



TI Technology Days 2010

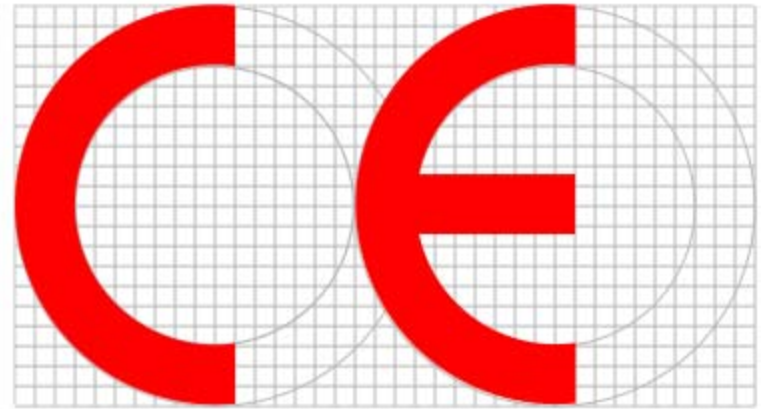
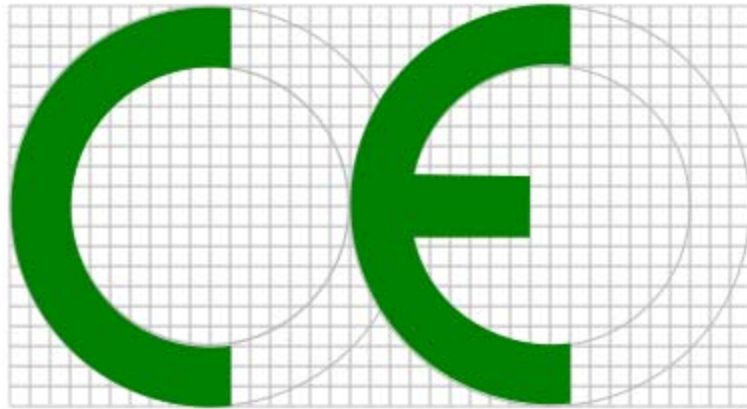
EMV in Theorie und Praxis fuer Jedermann

Josef Warta

AGENDA

- Rechtsgrundlagen
- Theorie
- Praktische Tipps

CE Kennzeichnung



<http://www.ce-richtlinien.eu/index.html>

CE Richtlinien

fuer unterschiedliche Anwendungsgebiete, z.B.

- Spielzeug-Richtlinie 2009/48/EG
- Aktive implantierbare medizinische Geräte 90/385/EWG
- Richtlinie 2004/108/EG:
Elektromagnetische Verträglichkeit von Elektro- und
Elektronikprodukten – EMV
- Niederspannungsrichtlinie 2006/95/EG
- Telekommunikations-Richtlinie 1999/5/EG
- .
- .
- .

**RICHTLINIE 2004/108/EG DES EUROPÄISCHEN PARLAMENTS UND DES
RATES**

vom 15. Dezember 2004

**zur Angleichung der Rechtsvorschriften der Mitgliedstaaten über die
elektromagnetische Verträglichkeit
und zur Aufhebung der Richtlinie 89/336/EWG**

“...die Fähigkeit eines Apparates, einer Anlage oder eines Systems, in der elektromagnetischen Umwelt zufriedenstellend zu arbeiten, ohne dabei selbst elektromagnetische Störungen zu verursachen, die für alle in dieser Umwelt vorhandenen Apparate, Anlagen oder Systeme unannehmbar wären.”

Weitere Links:

- Gesetz über die elektromagnetische Verträglichkeit von Betriebsmitteln (EMVG)
- Harmonisierte Normen (z.B. Fachgrundnormen EN-61000-6, Produktnormen EN-61326, Prüfnormen EN-61004-4,...)

Begriffsdefinition

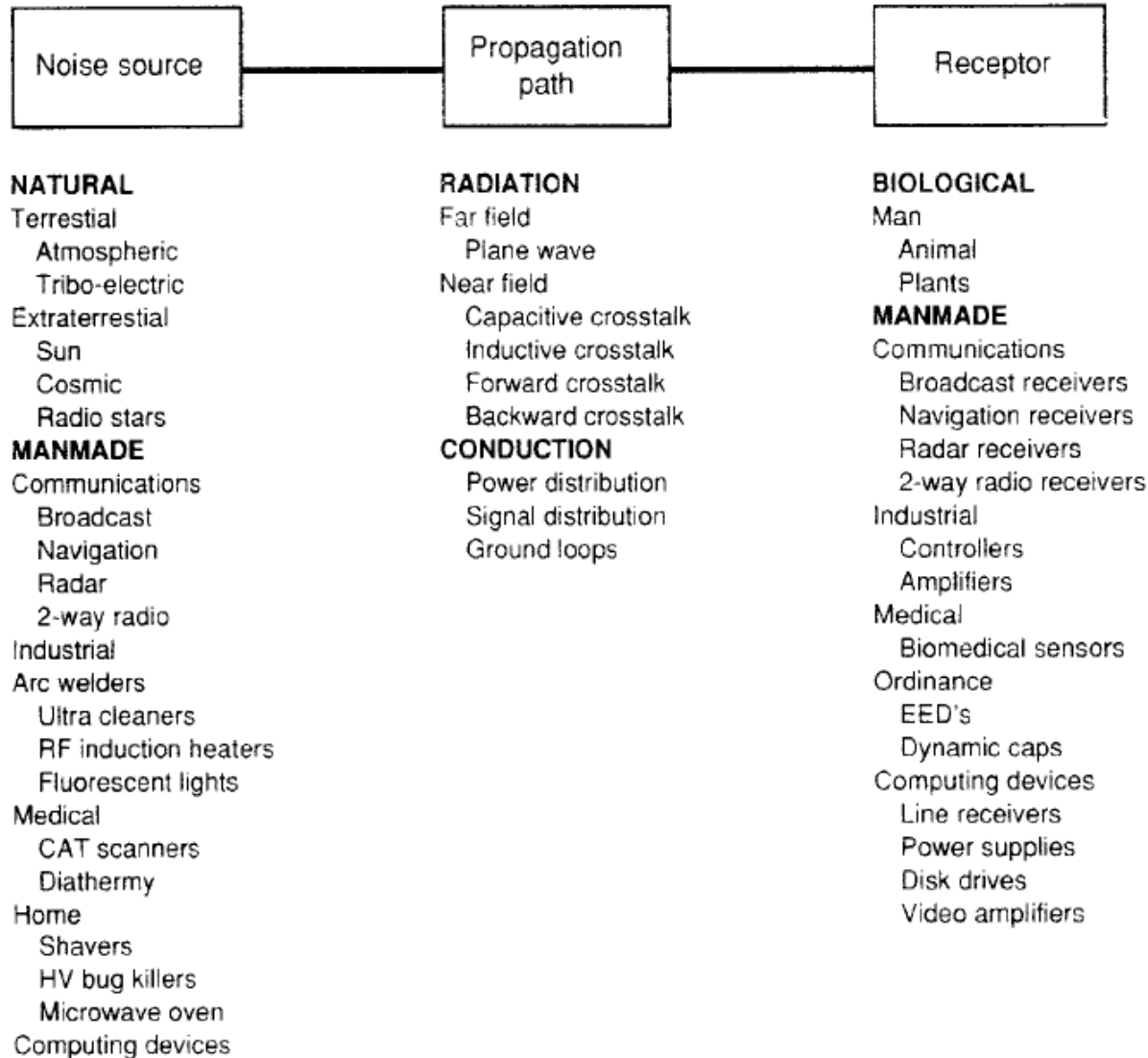
Kopplungsmechanismen

- Galvanische Kopplung
- Kapazitive Kopplung (Nahfeld)
- Induktive Kopplung (Nahfeld)
- Strahlungskopplung (Fernfeld)

Arten von Störungen

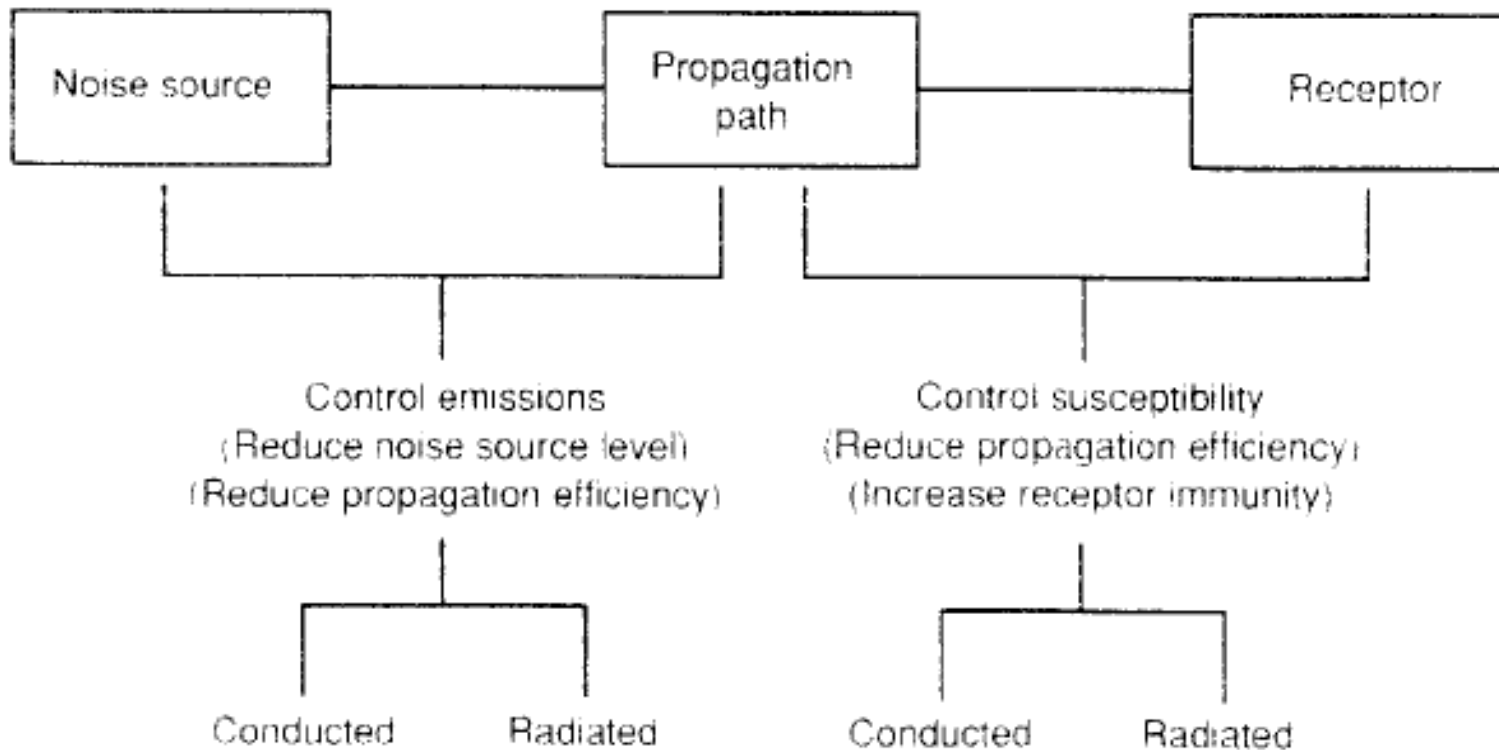
- **leitungsgebundenen Störungen** werden von der Störquelle direkt über Versorgungs- oder Signalleitungen zur Störsenke übertragen.
- **feldgebundenen Störungen** werden zum Beispiel als elektromagnetisches Feld auf die Störsenke übertragen und dort beispielsweise von einem als Antenne fungierenden Leiter empfangen (Fernfeld).
Auch kapazitive und induktive Beeinflussungen elektrischer bzw. magnetischer Felder werden als feldgebundene Störungen bezeichnet. (Nahfeld)

Elemente der EMV Umgebung



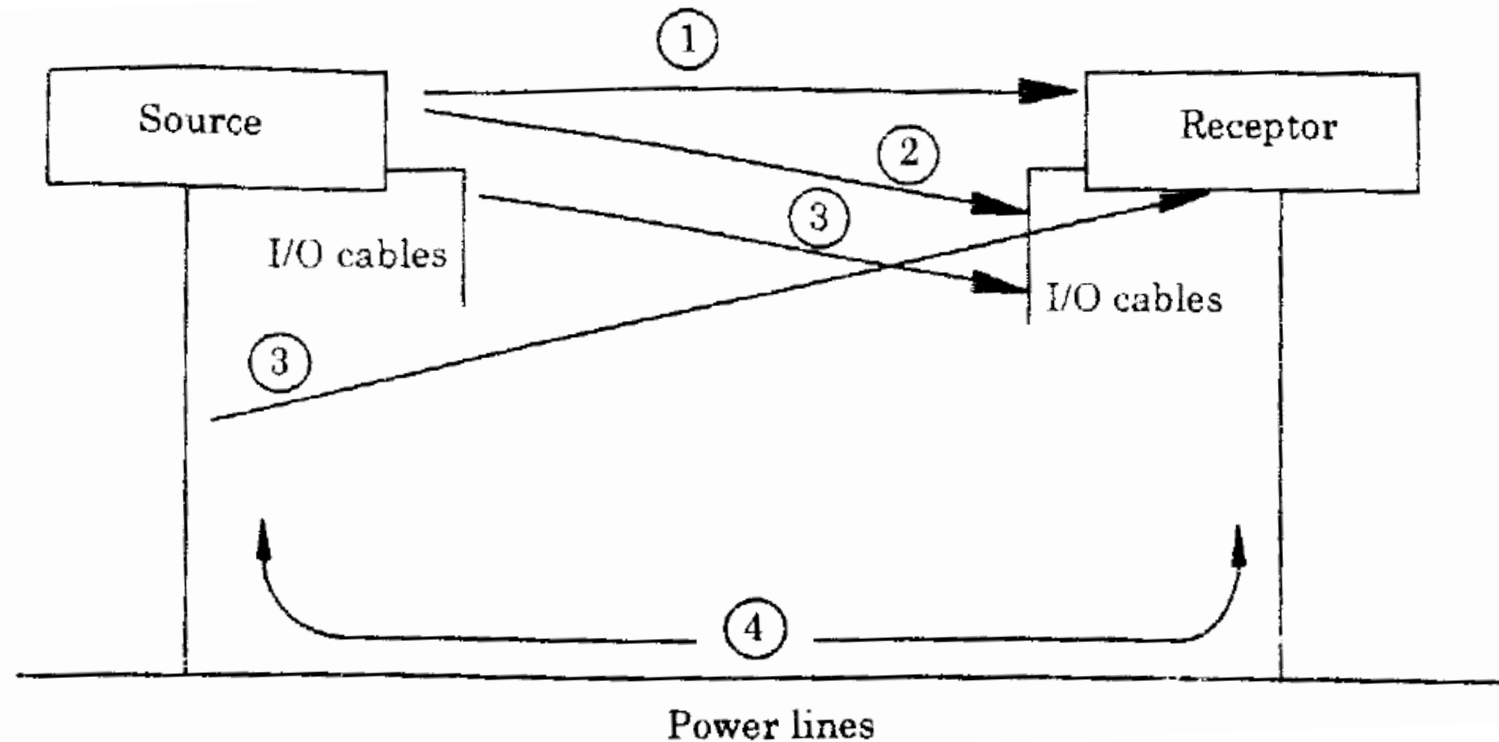
(Quelle: EMC and the printed circuit board : design, theory, and layout made simple/ Mark I. Montrose [1])

Kopplungen



(Quelle: EMC and the printed circuit board : design, theory, and layout made simple/ Mark I. Montrose [1])

Kopplungspfade



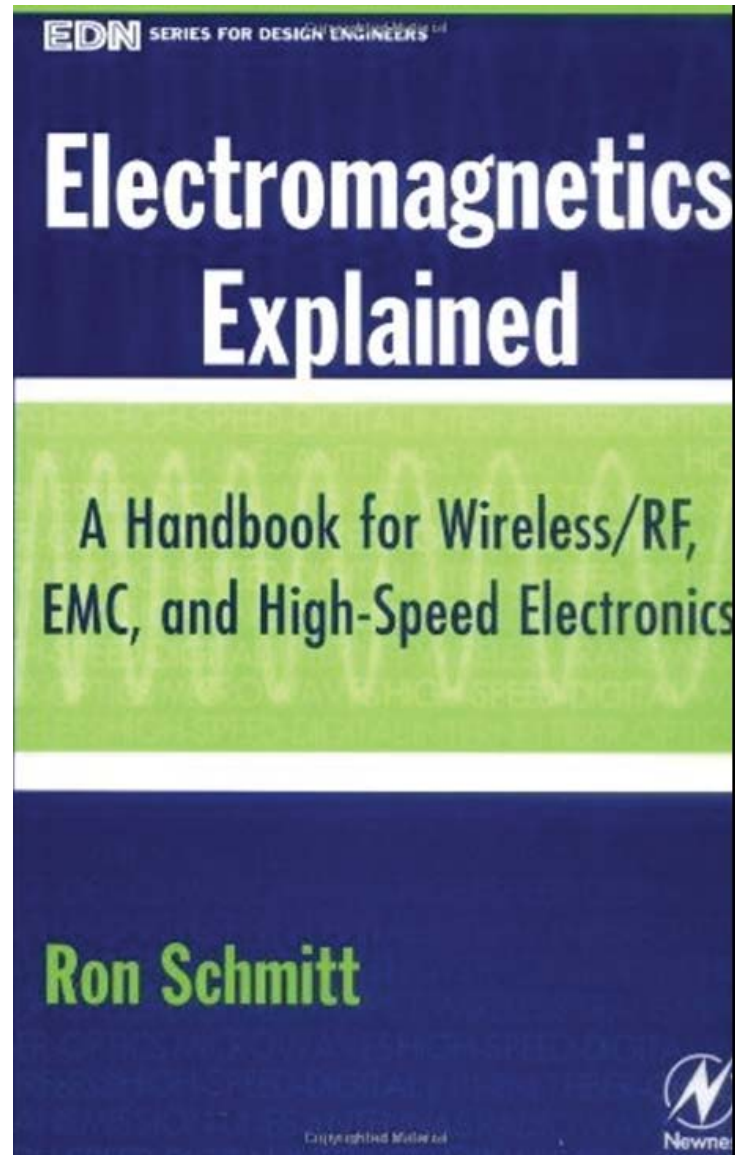
- 1 – Abstrahlung von Source auf Receptor
- 2 – Abstrahlung von Source auf Stromversorgung oder Interfaceleitungen
- 3 – Abstrahlung von Stromversorgung oder Interfaceleitung auf Receptor
- 4 – Störübertragung über Stromversorgung oder Interfaceleitung

(Quelle: EMC and the printed circuit board : design, theory, and layout made simple/ Mark I. Montrose [1])

Theorie

Die elektromagnetische Welle

Grundlagen: Electromagnetics



Elektromagnetisches Spektrum

$$\lambda = \frac{c}{f} \quad \lambda' = \frac{\lambda_0}{\sqrt{\mu_r \epsilon_r}} = \frac{c}{f} \frac{1}{\sqrt{\mu_r \epsilon_r}}$$

Permittivität ϵ (*dielektrische Leitfähigkeit*, gibt die Durchlässigkeit eines Materials für elektrische Felder an)

$$T = \frac{1}{f}$$

Permeabilität μ (*magnetische Leitfähigkeit* bestimmt die Durchlässigkeit von Materie für magnetische Felder)

$$E = h \times f$$

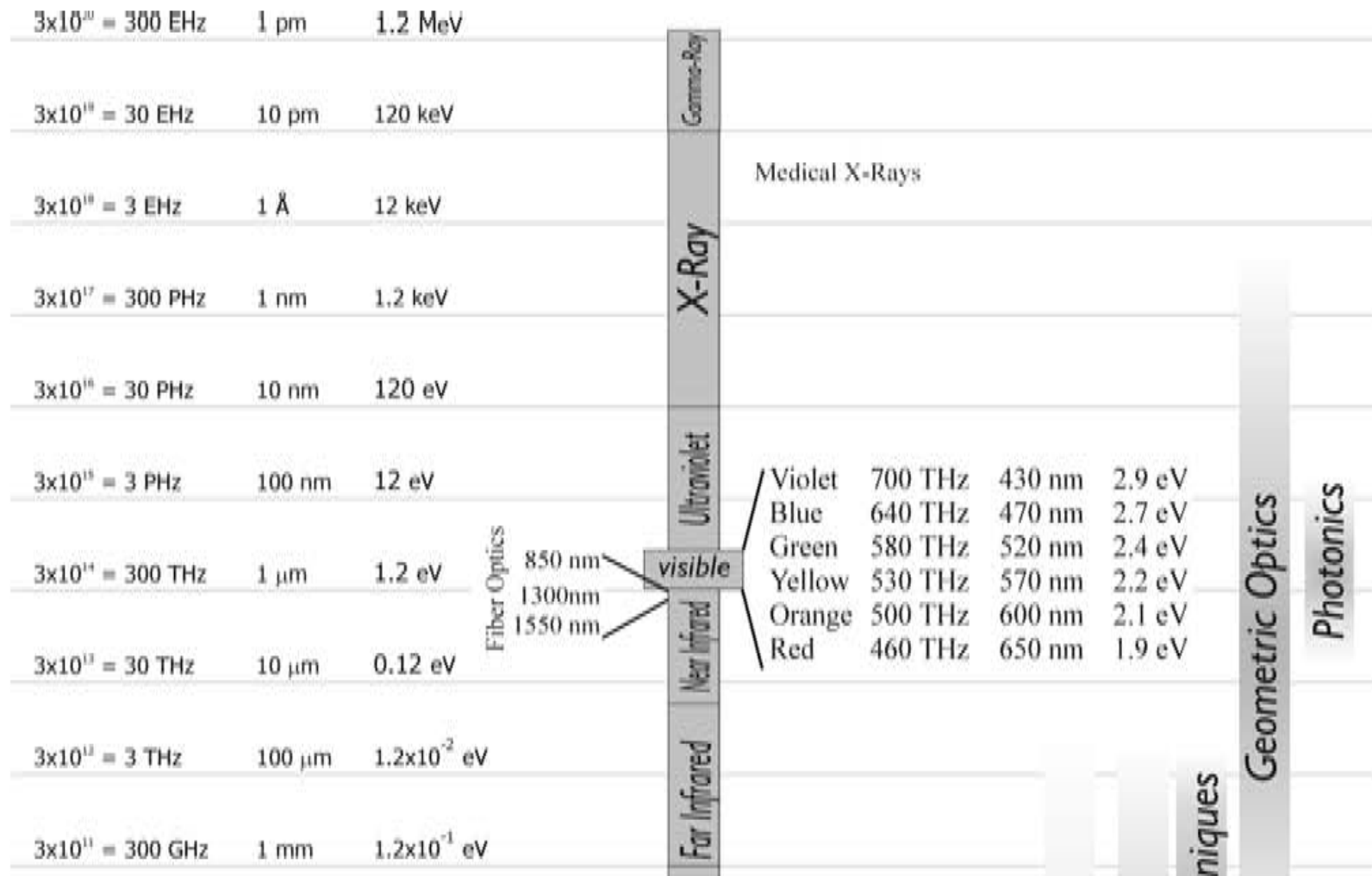
$$\text{Electrical length} = \frac{L}{\lambda}$$

Elektromagnetisches Spektrum (1)

$3 \times 10^{10} = 30 \text{ GHz}$	1 cm	$1.2 \times 10^{-4} \text{ eV}$							Aircraft Radar Police Radar
									Satellite TV
$3 \times 10^9 = 3 \text{ GHz}$	10 cm	$1.2 \times 10^{-5} \text{ eV}$							Cellular
									Microwave oven 2.45 GHz
$3 \times 10^8 = 300 \text{ MHz}$	1 m	$1.2 \times 10^{-6} \text{ eV}$							Cellular
									UHF TV
$3 \times 10^7 = 30 \text{ MHz}$	10 m	$1.2 \times 10^{-7} \text{ eV}$							VHF TV
									FM radio 88-108 MHz
$3 \times 10^6 = 3 \text{ MHz}$	100 m	$1.2 \times 10^{-8} \text{ eV}$							VHF TV
									shortwave radio
$3 \times 10^5 = 300 \text{ kHz}$	1 km	$1.2 \times 10^{-9} \text{ eV}$							AM radio 535-1605 kHz
									Radio beacons
$3 \times 10^4 = 30 \text{ kHz}$	10 km	$1.2 \times 10^{-10} \text{ eV}$							submarine radio
$3 \times 10^3 = 3 \text{ kHz}$	100 km	$1.2 \times 10^{-11} \text{ eV}$							
$3 \times 10^2 = 300 \text{ Hz}$	1 Mm	$1.2 \times 10^{-12} \text{ eV}$							
$3 \times 10^1 = 30 \text{ Hz}$	10 Mm	$1.2 \times 10^{-13} \text{ eV}$							power-lines 60Hz
$3 \times 10^0 = 3 \text{ Hz}$	100 Mm	$1.2 \times 10^{-14} \text{ eV}$							

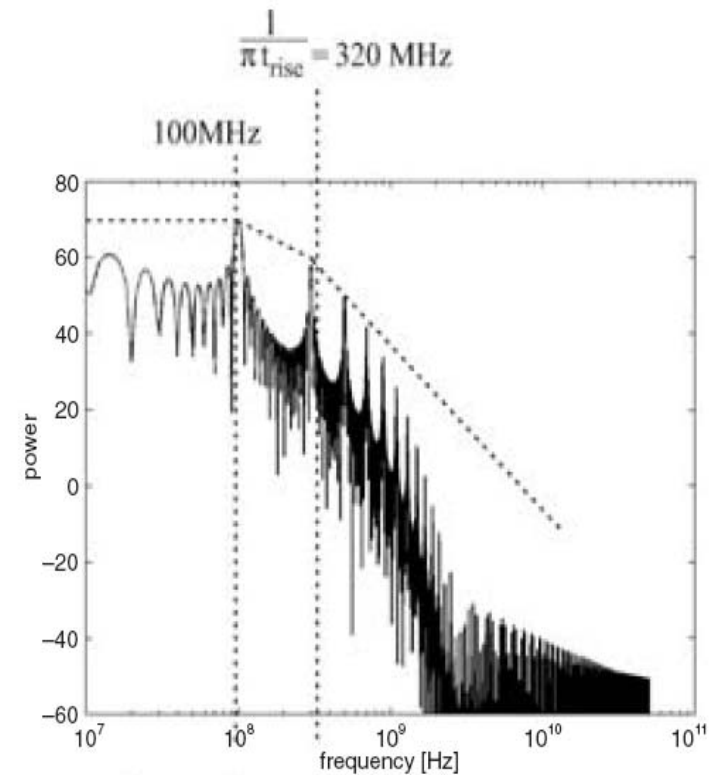
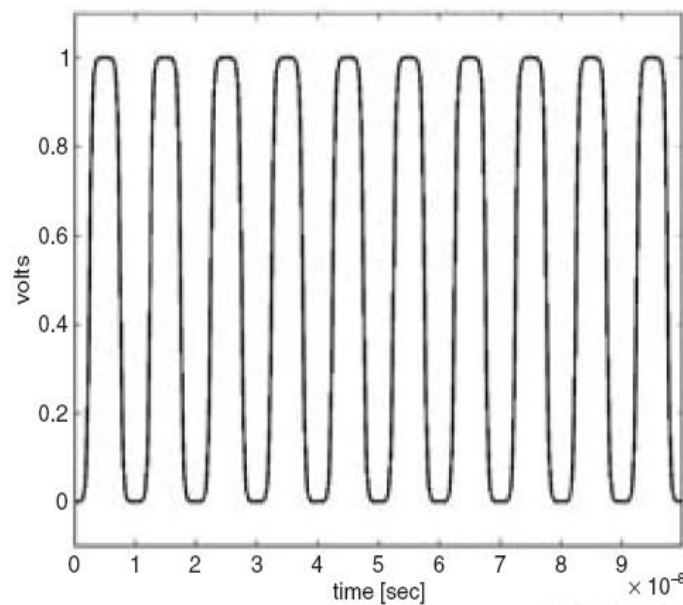
(Quelle: Electromagnetics explained [2])

Elektromagnetisches Spektrum (2)



(Quelle: Electromagnetics explained [2])

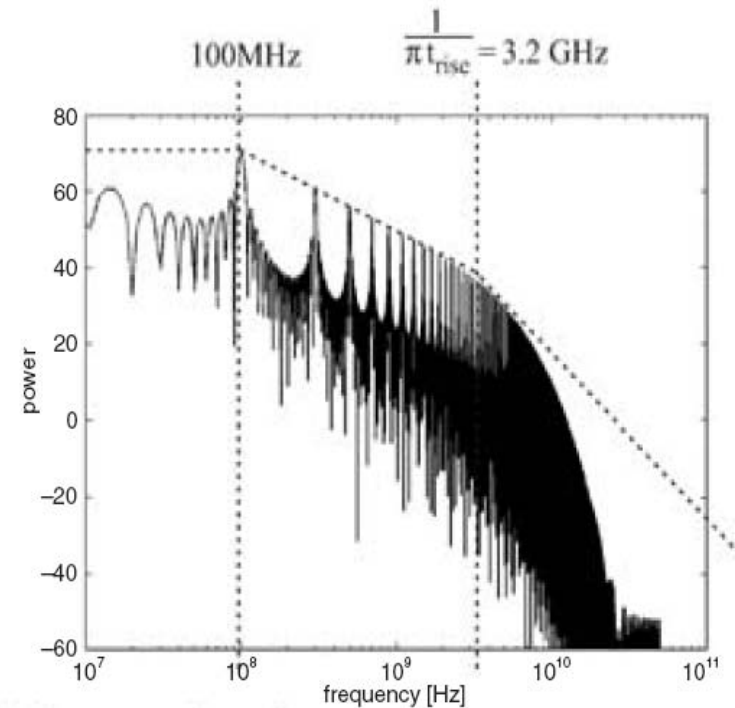
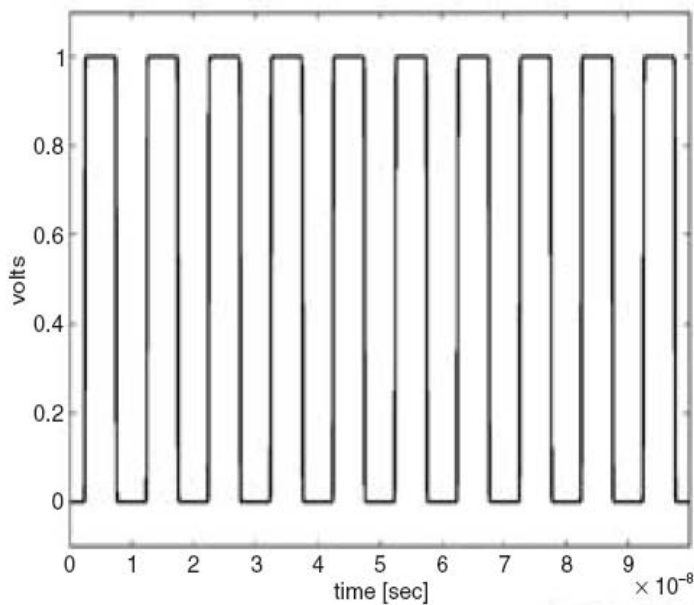
Typ. Signal/Frequenzspektrum (1)



