

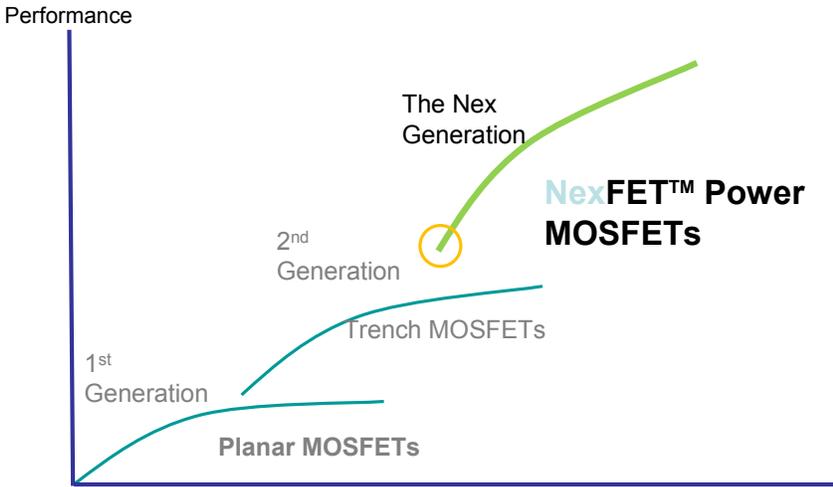


# **NexFET™**

## **How To Design with Highly Efficient MOSFETs**



# Just the Beginning

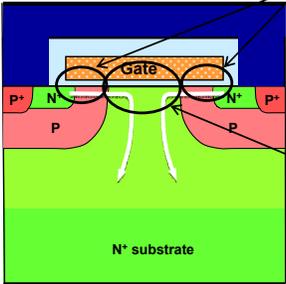




# Technology Comparison

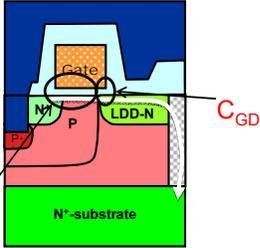
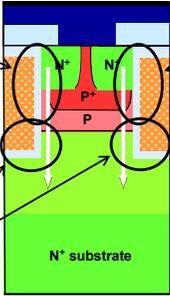
### Planar

- Commercialized in 1980's
- Lower density structure
- Relative large gate area
- Mid resistance and charge



### Trench

- Commercialized in the 1990's
- Very High Density structure
- Large gate area
- Low resistance, high charge



### NexFET™ Technology

- Commercialized in 2007
- High density structure
- Low gate charge
- Low resistance & charge

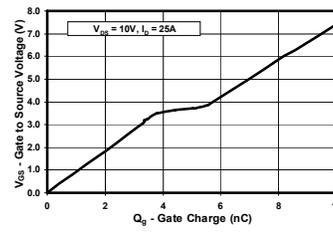
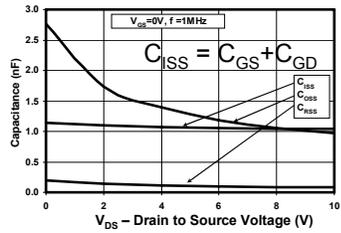
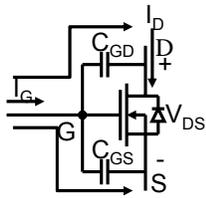


# Total Gate Charge

$$Q_G$$

- Total Gate Charge ( $Q_G$ ) is the charge required to drive the Input Capacitance ( $C_{ISS}$ ) from 0V to a specified Gate Voltage under specified  $I_D$  and  $V_{DS}$  Conditions.
  - $Q_G$  is the Area under the  $C_{ISS}$  vs.  $V_{GS}$  curve.  $Q_G = \int_0^{V_{GS}} C_{ISS} dV_{GS}$
- Energy is required to charge the gate, and is lost when it is discharged.
  - In each Charge/Discharge cycle, energy lost is:  $E_G = Q_G V_{GS}$

$Q_g$	Gate Charge Total (4.5V)	4	5.6	nC
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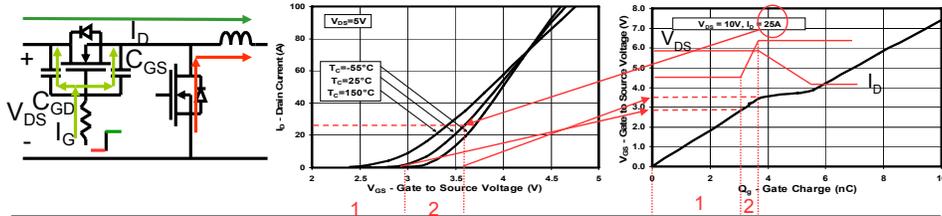


# Gate to Source Charge

$$Q_{GS}$$

- Gate to Source Charge ( $Q_{GS}$ ) is the Charge required to Switch a specified Current.
- There are two distinct regions of  $Q_{GS}$ :
  1. Pre Conduction – From 0V to the gate voltage where current begins to rise on the Transfer Characteristics curve – Nothing much happens besides an increase in Gate Leakage.
  2. Switching ( $\sim 1/4 Q_{GS}$ ) – Current rises along transfer characteristics curve to the Drain current while  $V_{DS}$  remains high.
- Under an Inductive Load,  $V_{DS}$  remains high while the Current is switched with energy loss per cycle as:  $E_{SW(GS)} \approx V_{DS} I_D \frac{1}{4} Q_{GS} \div I_G$

$Q_{gs}$	Gate Charge Gate to Source	$V_{DS} = 12.5V, I_D = 11A$	2.1	nC
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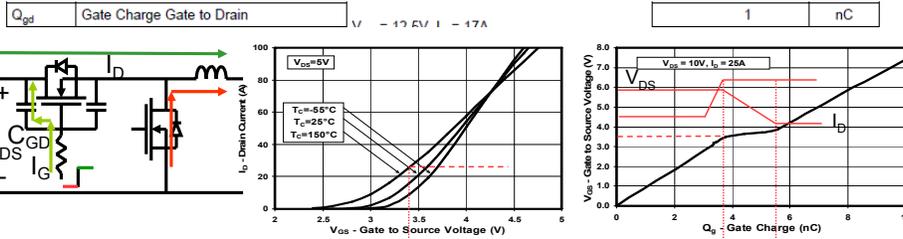




# Gate to Drain Charge

$$Q_{GD}$$

- Gate to Drain (Miller) Charge ( $Q_{GD}$ ) is the Charge required to Switch a specified Voltage.
- $Q_{GD}$  is typically specified at  $\frac{1}{2} BV_{DSS}$ .
  - When  $V_{DS}$  is different,  $Q_{GD}$  must be adjusted.
  - In the applicable range,  $Q_{GD}$  vs.  $V_{DS}$  is fairly linear and can be approximated by 1.75%  $\Delta V_{DS}$  per  $\Delta Q_{GD}$ .
- Under an Inductive Load,  $I_D$  is high while the Voltage is switched with energy loss per cycle as:  $E_{SW(GD)} \approx V_{DS} I_D Q_{GD} \div I_G$





# Gate Charge

## $Q_G$ , $Q_{GS}$ , $Q_{GD}$

- Gate Charge is the amount of charge required to be put into or taken out of the Gate to Drain and Gate to Source Capacitances to Switch the MOSFET.

