

Power management integrated buck controllers for distant point-of-load applications



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Power management integrated circuits (PMICs) are capable of powering multiple processors and FPGAs with flexibility and programmability in individual supply voltages for efficient power management in aggressive dynamic voltage scaling (DVS) environments.

The power-management integrated circuit (PMIC) is a cost-effective power-supply solution for applications that requires multiple power-supply rails. PMICs are commonly used to for system level power including processor, FPGA and peripheral power. Typical applications include personal electronics devices, industrial devices, automotive devices and much more. PMICs typically consist of multiple supply rails powered by buck/boost converters, buck controllers, low-dropout regulators and others. Because PMICs combine multiple supply rails into a single IC, external components required by individual regulators such as capacitors, inductors and power MOSFETs need to be well-managed in a printed circuit board (PCB) design and layout. Along with the PMIC, you need to identify potential solutions close to specific bias power requirements. References to sample designs and resources are provided in this paper to get designers up and running with isolated power solutions for their systems.

There is a common misperception regarding placement in that all external components need to be placed close to the PMIC. This leads to a belief that design with PMICs are restrictive and inflexible, especially for very-high-power integrated power controllers used for distant point-of-load (POL) applications. However, in reality, this is not necessarily true. This paper discusses PCB design and layout strategies for integrated buck controllers to better manage external-component placement and enable a more cost-effective solution for distant POL conditions.

Buck controller

Figure 1 shows a typical buck controller block diagram. External components typically consist of single or multiple input capacitors (C_{IN}), single or multiple output capacitors (C_{OUT}), and an output inductor (L_{OUT}). Additionally, it requires two external power MOSFETs (M_{HSD} and M_{LSD}) and a bootstrap capacitor (C_{BOOT}) for the high-side drive. Since buck controllers are typically designed for high-power applications, it is best to keep the power train (M_{HSD} , M_{LSD} , C_{IN} , L_{OUT} , and C_{OUT}) very close to the POL to achieve optimal efficiency. However, the controller IC need not be placed very close to the power train to achieve good performance.

Based on the application, certain layout strategies can achieve less-restrictive placement of the IC. The following section discusses the function and placement of the external components and IC along with PCB layout strategies.

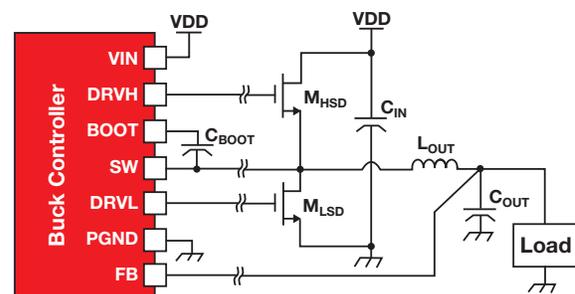


Figure 1. Typical buck controller block diagram and external components.

Power MOSFETs, input capacitor, output inductor and output capacitor considerations

Power MOSFETs, input capacitors, output inductors, and output capacitors form the power train of a buck controller. The input capacitor acts as a local power supply, the output inductor and capacitor function as a low-frequency filter, and power MOSFETs perform switching power conversion. All of these components need to be placed close together on the PCB to achieve reliable and efficient performance. As mentioned earlier, buck controllers are typically used for high-power applications. Therefore, it's best to keep the power train close to the POL to minimize power loss. However, the controller IC can be placed relatively further away from these components, as long as proper layout guidelines are followed to route the high-side driver (DRVH), low-side driver (DRVL) and switching (SW) signals.

Layout routing strategies

The route length of DRVH and DRVL signals determines how far away the PMIC can be placed from the POL. As long as the integrity of these two signals are maintained, the controller will not experience any performance degradations. In particular, if the DRVH and DRVL signals are distorted enough to turn on the high-side-drive (HSD) FET and low-side-drive (LSD) FET at the same time, there will be reliability or power loss issues due to cross-conduction. Since DRVH and DRVL are high-speed gate drive signals with fast slew rates, their routings have to be treated as transmission lines in the PCB layout to maintain good signal integrity.