100 MHz signal with 1 nsec rise time

(Quelle: Electromagnetics explained [2])

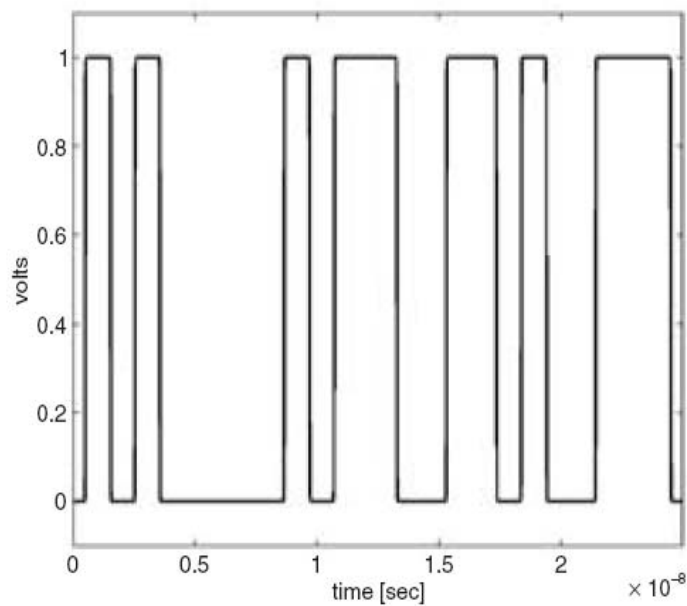
Typ. Signal/Frequenzspektrum (2)



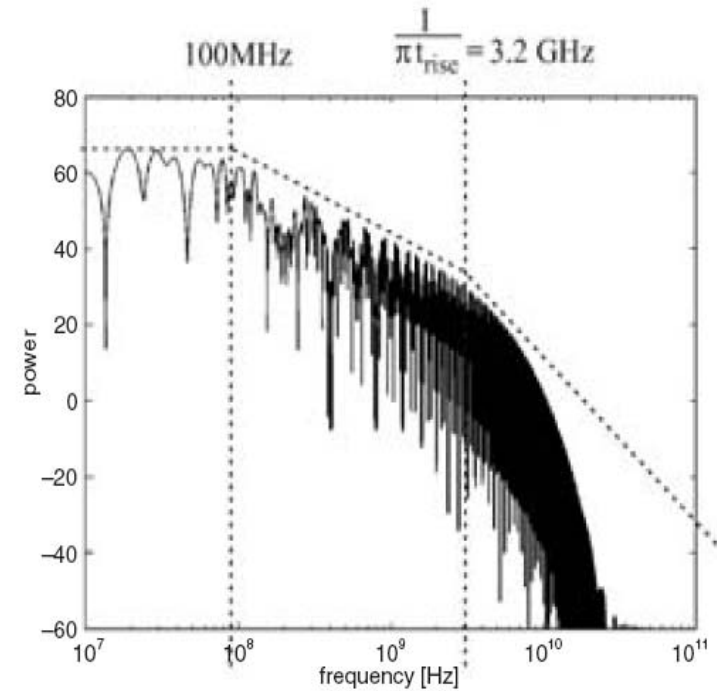
100 MHz signal with 100psec rise time

(Quelle: Electromagnetics explained [2])

Typ. Signal/Frequenzspektrum (3)

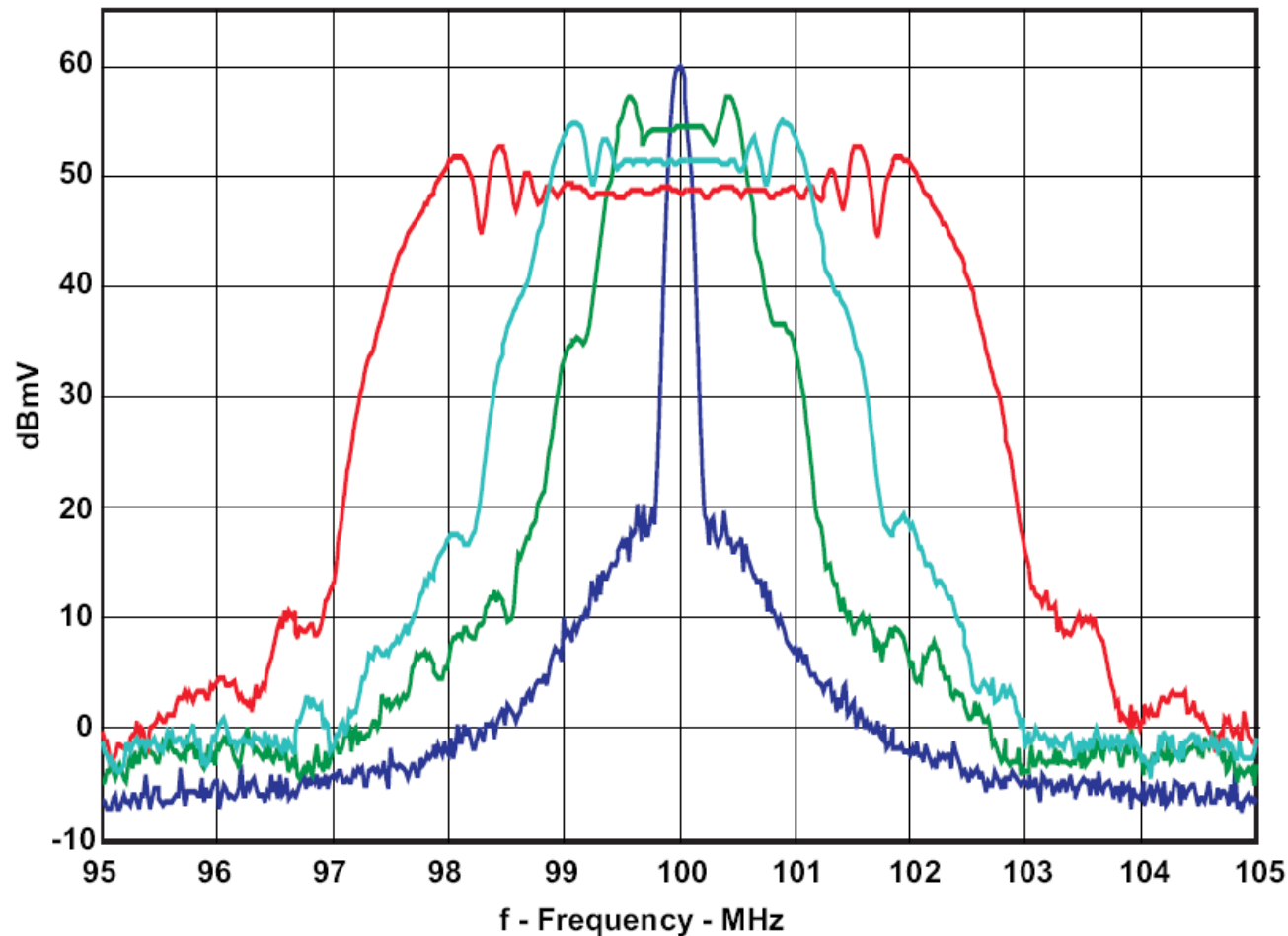


arbitrary data signal with 100psec rise time



(Quelle: Electromagnetics explained [2])

Spread Spectrum Clocking



CDCS502 With a 25-MHz Crystal, FS = 1, Fout = 100 MHz, and 0%, ±0.5, ±1%, and ±2% SSC

CDCS502

Xtal-In Clock Generator with Optional Spread Spectrum Clocking (SSC)

Features

- Crystal input from 8MHz to 32MHz
- Selectable multiplier rates of 1x and 4x so that generate output frequency from 8MHz to 110MHz
- Selectable Spread-Spectrum Modulation of $\pm 0.5\%$, $\pm 1.0\%$, and $\pm 2.0\%$
- 8 pin TSSOP package
- Single 3.3V power supply, wide temperature range -40 , 85

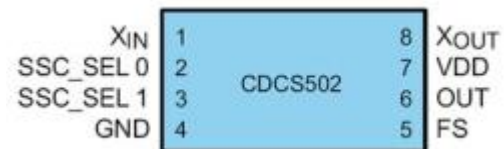
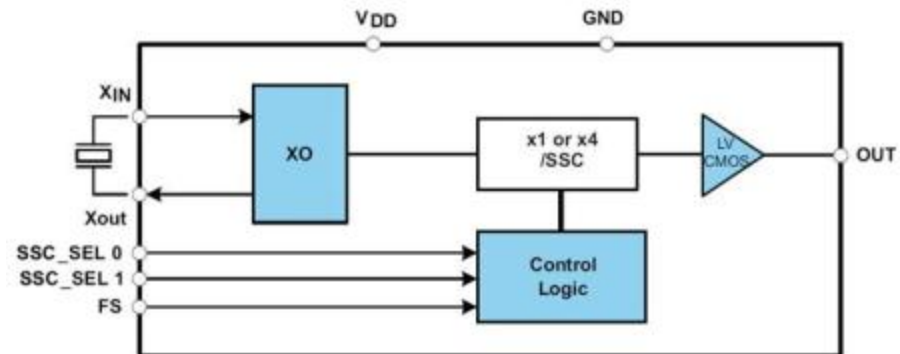
Applications

XO replacement with EMI reduction need:

- Digital Audio/Video Entertainment
 - Flat Panel TV; Set-top Boxes; Blu-Ray DVDR
- PCs, Printers
- Communications access point / Gateway / Networking card
- Industrial

Benefits

- Replacing more costly crystal oscillators
- Wider output frequency range enables one device across multiple designs
- Reduce EMI thru selectable amount of SSC modulation up to 10dB
- Low board space consumption
- Simple power supply scheme; Applicable to wider applications with improved reliability



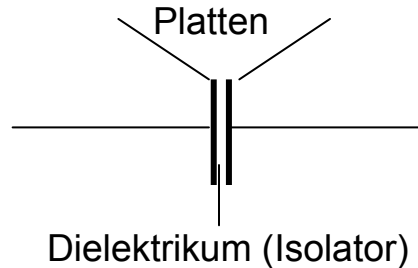
Elektrisches Feld - Kondensator

Grundeigenschaft: Speicherfähigkeit von elektrischen Ladungen (elektrisches Feld) - **Kapazität C**.

Kapazität allgemein:

$$C = \frac{Q}{U}$$

Einheit: $[C] = \frac{1As}{V} = 1F$



Kapazität Plattenkondensator:

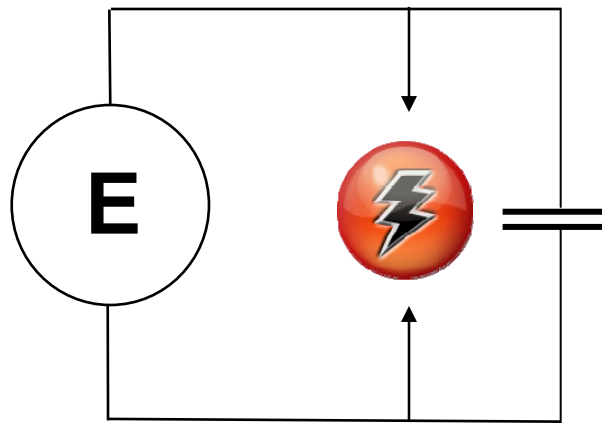
$$C = \varepsilon \frac{A}{d}$$

Abgewandelte Einheiten: $1F = 10^6\mu F = 10^9nF = 10^{12}pF$

Strom-Spannungs-Beziehung: $i = C \cdot \frac{du}{dt}$

(Quelle: Uni Muenster, IVV4Naturwissenschaften [3])

Elektrisches Feld - Kondensator



TPD1E14A4YFW

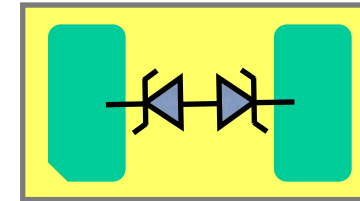
Single-Channel ESD in 0201 Package

Key Performance Parameters

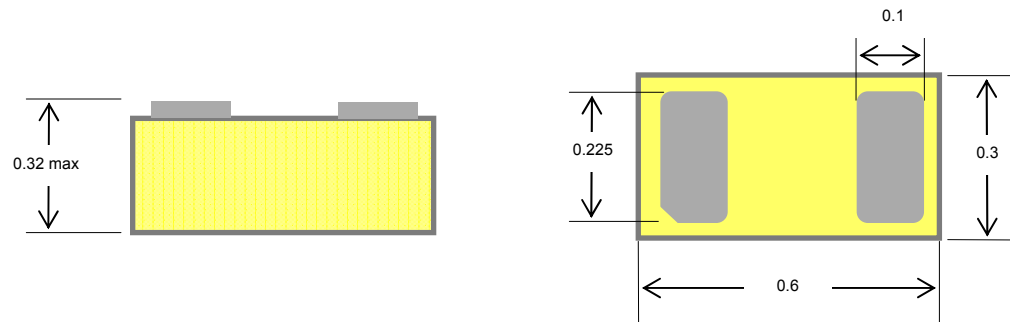
- Industry standard 0201 package
- Multiple Break-down voltage
Options: $\pm 4.5\text{V}$, $\pm 8\text{V}$, $\pm 14\text{V}$, $\pm 20\text{V}$, $\pm 30\text{V}$, and $+14\text{V}/-8\text{V}$
- ESD Protection exceeds IEC 61000-4-2 (Level 4)
- 1-A Peak Pulse Current (8/20 ms Pulse)
- Low 50-nA Leakage Current

Applications

- Audio Interface Connection
- USB Interface
- RS-232/422/485
- LVDS



Circuit Diagram



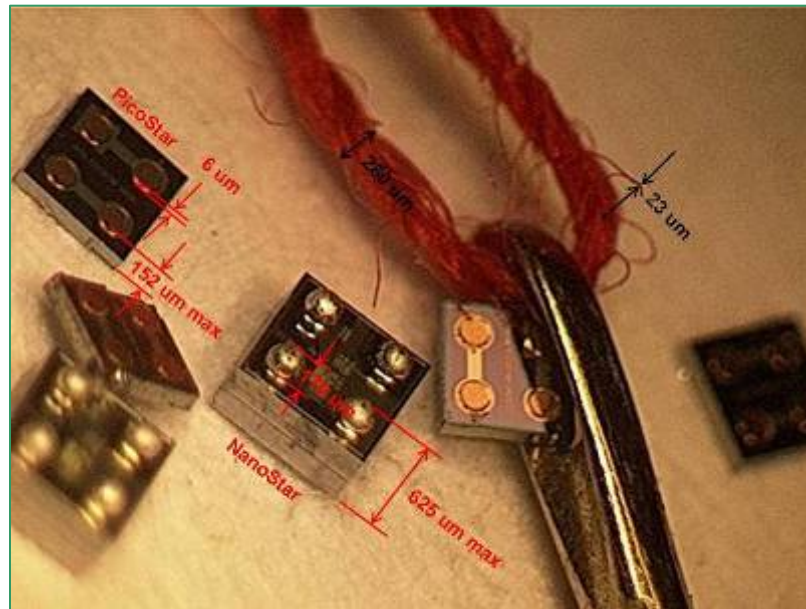
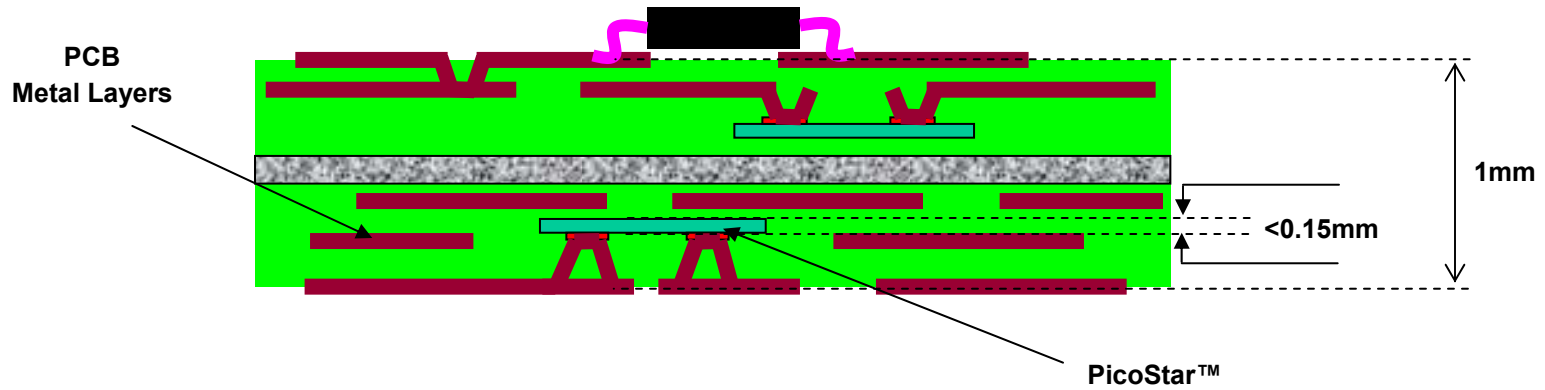
0201 Dimension

TI Packages for ESD/ EMI Solutions



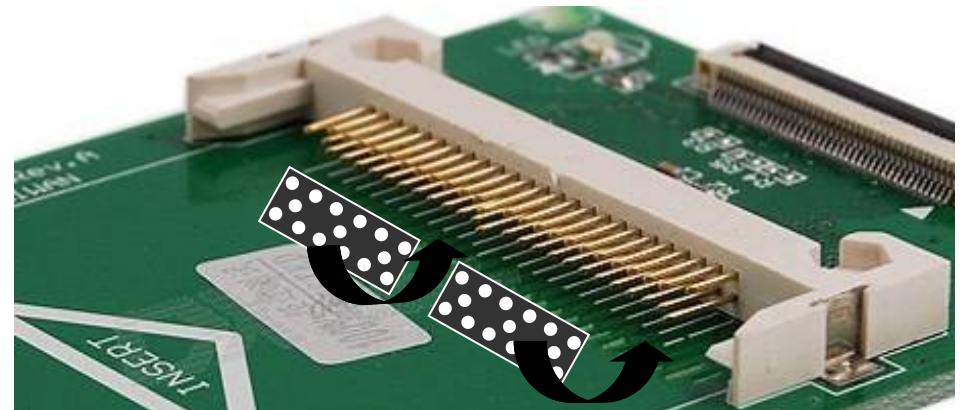
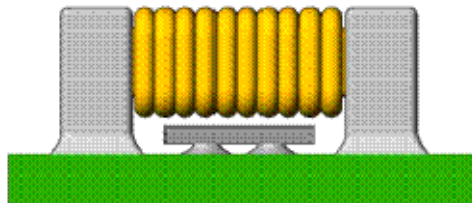
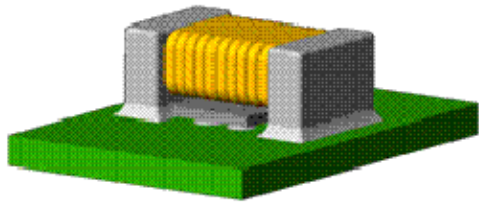
PicoStar Embedded Package Technology

Board Cross Section



TI's Ultra Thin Surface Mount Packages Open New Dimension in the PCB!

Component Placement is more Flexible with PicoStar or Ultra low-profile WCSP



0.13-mm (height) PicoStar Under Ceramic Inductor

0.3-mm (height) YFU Package Under the Zif Connector

Magnetisches Feld / Spule

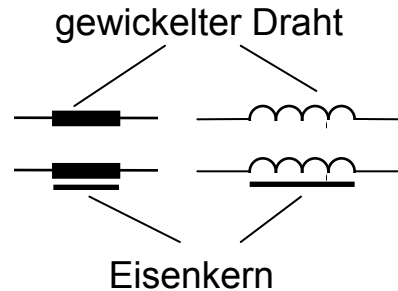
Grundeigenschaft: Zeitlich begrenzte Speicherfähigkeit des magnetischen Feldes - **Induktivität L**.

Induktivität
allgemein:

$$L = \frac{N \cdot \phi}{I}$$

Einheit:

$$[L] = \frac{1Vs}{A} = 1H$$



Induktivität der Spule:

$$L = \frac{\mu_0 \cdot \mu_r \cdot N^2 \cdot A}{l}$$

Abgewandelte Einheiten:

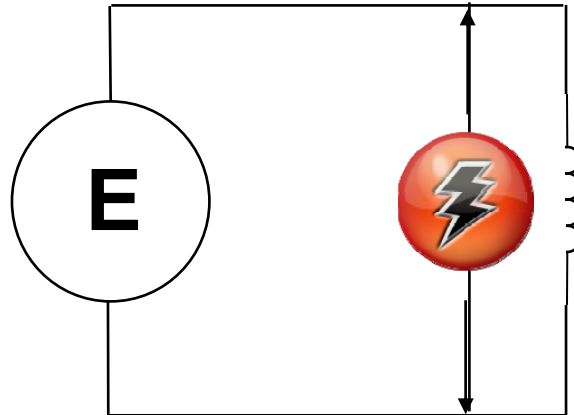
$$1H = 10^3mH = 10^6\mu H$$

Strom-Spannungs-Beziehung:

$$u = L \bullet \frac{di}{dt}$$

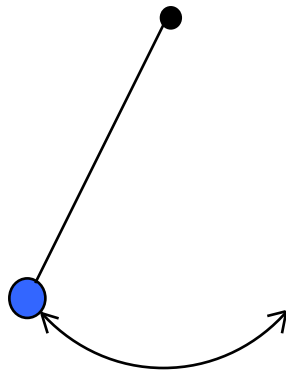
(Quelle: Uni Muenster, IVV4Naturwissenschaften [3])

Magnetisches Feld / Spule

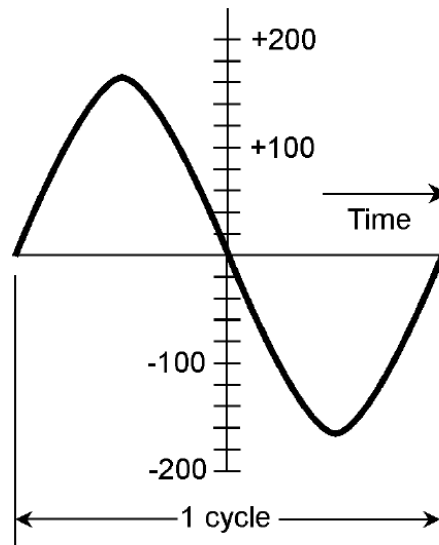
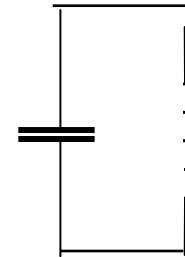


Elektro-Magnetischer Wechsel

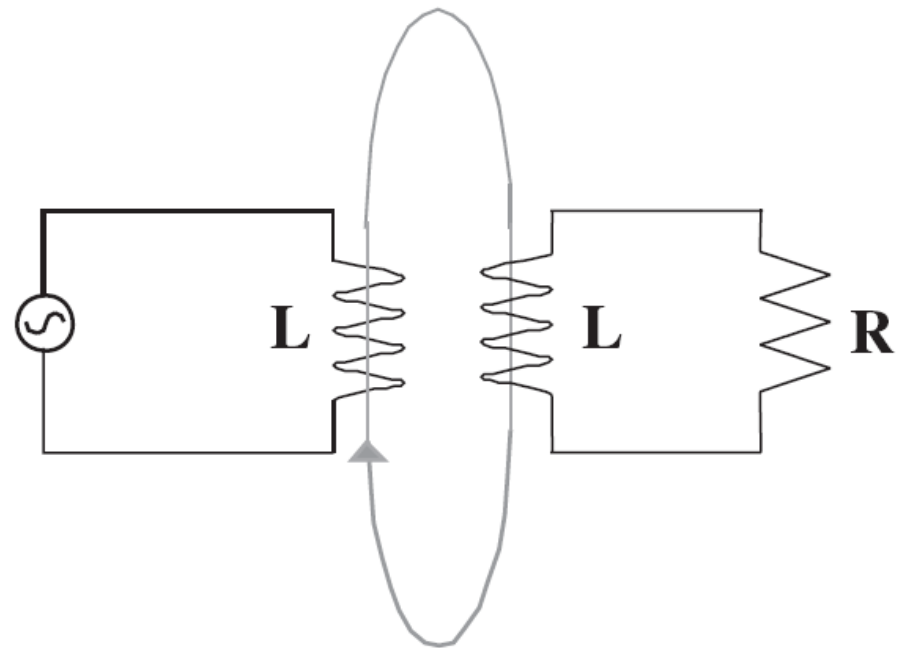
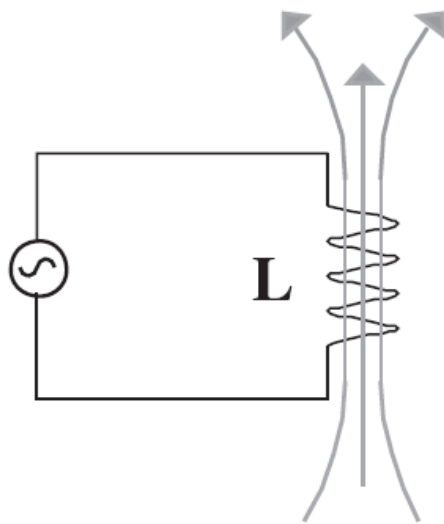
Mechanische Modell
"Pendel"



Elektrisches Modell
"Schwingkreis"

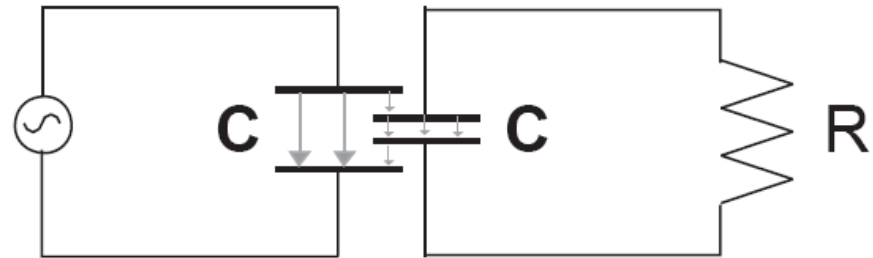
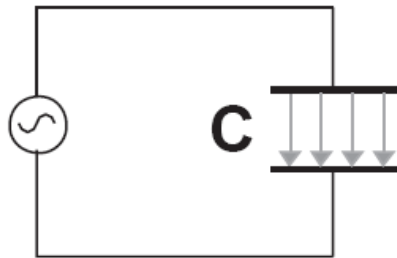


Nah-Strahlung Induktiv



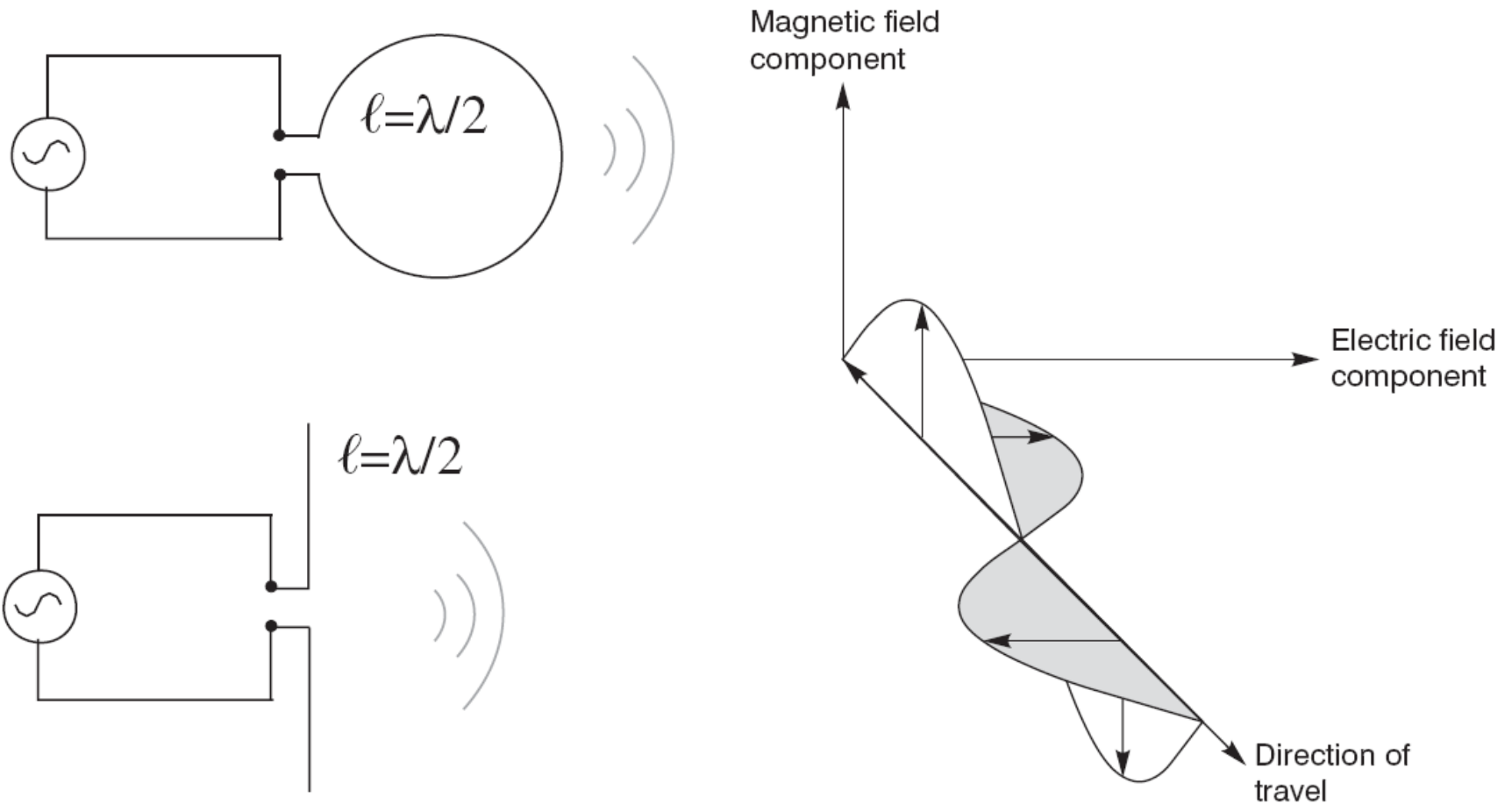
(Quelle: Electromagnetics explained [2])

Nah-Strahlung Kapazitiv



(Quelle: Electromagnetics explained [2])

Fern-Strahlung



(Quelle: Electromagnetics explained [2])

Nah/Fern-Strahlung

	<i>Near (Reactive) Field</i>	<i>Far (Radiated) Field</i>
Carrier of Force	Virtual photon	Photon
Energy	Stores energy. Can transfer energy via inductive or capacitive coupling.	Propagates (radiates) energy.
Longevity	Extinguishes when source power is turned off.	Propagates until absorbed.
Interaction	Act of measuring field or receiving power from field causes changes in voltages/currents in source circuit.	Act of measuring field or receiving power from field has no effect on source.
Shape of Field	Completely dependent on source circuit.	Spherical waves. At very long distances, field takes shape of plane waves.
Wave impedance	Depends on source circuit and medium.	Depends solely on propagation medium ($\eta = 120\pi \approx 377 \Omega$ in free space).
Guiding	Energy can be transported and guided using a transmission line.	Energy can be transported and guided using a wave guide.

