amplifies a differential voltage that represents output current which acts as feedback to regulate current. The INA828 device uses super-beta input transistors which allows for lower input bias current and current noise while also improving input offset voltage and offset drift.

Other important features include:
- Gain drift: 50 ppm/ºC (G > 1) which limits the variation of calibration at high temperatures
- Bandwidth: 2 MHz (G = 1), 260 kHz (G = 100) which allows for fast transients
- Inputs protected up to ±40 V which provides protection to the device
- Power-supply rejection: 100 dB, minimum (G = 1) which limits the noise observed on the signal chain

Alternatives:

The INA828 device offers lower noise than its predecessor, the INA188 device, but has a narrower bandwidth than the INA821. The INA828 device is pin-to-pin compatible with the SOIC package of the INA188 device. The INA819 has the best performance for error with only slightly more noise than the INA828.

<table>
<thead>
<tr>
<th></th>
<th>INA828</th>
<th>INA821</th>
<th>INA188</th>
<th>INA819</th>
</tr>
</thead>
<tbody>
<tr>
<td>Quiescent current</td>
<td>0.6 mA</td>
<td>0.6 mA</td>
<td>1.4 mA</td>
<td>350 µA</td>
</tr>
<tr>
<td>Noise density @ 1 kHz</td>
<td>7 nV/√Hz</td>
<td>7 nV/√Hz</td>
<td>12 nV/√Hz</td>
<td>8 nV/√Hz</td>
</tr>
<tr>
<td>Gain error (±)</td>
<td>0.15%</td>
<td>0.15%</td>
<td>0.50%</td>
<td>0.005%</td>
</tr>
<tr>
<td>Bandwidth at G = 1</td>
<td>2 MHz</td>
<td>4.7 MHz</td>
<td>0.6 MHz</td>
<td>2 MHz</td>
</tr>
</tbody>
</table>
2.4.3 DAC80004 16-Bit DAC With 1 LSB INL/DNL

The DAC80004 device is low-power, quad-channel, 16-bit digital-to-analog converter. Hexadecimal values are written to the DAC using a computer which produce voltages at two channels. These voltages set the battery voltage charge and discharge rate. The four channels of the DAC80004 are used for the generation of high accuracy, user-defined voltage references.

Other important features include:
- True 16-bit performance: 1 LSB INL/DNL (maximum) which ensures accurate references for current and voltage
- Output buffer with rail-to-rail operation which provides clean references for current and voltage
- 50 MHz, 4- or 3-wire SPI-compatible which allows for simplified user interface

Figure 19. DAC80004 Simplified Block Diagram

Alternatives:
The DAC80508 device is an eight channel DAC from the same family as the DAC80004.

Table 3. DAC80004 Alternatives

<table>
<thead>
<tr>
<th>Feature</th>
<th>DAC80004</th>
<th>DAC80508</th>
</tr>
</thead>
<tbody>
<tr>
<td>INL/DNL</td>
<td>1 LSB (Max)</td>
<td>1 LSB (Max)</td>
</tr>
<tr>
<td># of Channels</td>
<td>4</td>
<td>8</td>
</tr>
<tr>
<td>Glitch Energy</td>
<td>1 nV-s</td>
<td>4 nV-s</td>
</tr>
</tbody>
</table>
2.4.4 ADS131A04 24-Bit, 128-kSPS, 4-Channel, Simultaneous-Sampling Delta-Sigma ADC

The ADS131A04 device uses four channels to simultaneously and continuously sample voltage or current measurements. The ADC is the front-end of the battery tester and interface with a computer to display voltage and current values in TI’s EvaluaTIon software. The ADS131A04 device is well equipped for measuring current and voltage signals due to it being a simultaneous sampling 4-channel converter, with a flexible SPI and data integrity to check and correct single-bit errors during data transmission.

Other important features include:
- Single-channel accuracy: Better than 0.01% at 10,000:1 dynamic range which enables high accuracy data acquisition
- Effective resolution: 20.6 bits at 8 kSPS which allows for high accuracy data acquisition
- Low-drift internal voltage reference: 6 ppm/ºC which limits the effects that temperature has on the data acquisition
- Multiple SPI data modes which allows for a simplified user interface

Alternatives:
The ADS131E08 and ADS131E04, predecessors to the ADS131A04, have a lower data rate but implement integrated buffer amplifiers.