DRVH and DRVL signal routings can be modeled as shown in **Figure 2**. Note that the return path for the DRVH signal is the SW signal; for the DRVL signal the return path is the power ground (PGND).

In the case of long transmission-line routings, the most straightforward and cost-effective strategy is to adopt a microstrip-line layout technique, or strip-line layout technique, to control the line impedance.

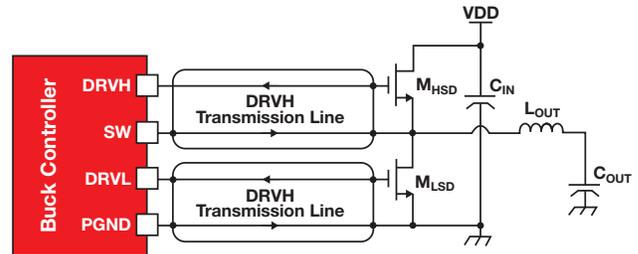


Figure 2. High-side drive (DRVH) and low-side drive (DRVL) as transmission lines.

Figure 3 illustrates PCB cross-sections for microstrip-line and strip-line routings. The microstrip-line method is good for routing signals at the top PCB layer, while the strip-line method is good for routing signals in the inner layer of the PCB. **Table 1** shows typical PCB parasitics for a microstrip line.

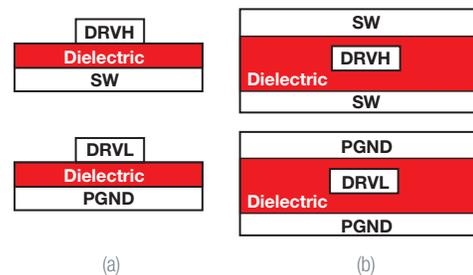


Figure 3. High-side drive (DRVH) and low-side drive (DRVL) PCB routing cross-section (a) microstrip line (b) strip line.

In order to demonstrate the effectiveness of the layout strategies discussed here, the TPS650860, a PMIC with three controllers and three converters is used to simulate a typical use case scenario. Simulation with estimated PCB parasitics from **Table 1** and the power FET model for the CSD87381P confirm that the PMIC controller can be easily placed 11 inches away from the POL.

Figure 4 depicts transmission-line models for DRVH and DRVL, where the SW plane is modeled to be four times wider than the DRVH line, and the PGND is modeled as a low-impedance ground plane. Simulation results shown in **Figure 5** compare the gate-source voltages of the power FETs in two scenarios. In the first case, power-train components are placed very close to the PMIC (<1 inch). In the second case, power-train components are placed close to the POL and 11 inches away from the PMIC. In this scenario, 11-inch microstrip lines are used to route gate-drive signals.

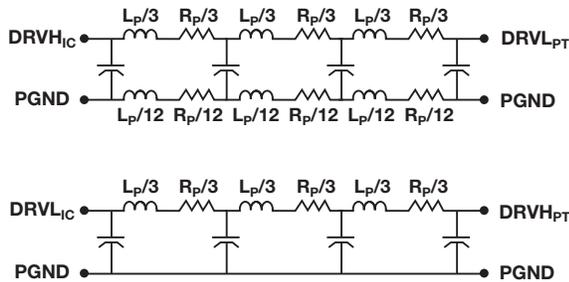


Figure 4. Transmission-line model used in the simulation.