(Quelle: Electromagnetics explained [2])

Maxwellsche Gleichungen elektromagnetischer Felder und Wellen

Maxwellsche Gleichungen

Differentialform

$$\nabla \times \underline{\mathbf{E}}(\underline{\mathbf{R}}, t) = -\frac{\partial}{\partial t} \underline{\mathbf{B}}(\underline{\mathbf{R}}, t) - \underline{\mathbf{J}}_m(\underline{\mathbf{R}}, t)$$

$$\nabla \times \underline{\mathbf{H}}(\underline{\mathbf{R}}, t) = \frac{\partial}{\partial t} \underline{\mathbf{D}}(\underline{\mathbf{R}}, t) + \underline{\mathbf{J}}_e(\underline{\mathbf{R}}, t)$$

$$\nabla \cdot \underline{\mathbf{D}}(\underline{\mathbf{R}}, t) = \rho_e(\underline{\mathbf{R}}, t)$$

$$\nabla \cdot \underline{\mathbf{B}}(\underline{\mathbf{R}}, t) = \rho_m(\underline{\mathbf{R}}, t)$$

Integralform

$$\oint_{\mathcal{C}=\partial S} \underline{\mathbf{E}}(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{R}} = -\iint_S \frac{\partial}{\partial t} \underline{\mathbf{B}}(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{S}} - \iint_S \underline{\mathbf{J}}_m(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{S}}$$

$$\oint_{\mathcal{C}=\partial S} \underline{\mathbf{H}}(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{R}} = \iint_S \frac{\partial}{\partial t} \underline{\mathbf{D}}(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{S}} + \iint_S \underline{\mathbf{J}}_e(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{S}}$$

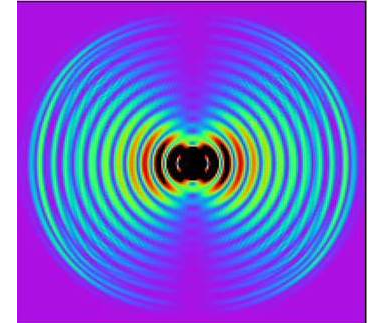
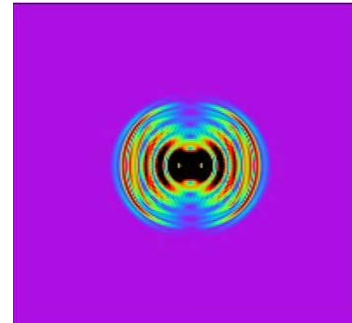
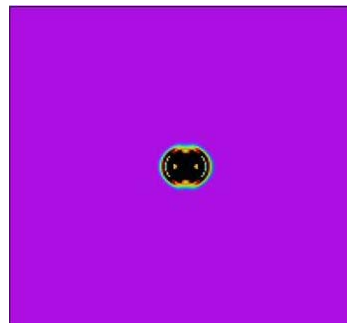
$$\oint_{S=\partial V} \underline{\mathbf{D}}(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{S}} = \iiint_V \rho_e(\underline{\mathbf{R}}, t) dV$$

$$\oint_{S=\partial V} \underline{\mathbf{B}}(\underline{\mathbf{R}}, t) \cdot d\underline{\mathbf{S}} = \iiint_V \rho_m(\underline{\mathbf{R}}, t) dV$$

Wasseroberflächenwellen

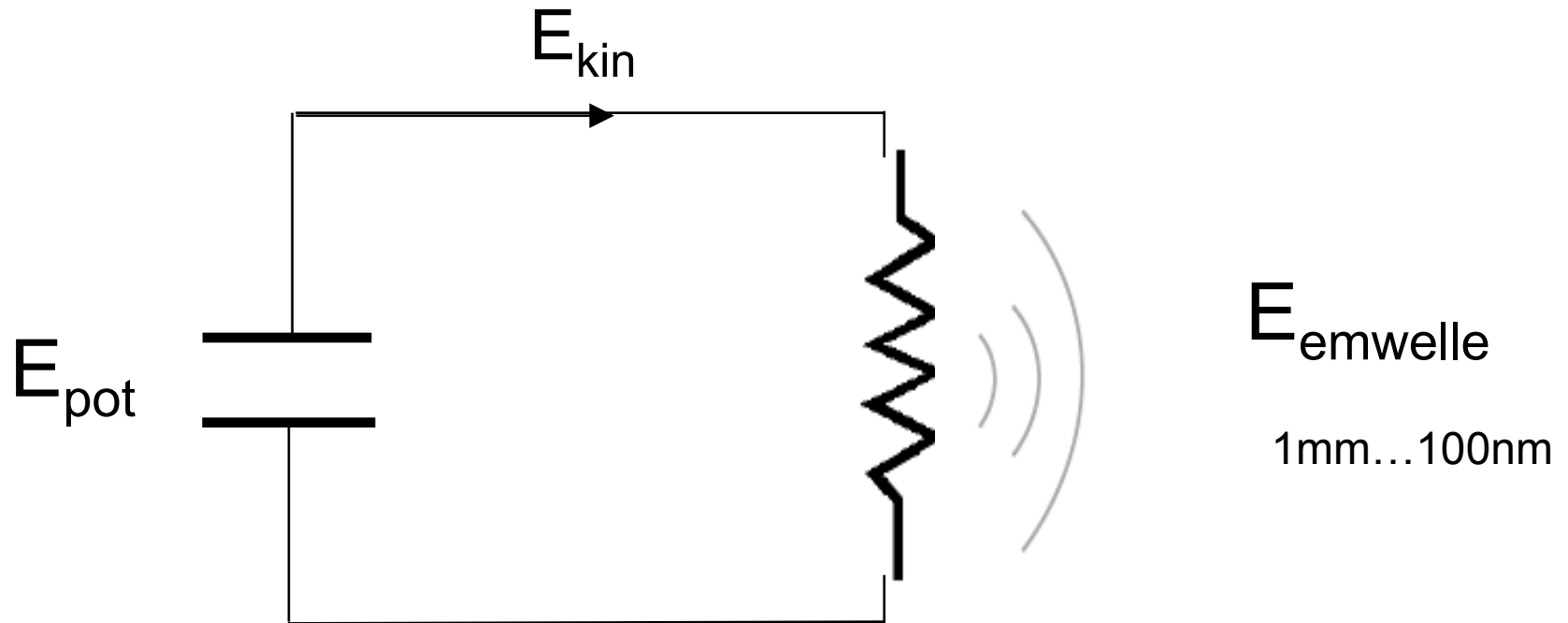


Hertzscher Dipol: EM Wellen

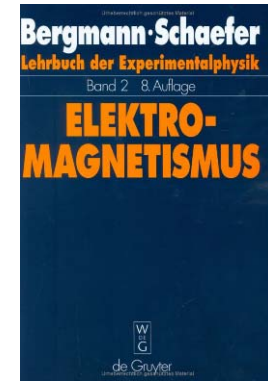
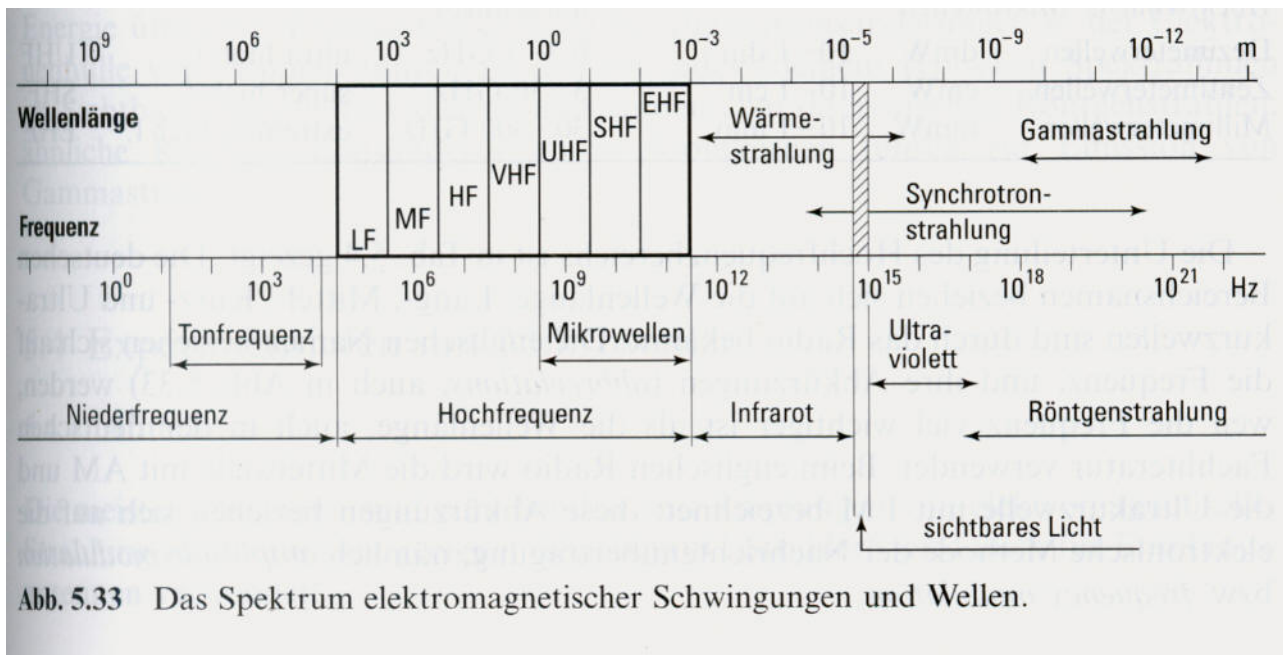


(Quelle: Uni Kassel – Elektromagnetische Feldtheorie I (EFT I) 1st Lecture [4])

Energieumwandlung



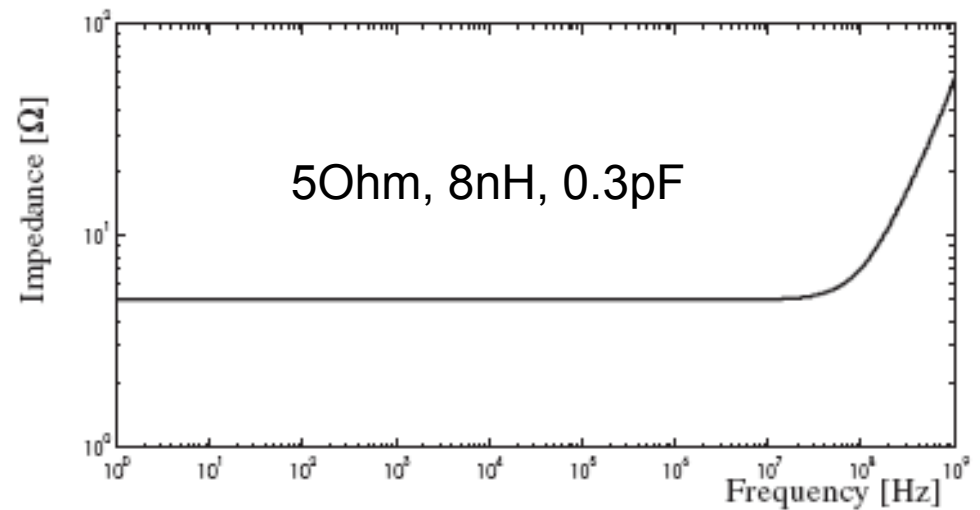
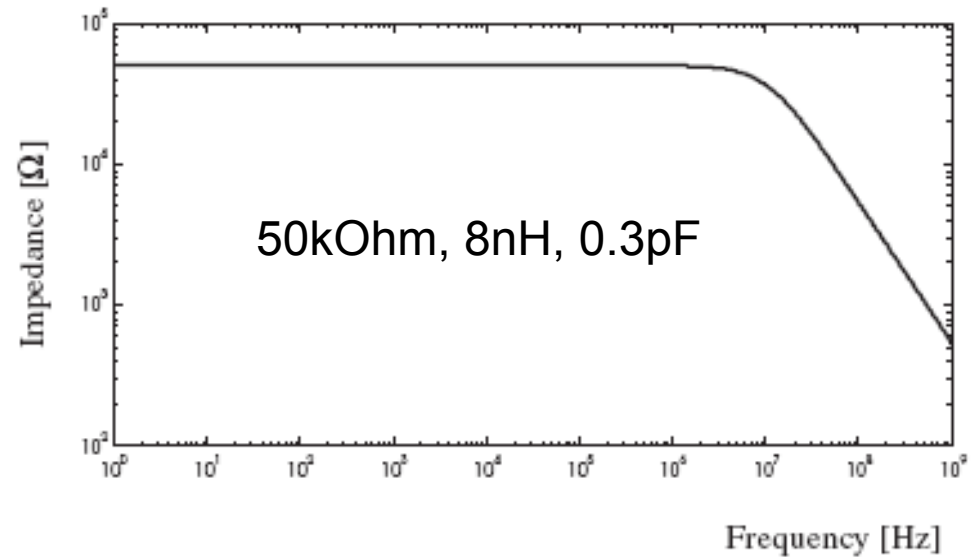
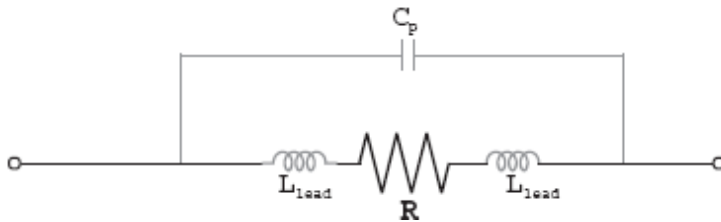
Spektrum



Bergmann-Schaefer, Band 2
Elektromagnetismus
S. 323 [5]

‘Versteckte’ Bauelemente

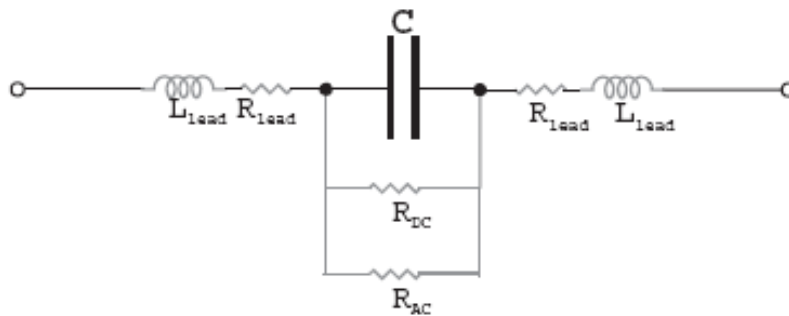
Realer Widerstand



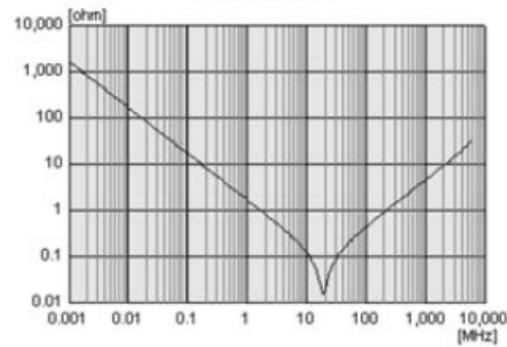
(Quelle: Electromagnetics explained [2])

‘Versteckte’ Bauelemente

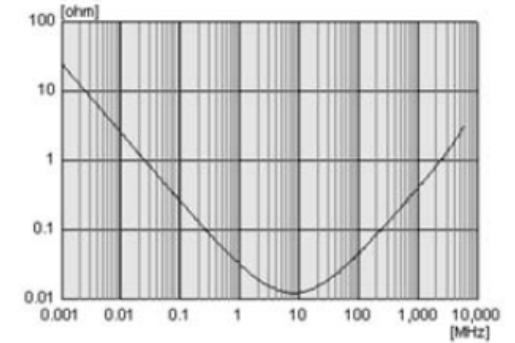
Realer Kondensator



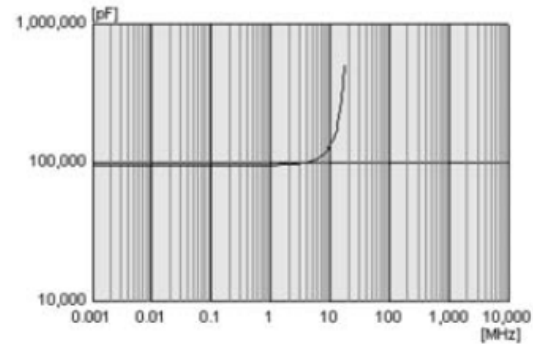
Impedance



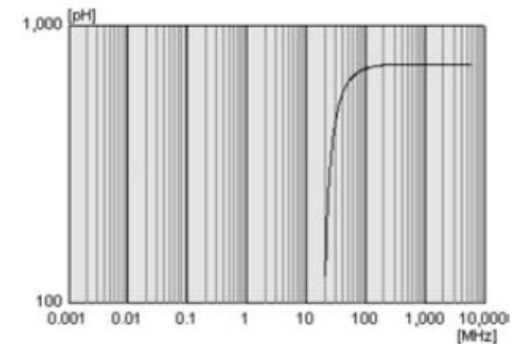
ESR



Apparent Capacitance



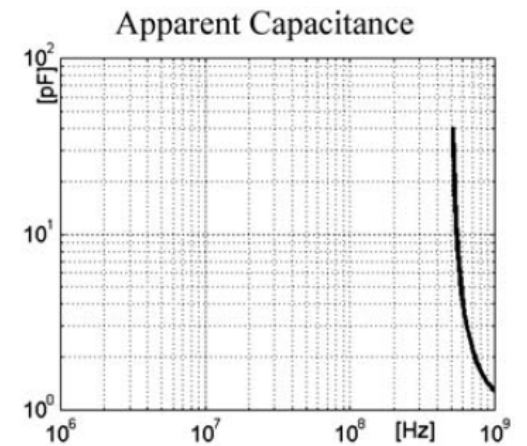
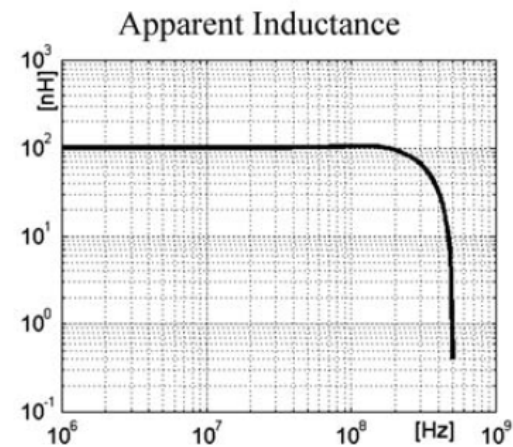
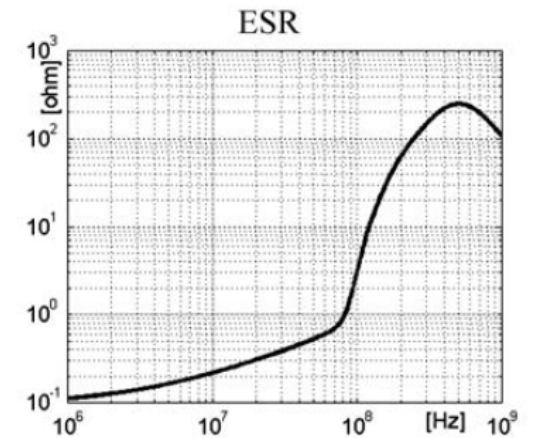
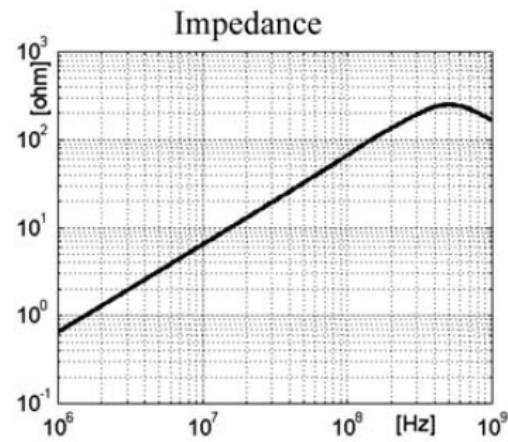
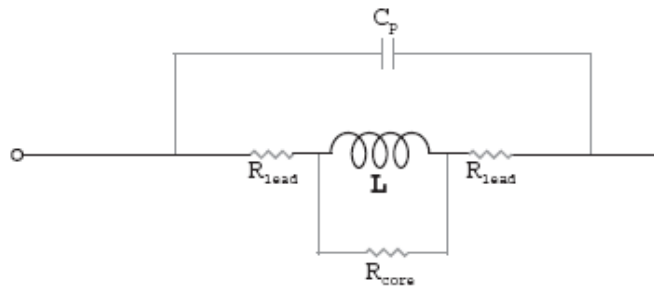
Apparent Inductance



(Quelle: Electromagnetics explained [2])

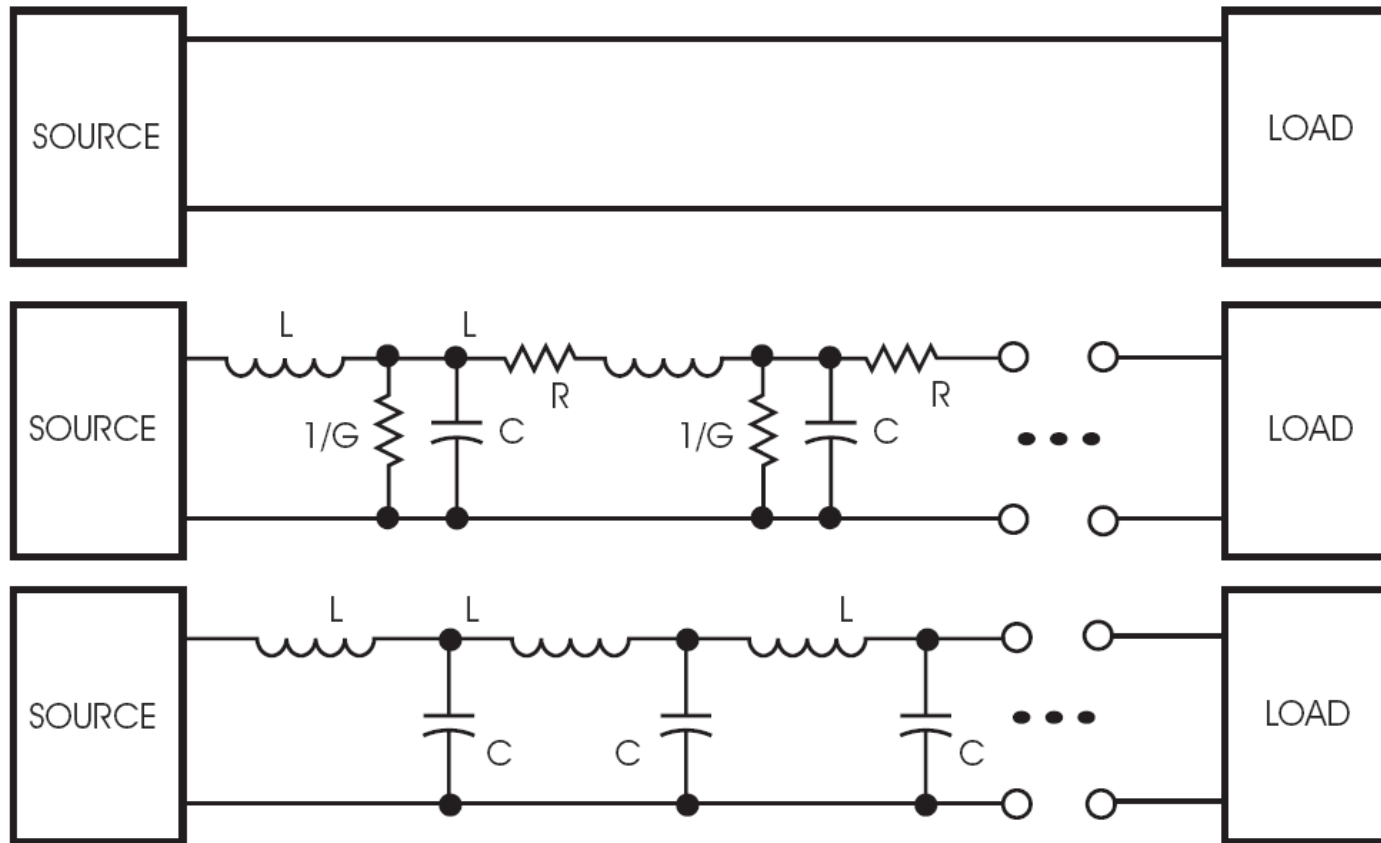
‘Versteckte’ Bauelemente

Reale Spule



(Quelle: Electromagnetics explained [2])

Signalleitung

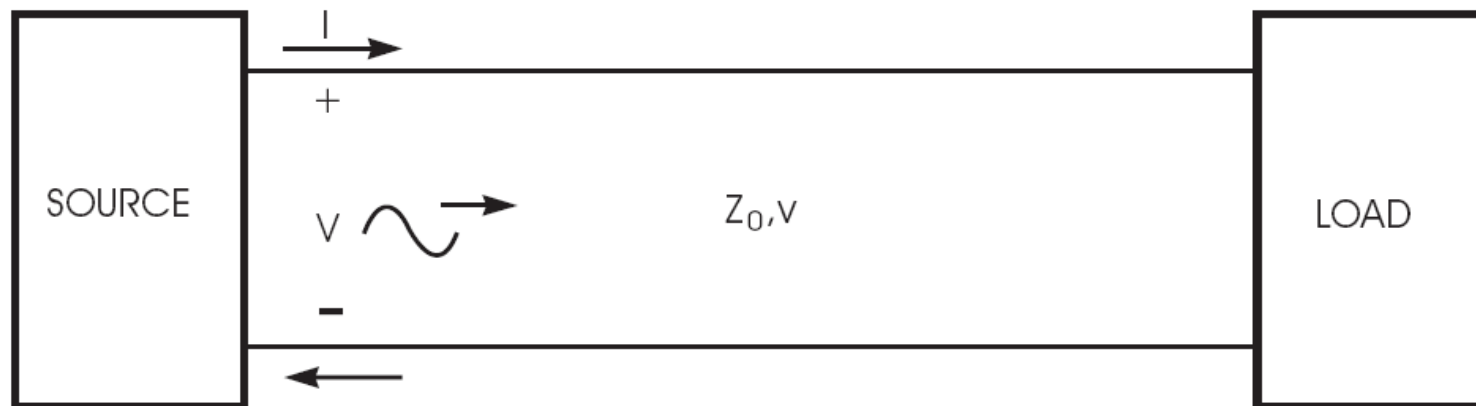


$$Z_o = \sqrt{\frac{R + i\omega L}{G + i\omega C}}$$

$$Z_o = \sqrt{\frac{L}{C}}$$

(Quelle: Electromagnetics explained [2])

