











SN65MLVD204B

ZHCSFW4A - NOVEMBER 2015-REVISED DECEMBER 2016

# SN65MLVD204B 具有 IEC ESD 保护的多点 LVDS 线路驱动器和接收器 (收发器)

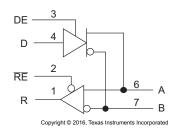
#### 1 特性

- 符合 M-LVDS 标准 TIA/EIA-899,适用于多点数据交换
- 低压差分  $30\Omega$  至  $55\Omega$  线路驱动器和接收器,适用于高达 100Mbps 的信号传输速率  $^{(1)}$ 、高达 50MHz 的时钟频率
  - 1 类接收器整合了 25mV 迟滞(200B 和 202B)
  - 2 类接收器可提供一个偏移阈值来检测开路和空 闲总线条件(204B 和 205B)
- 总线 I/O 保护
  - >±8kV HBM
  - >±8kV IEC 61000-4-2 接触放电
- 可控的驱动器输出电压转换时间可改进信号质量
- -1V 至 3.4V 共模电压范围允许在 2V 接地噪声下传输数据
- 总线引脚在禁用或 V<sub>CC</sub> ≤ 1.5V 时具有高阻抗
- 提供 200Mbps 器件(SN65MLVD201、203、 206、207)
- 是 SN65MLVD200A、202A、204A 和 205A 的改进替代方案
- (1) 线路的信号传输速率是指每秒钟的电压转换次数,单位为 bps (每秒比特数)

#### 2 应用

- 低功耗、高速和短行程 可替代 TIA/EIA-485
- 背板或电缆连接的多点数据和时钟传输
- 蜂窝基站
- 局端交換机
- 网络交换机和路由器

#### 简化电路原理图 SN65MLVD200B、SN65MLVD204B



#### 3 说明

SN65MLVD200B、SN65MLVD202B、

SN65MLVD204B 和 SN65MLVD205B 器件均为多点低压差分 (M-LVDS) 线路驱动器和接收器,它们均经过优化,支持的信号传输速率可高达 100Mbps。此器件系列将强大的 3.3V 驱动器和接收器整合在标准小外形尺寸集成电路 (SOIC) 封装中,适用于要求严格的工业应用。总线引脚可耐受 ESD 事件,具有针对人体模型和 IEC 接触放电规范的高级保护。

这些器件的每一个都组装有一个差分驱动器和一个差分接收器(收发器),这两个器件由一个 3.3V 单电源供电运行。收发器经过优化,支持的信号传输速率可高达100Mbps。

SN65MLVD20xB 较同类器件具有更多增强特性。这些增强特性包括驱动器输出端转换率可控,有助于尽量减少无端桩线的反射,从而提高信号完整性。保持了相同尺寸,可轻松替换,有助于提升系统性能。这些器件的额定工作温度范围为 -40°C 至 85°C。

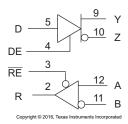
SN65MLVD20xB M-LVDS 收发器属于 TI 广泛的 M-LVDS 产品组合。

#### 器件信息<sup>(1)</sup>

器件型号	封装	封装尺寸 (标称值)	
SN65MLVD200B	COIC (0)	4.00	
SN65MLVD204B	SOIC (8)	4.90mm x 3.91mm	
SN65MLVD202B	COIC (44)	0.65mm v 2.04mm	
SN65MLVD205B	SOIC (14)	8.65mm x 3.91mm	

(1) 要了解所有可用封装,请参见数据表末尾的可订购产品附录。

#### 简化电路原理图 SN65MLVD202B、SN65MLVD205B





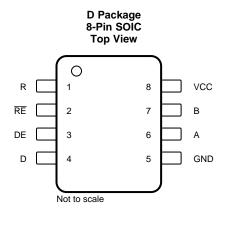
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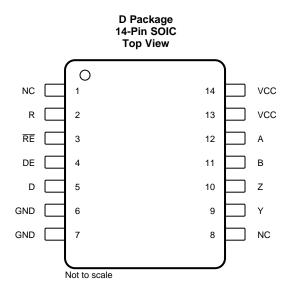
# 4 修订历史记录

Cł	hanges from Original (November 2015) to Revision A	Page
•	器件状态从预览更改为量产	1



#### 5 Pin Configuration and Functions





#### **Pin Functions**

	PIN		TVDE	DECORPORTOR
NAME	D8 NO.	D14 NO.	TYPE	DESCRIPTION
Α	6	12	I/O	Differential I/O
В	7	11	I/O	Differential I/O
D	4	5	Input	Driver input
DE	3	4	Input	Driver enable pin; High = Enable, Low = Disable
GND	5	6, 7	Power	Supply ground
NC	_	1, 8	NC	No internal connection
R	1	2	Output	Receiver output
RE	2	3	Input	Receiver enable pin; High = Disable, Low = Enable
$V_{CC}$	8	13, 14	Power	Power supply, 3.3 V
Υ	_	9	I/O	Differential I/O
Z	_	10	I/O	Differential I/O

# 6 Specifications

#### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Supply voltage range, V <sub>CC</sub> <sup>(2)</sup>		-0.5	4	V
	D, DE, RE	-0.5	4	V
Input voltage range	A, B (200B, 204B)	-1.8	4	V
	A, B (202B, 205B)	-4	6	
Output valta as vasas	R	-4 6 -0.3 4	V	
Output voltage range	A, B, Y or Z	-1.8	4	V
Continuous power dissipation	us power dissipation See the <i>Thermal Information</i> table			tion table
Storage temperature, T <sub>stg</sub> -65 150				°C

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values, except differential I/O bus voltages, are with respect to network ground terminal.