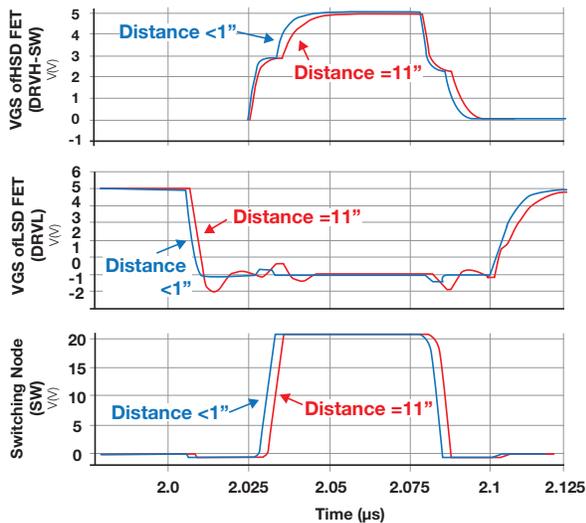


Figure 5. Simulation results of the controller placed less than one inch from the power train and POL, versus 11 inches.

Based on the simulation results, scenario two (**Figure 3b**) has a few more nanoseconds delay versus scenario one (**Figure 3a**), which has very

short routing for gate-drive signals. This extra delay time is caused by the delay experienced by the gate-drive signals through the transmission line. Further, the rise and fall times for the HSD gate signal (DRVH-SW) of the second scenario are slightly higher, but not significantly different from scenario one. The DRVL signal has minor overshoots and undershoots; these are as expected when a signal travels through a long transmission line. These overshoot levels are not severe enough to turn on the LSD MOSFET to pose any significant performance issues.

| Length (inches) | Width (mils) | Copper thickness | Inductance LP (nH) | Capacitance CP (pF) | Resistance RP (mΩ) |
|-----------------|--------------|------------------|--------------------|---------------------|--------------------|
| 4 | 20 | 1/2 oz | 1.5 | 200 | 200 |
| 7 | 20 | 1/2 oz | 2.6 | 300 | 290 |
| 11 | 20 | 1/2 oz | 4.0 | 560 | 550 |

Table 1. Typical microstrip line parasitic with return path modeled as a plane.

Bootstrap capacitor consideration

The function of the bootstrap capacitor is to act as a floating local power supply for the DRVH driver; therefore, the preferred placement is close to the controller IC. The routing resistance of the bootstrap capacitor will affect the charging time of the DRVH signal, so the routing resistance has to be maintained at around 100 mΩ. **Figure 6** illustrates the parasitic routing resistance, where R_{PARA} is a model of parasitic resistance and DRVH is the current drawn to turn on the HSD MOSFET.

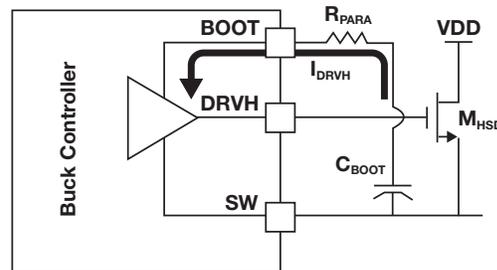


Figure 6. DRVH buffer with bootstrap capacitor with PCB routing parasitic.

Summary

Not all external components for an integrated buck controller need to be placed close to the PMIC. The power-train components can be placed close to the POL, as long as the layout guidelines presented in this paper are implemented. Texas Instruments PMICs with integrated buck controllers include the TPS65911 and TPS650680.

To use controllers as an effective solution for distant POL applications, key PCB layout concerns include:

- Placing the input capacitor and power FETs close to each other to achieve maximum reliable performance.
- Placing the inductor and output capacitor close to the FETs and input capacitor to achieve maximum power efficiency.
- Placing power-train components, including power FETs, inductors and input/ output capacitors at the POL.
- Treating DRVH and DRVL routings as transmission lines. Microstrip-line and strip-line layout techniques achieve the best performance.
- Placing the bootstrap capacitor close to the PMIC to maintain drive capability for DRVH.

References

Learn more about [power management multi-channel IC \(PMIC\) solutions](#)

Product folders: [CSD87381P](#), [TPS65911](#), [TPS650860](#)

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