Signalleitung



$$Z_o \cong \frac{60}{\sqrt{\epsilon_r}} \ln \left[\frac{D}{d} \right]$$

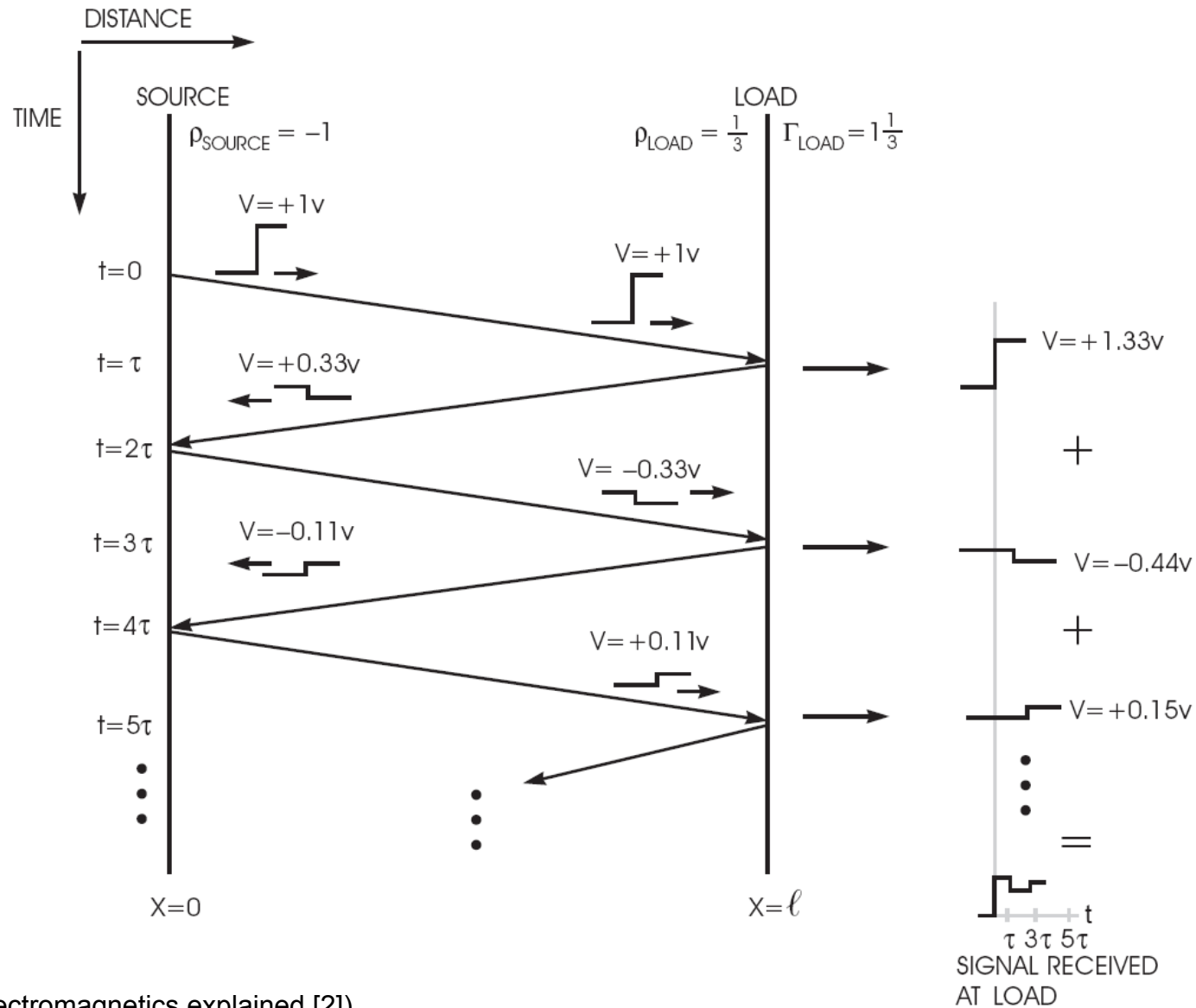
$$v = \sqrt{\frac{1}{\epsilon \mu}}$$

$$Z_o = \sqrt{\frac{L}{C}}$$

$$v = \sqrt{\frac{1}{LC}}$$

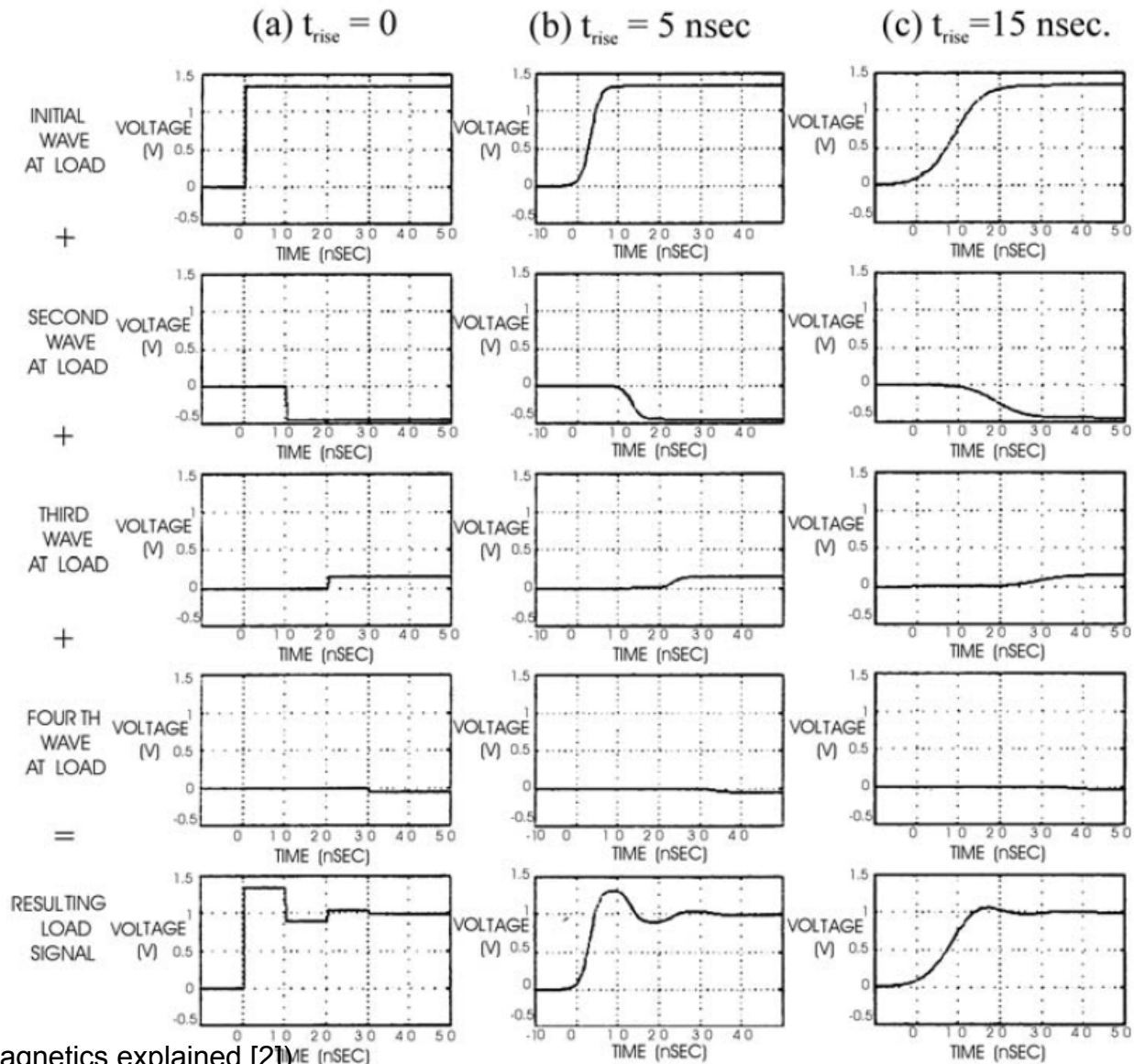
(Quelle: Electromagnetics explained [2])

Reflektion



(Quelle: Electromagnetics explained [2])

Reflektion (2)

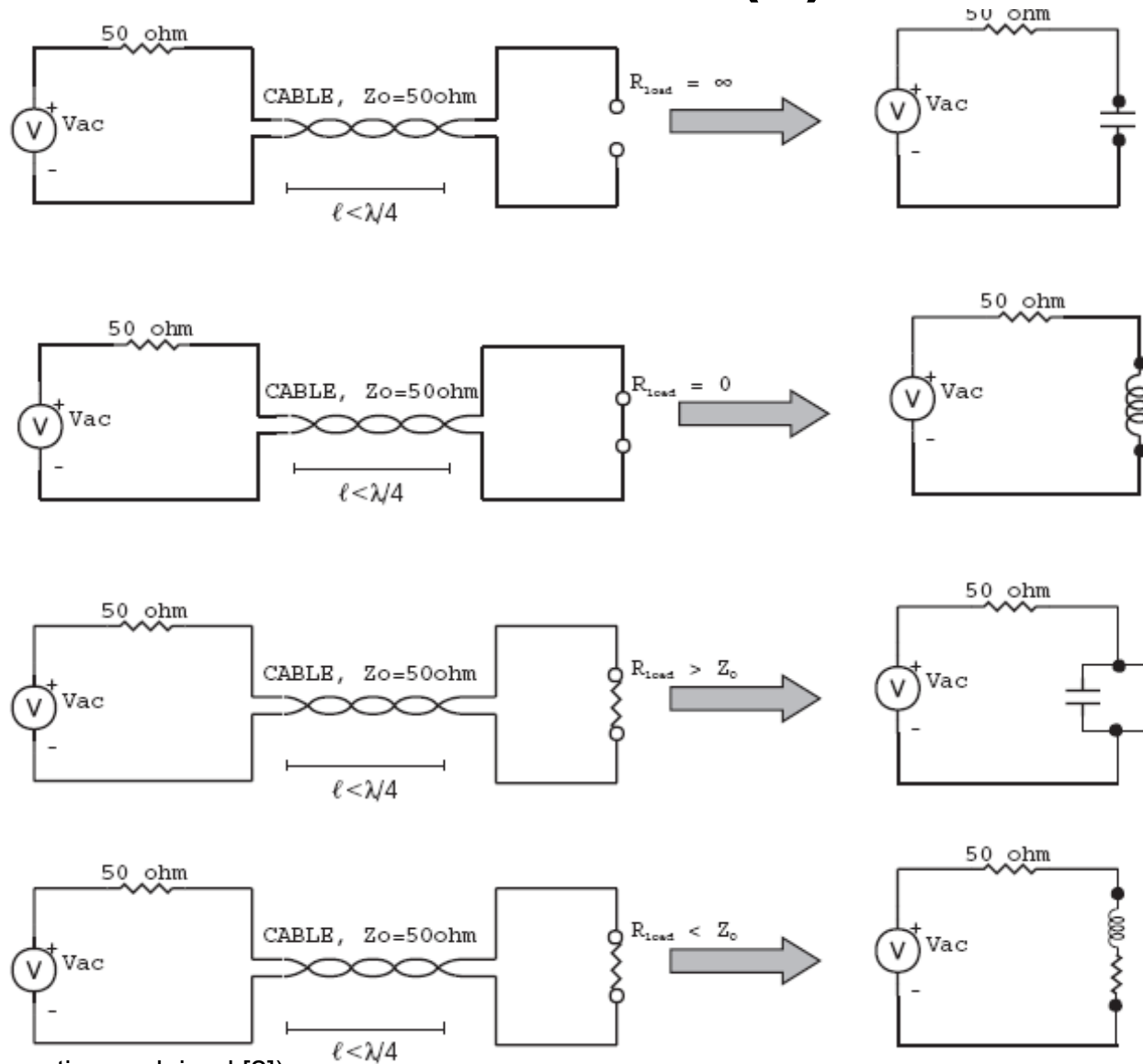


(Quelle: Electromagnetics explained [2])

Praktische Tipps zu EMV

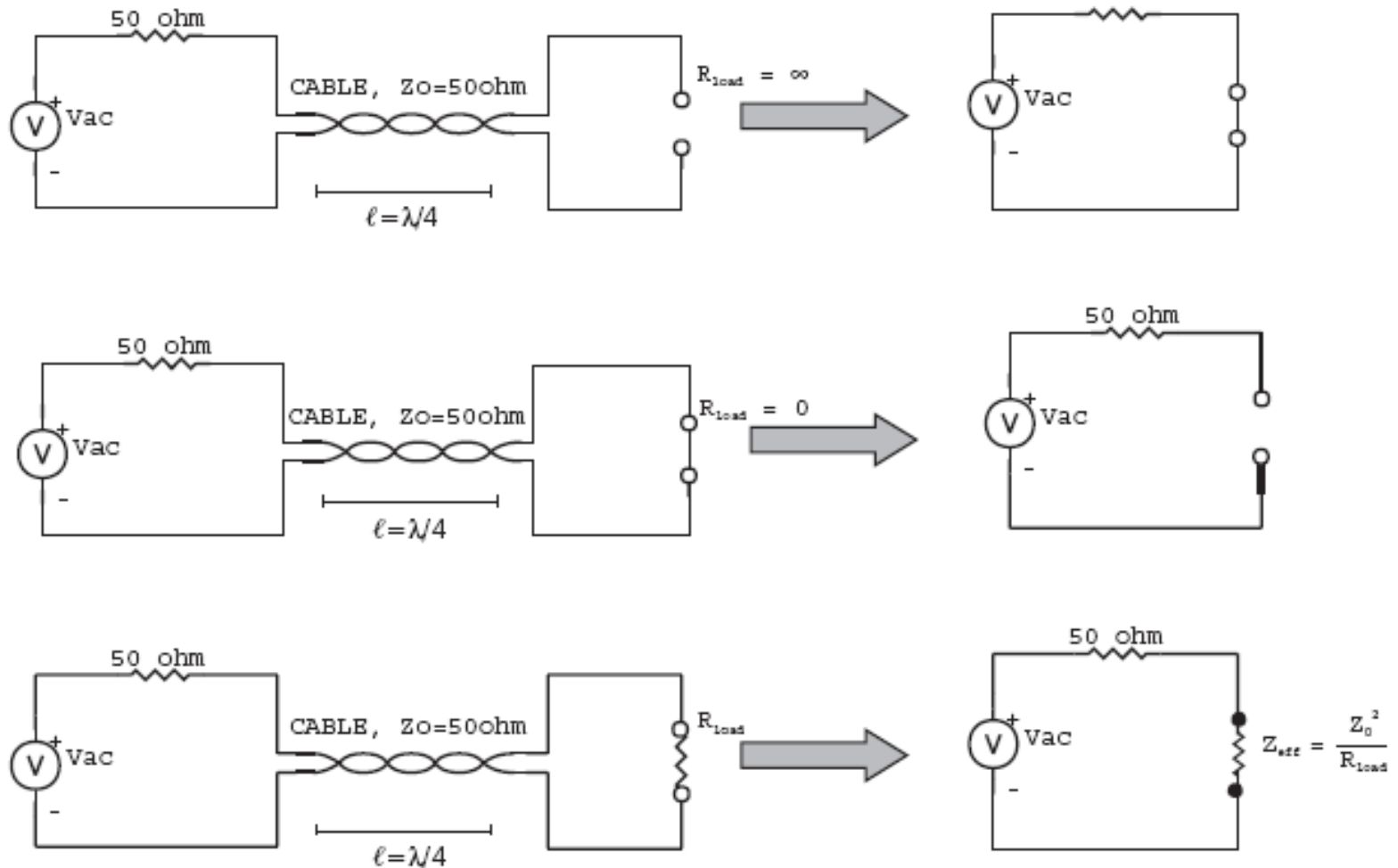
- Antennenbildung
- Taktleitung
- Leiterbahnfuehrung
- Kuehlkoerper

Reflektion (3)



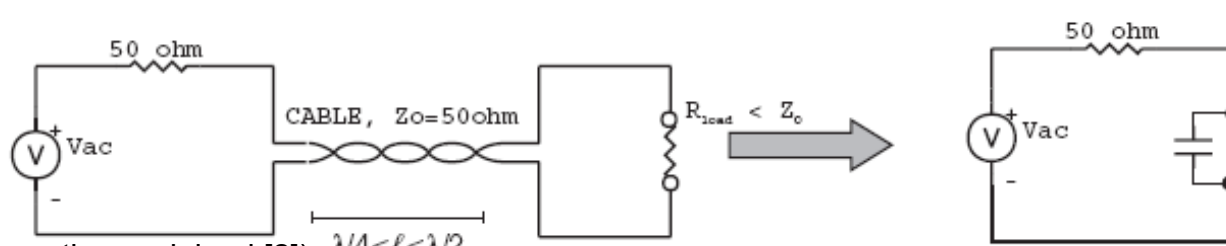
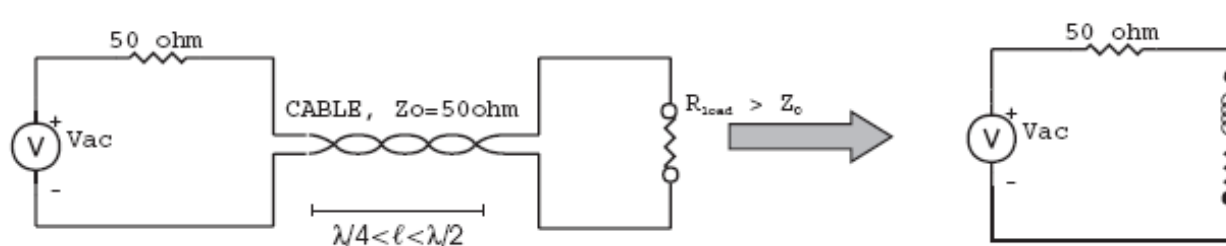
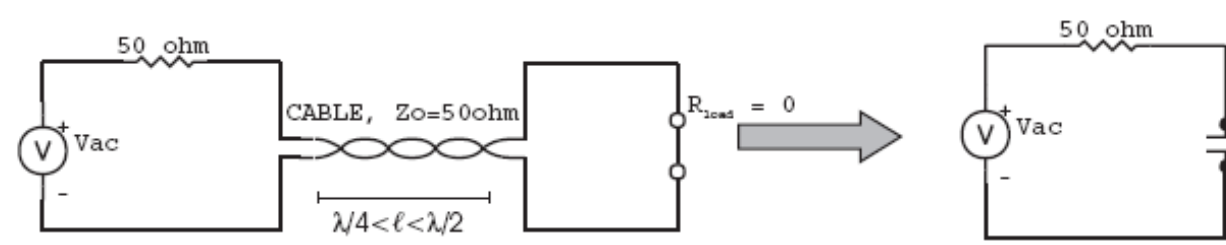
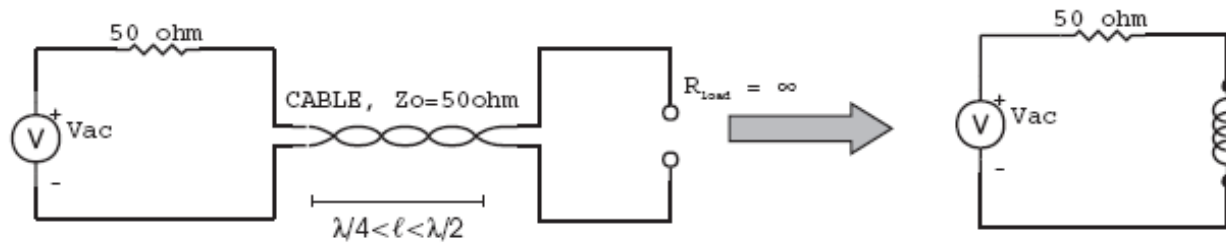
(Quelle: Electromagnetics explained [2])

Reflektion (4)



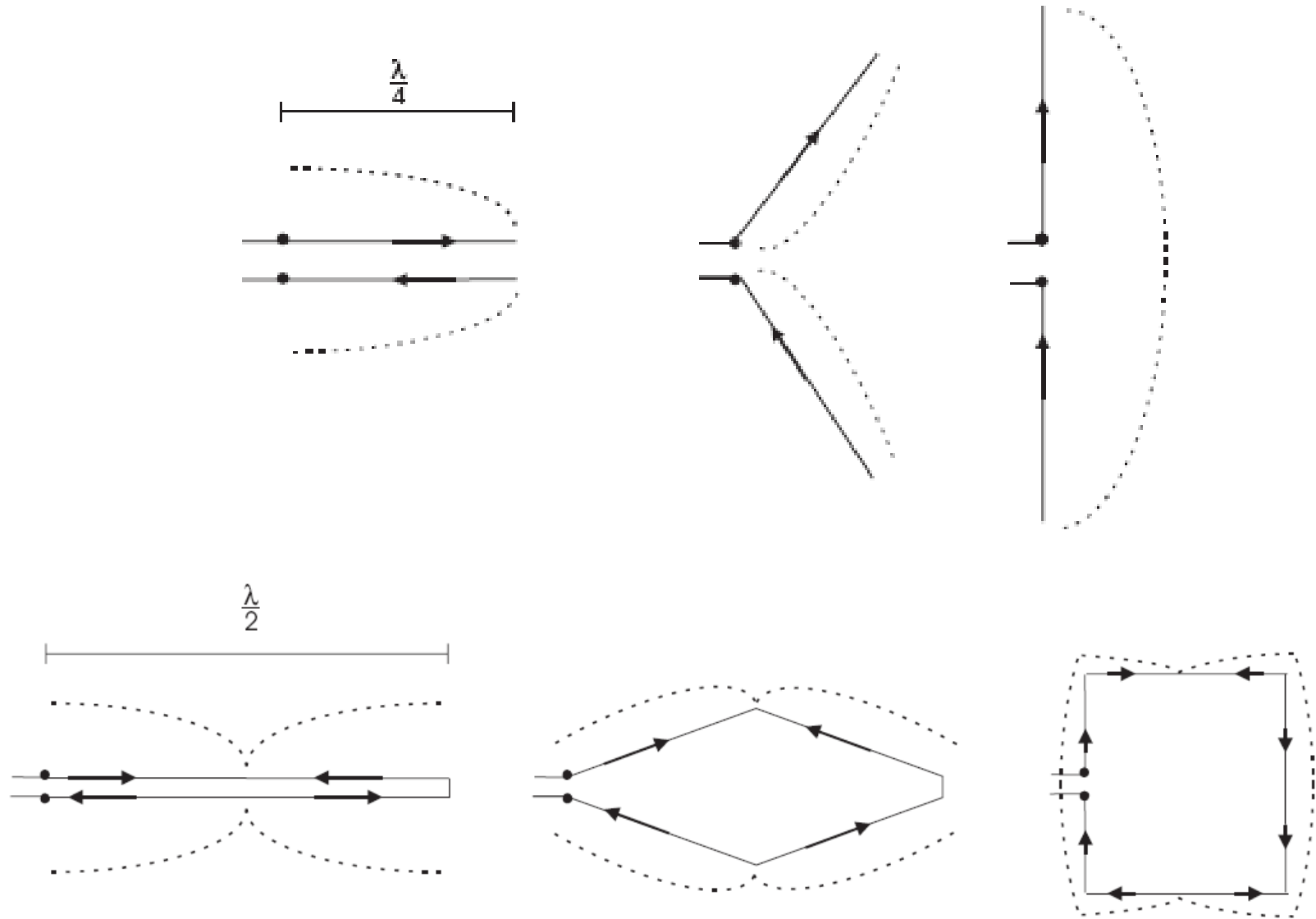
(Quelle: Electromagnetics explained [2])

Reflektion (5)



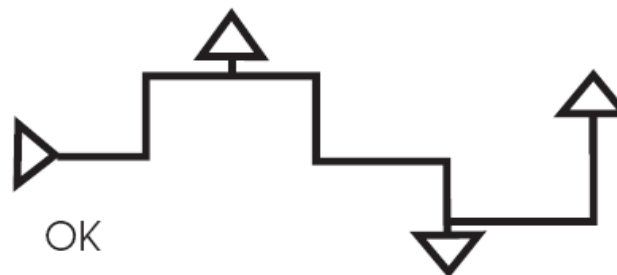
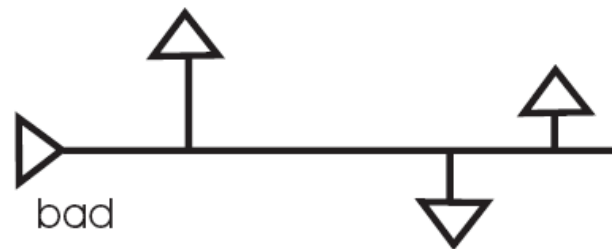
(Quelle: Electromagnetics explained [2])

Antennen



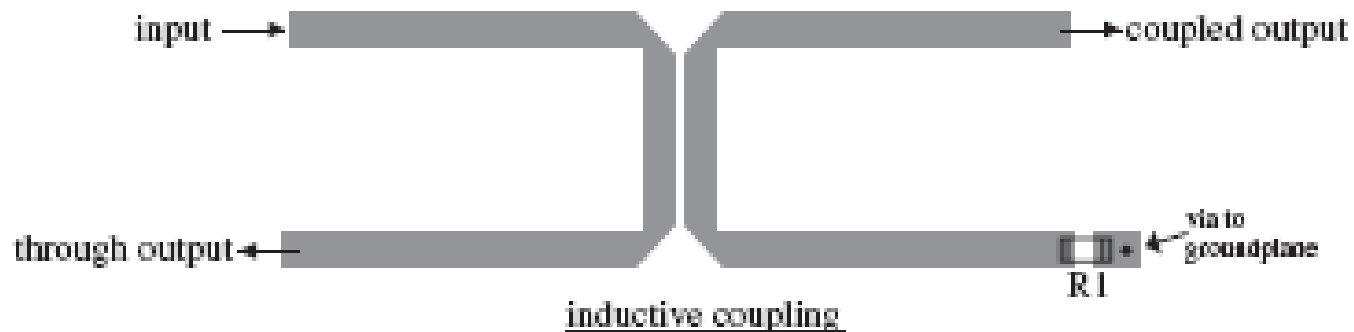
(Quelle: Electromagnetics explained [2])

Taktleitung



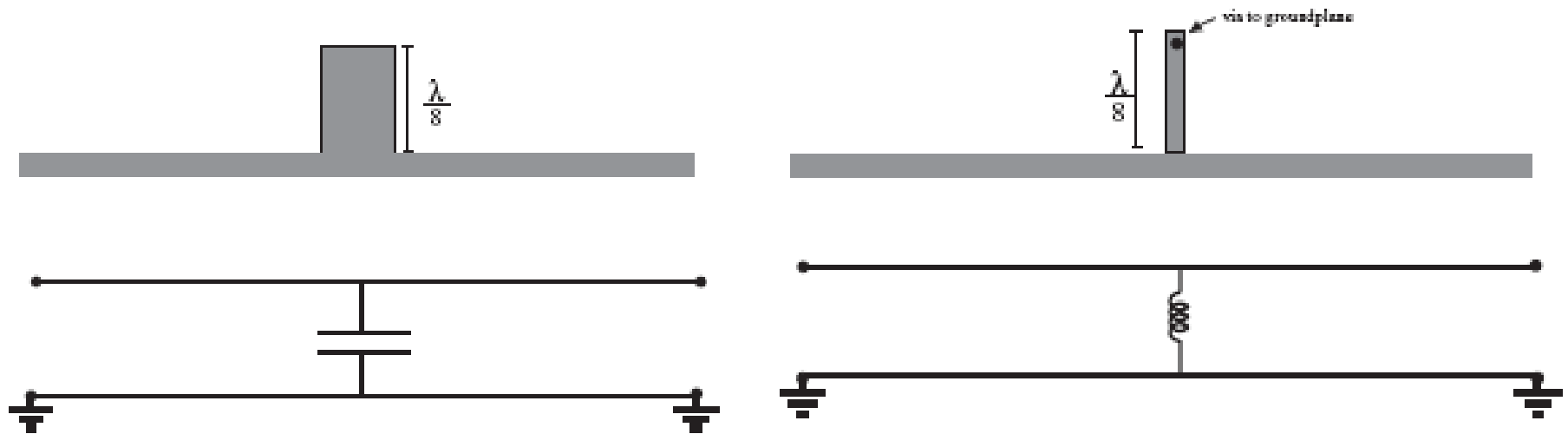
(Quelle: Electromagnetics explained [2])

Microstrip Transmission Lines



(Quelle: Electromagnetics explained [2])

Microstrip Transmission Lines

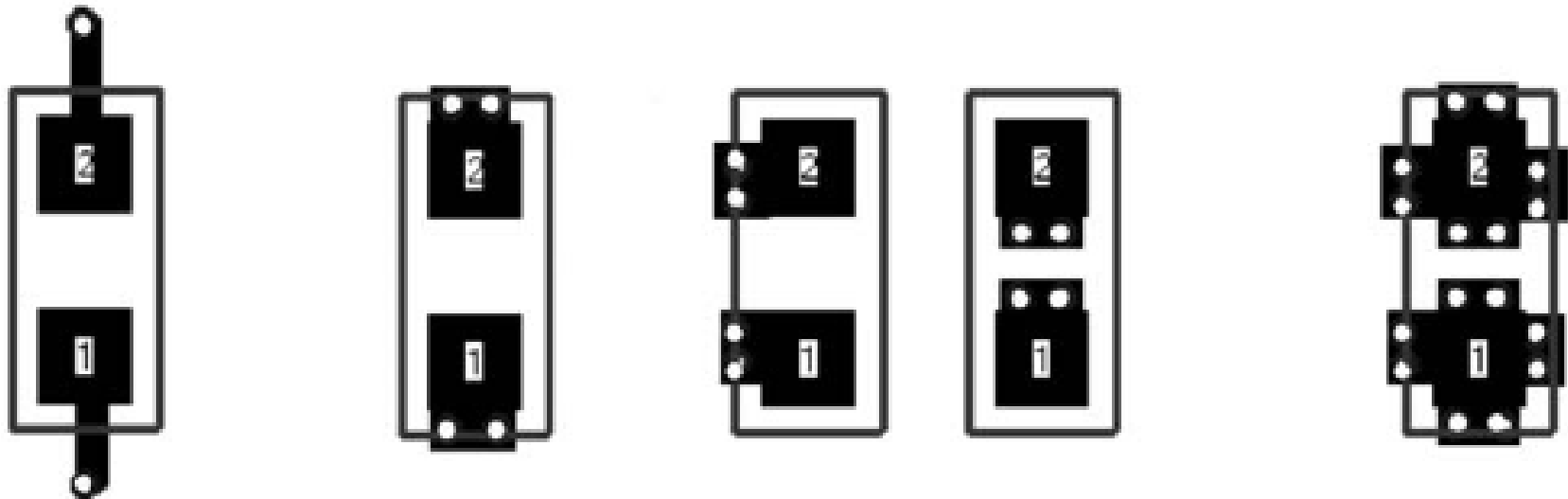


(Quelle: Electromagnetics explained [2])