#### 6.2 ESD Ratings

				VALUE	UNIT
V <sub>(ESD)</sub>	Contact discharge, per IEC 61000-4-2  Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins  Charged device model (CDM), per JEDEC specification JESD22-C101, all pins	Contact discharge, per IEC 61000-4-2	A, B, Y and Z	±8000	
		A, B, Y and Z	±8000		
		, ,,,,	All pins except A, B, Y and Z	±4000	V
			All pins	±1500	

# 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
$V_{CC}$	Supply voltage	3	3.3	3.6	V
$V_{IH}$	High-level input voltage	2		$V_{CC}$	V
$V_{IL}$	Low-level input voltage	GND		8.0	V
	Voltage at any bus terminal V <sub>A</sub> , V <sub>B</sub> , V <sub>Y</sub> or V <sub>Z</sub>	-1.4		3.8	V
$ V_{ID} $	Magnitude of differential input voltage			$V_{CC}$	V
$R_L$	Differential load resistance	30	50		Ω
1/t <sub>UI</sub>	Signaling rate			100	Mbps
T <sub>A</sub>	Operating free-air temperature	-40		85	°C

#### 6.4 Thermal Information

V. <del>T</del> 111				
		SN65MLVD200B SN65MLVD204B	SN65MLVD202B SN65MLVD205B	
THERMAL METRIC <sup>(1)</sup>		D (SOIC)	D (SOIC)	UNIT
		8 PINS	14 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	112.2	87.4	
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	56.7	46.6	
$R_{\theta JB}$	Junction-to-board thermal resistance	52.8	42	°C/W
ΨЈТ	Junction-to-top characterization parameter	10.3	11.3	
ΨЈВ	Junction-to-board characterization parameter	52.3	71.7	

<sup>(1)</sup> For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

#### 6.5 Electrical Characteristics

over recommended operating conditions (unless otherwise noted)<sup>(1)</sup>

PARAMETER		ΓER	TEST CONDITIONS		TYP	MAX	UNIT
I <sub>CC</sub>	Supply current	Driver only	$\overline{\text{RE}}$ and DE at V <sub>CC</sub> , R <sub>L</sub> = 50 $\Omega$ , All others open		13	22	
		Both disabled	$\overline{RE}$ at $V_{CC}$ , DE at 0 V, $R_L$ = No Load, All others open		1	4	mΛ
		Both enabled	$\overline{\text{RE}}$ at 0 V, DE at V <sub>CC</sub> , R <sub>L</sub> = 50 $\Omega$ , All others open		16	24	mA
		Receiver only	RE at 0 V, DE at 0 V, All others open		4	13	
P <sub>D</sub> Device power dissipation		sipation	$R_L$ = 50 Ω, Input to D is a 50-MHz 50% duty cycle square wave, DE = high, $\overline{RE}$ = low, $T_A$ = 85°C			100	mW

(1) All typical values are at 25°C and with a 3.3-V supply voltage.



#### 6.6 Electrical Characteristics – Driver

over recommended operating conditions unless otherwise noted

	PARAMETER	TEST CONDITIONS	MIN <sup>(1)</sup>	TYP <sup>(2)</sup> MAX	UNIT
V <sub>AB</sub>   or  V <sub>YZ</sub>	Differential output voltage magnitude (3)	See № 3	480	650	mV
$\Delta  V_{AB} $ or $\Delta  V_{YZ} $	Change in differential output voltage magnitude between logic states	See 🗈 S	-50	50	mV
V <sub>OS(SS)</sub>	Steady-state common-mode output voltage		0.8	1.2	<b>V</b>
$\Delta V_{OS(SS)}$	Change in steady-state common-mode output voltage between logic states	See 图 4	-50	50	mV
V <sub>OS(PP)</sub>	Peak-to-peak common-mode output voltage			150	mV
$V_{Y(OC)}$ or $V_{A(OC)}$	Maximum steady-state open-circuit output voltage	See № 8	0	2.4	<b>V</b>
$V_{Z(OC)}$ or $V_{B(OC)}$	Maximum steady-state open-circuit output voltage	See 🖸 o	0	2.4	V
$V_{P(H)}$	Voltage overshoot, low-to-high level output	See 图 6		1.2 V <sub>SS</sub>	٧
$V_{P(L)}$	Voltage overshoot, high-to-low level output	See 🖸 0	$-0.2~\mathrm{V_{SS}}$		٧
I <sub>IH</sub>	High-level input current (D, DE)	$V_{IH} = 2 V \text{ to } V_{CC}$	0	10	μΑ
I <sub>IL</sub>	Low-level input current (D, DE)	$V_{IL}$ = GND to 0.8 V	0	10	μΑ
I <sub>OS</sub>	Differential short-circuit output current magnitude	See 图 5		24	mA
I <sub>OZ</sub>	High-impedance state output current (driver only)	$-1.4 \text{ V} \le (\text{V}_{\text{Y}} \text{ or } \text{V}_{\text{Z}}) \le 3.8 \text{ V},$ Other output = 1.2 V	-15	10	μΑ
I <sub>O(OFF)</sub>	Power-off output current	$-1.4 \text{ V} \le (V_{\text{Y}} \text{ or } V_{\text{Z}}) \le 3.8 \text{ V}, \text{ Other}$ output = 1.2 V, 0 V $\le$ V <sub>CC</sub> $\le$ 1.5 V	-10	10	μΑ
C <sub>Y</sub> or C <sub>Z</sub>	Output capacitance	$V_I = 0.4 \sin(30E6\pi t) + 0.5 V$ , (4) Other input at 1.2 V, driver disabled		3	pF
C <sub>YZ</sub>	Differential output capacitance	$V_{AB} = 0.4 \sin(30E6\pi t) \text{ V, }^{(4)}$ Driver disabled		2.5	pF
C <sub>Y/Z</sub>	Output capacitance balance, (C <sub>Y</sub> /C <sub>Z</sub> )		0.99	1.01	pF

The algebraic convention in which the least positive (most negative) limit is designated as minimum is used in this data sheet. All typical values are at 25°C and with a 3.3-V supply voltage.