Table 4. ADS131A04 Alternatives

<table>
<thead>
<tr>
<th></th>
<th>ADS131A04</th>
<th>ADS131E08</th>
<th>ADS131E04</th>
</tr>
</thead>
<tbody>
<tr>
<td>Data Rates (Max)</td>
<td>128 kSPS</td>
<td>64 kSPS</td>
<td>64 kSPS</td>
</tr>
<tr>
<td># of Channels</td>
<td>4</td>
<td>8</td>
<td>4</td>
</tr>
<tr>
<td>SNR</td>
<td>115 dB</td>
<td>107 dB</td>
<td>107 dB</td>
</tr>
</tbody>
</table>
2.4.5 Other Highlighted Products

In addition to the key products highlighted in the previous sections this reference design also showcases the following Texas Instruments devices:

1. OPA2277 precision op amp; DAC driver buffer
2. OPA827 precision op amp; ADC current and voltage measurement buffers
3. TPS709 LDO regulators; 5-V DAQ and control power rails
4. TLV07 36-V precision, rail-to-rail output, op amp; CC control amplifier
5. THS4561 low-power, 70-MHz, high-supply range, fully differential amplifier; differential signal input for ADC
6. LM2664 switched capacitor voltage converter; –5-V power rail
7. LM7705 low-noise negative bias generator; –0.2 power rail
8. LM5118 non-synchronous buck-boost controller; 10-V power rail
9. LM6142 rail-to-rail I/O op amp; CV control amplifier
10. SN74LVC1G04 single inverter; boost control logic
11. SN74LV1T32 2-input positive OR gate; boost control logic
12. SN74LV1T00 2-input positive NAND gate; buck control logic
3 Hardware, Software, Testing Requirements, and Test Results

3.1 Testing and Results

3.1.1 Getting Started: Hardware

See the TIDA-01040 design guide for general details on each hardware subsystem in this design.

Figure 21. TIDA-01041 Hardware

This section gives brief information to set up and run the board. Figure 21 shows the sections of the board.

This system has some configuration options. Table 5 highlights the purpose of each jumper as well as the default configurations.

Table 5. Jumper Configuration

<table>
<thead>
<tr>
<th>HEADER</th>
<th>SIGNAL</th>
<th>PINS</th>
<th>FUNCTION DESCRIPTION</th>
<th>DEFAULT</th>
</tr>
</thead>
<tbody>
<tr>
<td>J1</td>
<td>UVLO</td>
<td>(1,2)</td>
<td>Enable from V_HV</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Enable from V_LV</td>
<td></td>
</tr>
<tr>
<td>J3</td>
<td>SYNCOUT</td>
<td>(1,2)</td>
<td>Clock output for multiphase configuration</td>
<td>Y</td>
</tr>
<tr>
<td>J4</td>
<td>V10-Aux</td>
<td>(1,2)</td>
<td>Auxiliary power</td>
<td>Y</td>
</tr>
<tr>
<td>J5</td>
<td>OPT</td>
<td>(1,2)</td>
<td>Multiphase configuration</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>No multiphase configuration</td>
<td></td>
</tr>
<tr>
<td>J6</td>
<td>DIR</td>
<td>(1,2)</td>
<td>Buck mode</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Boost mode</td>
<td></td>
</tr>
<tr>
<td>J7</td>
<td>EN1</td>
<td>(1,2)</td>
<td>Onboard CH-1 enable</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Onboard CH-1 disable</td>
<td>Y</td>
</tr>
<tr>
<td>J8</td>
<td>EN2</td>
<td>(1,2)</td>
<td>Onboard CH-2 enable</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Onboard CH-2 disable</td>
<td>Y</td>
</tr>
<tr>
<td>J13</td>
<td>UVLO</td>
<td>(1,2)</td>
<td>Enable from V_HV</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Enable from V_LV</td>
<td></td>
</tr>
<tr>
<td>HEADER</td>
<td>SIGNAL</td>
<td>PINS</td>
<td>FUNCTION DESCRIPTION</td>
<td>DEFAULT</td>
</tr>
<tr>
<td>---------</td>
<td>----------</td>
<td>----------</td>
<td>--------------------------------------------------------</td>
<td>---------</td>
</tr>
<tr>
<td>J14</td>
<td>V5</td>
<td>(1,2)</td>
<td>Enable power supply for CC control</td>
<td>Y</td>
</tr>
<tr>
<td>J16</td>
<td>V-5</td>
<td>(1,2)</td>
<td>Enable –5-V power supply</td>
<td>Y</td>
</tr>
<tr>
<td>J18</td>
<td>IREF/VREF</td>
<td>(1,2),(7,8)</td>
<td>Enable DAC output signal for CC/CV control loop</td>
<td>Y</td>
</tr>
<tr>
<td>J24</td>
<td>INA828 GAIN</td>
<td>(1,2)</td>
<td>High current (50–100 A) gain</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Low current (0–50 A) gain</td>
<td>Y</td>
</tr>
<tr>
<td>J25</td>
<td>EN3</td>
<td>(1,2)</td>
<td>Onboard CH-3 enable</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Onboard CH-3 disable</td>
<td>Y</td>
</tr>
<tr>
<td>J26</td>
<td>EN4</td>
<td>(1,2)</td>
<td>Onboard CH-4 enable</td>
<td>Y</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>Onboard CH-4 disable</td>
<td>Y</td>
</tr>
<tr>
<td>J27</td>
<td>SYNCOUT2</td>
<td>(1,2)</td>
<td>Clock output for multiphase configuration</td>
<td>N</td>
</tr>
<tr>
<td>J29</td>
<td>OPT2</td>
<td>(1,2)</td>
<td>Multiphase Configuration</td>
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<tr>
<td></td>
<td></td>
<td>(2,3)</td>
<td>No multiphase configuration</td>
<td>Y</td>
</tr>
<tr>
<td>J34</td>
<td>V_HV</td>
<td>(1,2)</td>
<td>Enable CV control for bus voltage(V_HV)</td>
<td>N</td>
</tr>
<tr>
<td>J35</td>
<td>V_LV</td>
<td>(1,2)</td>
<td>Enable CV control for battery voltage(V_LV)</td>
<td>Y</td>
</tr>
<tr>
<td>J37</td>
<td>V5A</td>
<td>(1,2)</td>
<td>Enable power supply for CV control</td>
<td>Y</td>
</tr>
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</table>
3.1.2 Getting Started: Software