Leiterbahnfuehrung

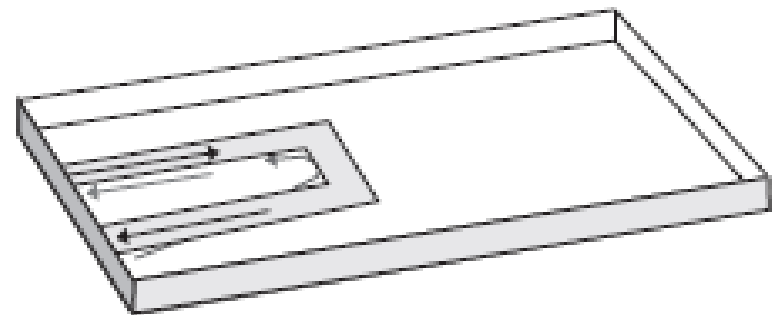
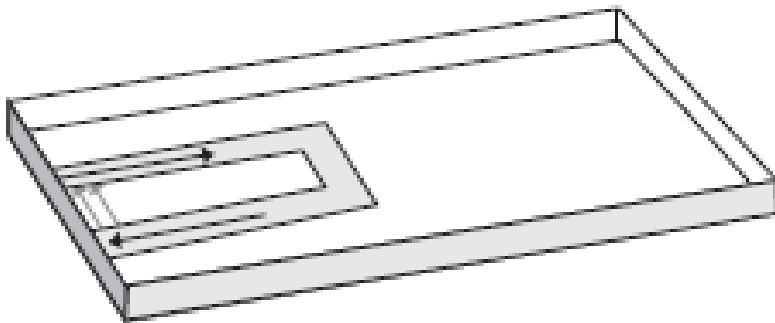
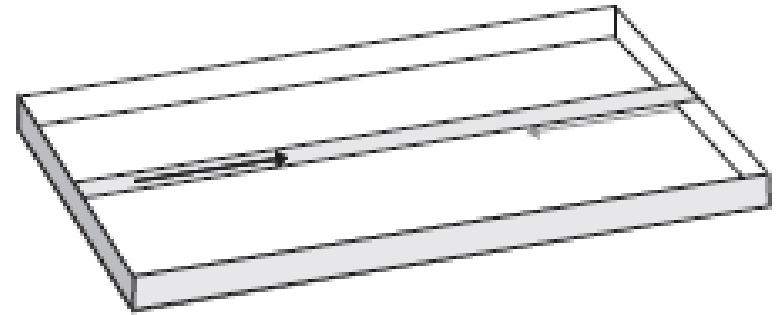
worst

best



(Quelle: Electromagnetics explained [2])

Leiterbahnfuehrung

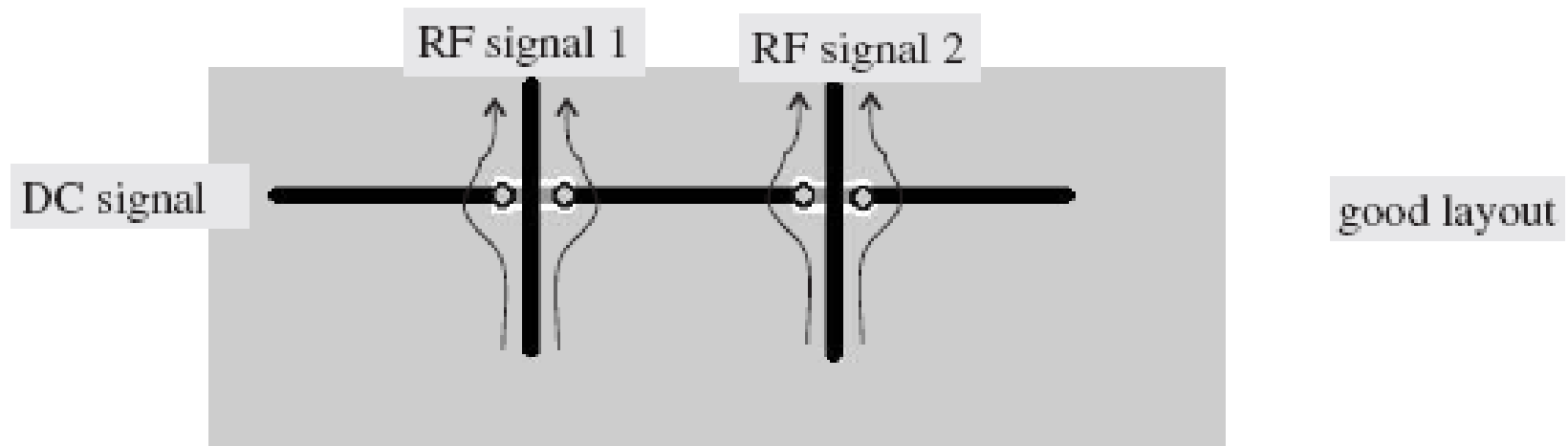
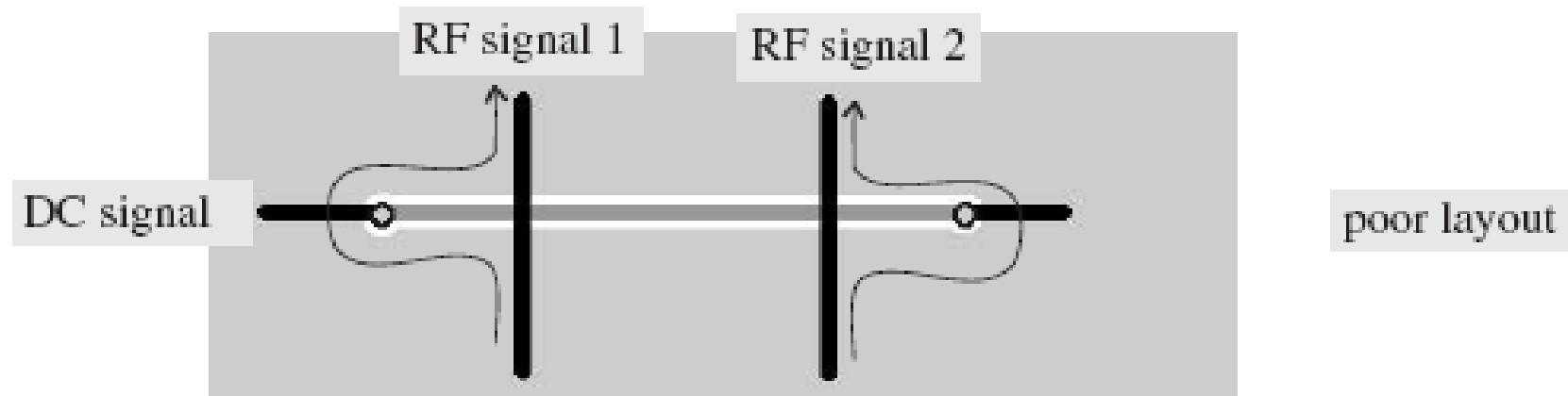


Low-Frequency

High-Frequency

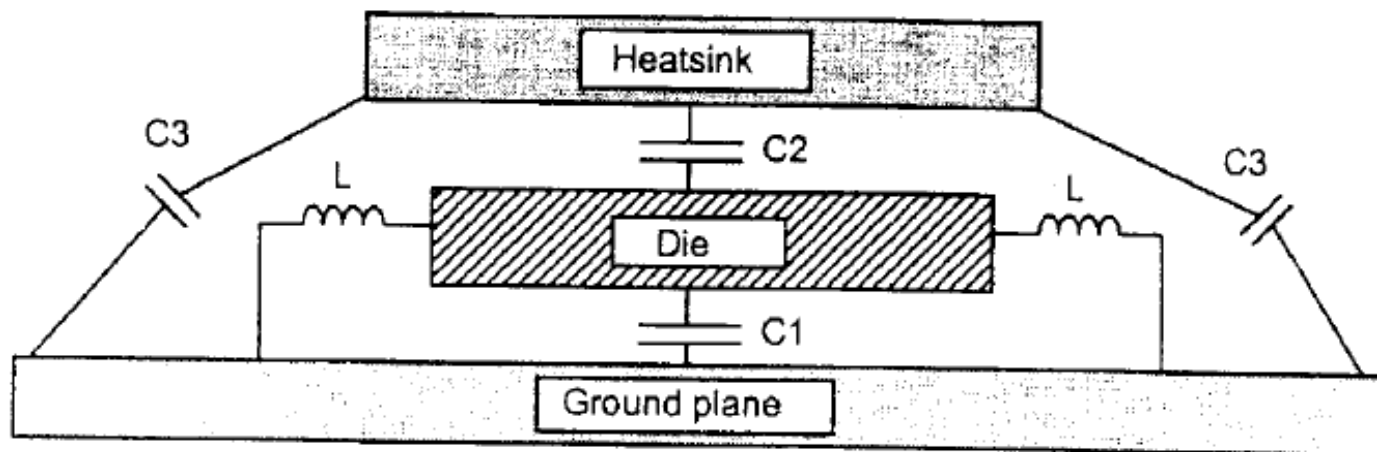
(Quelle: Electromagnetics explained [2])

Leiterbahnfuehrung



(Quelle: Electromagnetics explained [2])

Kuehlkoerper



- L = Package lead inductance
- C1 = Distributed capacitance from the die to the ground plane
- C2 = Distributed capacitance from the heatsink to the die
- C3 = Distributed capacitance from heatsink to ground plane or chassis

(Quelle: EMC and the printed circuit board : design, theory, and layout made simple/ Mark I. Montrose [1])

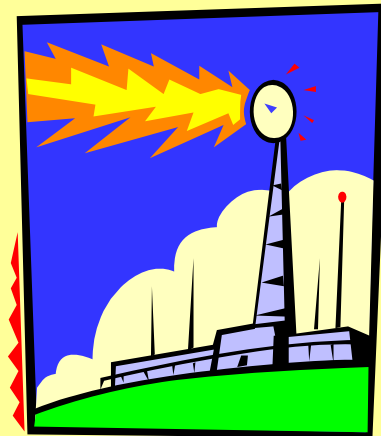
EMI – RFI

EMI – Electromagnetic Interference

RFI – Radio frequency Interference

Why are EMI and RFI a concern?

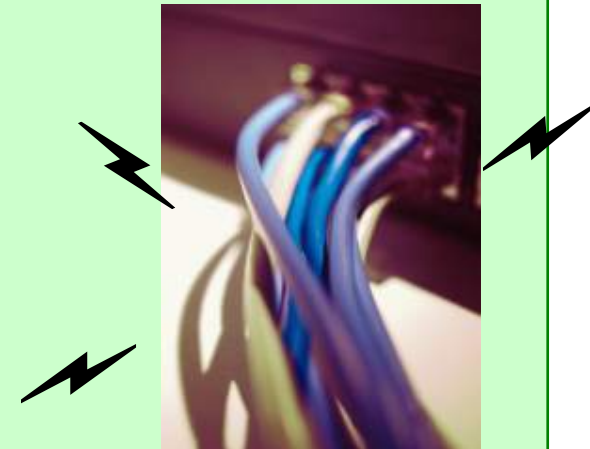
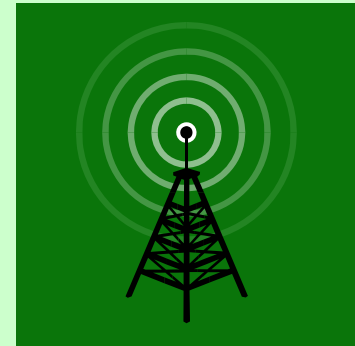
- RF Spectrum pollution
- Compatibility within circuits
- System disturbance or malfunction
- Damage and liability
- Regulation conformance



EMI or RFI?

Both are sources of radio frequency (RF) disturbance

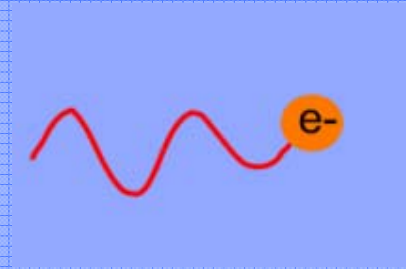
- EMI – electromagnetic interference
 - Often a broadband RF source
- RFI – radio frequency interference
 - Often a narrowband RF source
- Terms are often used interchangeably



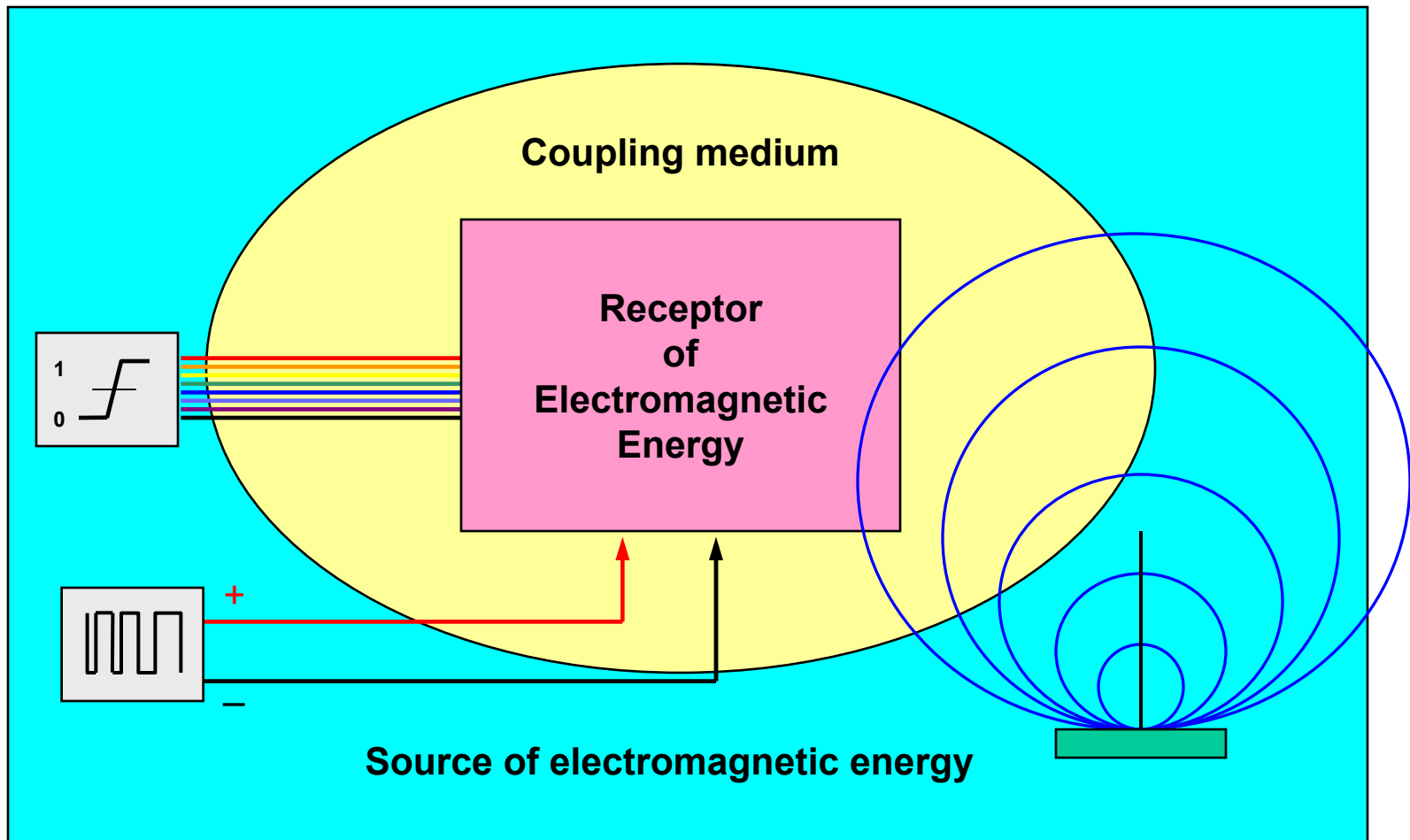
Fields – EMI can propagate by one or more types

- Electric Field (E) – Force created by uneven charge distribution
- Magnetic Induction Field (H) – Force created by moving charges
- Electromagnetic Field – Created whenever charges are accelerated

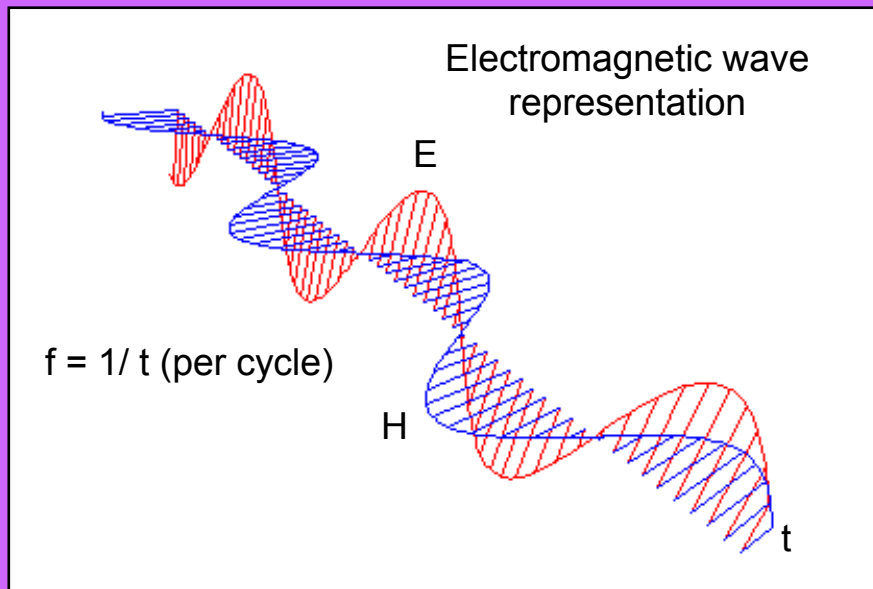
Source http://www.w8ji.com/radiation_and_fields.htm



The necessary elements for EMI



Source of Electromagnetic Energy



RF generating sources

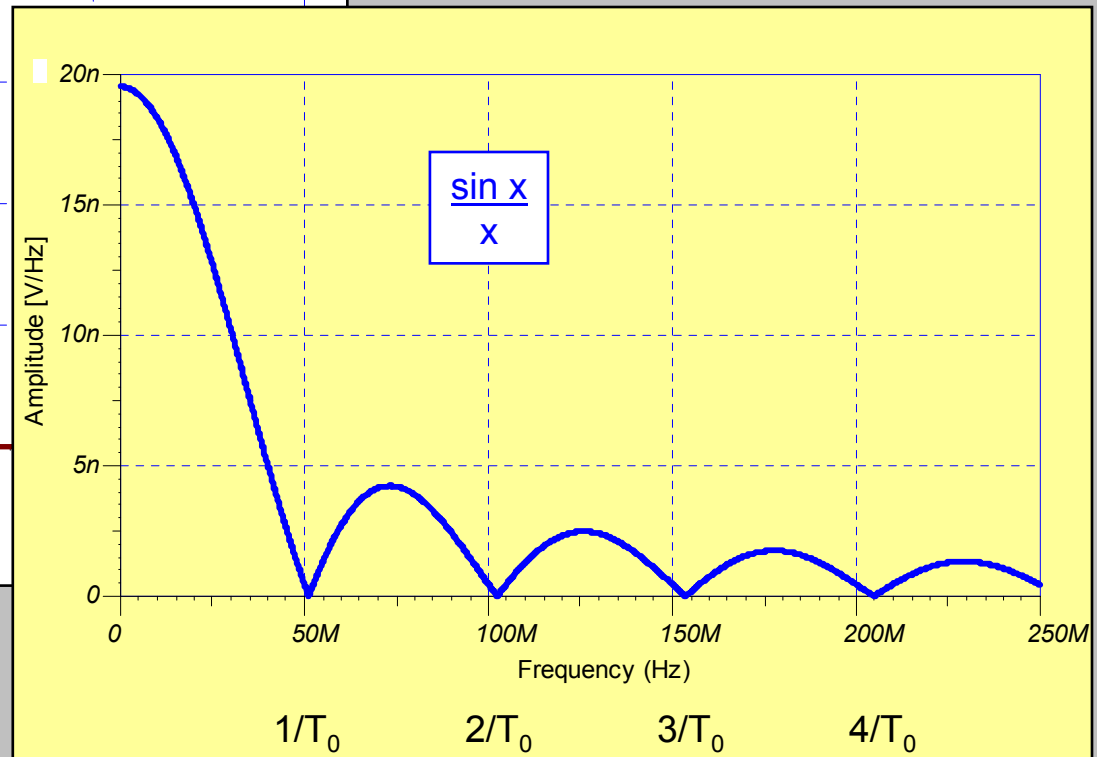
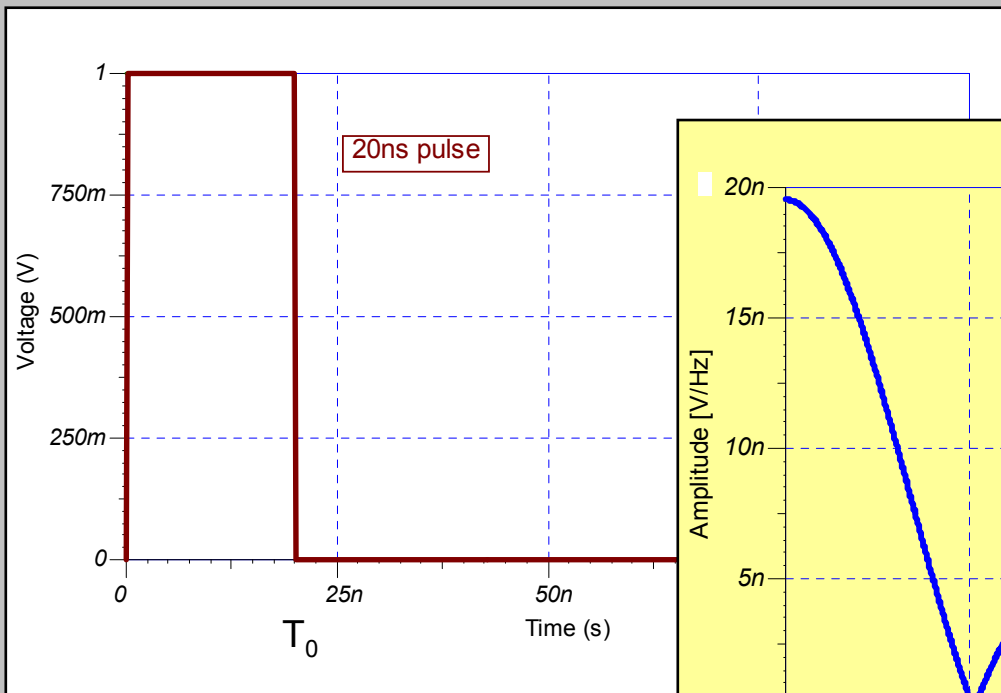
Intentional radiators

- cell phones
- transmitters & transceivers
- wireless routers, peripherals

Unintentional radiators

- System clocks & oscillators
- Processors & logic circuits
- Switching power supplies
- Switching amplifiers (class D)
- Electromechanical devices
- Electrical power line services

How radio frequency energy comes about in circuitry



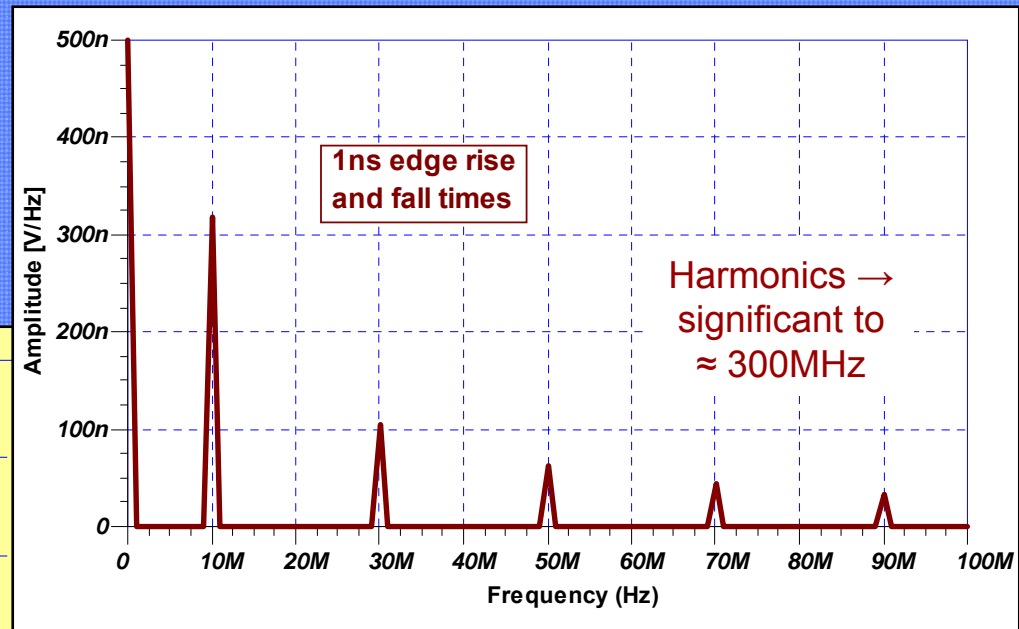
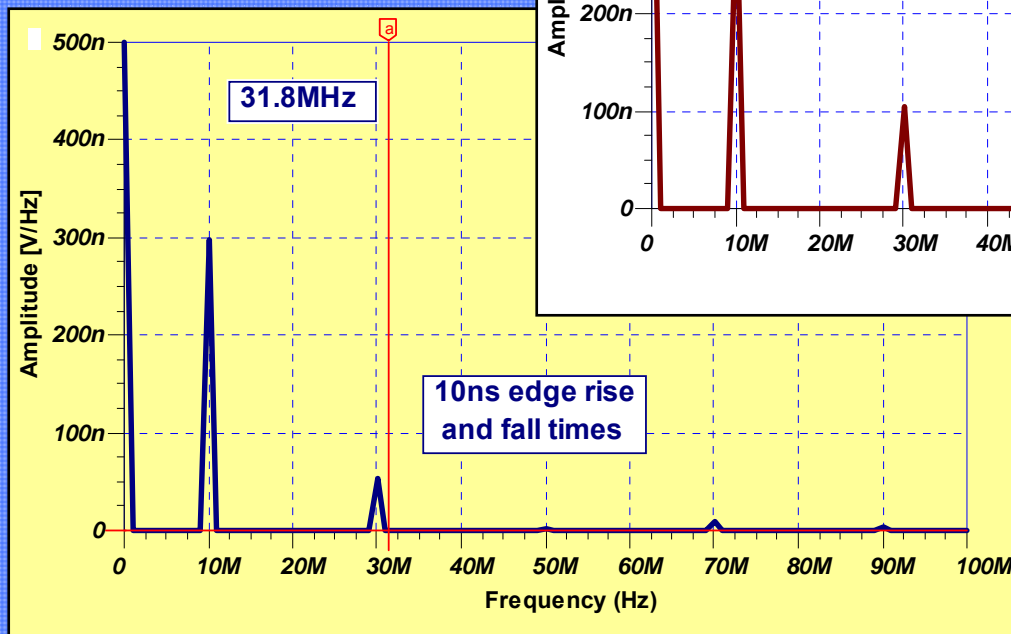
$$|X(f)| = \sqrt{\text{Re}(f)^2 + \text{Im}(f)^2}$$

Complex frequency domain in
Polar form

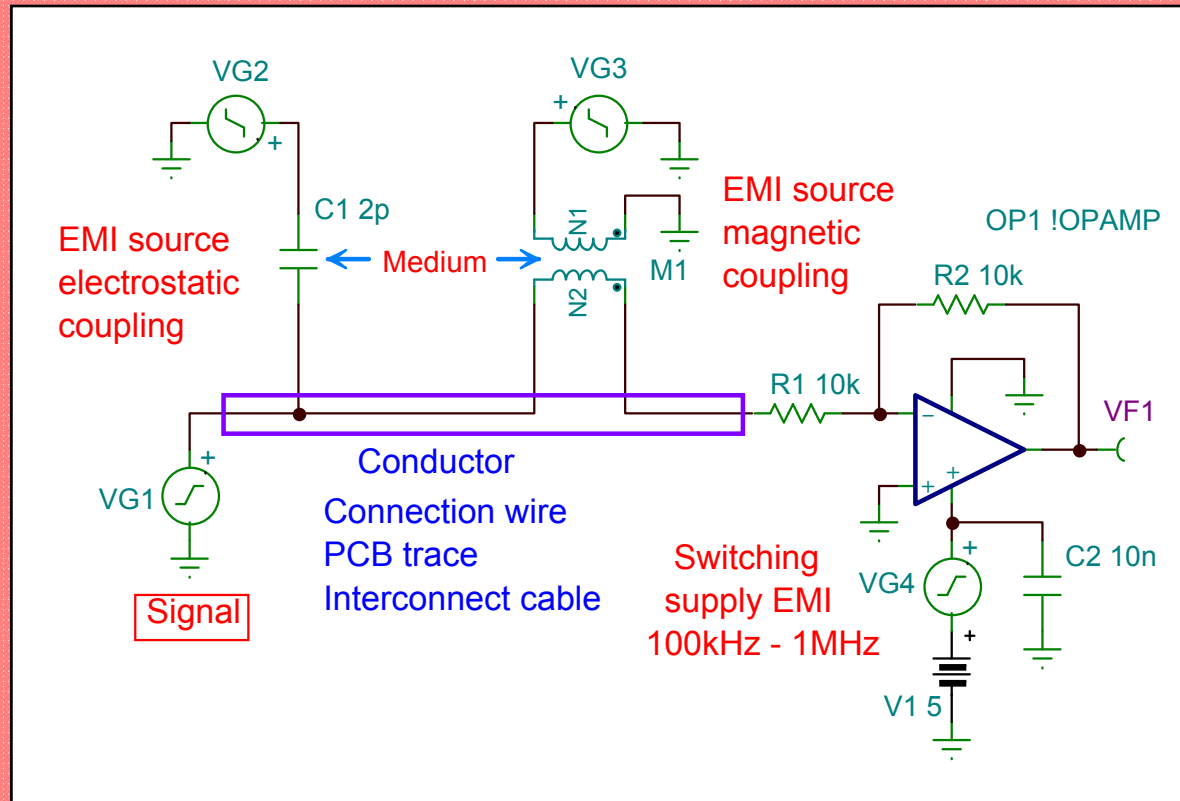
It's all about edge rates

A rule of thumb for digital signals and transients

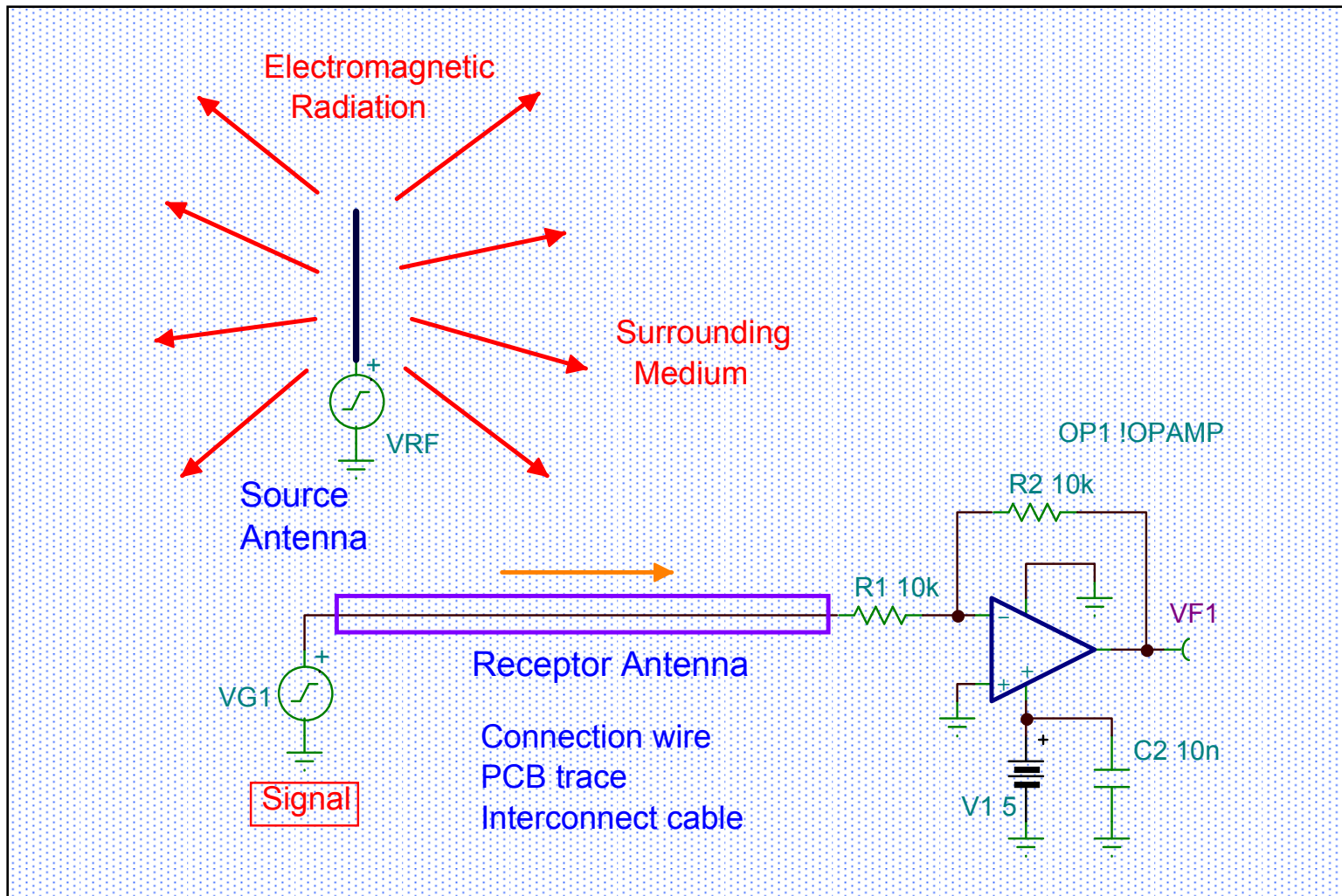
$$f_{\max} = (\pi * t_{\text{rise}})^{-1}$$