Measurement equipment accuracy is 10 mV at -40°C

HP4194A impedance analyzer (or equivalent)

<sup>(2)</sup> 

<sup>(3)</sup> (4)



#### 6.7 Electrical Characteristics - Receiver

over recommended operating conditions unless otherwise noted

	PARAMETER		TEST CONDITIONS	MIN	TYP <sup>(1)</sup>	MAX	UNIT
.,	Positive-going differential input voltage	Type 1				50	mV
V <sub>IT+</sub>	threshold (2)	Type 2				150	IIIV
V	Negative-going differential input voltage	Type 1	一 ─ See 图 10, 表 1, and 表 2	-50			mV
V <sub>IT-</sub>	threshold (2)	Type 2	See & 10, to 1, and to 2	50			IIIV
\/	Differential input valtege by storesia (// // )	Type 1			25		mV
V <sub>HYS</sub>	Differential input voltage hysteresis, $(V_{IT+} - V_{IT-})$	Type 2			0		IIIV
$V_{OH}$	High-level output voltage (R)		$I_{OH} = -8 \text{ mA}$	2.4			V
V <sub>OL</sub>	Low-level output voltage (R)		I <sub>OL</sub> = 8 mA			0.4	V
I <sub>IH</sub>	High-level input current (RE)		V <sub>IH</sub> = 2 V to V <sub>CC</sub>	-10		0	μΑ
I <sub>IL</sub>	Low-level input current (RE)		V <sub>IL</sub> = GND to 0.8 V	-10		0	μΑ
l <sub>OZ</sub>	High-impedance output current (R)		V <sub>O</sub> = 0 V or 3.6 V	-10		15	μΑ
C <sub>A</sub> or C <sub>B</sub>	Input capacitance		$V_I = 0.4 \sin(30E6\pi t) + 0.5 V^{(3)}$ , Other input at 1.2 V		3		pF
C <sub>AB</sub>	Differential input capacitance		$V_{AB} = 0.4 \sin(30E6\pi t) V^{(3)}$			2.5	рF
C <sub>A/B</sub>	Input capacitance balance, (C <sub>A</sub> /C <sub>B</sub> )			0.99		1.01	pF

- (1) All typical values are at 25°C and with a 3.3-V supply voltage.
- (2) Measurement equipment accuracy is 10 mV at -40°C
- (3) HP4194A impedance analyzer (or equivalent)

#### 6.8 Electrical Characteristics - BUS Input and Output

over recommended operating conditions unless otherwise noted

	PARAMETER	TEST CONDITIONS	MIN	TYP <sup>(1)</sup> MAX	UNIT
		$V_A = 3.8 \text{ V}, \qquad \qquad V_B = 1.2 \text{ V},$	0	32	
I <sub>A</sub>	Receiver or transceiver with driver disabled input current	$V_A = 0 \text{ V or } 2.4 \text{ V}, \qquad V_B = 1.2 \text{ V}$	-20	20	μΑ
		$V_A = -1.4 \text{ V}, \qquad \qquad V_B = 1.2 \text{ V}$	-32	0	
		$V_B = 3.8 \text{ V}, \qquad V_A = 1.2 \text{ V}$	0	32	
I <sub>B</sub>	Receiver or transceiver with driver disabled input current	$V_B = 0 \text{ V or } 2.4 \text{ V}, \qquad V_A = 1.2 \text{ V}$	-20	20	μΑ
		$V_B = -1.4 \text{ V}, \qquad \qquad V_A = 1.2 \text{ V}$	-32	0	
I <sub>AB</sub>	Receiver or transceiver with driver disabled differential input current $(I_A - I_B)$	$V_A = V_{B_1}$	-4	4	μΑ
		$V_A = 3.8 \text{ V}, \qquad \qquad V_B = 1.2 \text{ V}, \qquad 0 \text{ V} \le V_{CC} \le 1.5 \text{ V}$	0	32	
I <sub>A(OFF)</sub>	Receiver or transceiver power-off input current	$V_A = 0 \text{ V or } 2.4 \text{ V}, \qquad V_B = 1.2 \text{ V}, \qquad 0 \text{ V} \leq V_{CC} \leq 1.5 \text{ V}$	-20	20	μΑ
		$V_{A} = -1.4 \text{ V}, \hspace{1cm} V_{B} = 1.2 \text{ V}, \hspace{1cm} 0 \text{ V} \leq V_{CC} \leq 1.5 \text{ V}$	-32	0	
		$V_B = 3.8 \text{ V}, \qquad \qquad V_A = 1.2 \text{ V}, \qquad 0 \text{ V} \leq V_{CC} \leq 1.5 \text{ V}$	0	32	
I <sub>B(OFF)</sub>	Receiver or transceiver power-off input current	$V_B = 0 \text{ V or } 2.4 \text{ V}, \qquad V_A = 1.2 \text{ V}, \qquad 0 \text{ V} \le V_{CC} \le 1.5 \text{ V}$	-20	20	μΑ
		$V_B = -1.4 \text{ V}, \qquad \qquad V_A = 1.2 \text{ V}, \qquad 0 \text{ V} \le V_{CC} \le 1.5 \text{ V}$	-32	0	
I <sub>AB(OFF)</sub>	Receiver input or transceiver power-off differential input current $(I_A - I_B)$	$V_A = V_B, \ 0 \ V \le V_{CC} \le 1.5 \ V, -1.4 \le V_A \le 3.8 \ V$	-4	4	μΑ
C <sub>A</sub>	Transceiver with driver disabled input capacitance	$V_A = 0.4 \sin (30E6\pi t) + 0.5 V^{(2)}, V_B = 1.2 V$		5	pF
Св	Transceiver with driver disabled input capacitance	$V_B = 0.4 \sin (30E6\pi t) + 0.5 V^{(2)}, V_A = 1.2 V$		5	pF
C <sub>AB</sub>	Transceiver with driver disabled differential input capacitance	V <sub>AB</sub> = 0.4 sin (30E6πt)V <sup>(2)</sup>		4	pF
C <sub>A/B</sub>	Transceiver with driver disabled input capacitance balance, (C <sub>A</sub> /C <sub>B</sub> )		0.99	1.01	pF