- Gate Charge can be split into:

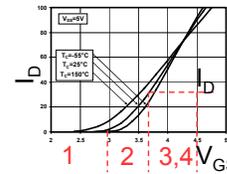
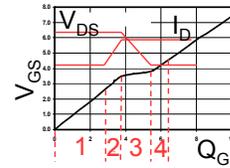
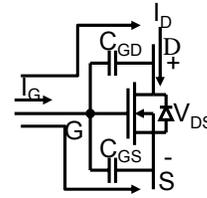
1. Gate to Source Charge ( $Q_{GS}$ ), Pre Conduction – From 0V to the gate voltage where current begins to rise on the Transfer Characteristics curve – Nothing really happens.
2.  $Q_{GS}$ , Switching ( $\sim 1/4 Q_{GS}$ ) – Current rises along transfer characteristics curve to the Drain current while  $V_{DS}$  remains high.
3. Gate to Drain (Miller) Charge ( $Q_{GD}$ ), - While Current is high,  $V_{DS}$  collapses.
4. Overdrive Charge –  $V_{GS}$  rises to its final value, driving down  $R_{DS(ON)}$ .

- Energy required to switch the gate in one cycle (on and off):

$$E_G = Q_G V_{GS}$$

- Energy dissipated in the switching action in one cycle:

$$E_{SW} = V_{DS} I_D \left( \frac{1}{4} Q_{GS} + Q_{GD} \right) \div I_G$$



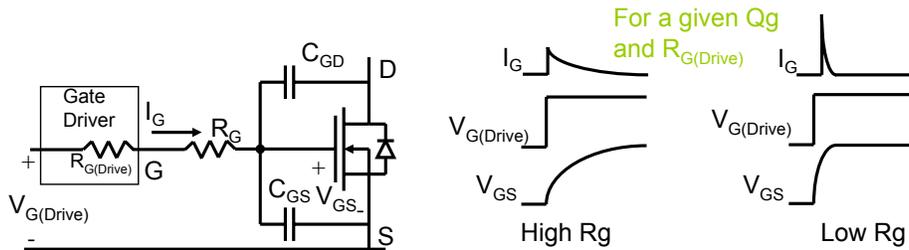


# Series Gate Resistance

## $R_G$

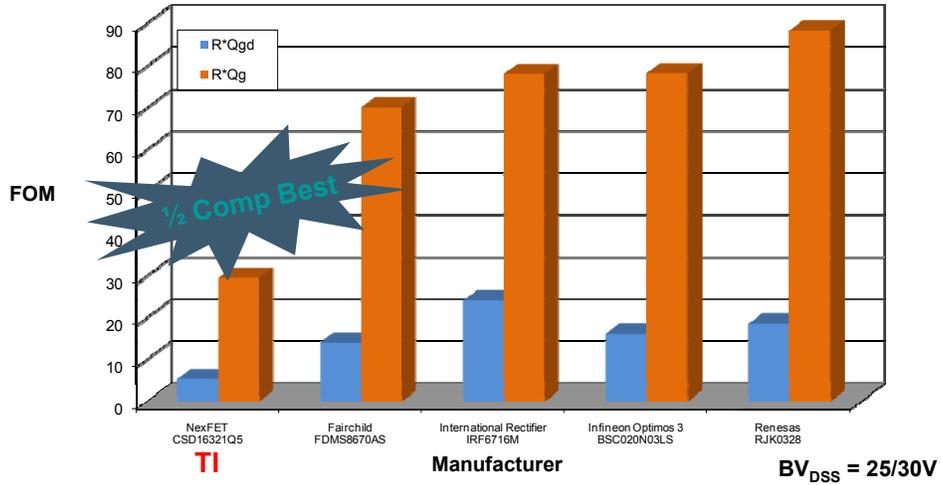
- **Series Gate Resistance is the internal resistance which impedes the flow of Charge into the gate capacitance, slowing the switching transition.**
- **It is important in High Frequency DC-DC converters.**
- **It is in Series with the Gate Driver's Resistance.**

$R_g$	Series Gate Resistance		0.9	$\Omega$
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# Inherently Better FOM

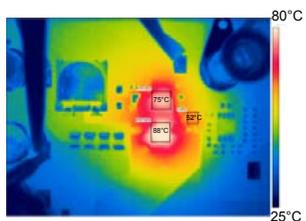




## Efficiency Delivering Cooler Systems



NexFET Devices



Industry Standard Devices

- Up to 30% cooler operation of MOSFET

- Up to 15% cooler driver operation

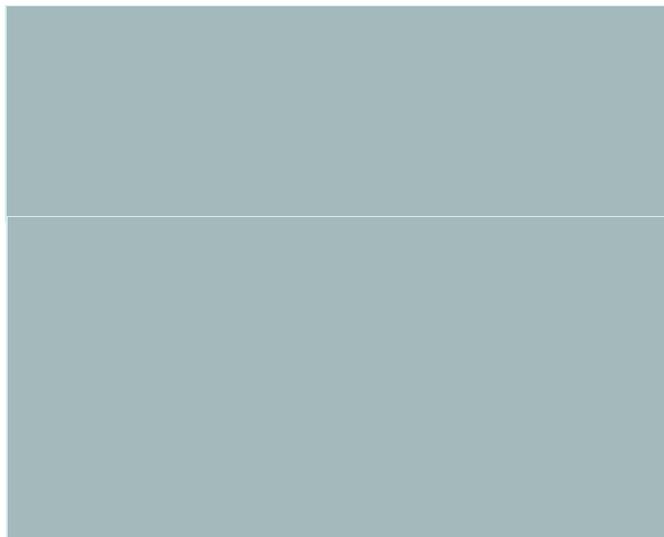
- Increased Reliability

25A, 500kHz,  $V_{IN} = 12V$ ,  $V_{OUT} = 1.3V$ ,  $V_{GS} = 5V$





## N-Ch devices





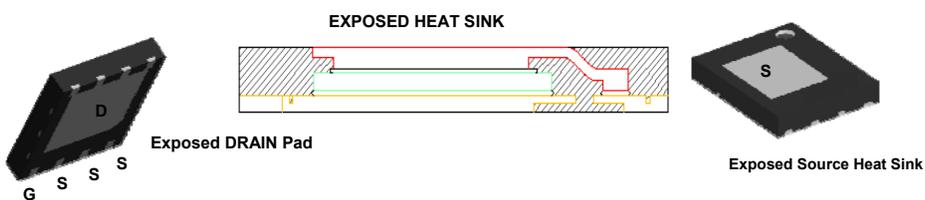
# Current Package Offering

	QxA	Qx
Construction		
Outline	 5x6, 2x2	 5x6, 3x3
Profile	<1mm	<1mm
RoHS Compliant	Yes	Yes
Package Resistance	0.7mΩ	0.3mΩ
Ls	~0.8nH	~0.4nH