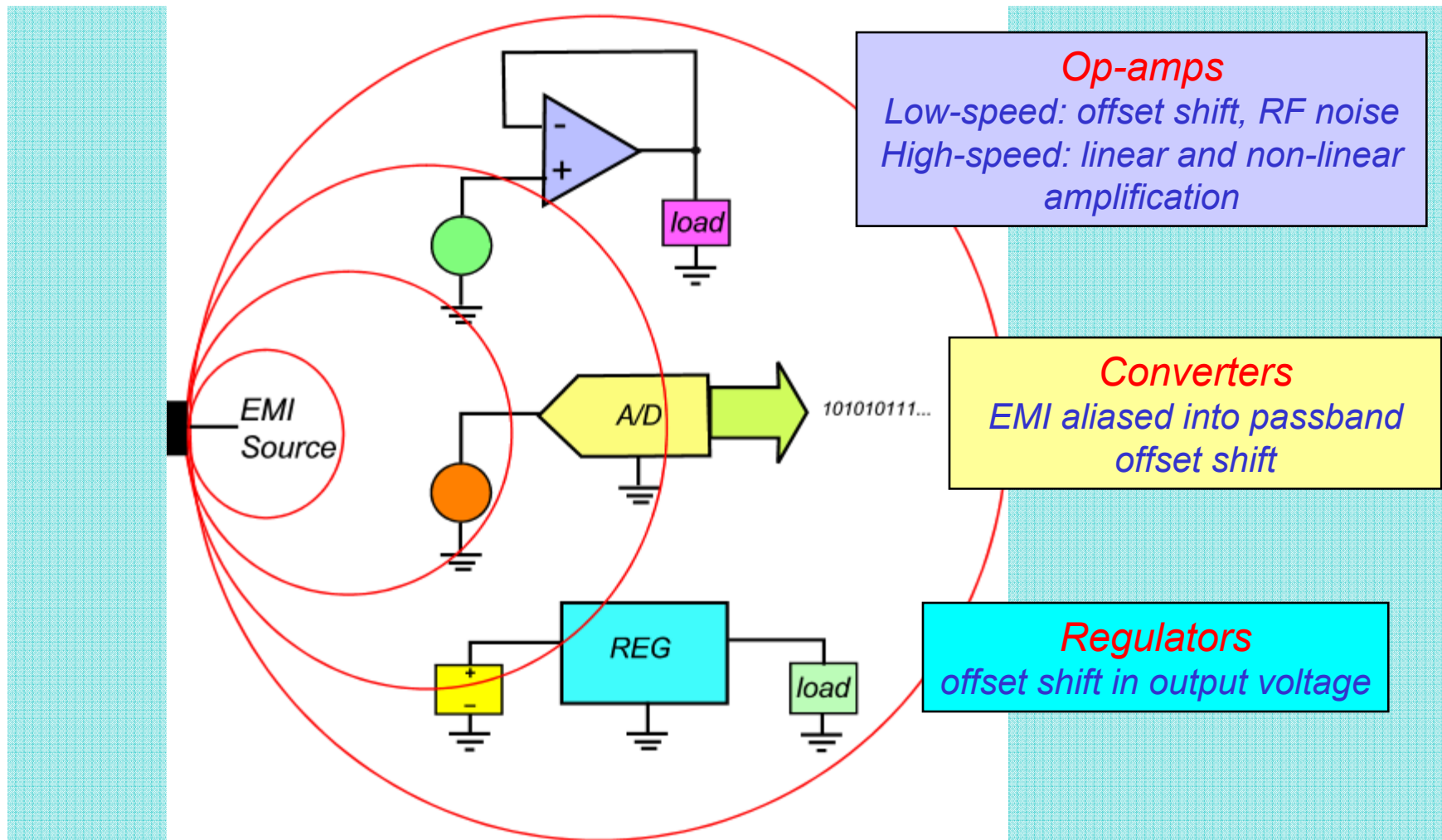
Coupling Medium: Conducted Emissions



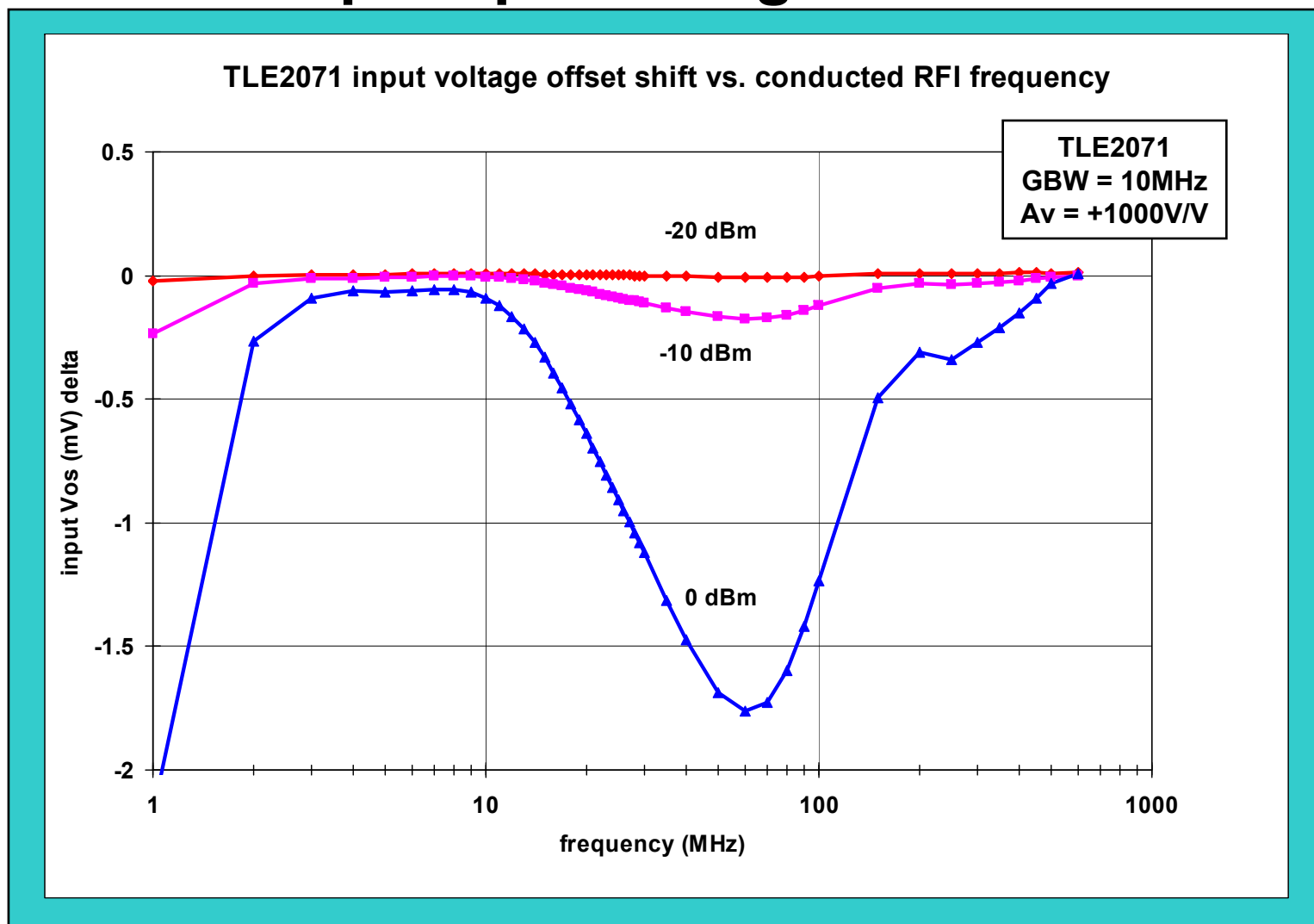
Coupling Medium: Radiated Emissions



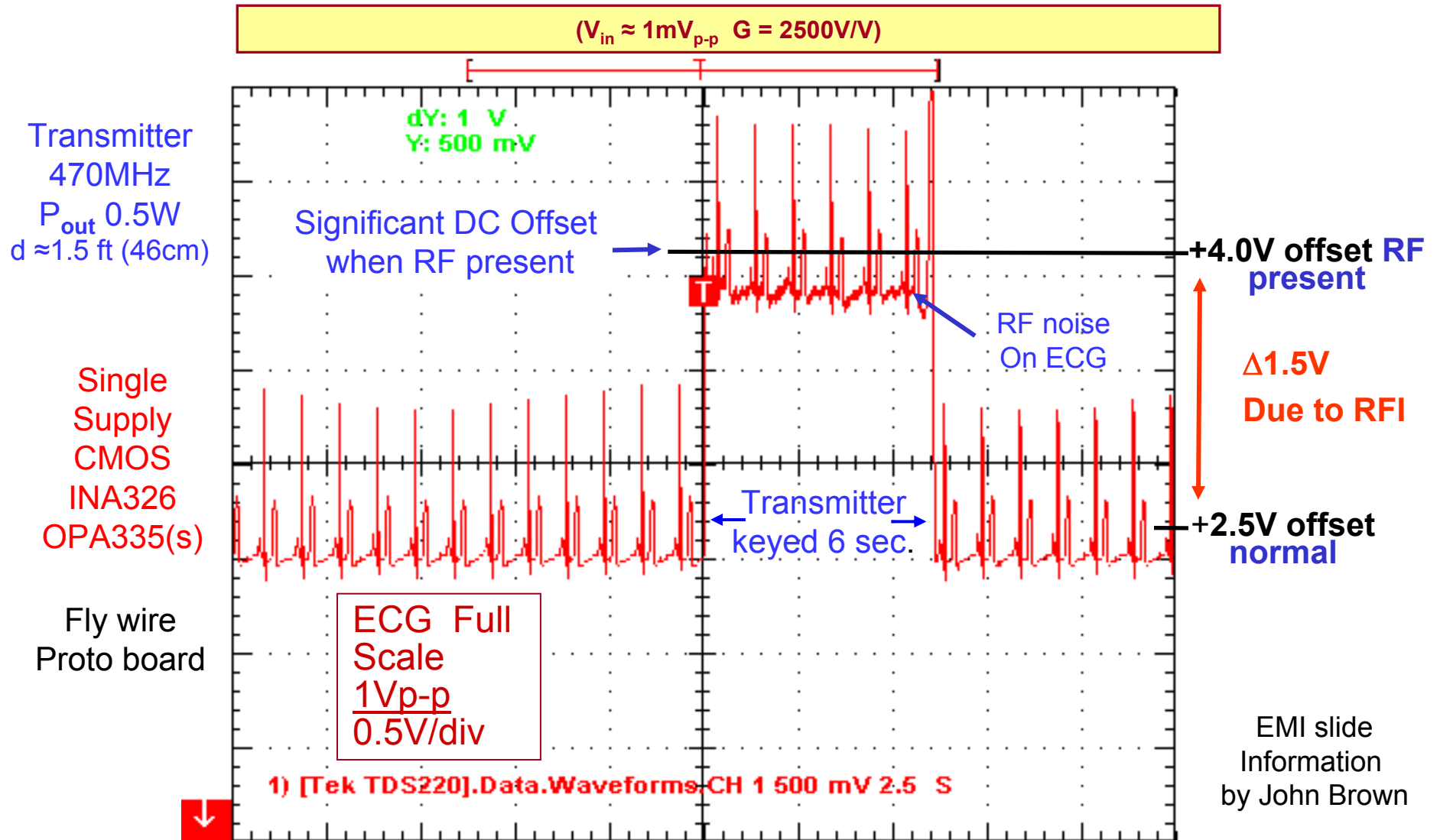
Analog receptors: electromagnetic energy



Conducted EMI and its effect on an op-amp's voltage offset



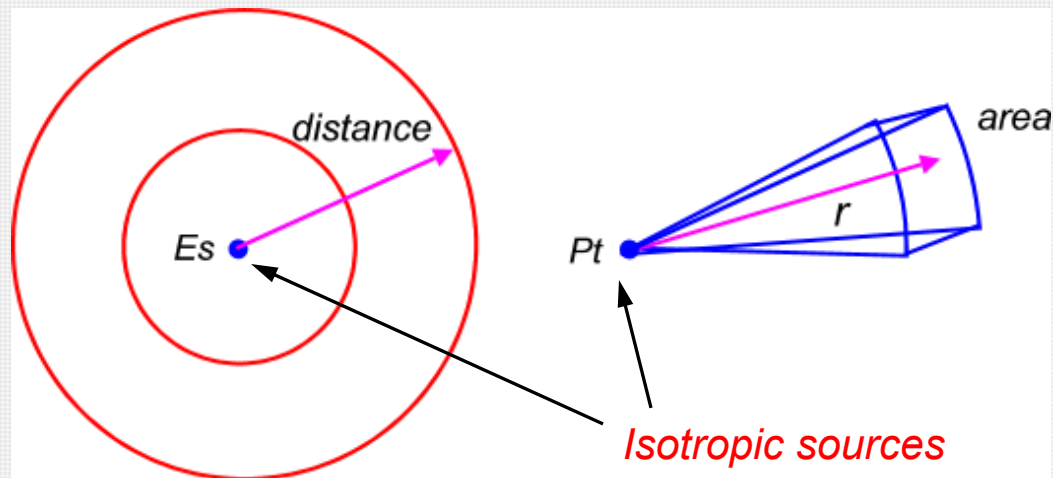
Radiated RFI and its effect on an ECG simulator



Electric-Field Strength, Power Density

EMI - electric-field strength units

Communications - power density units



$$E \text{ (V/m)} = 61.4 [P(\text{mW}) / \text{cm}^2]^{1/2}$$

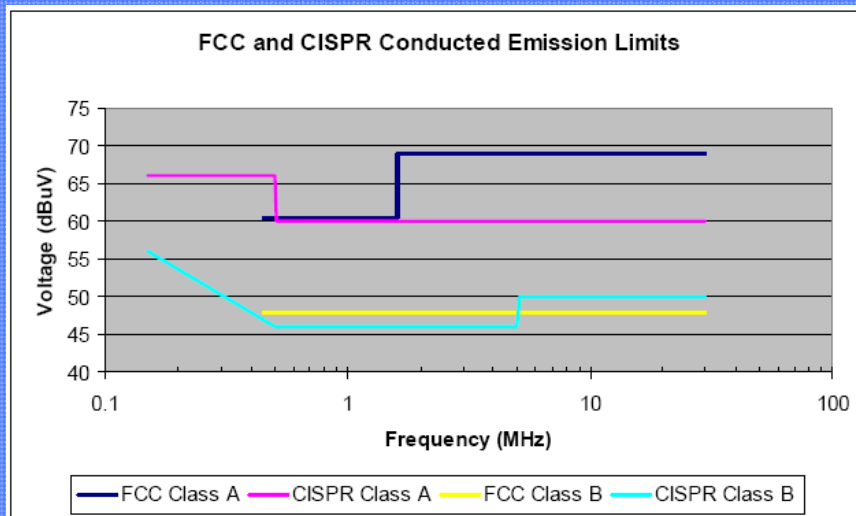
For free space $Z = 377\Omega$

$$P_d = P_t / 4\pi \cdot r^2 \quad (\text{W/m}^2 \text{ or mW/cm}^2)$$

100V/m = 2.65mW/cm ²	10mW/cm ² = 194V/m
10V/m = 26uW/cm ²	1mW/cm ² = 61V/m
1V/m = 0.26uW/cm ²	0.1mW/cm ² = 1.9V/m

Emission Source Limits

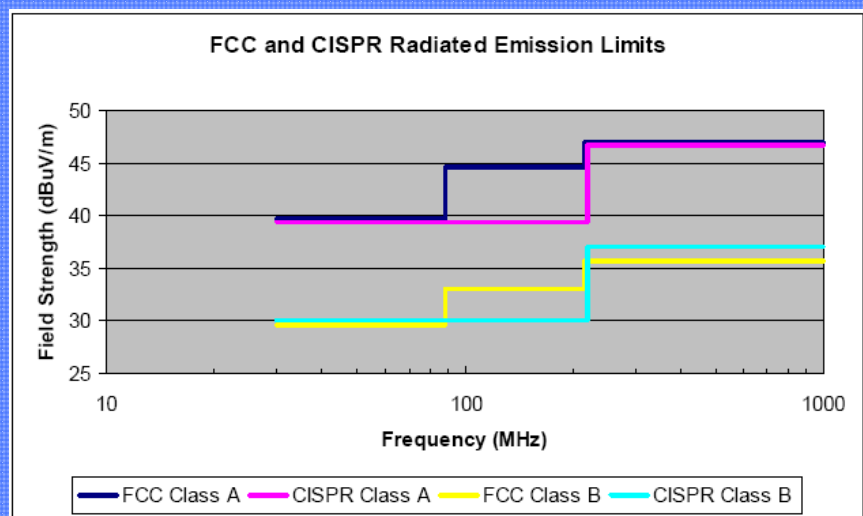
Conducted Emissions - 10kHz to 30MHz



Freq (MHz)	Class A dBuV	Class B dBuV
0.45 - 1.6	60	48
1.6 - 30	69.5	48

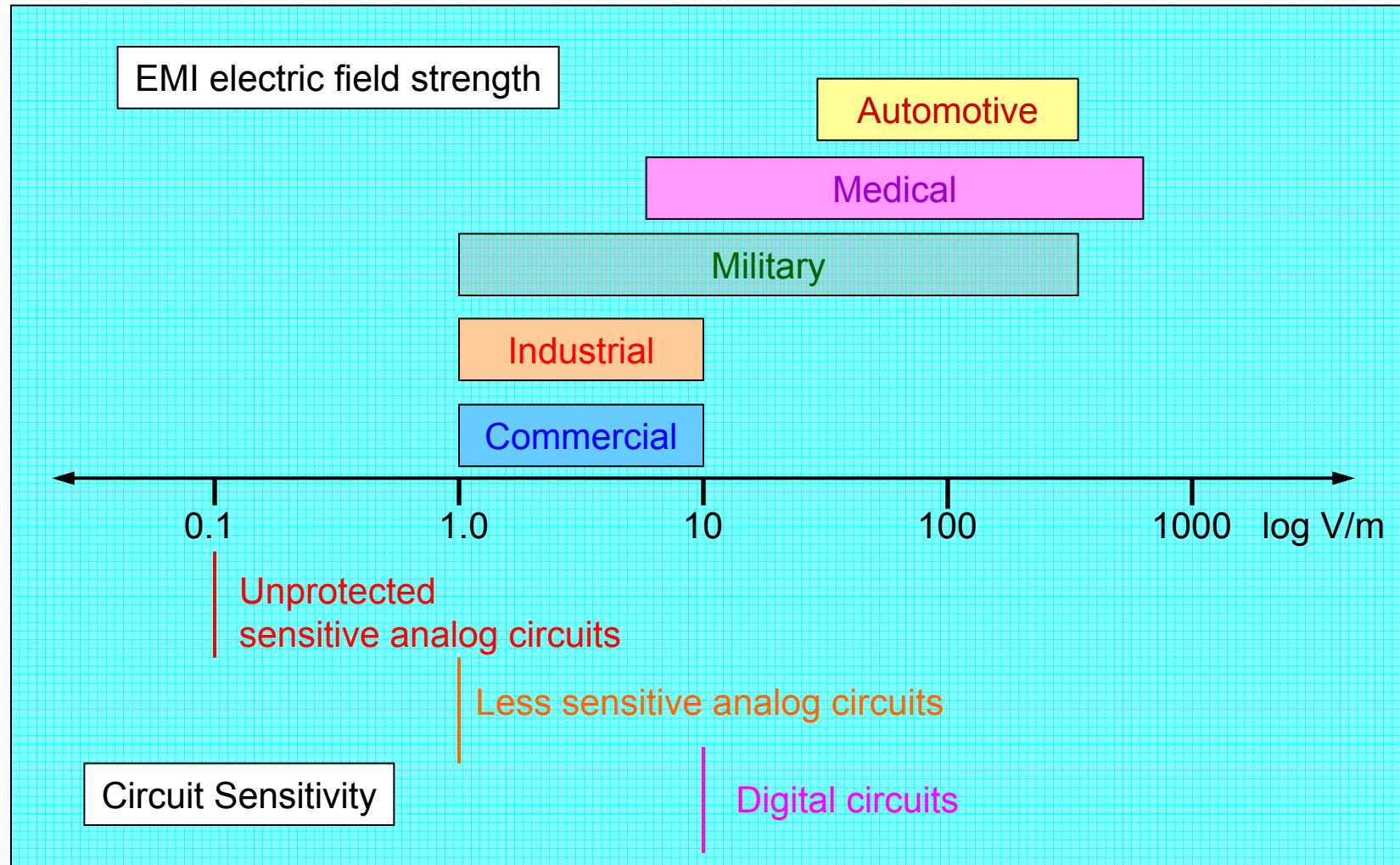
Sources: SynQor app. note 00-08-02 Rev. 04
& www.cclab.com/engnotes/eng290.htm

Radiated Emissions - 30MHz to 1GHz measurement distance 10m



Freq (MHz)	Class A dBuV/m	Class B dBuV/m
30 - 80	39	29.5
88 - 216	43.5	33
216 - 960	46.4	35.6
960 - 1000	49.5	43.5

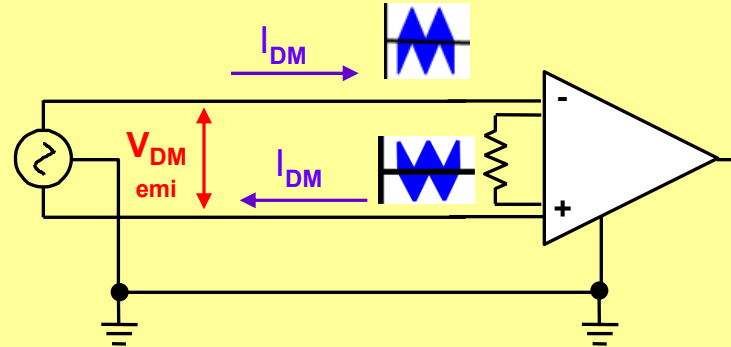
Typical RF field levels



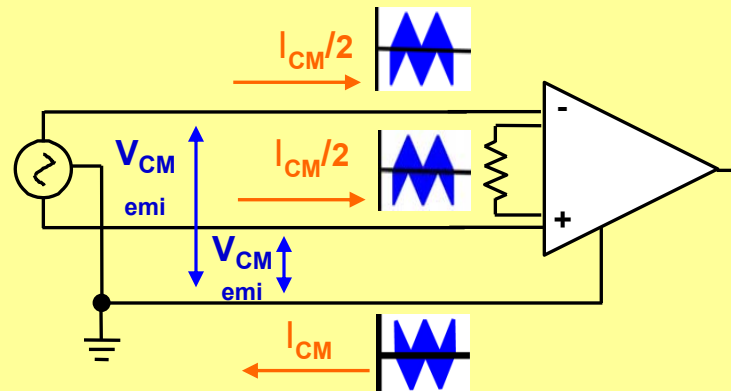
Differential and Common-mode EMI

Common-mode interference is most frequently encountered

Differential-mode EMI dominates
 $f < 1\text{MHz}$
Often results through conduction



Differential-mode EMI produces a voltage difference between the inputs

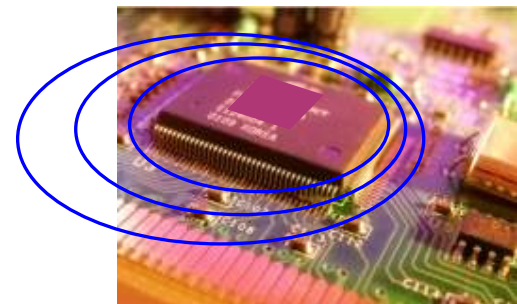
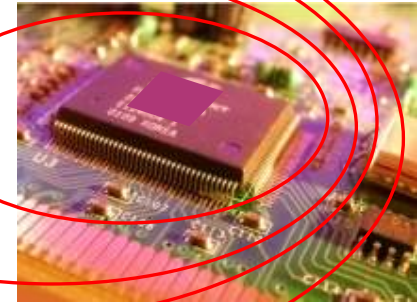


Common-mode EMI dominates
 $f > 1\text{MHz}$
Often originates as radiation

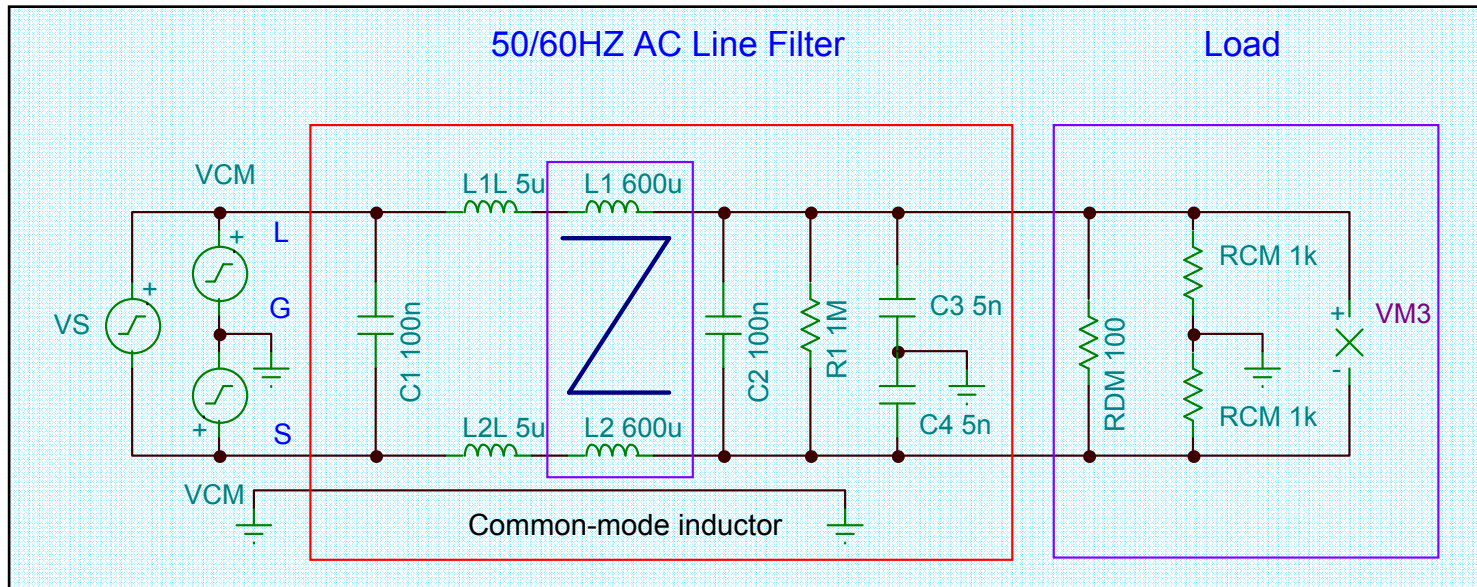
Common-mode EMI produces the same voltage on each input with respect to ground

Taming the EMI environment

- Minimize EMI radiation at source
- Minimize coupling medium's effectiveness
- Minimize receptor susceptibility to EMI



An AC line filter for conducted EMI

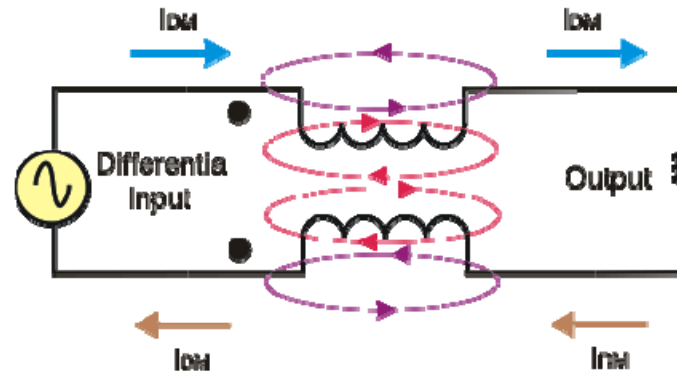


Mode	150kHz	500kHz	1MHz	5MHz	10MHz	20MHz	30MHz	
Common	6	20	28	42	45	45	48	dB
Differential	10	13	30	50	50	40	40	dB