3.1.2.1 DAC Setup

This reference design uses the USB2ANY interface adapter to communicate with the DAC80004 device to generate a reference signal for current and voltage control. First, open the USB2ANY Explorer, click Select Interface to choose the SPI, then click the 3.3V ON button. Click the SPI tab above the Activity Logging section. If the SPI tab does not appear, click around the words “Activity Logging” as sometimes the tabs are hidden. Configure the GUI parameters as Figure 22 shows.

**Figure 22. USB2ANY Configuration**

![USB2ANY Configuration](image)

3.1.2.2 ADC Setup

Delta-Sigma ADC Evaluation Software is used to communicate with the ADS131A04 device. See the *Delta-Sigma ADC Evaluation software user's manual* and *ADS131A04 evaluation module user's guide* for detailed information.
After launching this software, click the Scripts menu, then click Predefined and choose Basic startup with Datarate at 8 kSPS as Figure 23 shows. Finally, click the Run button at the right side of the window.

**Figure 23. ADC GUI Setting**

![Figure 23. ADC GUI Setting](image)

The second step is to set the registers of the ADC. Figure 24 highlights the registers that need to be changed and their correct values for this design. It can also modify clock and OSR settings.

**Figure 24. ADC Register Setting**

![Figure 24. ADC Register Setting](image)
After setting the GUI and registers, the software can now capture data: click the Data Analysis menu, choose "ADC0" and "ADC1", change the Clock and VRef (V), and click the Collect Data button as Figure 25 shows.

Figure 25. ADC GUI Collect Data

The raw data is shown on the GUI, but the mean value of current and voltage is needed.
Figure 26. ADC GUI Data Analysis

Figure 26 illustrates the GUI when the Histogram menu at the left corner is clicked. It shows the mean value on the bottom after analysis in full scale format. Divide by 8388607 (DEC of 0X7FFFFF), and multiply by the reference voltage of the ADC, resulting in the current and voltage values as seen in Equation 6 and Equation 7. This example was tested under CC control: the control current is 5 A, the battery voltage is 3.1 V.

\[
\text{ADC}_{\text{current}} = \frac{\text{ADC}_{\text{mean}}}{8388607} \times V_{\text{Ref}} = \frac{785343.6}{8388607} \times 2.5 \quad \text{V} = 234.05 \quad \text{mV}
\]

\[
\text{ADC}_{\text{voltage}} = \frac{\text{ADC}_{\text{mean}}}{8388607} \times V_{\text{Ref}} = \frac{4833489.7}{8388607} \times 2.5 \quad \text{V} = 1.4405 \quad \text{V}
\]