# Next Gen: Dual Cool™ QFN



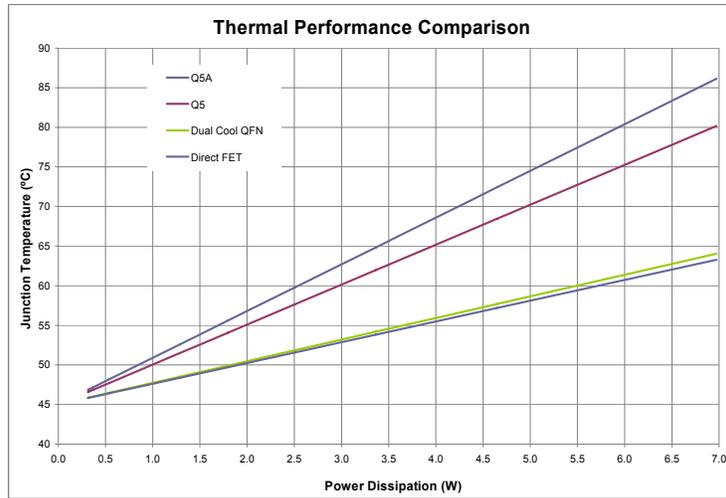
Part No	V <sub>DS</sub>	V <sub>GS</sub>	R @ 10V	R@ 4.5V	Qg	Qgd	Sample	Prod
CSD16407Q5C	25V	16V	1.8mΩ	2.5mΩ	13.3nC	3.5nC	Now	Q3CY09
CSD16325Q5C	25V	10V	-	1.7mΩ	19nC	4nC	Jun 09	Q3CY09
CSD16321Q5C	25V	10V	-	2.1mΩ	14nC	2.5nC	Jun 09	Q3CY09
CSD16322Q5C	25V	10V	-	4.4mΩ	6.2nC	1.3nC	Jun 09	Q3CY09

	Samples	Prod
QFN3x3	Q3 CY09	Q4 CY09





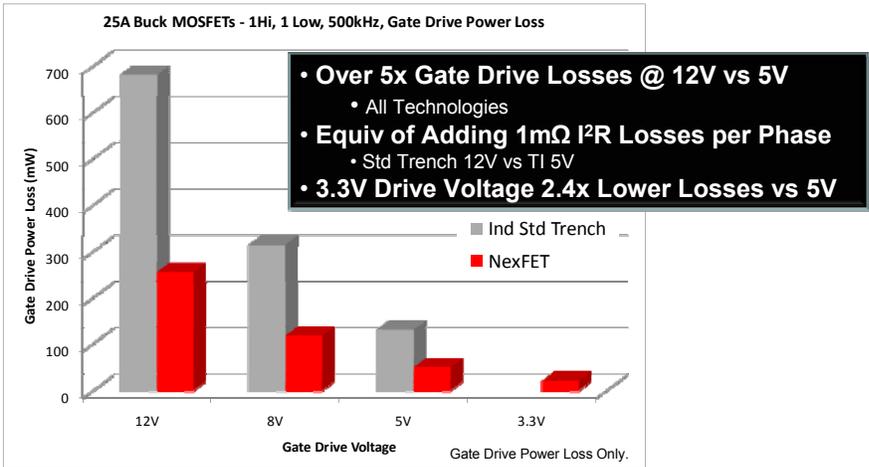
# Excellent Thermal Capability



Same Thermal Performance as DirectFET package



# Gate Drive Loss Increase with $V_{GS}$



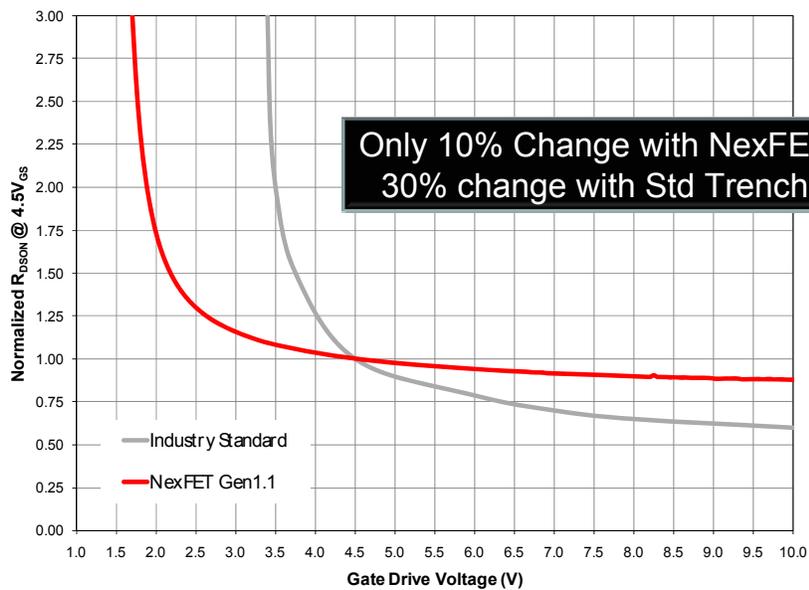
$V^2$  Relationship of Drive Voltage to Energy wasted  
 $E = CV_{GS}^2$

E = 1/2 CV<sub>gs</sub><sup>2</sup> for charge and discharge of gate





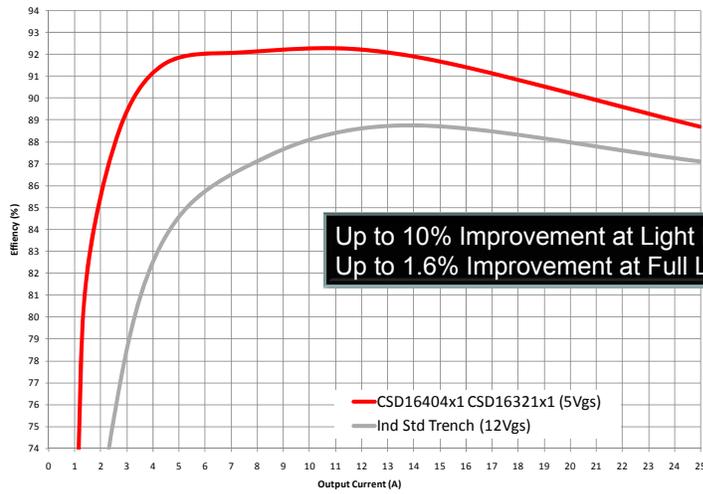
# Gen1.1 – Optimized for 5V<sub>GS</sub>