<sup>(1)</sup> All typical values are at 25°C and with a 3.3-V supply voltage.

<sup>(2)</sup> HP4194A impedance analyzer (or equivalent)



#### 6.9 Switching Characteristics – Driver

over recommended operating conditions unless otherwise noted

	PARAMETER	TEST CONDITIONS	MIN	TYP <sup>(1)</sup>	MAX	UNIT
t <sub>pLH</sub>	Propagation delay time, low-to-high-level output		2	2.5	3.5	ns
$t_{pHL}$	Propagation delay time, high-to-low-level output		2	2.5	3.5	ns
t <sub>r</sub>	Differential output signal rise time	See 图 6		2		ns
t <sub>f</sub>	Differential output signal fall time			2		ns
t <sub>sk(p)</sub>	Pulse skew ( t <sub>pHL</sub> - t <sub>pLH</sub>  )			30	150	ps
t <sub>sk(pp)</sub>	Part-to-part skew (2)				0.9	ns
t <sub>jit(per)</sub>	Period jitter, rms (1 standard deviation) <sup>(3)</sup>	50-MHz clock input <sup>(4)</sup>		2	3	ps
t <sub>jit(pp)</sub>	Peak-to-peak jitter <sup>(3)(5)</sup>	100 Mbps 2 <sup>15</sup> –1 PRBS input <sup>(6)</sup>		55	150	ps
t <sub>PHZ</sub>	Disable time, high-level-to-high-impedance output			4	7	ns
t <sub>PLZ</sub>	Disable time, low-level-to-high-impedance output	C @ 7		4	7	ns
t <sub>PZH</sub>	Enable time, high-impedance-to-high-level output	See 图 7		4	7	ns
t <sub>PZL</sub>	Enable time, high-impedance-to-low-level output			4	7	ns

- (1) All typical values are at 25°C and with a 3.3-V supply voltage.
- Part-to-part skew is defined as the difference in propagation delays between two devices that operate at the same V/T conditions.
- Jitter is ensured by design and characterization. Stimulus jitter has been subtracted from the numbers.
- $t_r = t_f = 0.5$  ns (10% to 90%), measured over 30K samples.
- (5) Peak-to-peak jitter includes jitter due to pulse skew (t<sub>sk(p)</sub>).
- (6)  $t_r = t_f = 0.5 \text{ ns } (10\% \text{ to } 90\%), \text{ measured over } 100\text{K samples.}$

#### 6.10 Switching Characteristics – Receiver

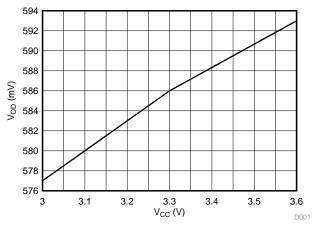
over recommended operating conditions unless otherwise noted

	PARAMETER		TEST CONDITIONS	MIN	TYP <sup>(1)</sup>	MAX	UNIT
t <sub>PLH</sub>	Propagation delay time, low-to-high-level output			2	6	10	ns
t <sub>PHL</sub>	Propagation delay time, high-to-low-level output			2	6	10	ns
t <sub>r</sub>	Output signal rise time					2.3	ns
t <sub>f</sub>	Output signal fall time		C <sub>L</sub> = 15 pF, See 图 11			2.3	ns
t <sub>sk(p)</sub> Pulse skew (	Dulgo alroys (It to 1)	Type 1			100	300	ps
	Pulse skew ( $ t_{pHL} - t_{pLH} $ )				400	750	ps
t <sub>sk(pp)</sub>	Part-to-part skew <sup>(2)</sup>					1	ns
t <sub>jit(per)</sub>	Period jitter, rms (1 standard deviation) (3)		50-MHz clock input <sup>(4)</sup>		2		ps
	2 1 (3) (5)	Type 1	100 Mbps 2 <sup>15</sup> –1 PRBS input <sup>(6)</sup>		200	700	ps
t <sub>jit(pp)</sub>	Peak-to-peak jitter <sup>(3)</sup> (5)	Type 2	100 Mibbs 2 - 1 FKB3 Iliput		225	800	ps
t <sub>PHZ</sub>	Disable time, high-level-to-high-impedance output				6	10	ns
t <sub>PLZ</sub>	Disable time, low-level-to-high-impedance output		See 图 12		6	10	ns
t <sub>PZH</sub>			See 🔯 12		10	15	ns
t <sub>PZL</sub>	Enable time, high-impedance-to-low-level output				10	15	ns