The expected value of channel 0 should be \((\text{Iset} \times \text{Rcs} \times \text{Gain}_{\text{INA188}} \times \text{Gain}_{\text{ADC0}}) = 5 \times 0.5 \, \text{m}^2 \times 88.96 \times 1 = 222.4 \, \text{mV}\), and the expected value of channel 1 should be \((\text{Vset} \times \text{Gain}_{\text{ADC1}}) = 3.1 \, \text{V} \times (1.5 \, \text{k}/3.30 \, \text{k}) = 1.4091 \, \text{V}\). Those values are close to the mean value from the histograms. Due to the offset and noise of the components, refer to Section 3.1.4.4 to calibrate the ADC. The result is a more accurate value.
3.1.3 Test Setup

The test setup for the buck and boost mode operations of the TIDA-01041 require different setups for current and voltage control tests. Figure 27 shows a block diagram of the hardware setup for the TIDA-01041 current control test.

**Figure 27. CC Mode Test Setup**

First and foremost, the power supplies need to be able to provide enough power in both buck and boost mode or the electronic load will not operate properly. Configure the TIDA-01041 board to buck or boost mode through the "DIR" header (J6). Once configured, write to the DAC to generate current and voltage reference signals to start both control loops. Configure the electronic load to operate in CV mode, the voltage at the electronic load must be smaller than the constant voltage reference set by the DAC, allowing the CV control loop to give enough forward voltage for D3, and the TIDA-01041 design can work in CC mode. The super capacitor is required to clamp the output voltage and simulate the battery performance.

Figure 28 shows the block diagram of the hardware setup for the TIDA-01041 voltage control loop test.

**Figure 28. CV Mode Test Setup**

For this design to operate in CV mode, set the electronic load to CC mode and write to the DAC to generate current and voltage reference signals to start both control loops. The current at the electronic load must be smaller than the constant current reference voltage set by the DAC.
3.1.4 Test Results

Battery test equipment must possess accurate voltage and current control, often better than ±0.05%, as well as a smooth transition between the two to maximize capacity, battery life, quality and performance. This section provides accuracy testing results for current and voltage control for this design as well as the performance of the system when transforming between CC and CV mode.

3.1.4.1 Current Control Accuracy

The current accuracy depends on the current sensing resistor, the gain, offset, and drift of the current amplifier, INA828, and TLV07 devices. For more information on current accuracy in this design as well as the calibration process for buck and boost mode operations, see the TIDA-01040 battery tester reference design for high current applications reference design.

Figure 29 shows the CC control accuracy of this reference design at buck (high side is 12 V, low side is 1 V) and boost (low side is 2 V, high side is 10 V) mode conditions.

![Figure 29. CC Control Accuracy](image)

The results show that CC control can maintain ±0.02% accuracy within the full current range of this design 0.5 A–100 A, meeting the accuracy range requirements to maximize battery performance.

3.1.4.2 Voltage Control Accuracy

This system requires calibration due to the voltage control accuracy being affected by the gain offset, offset of the resistor divider at the output of the LM6142, and the LM6142 itself. See the TIDA-01040 battery tester reference design for high current applications reference design for more information on the calibration method for these test results.

![Figure 30. CV Control Accuracy](image)

Figure 30 shows that the CV control can maintain ±0.01% accuracy within a battery voltage range of 1.0 V–4.2 V, meeting the accuracy range requirements to maximize battery performance.
### 3.1.4.3 CC, CV Transformation

It is critical to understand the performance of the system when transforming from CC to CV mode as this will affect its ability to eliminate overcharging in the battery.

Figure 31 and Figure 32 show the transformation under different current and different voltage settings.

**Figure 31. CC, CV Transformation Under Different Current Settings**

![Graph showing CC, CV transformation under different current settings](image)

In Figure 31, with the increase in current setting, the CC control will start transforming to CV control at lower voltage. The transformation remains linear throughout testing, indicating that the ability of the design to eliminate overcharging is not affected at higher currents.