# Improved Efficiency Across the Range

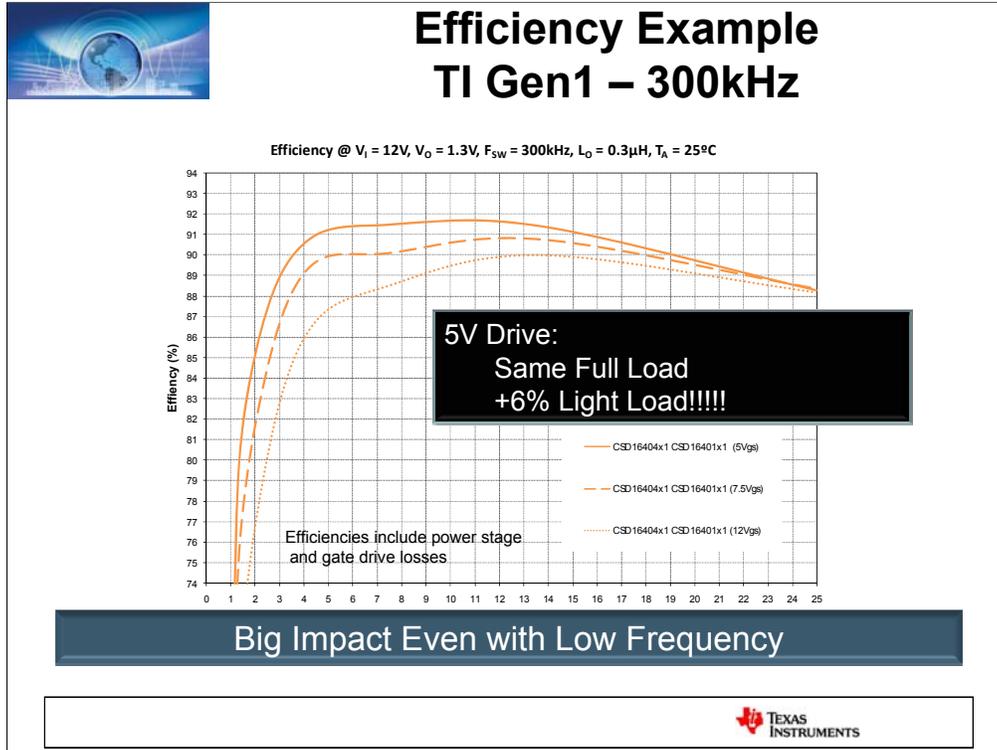
Efficiency @  $V_{IN} = 12V$ ,  $V_{OUT} = 1.3V$ ,  $F_{SW} = 300kHz$ ,  $L_O = 0.3\mu H$ ,  $T_A = 25^\circ C$



Up to 10% Improvement at Light Load  
Up to 1.6% Improvement at Full Load

5V<sub>GS</sub> Better Full Load Even with Comp FET Fully Enhanced @ 12V<sub>GS</sub>

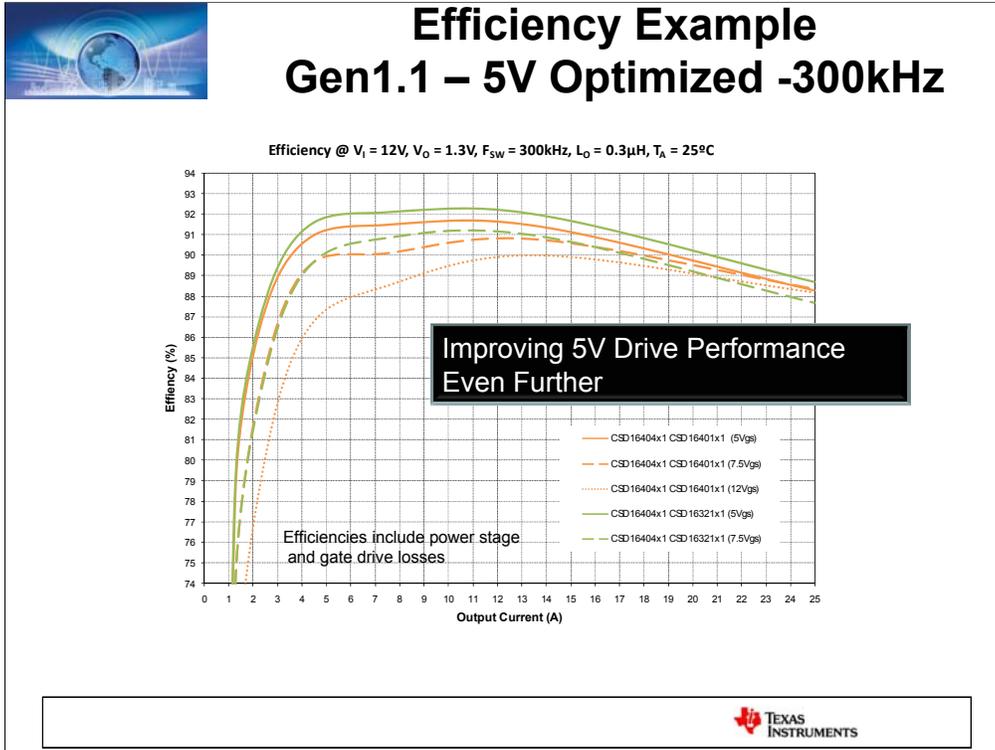




This shows that even at low frequencies with TI – 300kHz – the trade-off in going from 5V to 12V is the same, overall 5V is more efficient.

The 12V gate drive begins to cross over the 5Vgs efficiency @ 25A and if the current was extended it would be greater efficiency vs 5Vgs. But most systems today use 25A or less per phase so this is not as relevant, especially as there is a major impact on light and mid loads by going to higher drive voltage.

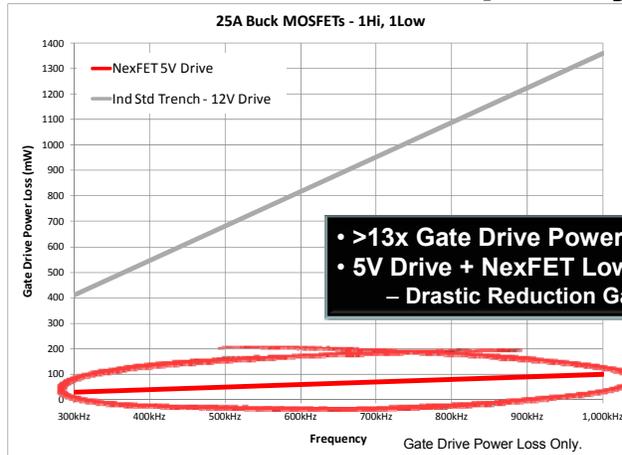
The 25A cross over is for this specific combination of devices. ~7mOhm high side & ~2-2.5mOhm low side. TI could insert a lower resistance low side or high side that would help extend this past 25A should higher current full load be required.