- All typical values are at 25°C and with a 3.3-V supply voltage.
- Part-to-part skew is defined as the difference in propagation delays between two devices that operate at the same V/T conditions.
- Jitter is ensured by design and characterization. Stimulus jitter has been subtracted from the numbers. (3)
- $V_{ID} = 200 \text{ mV}_{pp} \text{ (MLVD200B, 202B)}, V_{ID} = 400 \text{ mV}_{pp} \text{ (MLVD204B, 205B)}, V_{cm} = 1 \text{ V, } t_r = t_f = 0.5 \text{ ns (10\% to 90\%)}, \text{ measured over 30K}$
- (5) Peak-to-peak jitter includes jitter due to pulse skew (t<sub>sk(p)</sub>)
   (6) V<sub>ID</sub> = 200 mV<sub>pp</sub> (MLVD200B, 202B), V<sub>ID</sub> = 400 mV<sub>pp</sub> (MLVD204B, 205B), V<sub>cm</sub> = 1 V, t<sub>r</sub> = t<sub>f</sub> = 0.5 ns (10% to 90%), measured over 100K

# TEXAS INSTRUMENTS

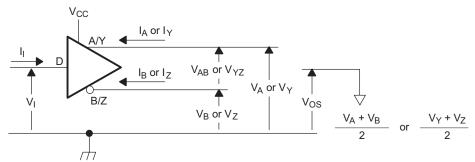
#### 6.11 Typical Characteristics



 $T_A = 25^{\circ}C$ 

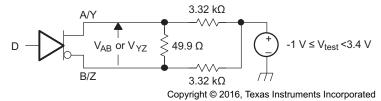
图 1. Differential Output Voltage vs Supply Voltage

# 7 Parameter Measurement Information



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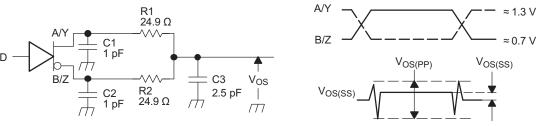
#### 图 2. Driver Voltage and Current Definitions



A. All resistors are 1% tolerance.

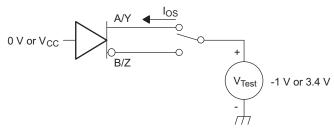
图 3. Differential Output Voltage Test Circuit





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- A. All input pulses are supplied by a generator having the following characteristics: t<sub>r</sub> or t<sub>f</sub>≤ 1 ns, pulse frequency = 1 MHz, duty cycle = 50 ± 5%.
- B. C1, C2 and C3 include instrumentation and fixture capacitance within 2 cm of the D.U.T. and are ±20%.
- C. R1 and R2 are metal film, surface mount, ±1%, and located within 2 cm of the D.U.T.
- D. The measurement of V<sub>OS(PP)</sub> is made on test equipment with a -3 dB bandwidth of at least 1 GHz.

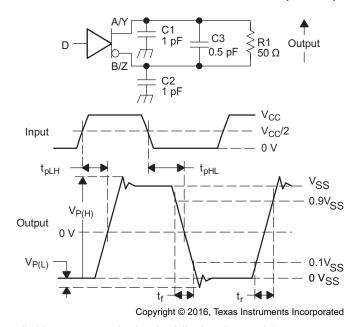
#### 图 4. Test Circuit and Definitions for the Driver Common-Mode Output Voltage



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图 5. Driver Short-Circuit Test Circuit

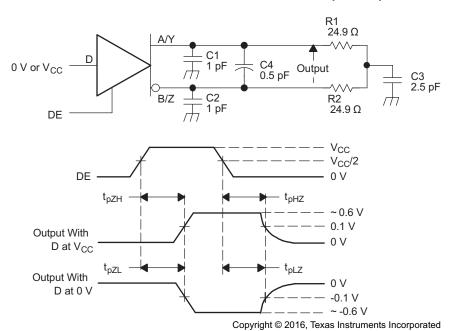




- A. All input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_l \le 1$  ns, frequency = 1 MHz, duty cycle = 50 ± 5%.
- B. C1, C2, and C3 include instrumentation and fixture capacitance within 2 cm of the D.U.T. and are ±20%.
- C. R1 is a metal film, surface mount, and 1% tolerance and located within 2 cm of the D.U.T.
- D. The measurement is made on test equipment with a -3 dB bandwidth of at least 1 GHz.

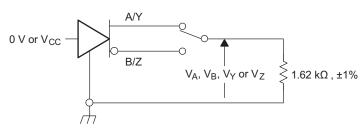
#### 图 6. Driver Test Circuit, Timing, and Voltage Definitions for the Differential Output Signal





- A. All input pulses are supplied by a generator having the following characteristics: t<sub>r</sub> or t<sub>f</sub>≤ 1 ns, frequency = 1 MHz, duty cycle = 50 ± 5%.
- B. C1, C2, C3, and C4 includes instrumentation and fixture capacitance within 2 cm of the D.U.T. and are ±20%.
- C. R1 and R2 are metal film, surface mount, and 1% tolerance and located within 2 cm of the D.U.T.
- D. The measurement is made on test equipment with a -3 dB bandwidth of at least 1 GHz.

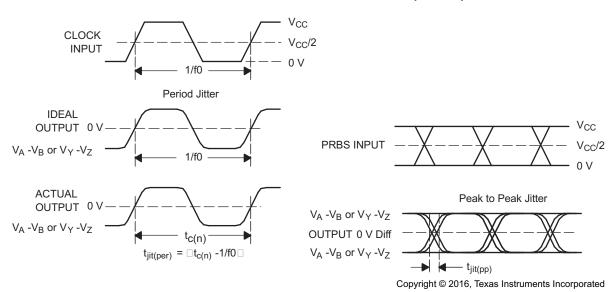
#### 图 7. Driver Enable and Disable Time Circuit and Definitions



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图 8. Maximum Steady State Output Voltage





- A. All input pulses are supplied by an Agilent 81250 Stimulus System.
- B. The measurement is made on a TEK TDS6604 running TDSJIT3 application software
- C. Period jitter is measured using a 100 MHz 50 ±1% duty cycle clock input.
- D. Peak-to-peak jitter is measured using a 100 Mbps 2<sup>15</sup>–1 PRBS input.