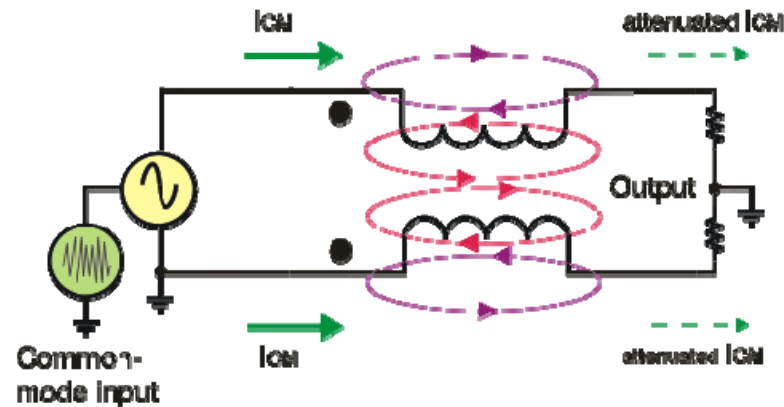
Attenuation characteristics for AC line filter (SAE GA1B-10)

The common-mode transformer

An effective common-mode filter

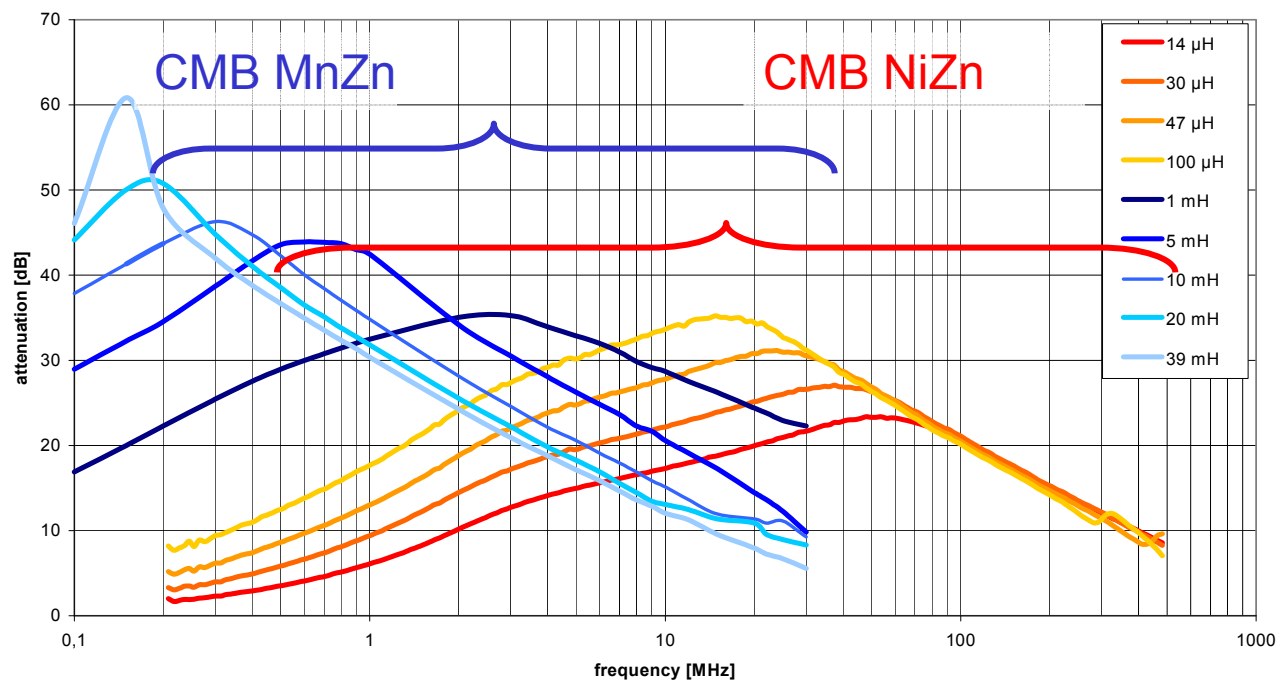


Opposing Fields - No voltage induced in either winding



Aiding Fields - Common-mode current sees full impedance of windings

Stromkompensierte Drosseln (Wuerth)

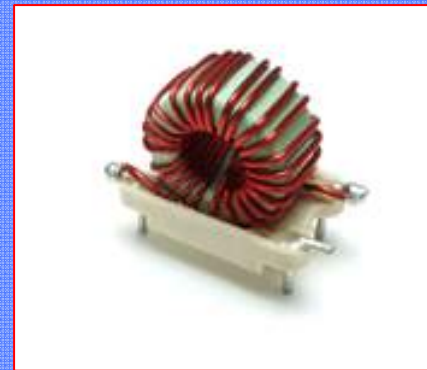


An AC line filter for conducted EMI

Common mode inductor

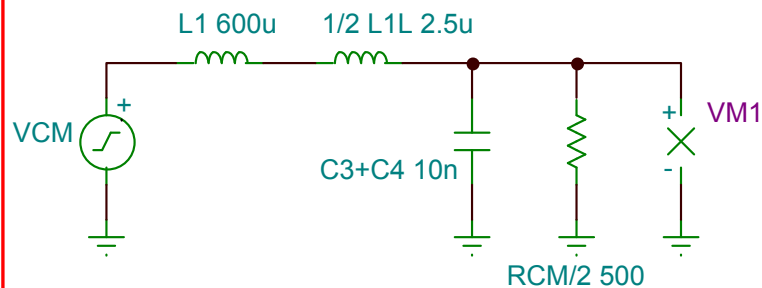


Torroid coil for DM inductor

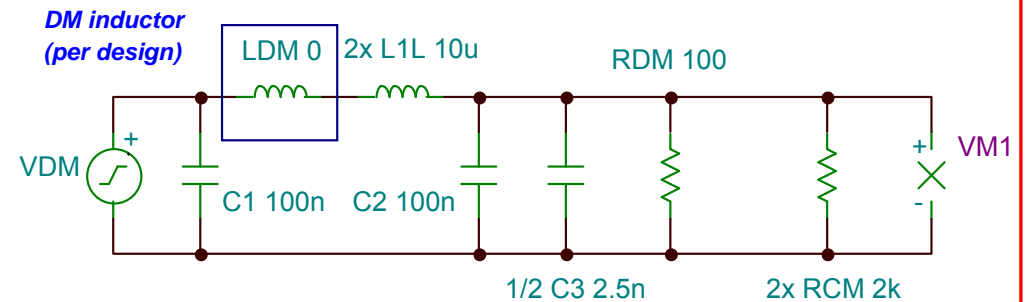


Examples from CWS - Coil Winding Services

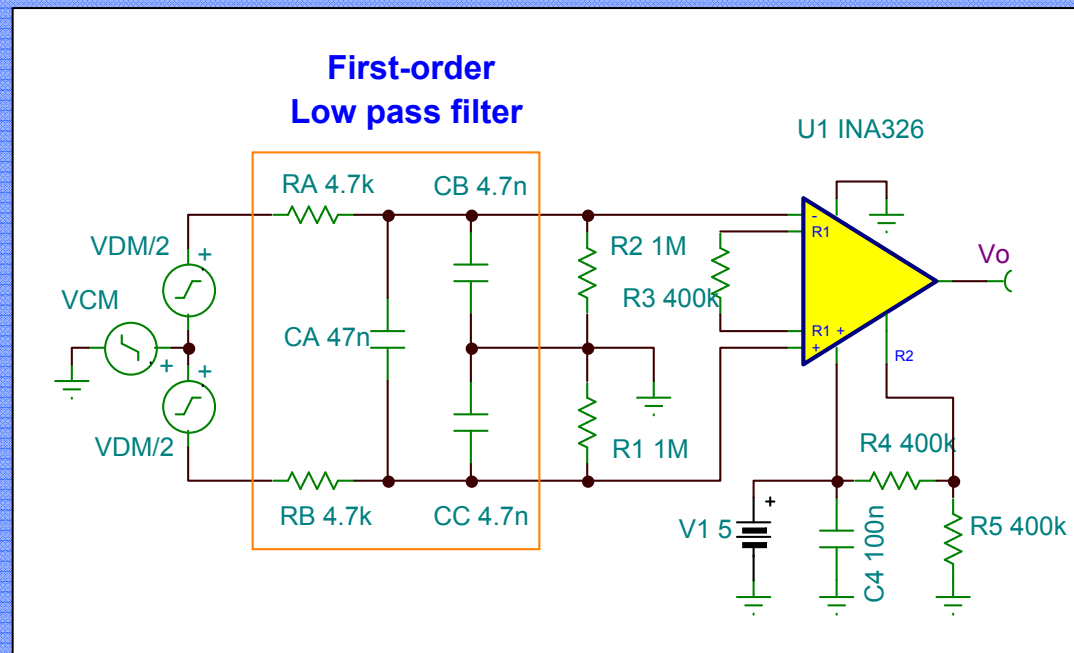
Common mode model



Differential mode model



Input RC filtering as applied to an instrumentation amplifier



Differential Mode

$$f_{-3dB} = [2\pi(R_A + R_B)(C_A + C_B/2)]^{-1}$$

$$\text{let } R_B = R_A \text{ and } C_C = C_B$$

$$f_{-3dB} = 343\text{Hz}$$

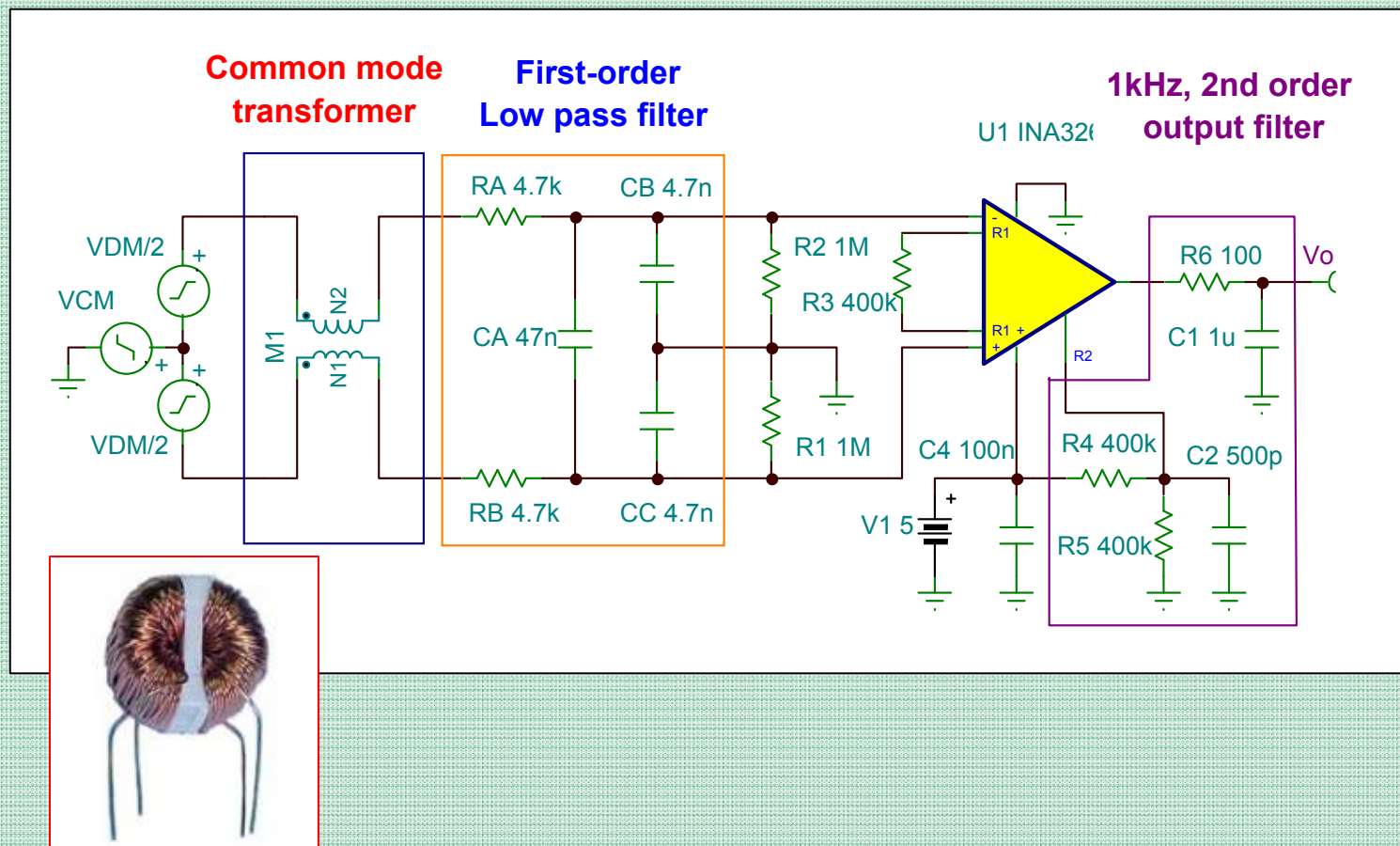
Common Mode

$$f_{-3dB} = [2\pi \cdot R_A \cdot C_B]^{-1}$$

$$\text{let } R_B = R_A \text{ and } C_C = C_B$$

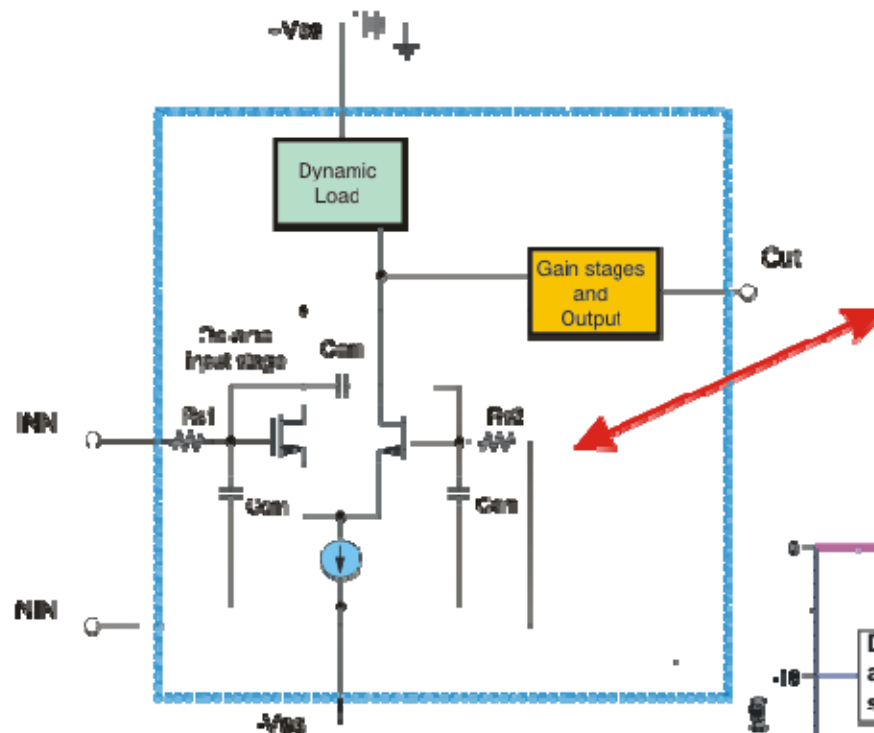
$$f_{-3dB} = 7.2\text{kHz}$$

Adding a common-mode transformer at low frequencies

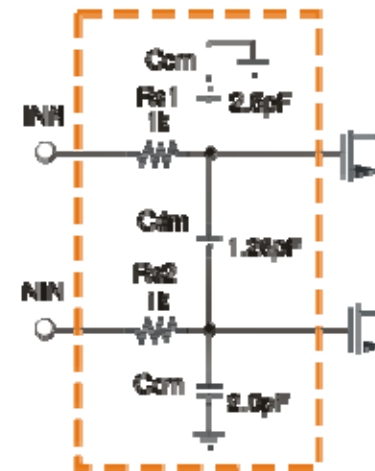


Newer Op-amps have EMI filtering

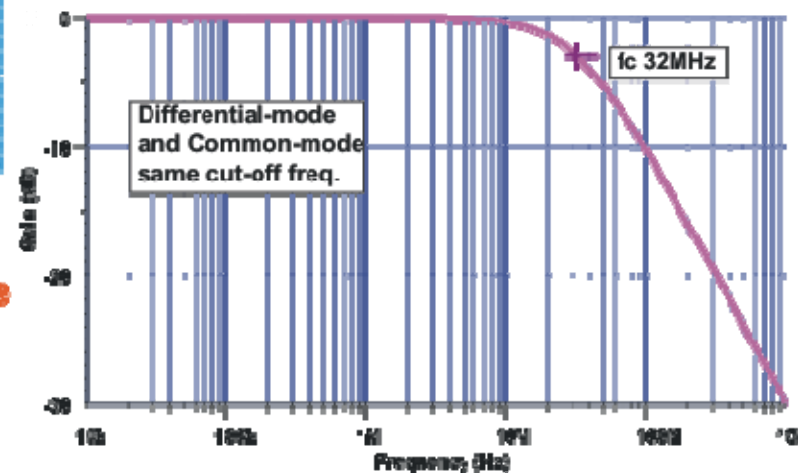
Simplified CMOS Op-amp



Built-In Input EMI Filter

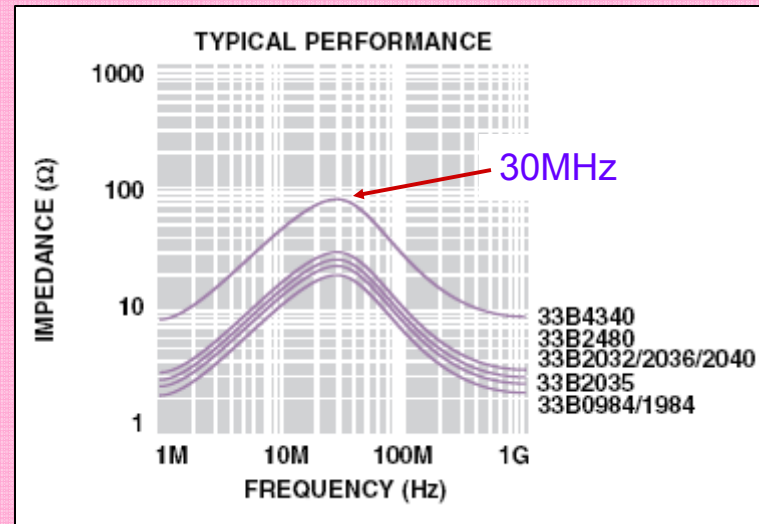


Filter response



Ferrites for EMI suppression

Ferrite surrounding the cable actually forms a common-mode transformer



Impedance of wire passing through
Wuerth ribbon cable ferrite

Was ist ein EMV-Ferrit?



...technisch gesehen:

→ gesintertes Ferritmaterial um einen Draht

Anwendung als:

- HF-Absorber
- frequenzabhängiger Filter

Bauformen:

Klappferrit

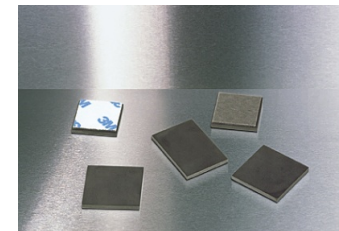
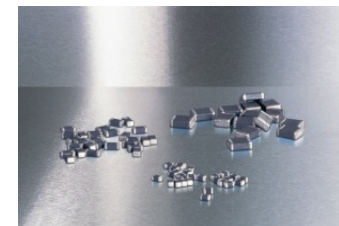
Ferrithülsen / -ringe

Blockkerne

Ferritplatten

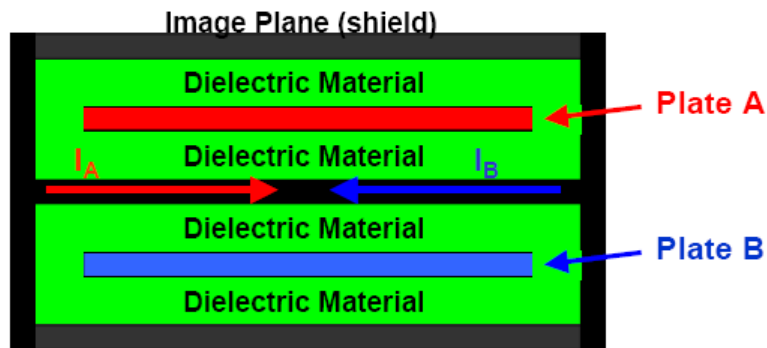
SMD-Ferrite

Ferritperlen



X2Y Capacitor Architecture

X2Y Architecture

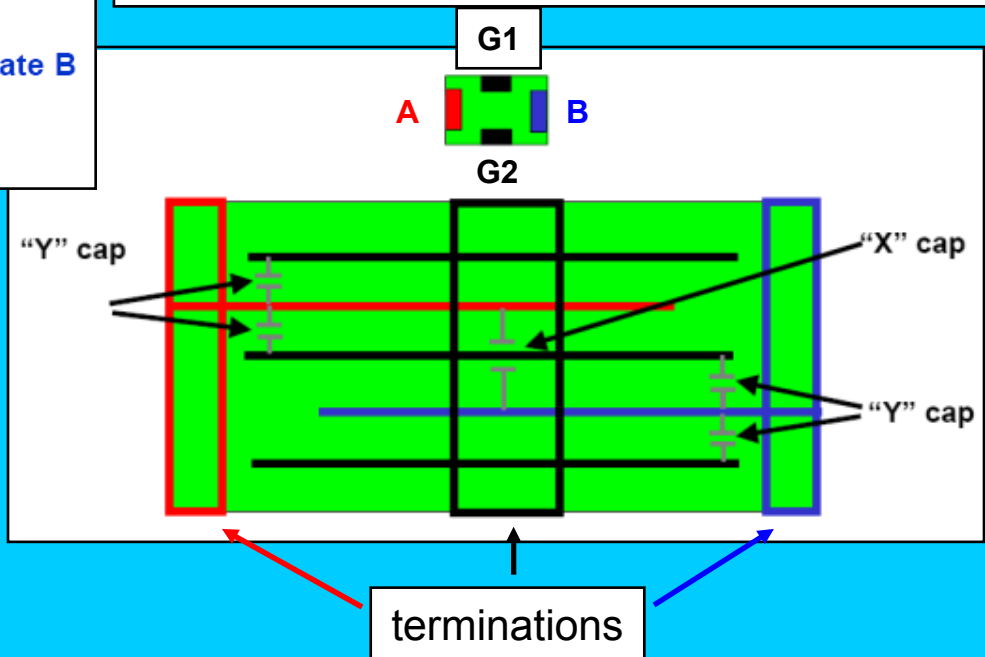


The X2Y capacitor:
1 “X” capacitor, 2 “Y” capacitors

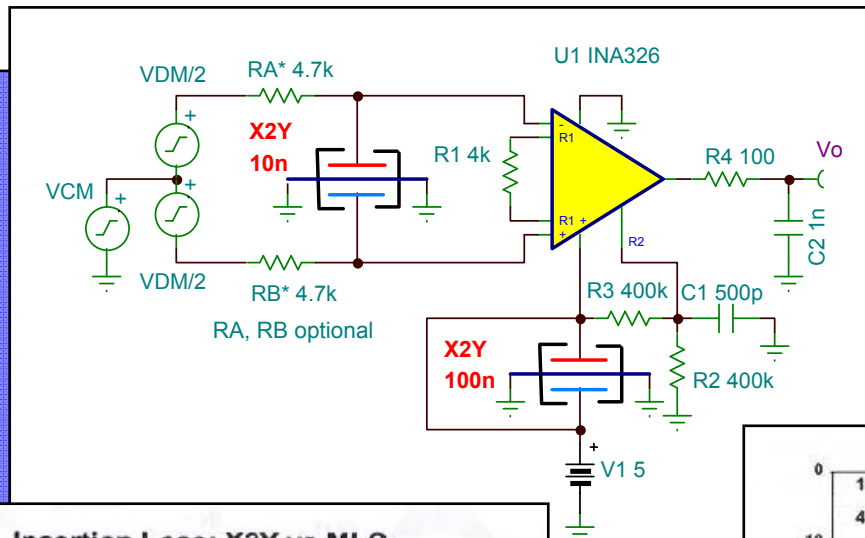
Simultaneous common-mode and differential-mode filtering

$$C_x = \frac{1}{2} C_y$$

From Yageo.com
website



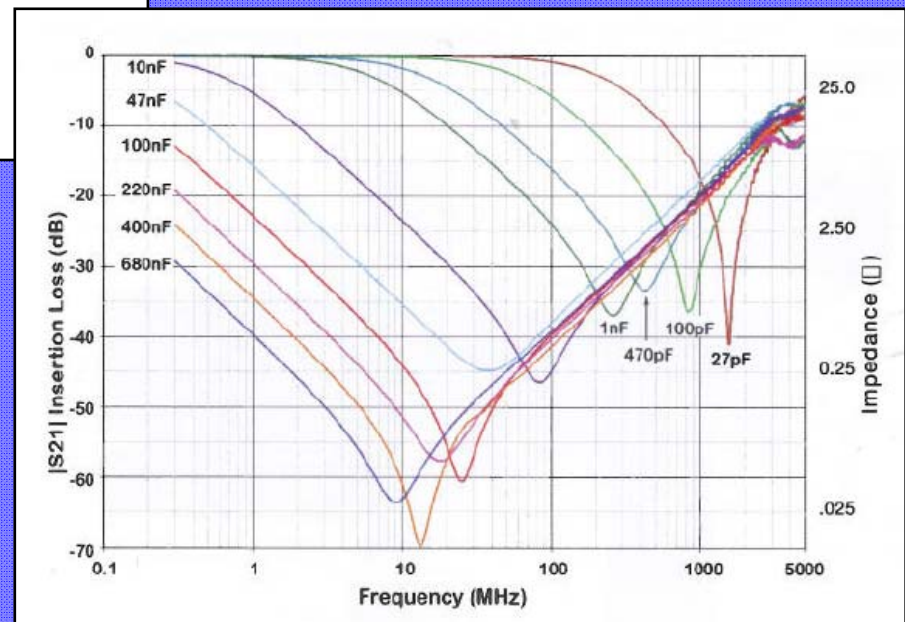
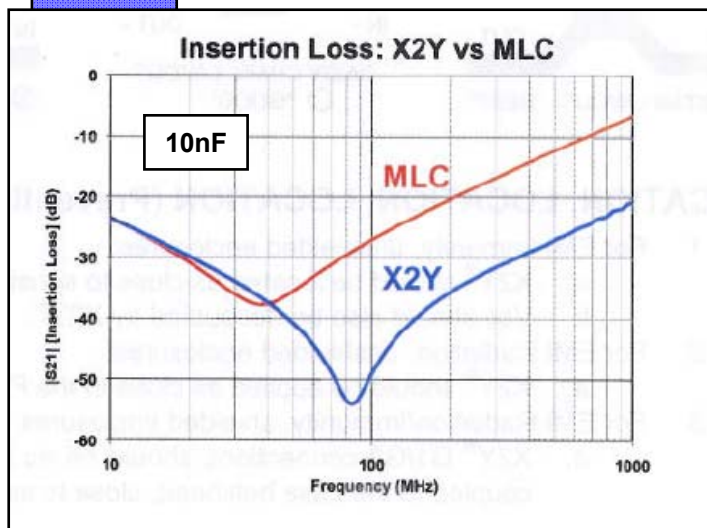
The X2Y[®] Capacitor



JOHANSON DIELECTRICS

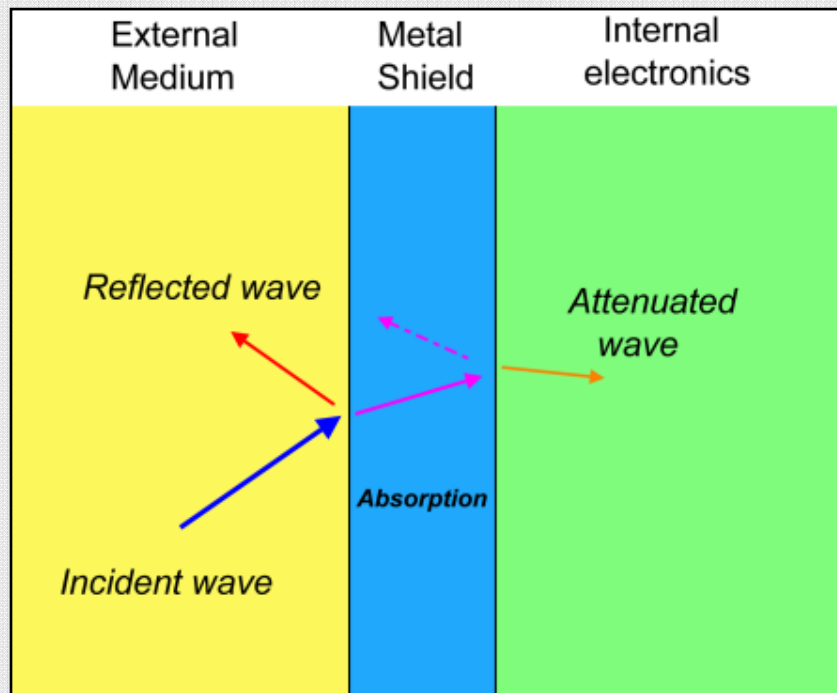
X2Y[®] Filter & Decoupling Capacitors

Input filtering s21
Signal-to-Ground



Shielding & Screening

Minimizing the medium's effectiveness



Derived from: *EDN – The Designer's Guide to Electromagnetic Compatibility*

Shielding Effectiveness (S.E.) of enclosed material

Emission Suppression

$$S.E_{dB} \text{ (Em. Supp.)} \approx A_{dB}$$

Susceptibility

$$S.E_{dB} \text{ (Sus.)} \approx A_{dB} + R_{dB} \text{ (appropriate)}$$

where: A: absorption loss in dB
R: reflection loss in dB

From: COTS Journal, January 2004 – “Design Considerations In Building Shielded Enclosures.”