This shows how TI Gen1.5 performs vs TI Gen1, CSD16321 being an improved cost/performance vs the CSD16401. Even at 300kHz with slightly higher resistance the CSD16321 manages improved full load efficiency and throughout the entire load range. By optimizing for 5Vgs systems TI has pushed the cross over point vs 12V systems out even further beyond 25A.



# Gate Drive Loss Increases with Frequency



• >13x Gate Drive Power Loss for 12V  
• 5V Drive + NexFET Low  $Q_G$   
– Drastic Reduction Gate Drive Losses

Linear Relationship to Voltage and Charge  
Gate Drive Loss =  $V_{GS} \times \text{Freq} \times \text{Total } Q_G$



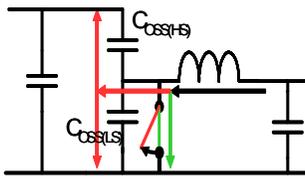
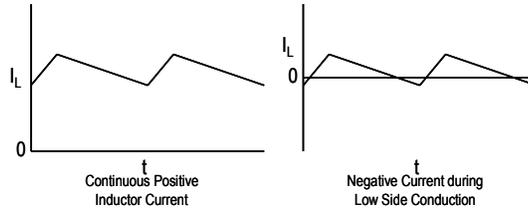
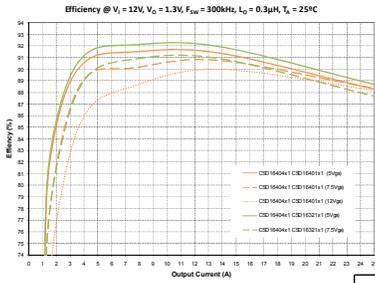


## Vgs Summary

- **5V<sub>GS</sub> Systems Delivers Highest Overall Efficiency**
- **NexFET Devices are Optimized for 5V<sub>GS</sub> Gate Drive Systems**
- **NexFET Devices Enable Higher System Efficiency or Frequency Running @ 5V<sub>GS</sub> versus @ 12V<sub>GS</sub>.**
- **Gate Drive Losses are Frequently Omitted from Efficiency Measurements.**

$$\frac{V_{IN} I_{SW(ON)} R_{Drive} Q_{G(SWHS)}}{2V_{GS(SW)}}$$

# NexFET™ “Bump”



	Positive Current	Negative Current	
$P_{OSS}$	$\frac{1}{2} (Q_{OSS(HS)} + Q_{OSS(LS)}) V_{IN} f$	Lossless	Constant with current
$P_{rr}$	$Q_{RR} V_{IN} f$	Lossless	Decreases with decreasing current
$P_{SW(ON)}$	$\frac{V_{IN} I_{SW(ON)} R_{Drive} Q_{G(SWHS)}}{2V_{GS(SW)}}$	$\frac{V_{IN} I_{SW(ON)} R_{Drive} Q_{G(SWLS)}}{2V_{GS(SW)}}$	Decreases with decreasing current
$P_{SD(ON)}$	$I_{SW(ON)} V_{SD(LS)} DT$	$I_{SW(ON)} V_{SD(HS)} DT$	Decreases with decreasing current





MOSFET Selection

**TEXAS INSTRUMENTS** **Power MOSFET Selection** Clear All

Part Number	Package	Ch	Configuration	Vds	Vgs	10V	Rds(on)(mΩ)	8V	4.5V	> 3V	Vgth (V)	O10 (nC)	O4.5 (nC)	Ogs (nC)	Ogd (nC)	Rg (Ω)	Orr (nC)	Info
				36			8.91		11.52									
				24			5.36		8.40									
▶ CSD16409Q3	OFN 3x3	N	Single	25	16	6.2	9.5				2	8	4	2.1	1	0.6	22.9	Prod 0.65
CSD16410Q5A	OFN 5x6	N	Single	25	16	6.8	9.6				1.9	7.95	3.9	1.8	1.1	0.65	24	Prod 0.81

Select Socket: Cross Reference

Part Number	Add Manufacturer	Package	Ch	Configuration	Vds	Vgs	10V	Rds(on)(mΩ)	8V	4.5V	3V	Vgth (V)	Og10 (nC)	Og4.5 (nC)	Ogs (nC)	Ogd (nC)	Rg (Ω)	Orr (nC)	Company
BSC080N03LS		OFN 5x6	N	Single	30	20	6.7	9.6				1.6	15.5	7	4	1.8	1	23	Infineon Technologies

Record: 14 of 2 (Filtered)



# Value!!!

**MOSFET Selection**

**TEXAS INSTRUMENTS** **Buck Control Switch** Clear All

Part Number	Package	Ch	Configuration	Vds	Vgs	R100 (mΩ)	Pon (W)	Ogd (nC)	Psw (n)	Psw (eff)	Og (nC)	Pgate (mW)	Ooss (mW)	Poss (mW)	Ptot (W)	η (%)	Info
CSD16323Q3	TOFN 3x3	N	Single	25	10	5.41	0.217	1.29	0.096	0.184	6.73	16.8	14	42	0.557	97.7	Info
CSD16409Q3	TOFN 3x3	N	Single	25	16	12.2	0.491	0.99	0.093	0.095	4.36	10.9	9.1	27.3	0.718	97.1	Info
BSC080N03LS	TOFN 5x6	N	Single	30	20	11.4	0.459	1.73	0.174	0.176	7.77	19.4	13	39	0.868	96.5	Info
CSD16411Q3	TOFN 3x3	N	Single	25	16	17.5	0.701	0.69	0.069	0.084	3.20	8	6.5	19.5	0.882	96.5	Info

Select Socket: **Buck Converter**

**Buck Converter**

Duty Cycle: 0.100  
ICRMS: 6.34  
IRecRMS: 19.01  
ISwOn: 17.84  
ISwOff: 22.16

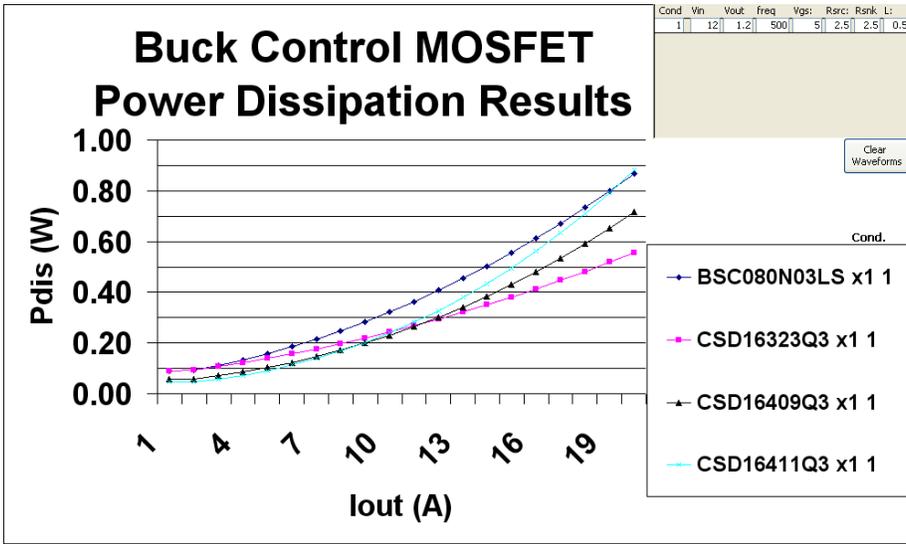
Control block: Control, Driver: TPS5124, Recifier, VgsCtrl: 5V, VgsRec: 5V, VgsSnk: 5V, Inductance: 0.5 μH, Ripple Current: 0.520 A, Iout: 20 A, Vout: 1.2 V