#### 图 9. Driver Jitter Measurement Waveforms

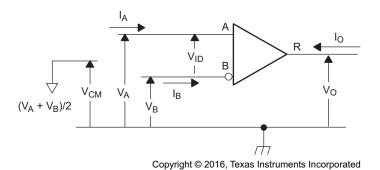


图 10. Receiver Voltage and Current Definitions



表 1	L	Type-1	Receiver	Input	<b>Threshold</b>	Test '	Voltages

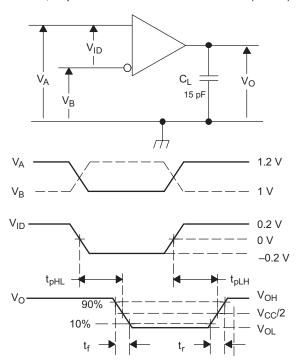
APPLIED V	OLTAGES	RESULTING DIFFERENTIAL INPUT VOLTAGE	RESULTING COMMON- MODE INPUT VOLTAGE	RECEIVER OUTPUT <sup>(1)</sup>
V <sub>IA</sub>	$V_{IB}$	V <sub>ID</sub>	V <sub>IC</sub>	OUIFUL
2.400	0.000	2.400	1.200	Н
0.000	2.400	-2.400	1.200	L
3.425	3.375	0.050	3.4	Н
3.375	3.425	-0.050	3.4	L
-0.975	-1.025	0.050	-1	Н
-1.025	-0.975	-0.050	-1	L

(1) H= high level, L = low level, output state assumes receiver is enabled ( $\overline{RE} = L$ )

表 2. Type-2 Receiver Input Threshold Test Voltages

APPLIED VOLTAGES		RESULTING DIFFERENTIAL INPUT VOLTAGE	RESULTING COMMON- MODE INPUT VOLTAGE	RECEIVER OUTPUT <sup>(1)</sup>
VIA	V <sub>IB</sub>	$V_{ID}$	V <sub>IC</sub>	OUTPUT
2.400	0.000	2.400	1.200	Н
0.000	2.400	-2.400	1.200	L
3.475	3.325	0.150	3.4	Н
3.425	3.375	0.050	3.4	L
-0.925	-1.075	0.150	<b>–1</b>	Н
-0.975	-1.025	0.050	<b>–1</b>	L

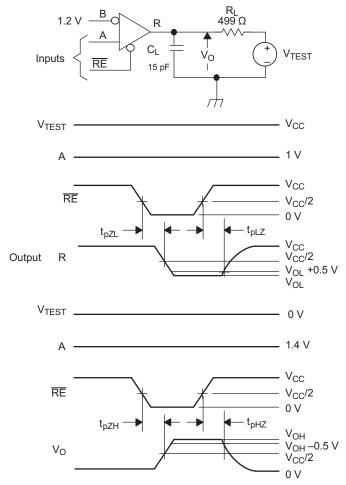
(1) H= high level, L = low level, output state assumes receiver is enabled ( $\overline{RE} = L$ )



- A. All input pulses are supplied by a generator having the following characteristics: t<sub>r</sub> or t<sub>f</sub> ≤ 1 ns, frequency = 1 MHz, duty cycle = 50 ± 5%. C<sub>L</sub> is a combination of a 20%-tolerance, low-loss ceramic, surface-mount capacitor and fixture capacitance within 2 cm of the D.U.T.
- B. The measurement is made on test equipment with a –3 dB bandwidth of at least 1 GHz.

#### 图 11. Receiver Timing Test Circuit and Waveforms

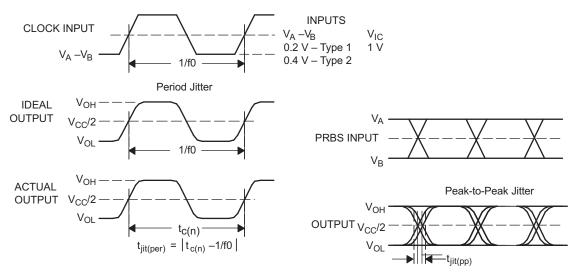




- A. All input pulses are supplied by a generator having the following characteristics:  $t_r$  or  $t_f \le 1$  ns, frequency = 1 MHz, duty cycle =  $50 \pm 5\%$ .
- B.  $R_L$  is 1% tolerance, metal film, surface mount, and located within 2 cm of the D.U.T.
- C.  $C_L$  is the instrumentation and fixture capacitance within 2 cm of the DUT and  $\pm 20\%$ .

#### 图 12. Receiver Enable and Disable Time Test Circuit and Waveforms





- A. All input pulses are supplied by an Agilent 8304A Stimulus System.
- B. The measurement is made on a TEK TDS6604 running TDSJIT3 application software
- C. Period jitter is measured using a 50 MHz 50 ±1% duty cycle clock input.
- D. Peak-to-peak jitter is measured using a 100 Mbps 2<sup>15</sup>-1 PRBS input.

图 13. Receiver Jitter Measurement Waveforms



#### 8 Detailed Description

#### 8.1 Overview

The SN65MLVD20xB family of devices are multipoint-low-voltage differential (M-LVDS) line drivers and receivers, which are optimized to operate at signaling rates up to 100 Mbps. All parts comply with the multipoint low-voltage differential signaling (M-LVDS) standard TIA/EIA-899. These circuits are similar to their TIA/EIA-644 standard compliant LVDS counterparts, with added features to address multipoint applications. The driver output has been designed to support multipoint buses presenting loads as low as 30  $\Omega$ , and incorporates controlled transition times to allow for stubs off of the backbone transmission line.