Shielding & Screening

Minimizing medium's effectiveness

Metal Shielding

Magnetic field $f < 20\text{kHz}$

Ferrous metals

- steel
- Mu-metal – nickel, iron

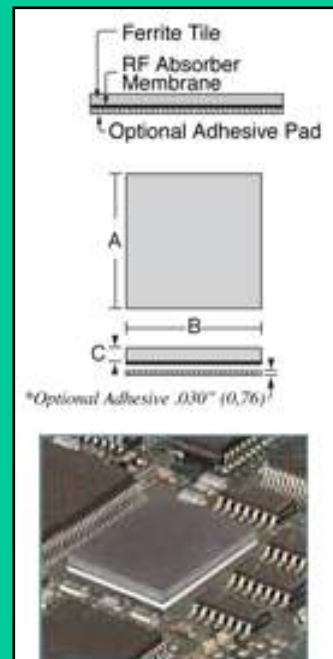
RF fields $10\text{kHz} < f < 1\text{GHz}$

Non-ferrous metals

- Al foil $I_{\text{Loss}} > 90\text{dB}$
- Cu, Ni $I_{\text{Loss}} 40\text{-}60\text{dB}$
- Vacuum plating $I_{\text{Loss}} > 80\text{dB}$
- Electroless deposition $I_{\text{Loss}} > 80\text{dB}$

From: EDN EMI/EMC guide

Ferrite shield



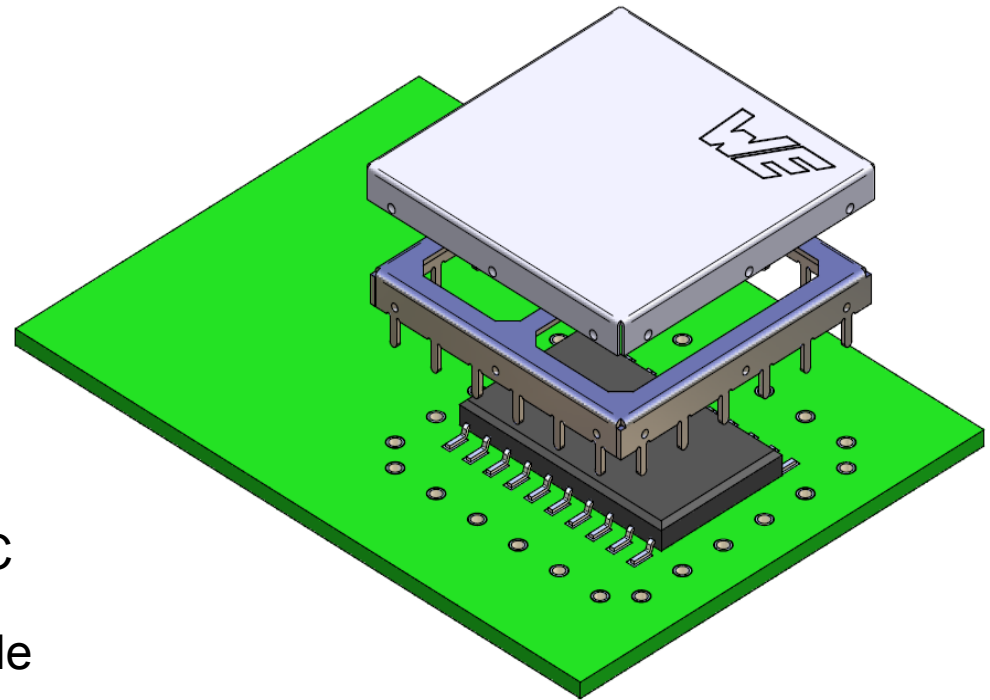
RF absorber shield



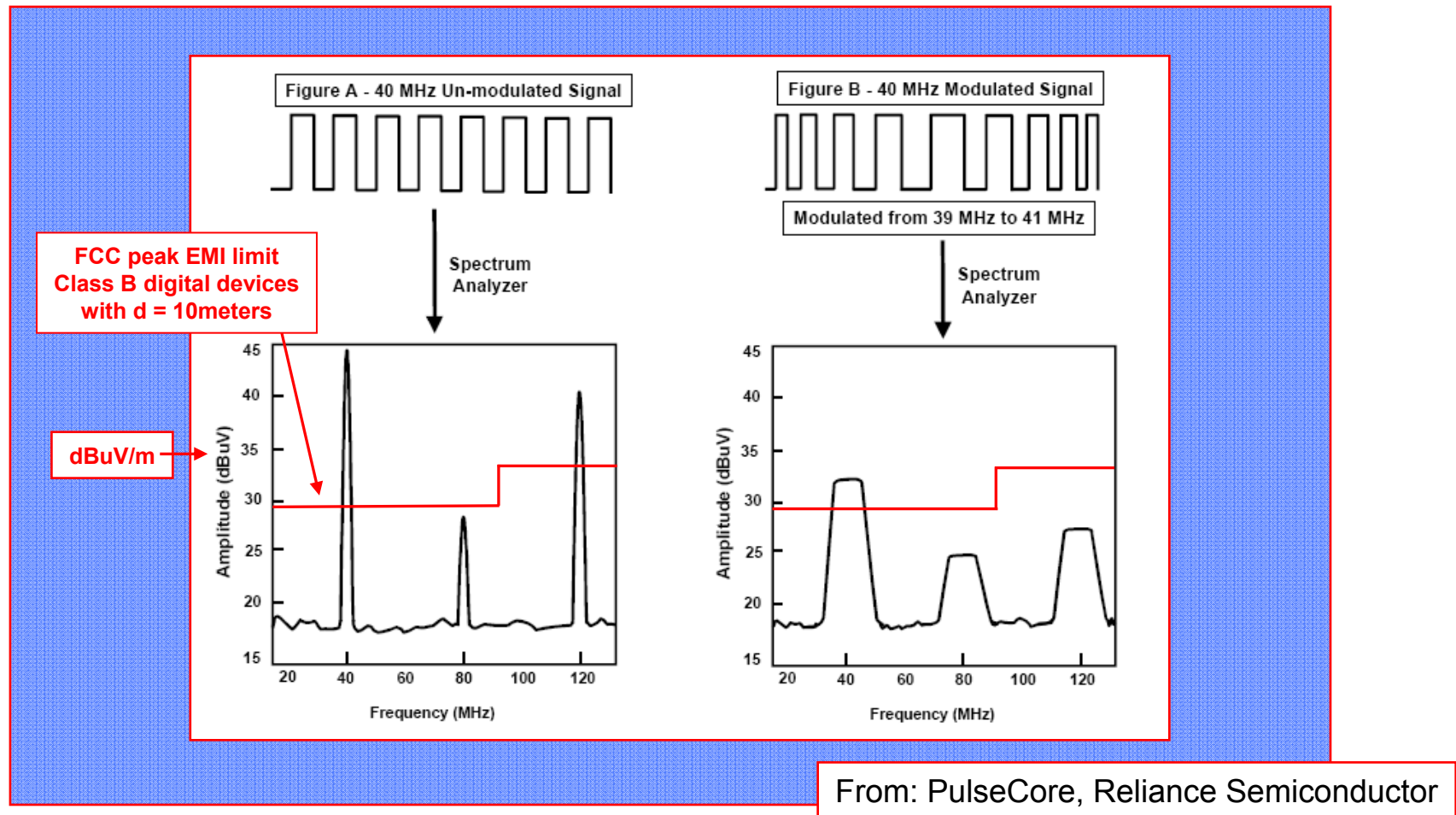
EMC Shielding Cabinet WE-SHC



- Applications are:
 - Oscillators
 - RF output stages
 - RF input & amplifier stages
 - EMC sensitive
- Overview of the materials WE-SHC
 - Different materials are available
 - Tinfoil is the standard material which we use for WE-SHC
- All materials can be lacquered, in particular in black for better thermal dissipation.



Frequency spreading of the system clock



a Loop – the path current follows

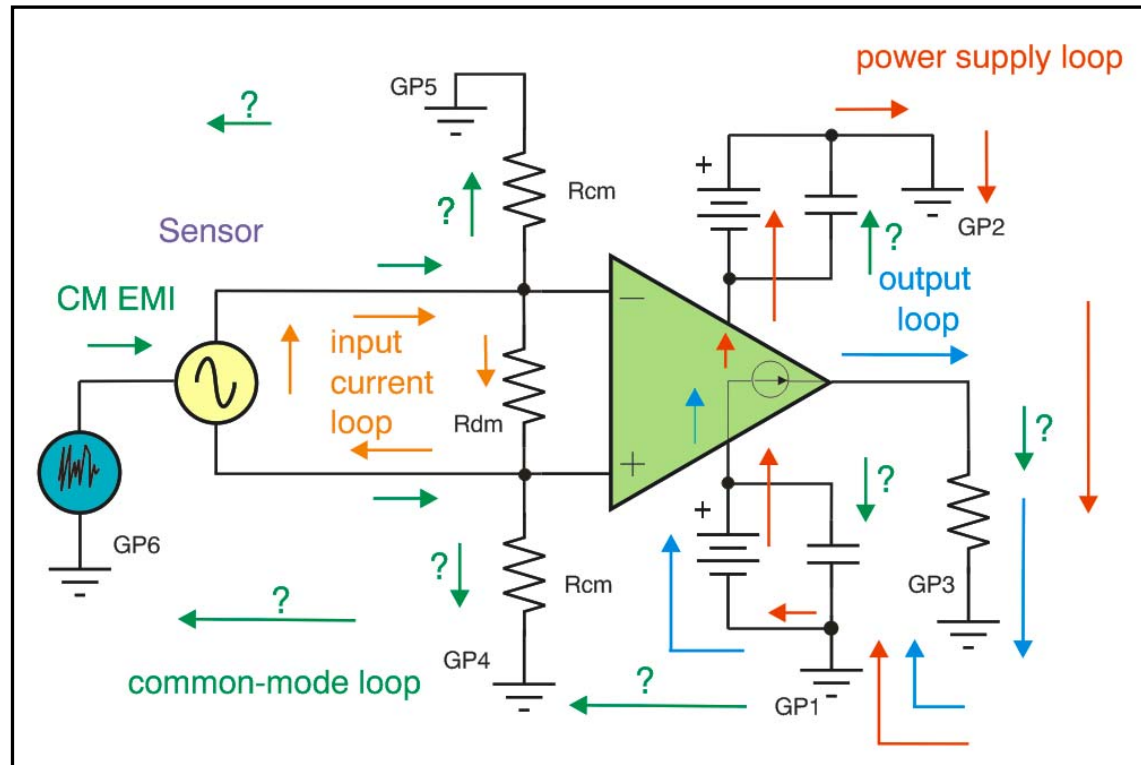
Loops

- Introduces unintended inductance in the current path where:

$$V_L = L \, di/dt$$

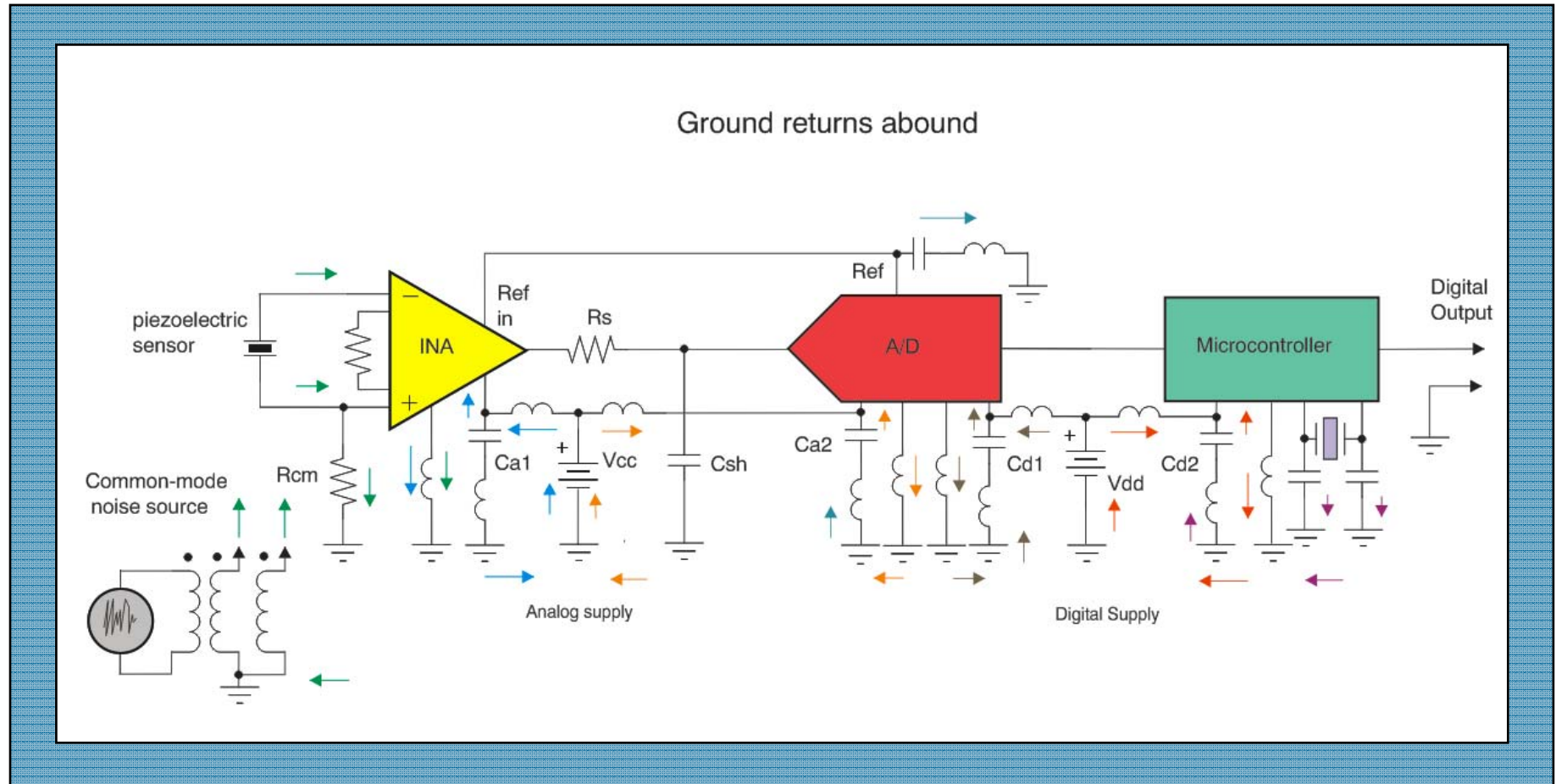
- May result in multiple AC signals sharing a current path
- May become a loop antenna that couples EMI/RFI

The common-mode return loop may be difficult to predict



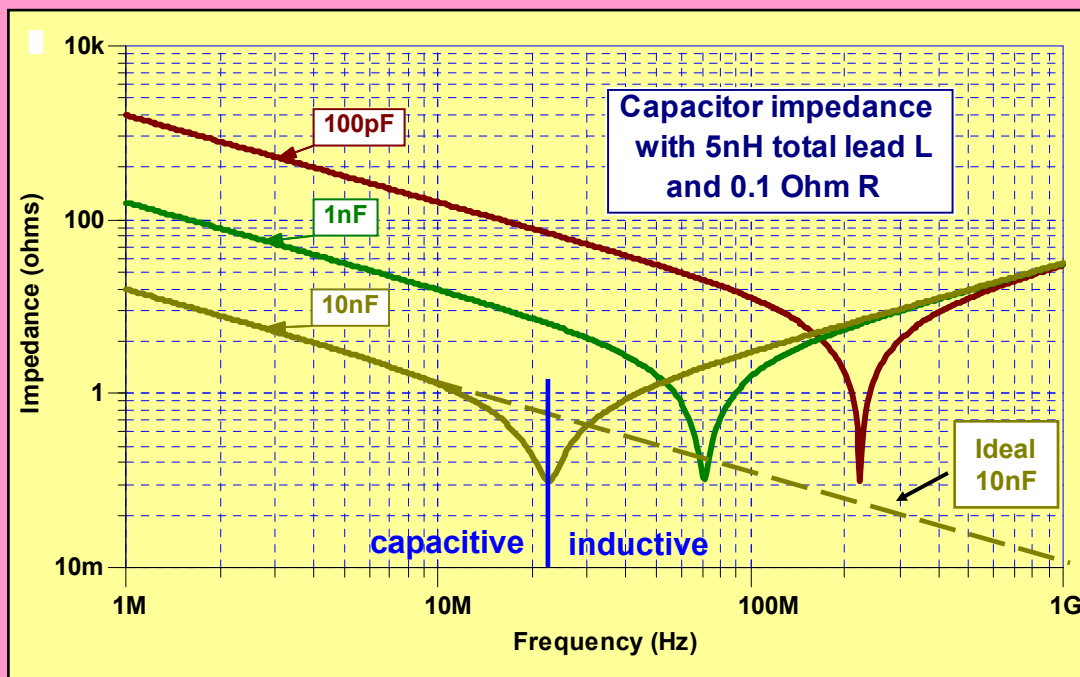
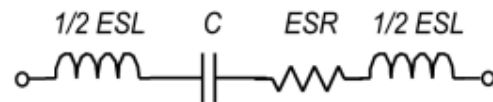
The ground return environment may be very complex

Current paths must be carefully considered to avoid long loops



Non-ideal passive components in the RF and EMI realms

Non-ideal
Capacitor
model



Other passives at RF

Conductors

- *skin effect*
- *inductance*
- *capacitance*

Inductors

- *resonance at f_r*
- *X_C above f_r*

PC board traces

- *ground loops*
- *traces and planes become monopole or loop antennas*

Use the correct capacitor to help minimize EMI

Capacitors

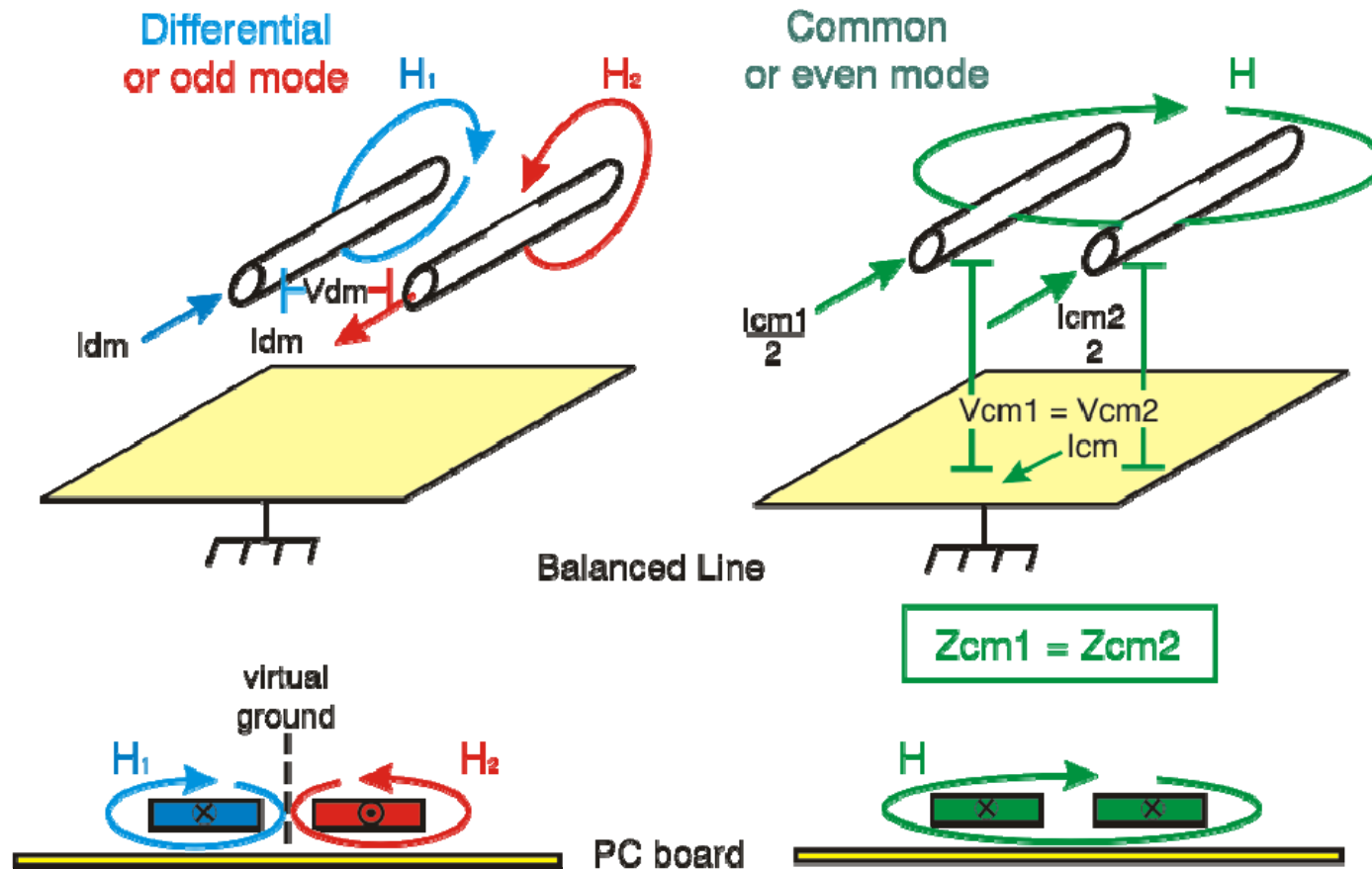
- Decoupling capacitors serve as charge reservoirs supplying transient current demands
- Decoupling capacitors must have low self-inductance and have low inductance circuit paths
- Distribute decoupling capacitors among pins having the same function; +Vdd, etc
- Use the correct capacitor type for the frequency range

Capacitor type	Maximum useable frequency*
aluminum	100kHz
tantalum	1MHz
plastic film	10MHz
silvered mica	500MHz
lead ceramic	> 500MHz
surface mount ceramic	> 1GHz
surface mount glass, porcelain	>1GHz
PCB embedded ceramic	1GHz +

*much dependent on total inductance

Balance helps limit CM EMI response

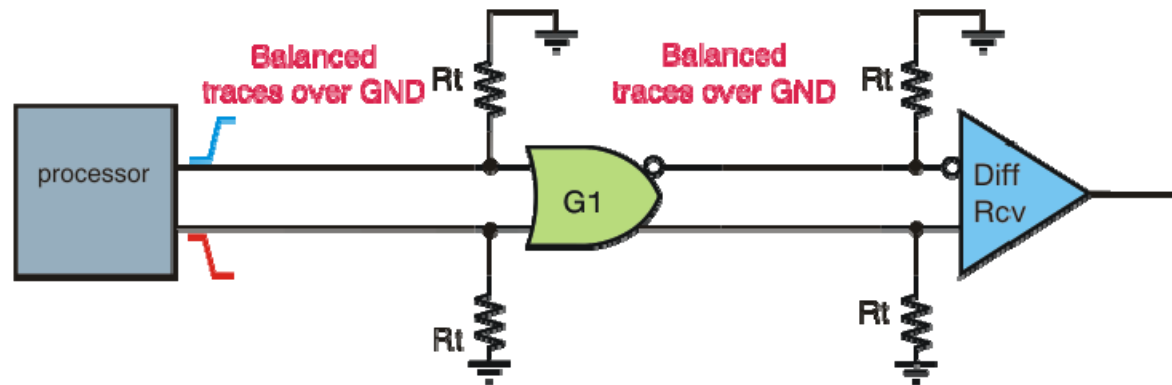
Balance helps prevent common-mode EMI from being converted to differential-mode EMI



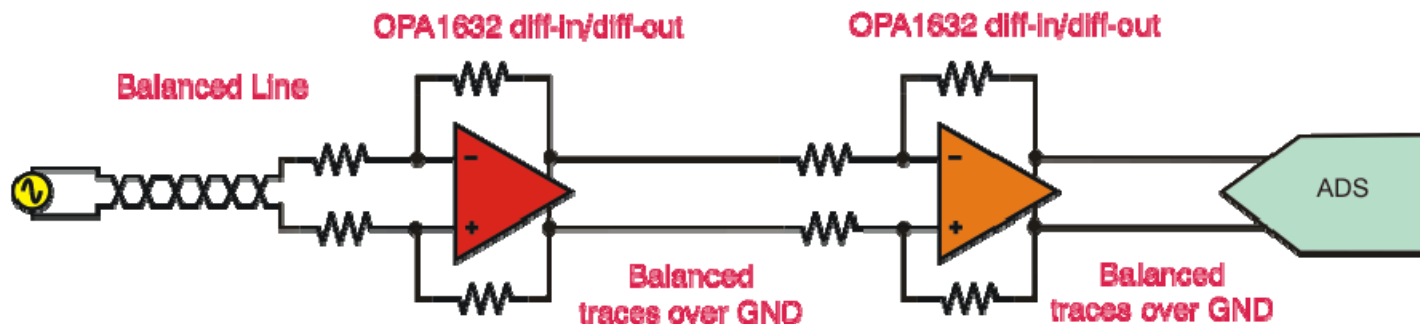
Balanced analog and digital circuit

(common-mode signals not welcome!)

Balanced digital logic: LVDS, PECL, HSTL



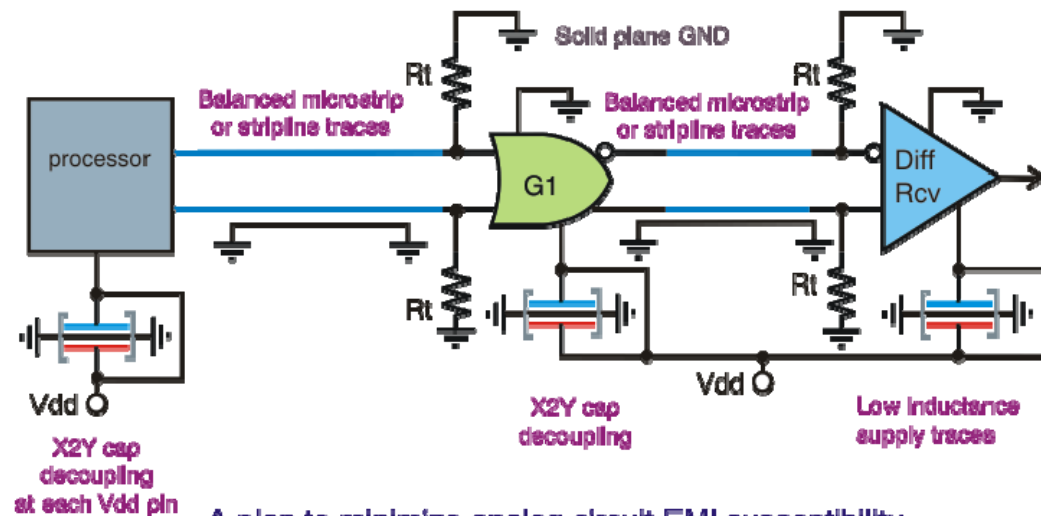
Balanced differential analog circuitry



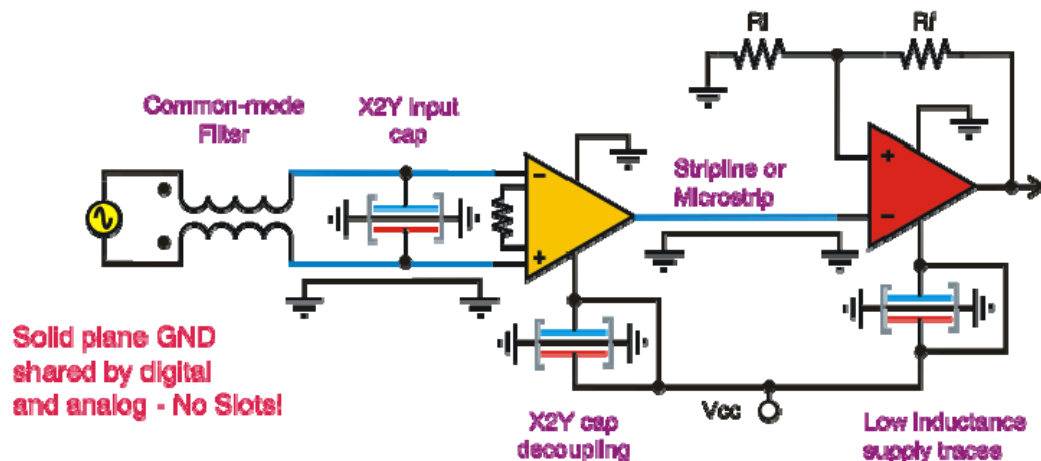
Circuit techniques to minimize EMI

- Strive for a zero impedance ground
- Design for a differential signal environment, both logic and analog
- Minimize PCB loops that act as EMI antennas
- Use X2Y capacitors for filtering and decoupling
- Make use of common-mode transformers
- Use balanced lines and traces

A plan to reduce digital circuit EMI generation



A plan to minimize analog circuit EMI susceptibility

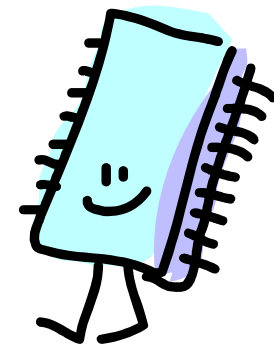


PCB layout tips to minimize EMI

- Minimize path inductance - especially ground
- Use a continuous ground plane - without slots!
- Partition potential EMI sources on one end of board, receptors on the other end
- Utilize true differential signals and paths when possible
- Use microstrip and stripline traces between circuits
- Use terminated transmission lines for high-speed and wide-band signals
- Fill open areas on signal plane with ground

In Conclusion EMI/RFI

- May constitute an operational, liability or regulatory concern
- Is best confronted at the onset of a design
- Requires a source, medium and receptor
- Propagates by conduction and/or radiation
- May require one or more reduction techniques
 - striving for a near-zero impedance ground
 - effective decoupling
 - minimizing circuit loops and loop areas
 - shielding > cables and metal cabinets
 - filtering > RC, LC and CM/DM transformers
 - balanced logic and/or analog circuits



A Happy IC - EMI Free!

References

- [1] Montrose, M.I. 1998, *EMC and the printed circuit board : design, theory, and layout made simple*, Piscataway NJ: IEEE Press)
- [2] Schmitt, Ron. 2002, *Electromagnetics explained: a handbook for wireless/RF, EMC, and high-speed electronics*. Woburn MA: Elsevier Science
- [3] http://www.uni-muenster.de/EUREGIO-team/team/inhalt_ss_05/elektronik/1.pdf
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- [5] Bergmann-Schaefer. 2006, *Lehrbuch der Experimentalphysik: Band 2: Elektromagnetismus*, Verlag Walter de Gruyter