Records: 4 of 3 (Filtered)  
Records: 4 of 4 (Filtered)

- Efficiency (of this component)
- Size



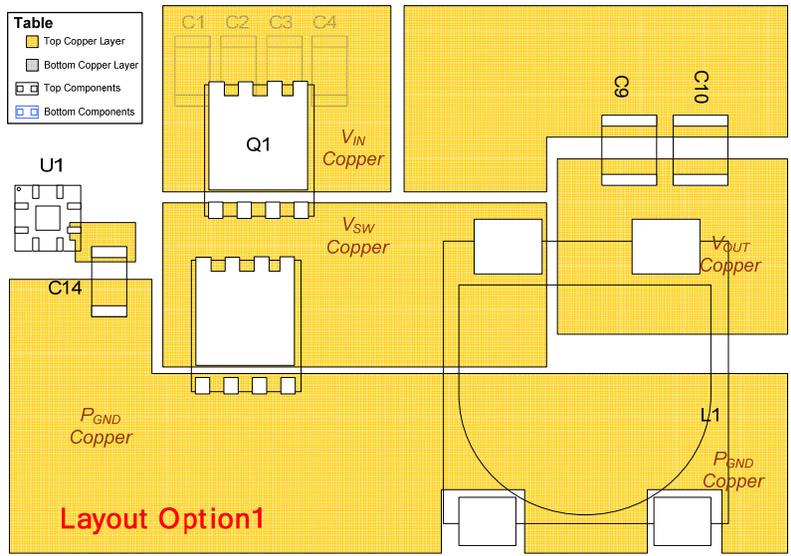
# More Value – Low Current





# Before

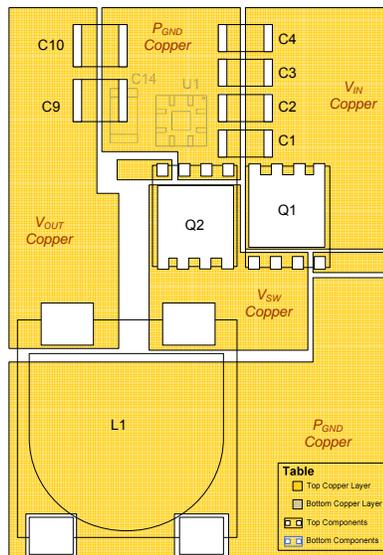
Table	
	Top Copper Layer
	Bottom Copper Layer
	Top Components
	Bottom Components



Layout Option1



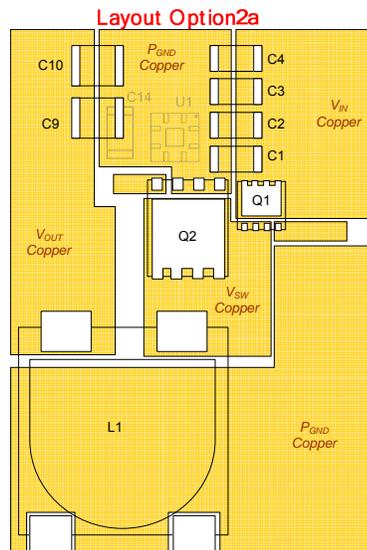
# Ideal Power Stage Placement



1. Minimize distance between Positive node of input ceramic cap & Drain pin of Control FET
2. Minimize distance between Negative node of input ceramic cap & Source pin of Sync FET
3. Use minimum 4x 10uF Ceramic capacitors for input caps
  1. TDK # C3216X5R1A106M
4. Continuous flow of Power Planes



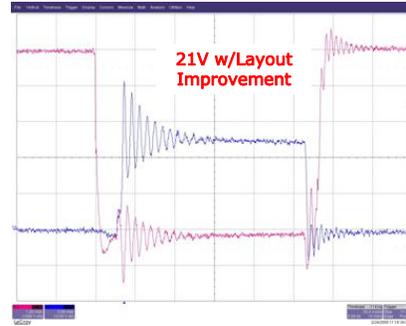
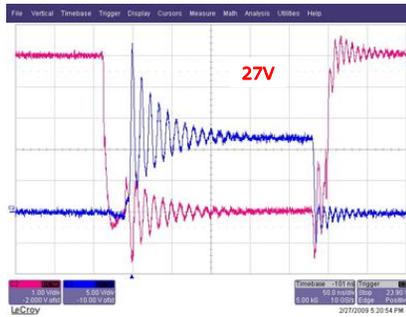
## 3x3mm QFN



1. Minimize distance between Positive node of input ceramic cap & Drain pin of Control FET
2. Minimize distance between Negative node of input ceramic cap & Source pin of Sync FET
3. Use minimum 4x 10uF Ceramic capacitors for input caps
  1. TDK # C3216X5R1A106M
4. Continuous flow of Power Planes

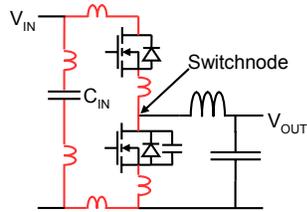


# Before and After Effects

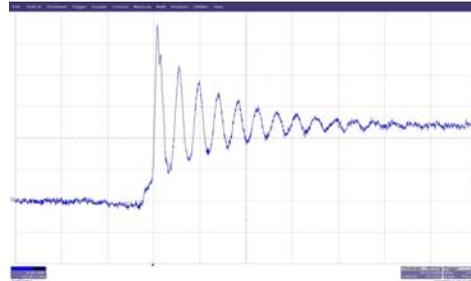
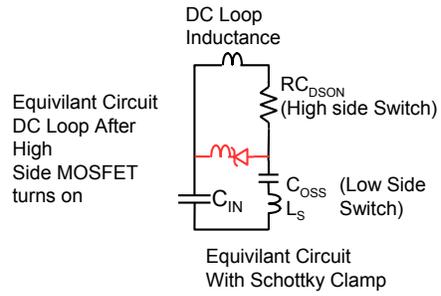
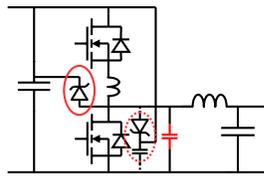