These devices have Type-1 and Type-2 receivers that detect the bus state with as little as 50 mV of differential input voltage over a common-mode voltage range of -1 V to 3.4 V. The Type-1 receivers exhibit 25 mV of differential input voltage hysteresis to prevent output oscillations with slowly changing signals or loss of input. Type-2 receivers include an offset threshold to provide a known output state under open-circuit, idle-bus, and other fault conditions.

#### 8.2 Functional Block Diagram

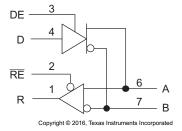


图 14. Block Diagram SN65MLVD200B, SN65MLVD204B

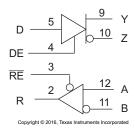


图 15. Block Diagram SN65MLVD202B, SN65MLVD205B

#### 8.3 Feature Description

#### 8.3.1 Power-On-Reset

The SN65MLVD20xB family of devices operates and meets all the specified performance requirements for supply voltages in the range of 3 V to 3.6 V. When the supply voltage drops below 1.5 V (or is turning on and has not yet reached 1.5 V), power-on reset circuitry set the driver output to a high-impedance state.

#### 8.3.2 ESD Protection

The bus terminals of the SN65MLVD20xB family possess on-chip ESD protection against ±8-kV human body model (HBM) and ±8-kV IEC61000-4-2 contact discharge. The IEC-ESD test is far more severe than the HBM-ESD test. The 50% higher charge capacitance, CS, and 78% lower discharge resistance, R<sub>D</sub> of the IEC model produce significantly higher discharge currents than the HBM-model.

As stated in the IEC 61000-4-2 standard, contact discharge is the preferred test method; although IEC air-gap testing is less repeatable than contact testing, air discharge protection levels are inferred from the contact discharge test results.



#### Feature Description (接下页)

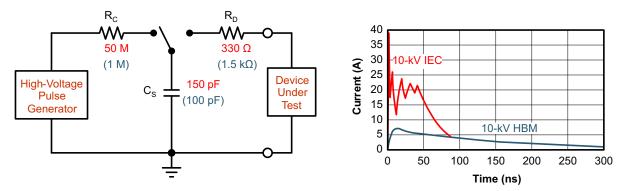


图 16. HBM and IEC-ESD Models and Currents in Comparison (HBM Values in Parenthesis)

#### 8.4 Device Functional Modes

#### 8.4.1 Operation with $V_{CC}$ < 1.5 V

Bus pins will be high impedance under this condition.

#### 8.4.2 Operations with 1.5 $V \le V_{CC} < 3 V$

Operation with supply voltages in the range of 1.5 V  $\leq$  V<sub>CC</sub> < 3 V is undefined and no specific device performance is guaranteed in this range.

#### 8.4.3 Operation with 3 V $\leq$ V<sub>CC</sub> < 3.6 V

Operation with the supply voltages greater than or equal to 3 V and less than or equal to 3.6 V is normal operation.

#### 8.4.4 Device Function Tables

表 3. Type-1 Receiver (200B and 202B)(1)

INPUTS	OUTPUT	
$V_{ID} = V_A - V_B$	RE	R
V <sub>ID</sub> ≥ 50 mV	L	Н
$-50 \text{ mV} < V_{\text{ID}} < 50 \text{ mV}$	L	?
V <sub>ID</sub> ≤ −50 mV	L	L
X	Н	Z
X	Open	Z

(1) H = high level, L = low level, Z = high impedance, X = Don't care, ? - indeterminate

表 4. Type-2 Receiver (204B and 205B)<sup>(1)</sup>

INPUTS	OUTPUT	
$V_{ID} = V_A - V_B$	RE	R
V <sub>ID</sub> ≥ 150 mV	L	Н
50 mV < V <sub>ID</sub> < 150 mV	L	?
V <sub>ID</sub> ≤ 50 mV	L	L
X	Н	Z
X	Open	Z

(1) H = high level, L = low level, Z = high impedance, X = Don't care, ? - indeterminate

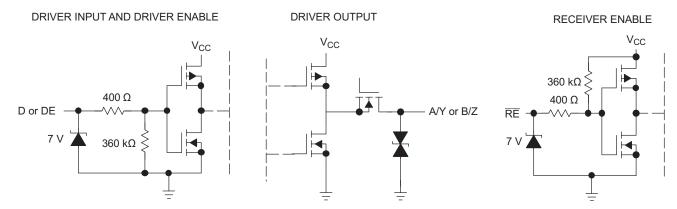


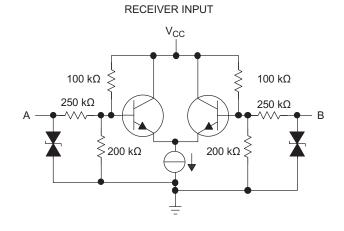
表 5. Driver<sup>(1)</sup>

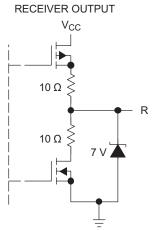
INPUTS	ENABLE	OUTPUTS			
D	DE	A	В		
L	Н	L	Н		
Н	Н	Н	L		
Open	Н	L	Н		
Х	Open	Z	Z		
Х	L	Z	Z		

(1) H = high level, L = low level, Z = high impedance, X = Don't care, ? - indeterminate

#### 8.4.5 Equivalent Input and Output Schematic Diagrams







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## 9 Application and Implementation

注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

#### 9.1 Application Information

The SN65MLVD20xB family of devices are multipoint line drivers and receivers. The functionality of these devices is simple, yet extremely flexible, leading to their use in designs ranging from wireless base stations to desktop computers.