**Figure 32. CC, CV Transformation Under Different Voltage Settings**

![Graph showing CC, CV transformation under different voltage settings](image)

Figure 32 shows that voltage setting has less effect on the switch from CC control to CV control.
3.1.4.4 ADC Calibration

Two channels are used to monitor the battery current and voltage. The accuracy of this data acquisition depends on the gain and offset of the THS4561 device and other components, so the output of the ADC should be calibrated. Use a similar method to calibrate those two channels as the previous current and voltage control loop.

Figure 33 and Figure 34 show the accuracy of this data acquisition after calibration.

The results show the ADC current acquisition accuracy is excellent. Although the ADC current acquisition accuracy is not good in the low current range, battery tester applications usually are more concerned with the accuracy at higher currents.
4 Design Files

4.1 Schematics
To download the schematics, see the design files at TIDA-01041.

4.2 Bill of Materials
To download the bill of materials (BOM), see the design files at TIDA-01041.

4.3 PCB Layout Recommendations

4.3.1 Layout Prints
To download the layer plots, see the design files at TIDA-01041.

4.4 Altium Project
To download the Altium Designer® project files, see the design files at TIDA-01041.

4.5 Gerber Files
To download the Gerber files, see the design files at TIDA-01041.

4.6 Assembly Drawings
To download the assembly drawings, see the design files at TIDA-01041.

4.7 Simulation Results
To download the simulation results, see the design files at TIDA-01041.

5 Software Files
To download the software files, see the design files at TIDA-01041.

6 Related Documentation
1. Texas Instruments, TIDA-01040 battery tester reference design for high current applications reference design
2. Texas Instruments, Multiphase buck design from start to finish (Part 1) application report
3. Texas Instruments, Merits of Multiphase Buck DC/DC Converters in Small Form Factor Applications
4. Texas Instruments, Benefits of a multiphase buck converter application note
5. Texas Instruments, LM5170-Q1 multiphase bidirectional current controller data sheet
6. Texas Instruments, LM2664 switched capacitor voltage converter data sheet
7. Texas Instruments, TPS709 150-mA, 30-V, 1-μA I_Q voltage regulators with enable data sheet
8. Texas Instruments, LM5118 wide voltage range buck-boost controller data sheet
9. Texas Instruments, INA188 precision, zero-drift, rail-to-rail out, high-voltage instrumentation amplifier data sheet
10. Texas Instruments, DACx0004, quad 16-,14-,12-bit, 1 LSB INL, buffered, voltage-output digital-to-analog converters data sheet
11. Texas Instruments, ADS131A0x 2- or 4-Chan, 24-bit, 128-kSPS, simultaneous-sampling, delta-sigma ADC data sheet
12. Texas Instruments, TLV07 36-V precision, rail-to-rail output operational amplifier data sheet
13. Texas Instruments, OPAx22x high precision, low noise operational amplifiers data sheet
14. Texas Instruments, OPA827 low-noise, high-precision, JFET-input operational amplifier data sheet
15. Texas Instruments, THS4561 low-power, high supply range, 70-MHz, fully differential amplifier data sheet
16. Texas Instruments, LM6142/LM6144 17 MHz rail-to-rail input-output operational amplifiers
17. Texas Instruments, PMP15038 test results technical reference

6.1 Trademarks
E2E is a trademark of Texas Instruments.
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7 About the Author

Maseo Browning is an application engineer at Texas Instruments, where he is responsible for developing reference design solutions for the test and measurement industry. Maseo earned his bachelors of science in electrical engineering (BSEE) degree from the Rochester Institute of Technology in Rochester, New York.

Taras Dudar is a systems design engineer and architect at Texas Instruments, where he is responsible for developing reference design solutions for the test and measurement industry. Previously, Taras designed high-speed analog SOC integrated circuits for Gbps data communications. Taras earned his master of science in electrical engineering (MSEE) degree from the Oregon State University in Corvallis, OR.

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Revision History
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

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<thead>
<tr>
<th>Changes from Original (March 2019) to A Revision</th>
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<tr>
<td>• Updated block diagram with TLV07.</td>
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<tr>
<td>• Changed 'CC, CV' to 'constant current (CC) and constant voltage (CV)'</td>
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<tr>
<td>• Updated Li-Ion Battery Formation Profile section.</td>
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<tr>
<td>• Changed wording throughout the System Overview section.</td>
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<tr>
<td>• Updated the Block Diagram section.</td>
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<td>• Updated block diagram with TLV07.</td>
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<td>• Changed information in Table 5</td>
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