# Schottky Clamp

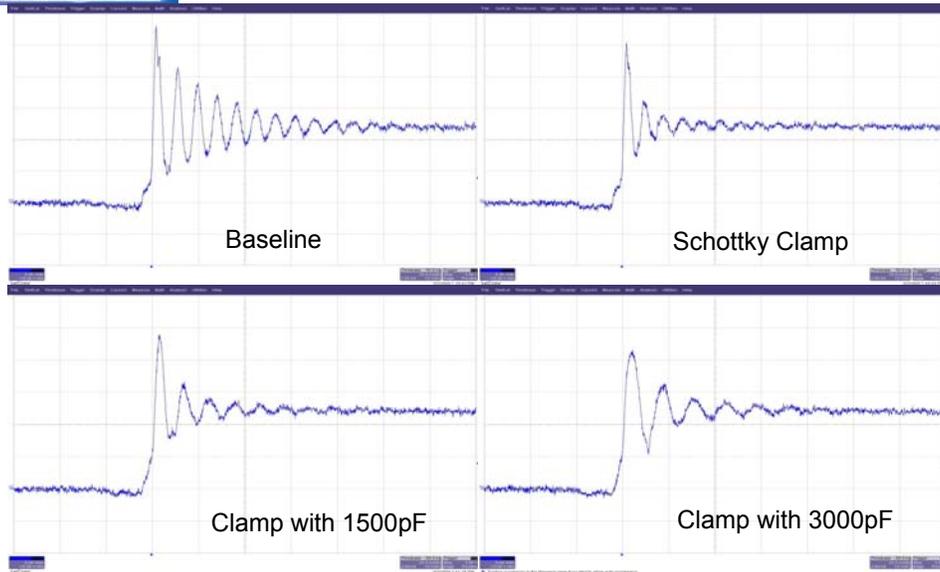


Buck Converter  
DC Loop and associated  
stray inductances in red



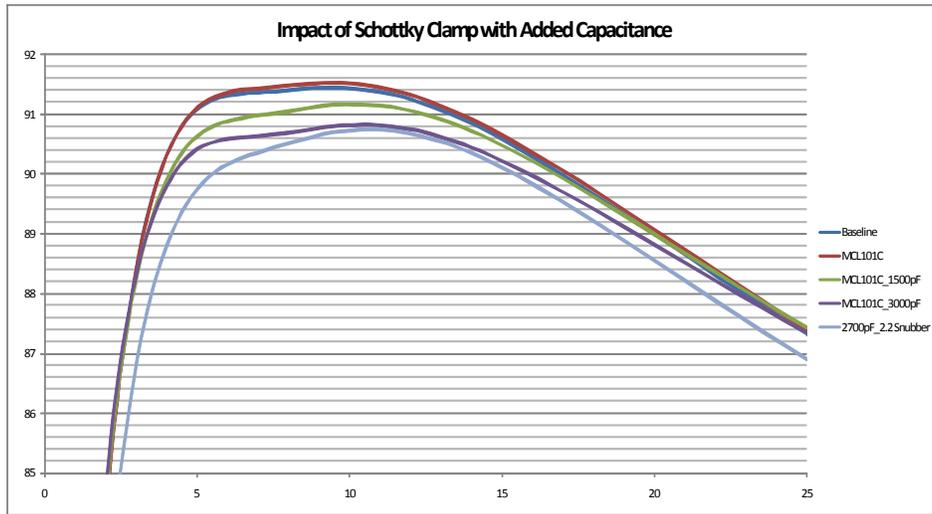


# Switchnode Waveforms





# Efficiency – Standard Demo Board

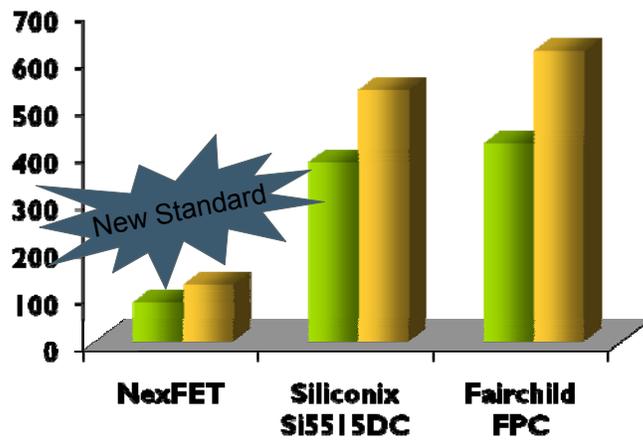




# P-Channel DC-DC Switch

6+ Year Technology Lead

■  $R(4.5)*Q_g$  ■  $R(2.5)*Q_g$



$BV_{DSS} = 20V$





# P-Ch devices





# Wafer Level Package vs Industry Std Packages

SOT-23



7.8mm<sup>2</sup>

25mΩ

Si2333

~8x Footprint Reduction  
~2x Resistance

Ciclon WLP

SC-70



4.2 mm<sup>2</sup>

70mΩ

Si1417

4x Footprint Reduction  
Same Resistance



SC-89



2.56 mm<sup>2</sup>

108mΩ

Si1065

2.5x Footprint Reduction  
~ 1/2 Resistance

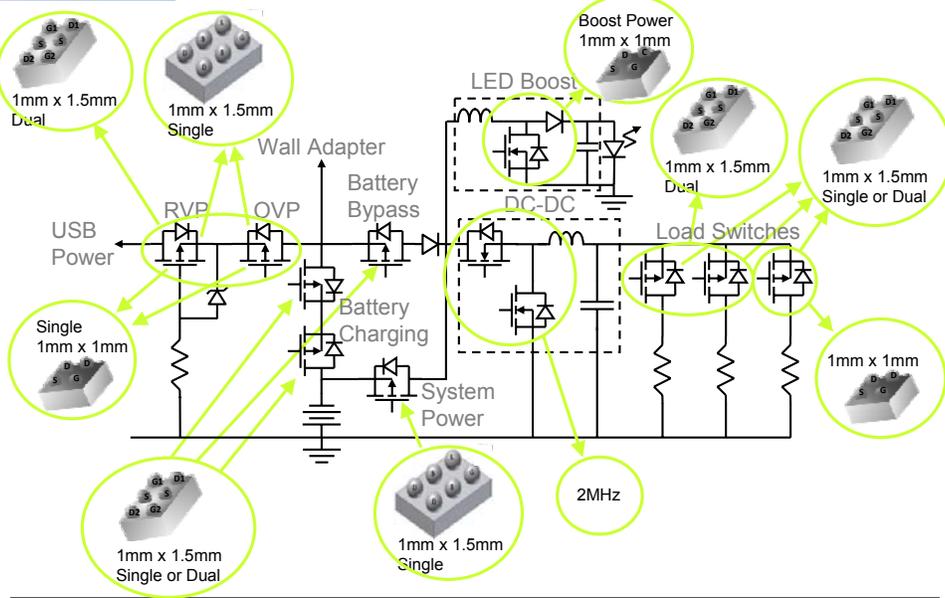
1mm<sup>2</sup>

66mΩ

CSD23201



# Saving Space & Cost

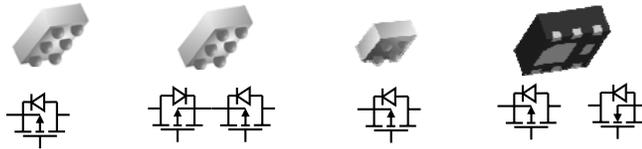




# NexFET Discrete Products

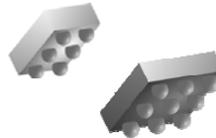
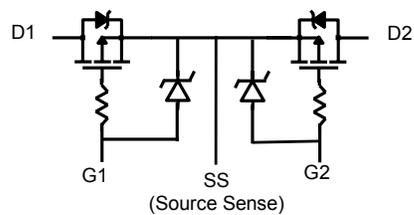
	CSD25301W1015	CSD75301W1015	CSD23201W10	CSD16301Q2* CSD25302Q2*
	Single P	Dual P Common Source	Single P	Single N & Single P 1MHz
	1mm x 1.5mm WLP	1mm x 1.5mm WLP	1mm x 1mm WLP	2mm x 2mm QFN
$BV_{DS}$	-20V	-20V	-12V	+25V / -20V
$V_{GS}$	8V	8V	5V	8V
	$R_{DS(on)}$ typical	$R_{DS(on)}$ Typical	$R_{DS(on)}$ typical	$R_{DS(on)}$ typical
4.5V	62m $\Omega$	80m $\Omega$	66m $\Omega$	28/39m $\Omega$
2.5V	80m $\Omega$	101m $\Omega$	77m $\Omega$	36/56m $\Omega$
1.5V	175m $\Omega$	165m $\Omega$ @ 1.8V	110m $\Omega$	Qg 1.9/2.7nC

\* - in development





# Dual Common Source with Clamp Diode

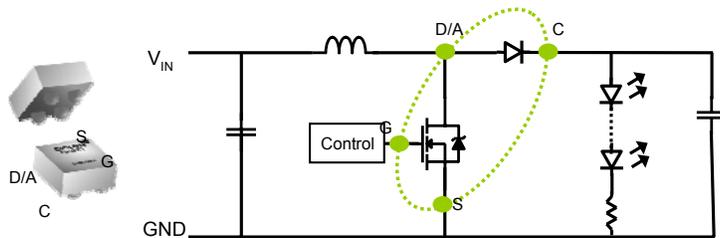


Part Number	Package	$BV_{D1/D2}$	$R_{DD}@4.5V$	$R_{DD}@2.5$	Gate Clamp $BV_{GSS}$	Gate ESD	Samples	Prod
CSD75204W15	WLP 1.5x1.5	20V	100mΩ (50mΩ each)	130mΩ (65mΩ each)	6.1V min	3kV	Now	Q2 CY09
CSD75205W1015	WLP 1x1.5	20V	144mΩ (77mΩ each)	190mΩ (95mΩ each)		3kV	Now	Q2 CY09





# Small Scale Integration Monolithic Boost LED Power Stage

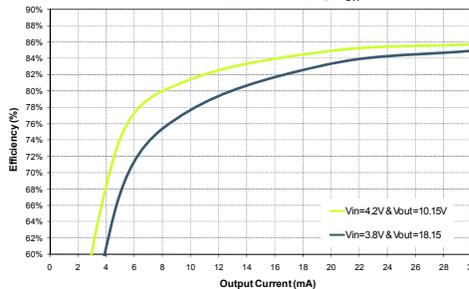


Up to 4x  
Smaller

## 24V Power Stage

Part Number	Function	BV <sub>DSS</sub>	V <sub>GS</sub>	R <sub>DS(on)</sub> @4.5V
CSD86301W10	Power Stage	24V	+10V/-6V	315mΩ
Q <sub>g</sub> @4.5V	Q <sub>gd</sub>	V <sub>F</sub> @ 20mA	Leakage @25°C	Package Size
0.14nC	0.03nC	0.59V	1μA	1mm x 1mm

Ciclon Boost Power Stage Efficiency @ F<sub>sw</sub> = 1MHz

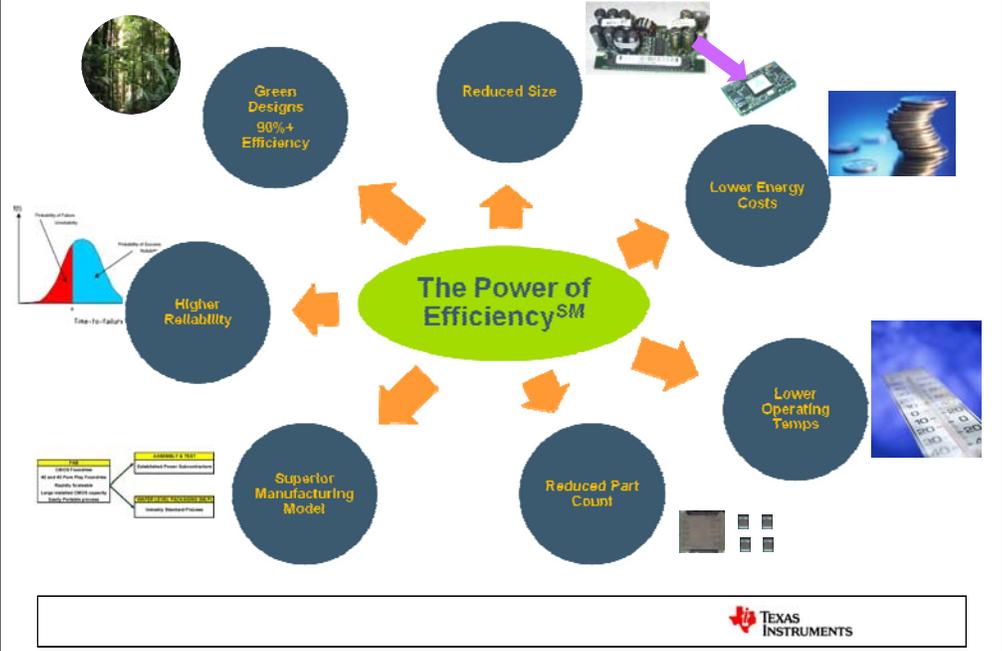




## *Unique* NexFET Technology Capabilities

- **Extremely low charge MOSFETs with low resistance**
  - RF Power LDMOS structure with vertical current flow
  - Enables higher switching frequency and high current
- **Low voltage gate drive capabilities**
  - Low loss high switching frequency
  - Planar gate. Using standard CMOS Gate Oxides
- **Enables integration in a cost effective process**
  - Planar structure
  - Chip scale packages
- **Technology in early stage of maturity**
  - In infancy leading 20 years of trench development

# Summary





**THANK YOU!!**