#### 9.2 Typical Application

#### 9.2.1 Multipoint Communications

In a multipoint configuration many transmitters and many receivers can be interconnected on a single transmission line. The key difference compared to multi-drop is the presence of two or more drivers. Such a situation creates contention issues that need not be addressed with point-to-point or multidrop systems. Multipoint operation allows for bidirectional, half-duplex communication over a single balanced media pair. To support the location of the various drivers throughout the transmission line, double termination of the transmission line is now necessary.

The major challenge that system designers encounter are the impedance discontinuities that device loading and device connections (stubs) introduce on the common bus. Matching the impedance of the loaded bus and using signal drivers with controlled signal edges are the keys to error-free signal transmissions in multipoint topologies.

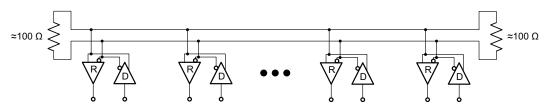


图 17. Multipoint Configuration

#### 9.2.2 Design Requirements

For this design example, use the parameters listed in 表 6.

#### 表 6. Design Parameters

PARAMETERS	VALUES
Driver supply voltage	3 to 3.6 V
Driver input voltage	0.8 to 3.3 V
Driver signaling rate	DC to 100 Mbps
Interconnect characteristic impedance	100 Ω
Termination resistance (differential)	100 Ω
Number of receiver nodes	2 to 32
Receiver supply voltage	3 to 3.6 V
Receiver input voltage	0 to (V <sub>CC</sub> – 0.8) V
Receiver signaling rate	DC to 100 Mbps
Ground shift between driver and receiver	±1 V



#### 9.2.3 Detailed Design Procedure

#### 9.2.3.1 Supply Voltage

The SN65MLVD20xB are operated from a single supply. The devices can support operation with a supply as low as 3 V and as high as 3.6 V.

#### 9.2.3.2 Supply Bypass Capacitance

Bypass capacitors play a key role in power distribution circuitry. At low frequencies, power supply offers very low-impedance paths between its terminals. However, as higher frequency currents propagate through power traces, the source is often incapable of maintaining a low-impedance path to ground. Bypass capacitors are used to address this shortcoming. Usually, large bypass capacitors (10  $\mu$ F to 1000  $\mu$ F) at the board level do a good job up into the kHz range. Due to their size and length of their leads, large capacitors tend to have large inductance values at the switching frequencies. To solve this problem, smaller capacitors (in the nF to  $\mu$ F range) must be installed locally next to the integrated circuit.

Multilayer ceramic chip or surface-mount capacitors (size 0603 or 0805) minimize lead inductances of bypass capacitors in high-speed environments, because their lead inductance is about 1 nH. For comparison purposes, a typical capacitor with leads has a lead inductance around 5 nH.

The value of the bypass capacitors used locally with M-LVDS chips can be determined by 公式 1 and 公式 2, according to *High Speed Digital Design – A Handbook of Black Magic* by Howard Johnson and Martin Graham (1993). A conservative rise time of 4 ns and a worst-case change in supply current of 100 mA covers the whole range of M-LVDS devices offered by Texas Instruments. In this example, the maximum power supply noise tolerated is 100 mV; however, this figure varies depending on the noise budget available for the design.

$$C_{chip} = \left(\frac{\Delta I_{Maximum Step Change Supply Current}}{\Delta V_{Maximum Power Supply Noise}}\right) \times T_{Rise Time}$$
(100 mA)

$$C_{\text{MLVDS}} = \left(\frac{100 \text{ mA}}{100 \text{ mV}}\right) \times 4 \text{ ns} = 0.004 \text{ }\mu\text{F}$$
(2)

 $\boxtimes$  18 shows a configuration that lowers lead inductance and covers intermediate frequencies between the board-level capacitor (>10  $\mu$ F) and the value of capacitance found above (0.004  $\mu$ F). Place the smallest value of capacitance as close as possible to the chip.



图 18. Recommended M-LVDS Bypass Capacitor Layout

#### 9.2.3.3 Driver Input Voltage

The input stage accepts LVTTL signals. The driver will operate with a decision threshold of approximately 1.4 V.

#### 9.2.3.4 Driver Output Voltage

The driver outputs a steady state common mode voltage of 1 V with a differential signal of 540 V under nominal conditions.



#### 9.2.3.5 Termination Resistors

As shown earlier, an M-LVDS communication channel employs a current source driving a transmission line which is terminated with two resistive loads. These loads serve to convert the transmitted current into a voltage at the receiver input. To ensure good signal integrity, the termination resistors should be matched to the characteristic impedance of the transmission line. The designer should ensure that the termination resistors are within 10% of the nominal media characteristic impedance. If the transmission line is targeted for  $100-\Omega$  impedance, the termination resistors should be between  $90~\Omega$  and  $110~\Omega$ . The line termination resistors are typically placed at the ends of the transmission line.

#### 9.2.3.6 Receiver Input Signal

The M-LVDS receivers herein comply with the M-LVDS standard and correctly determine the bus state. These devices have Type-1 and Type-2 receivers that detect the bus state with as little as 50 mV of differential voltage over the common mode range of -1 V to 3.4 V.

#### 9.2.3.7 Receiver Input Threshold (Failsafe)

The MLVDS standard defines a Type-1 and Type-2 receiver. Type-1 receivers have their differential input voltage thresholds near zero volts. Type-2 receivers have their differential input voltage thresholds offset from 0 V to detect the absence of a voltage difference. The impact to receiver output by the offset input can be seen in 表 7 and 图 19.

 RECEIVER TYPE
 OUTPUT LOW
 OUTPUT HIGH

 Type 1
  $-2.4 \text{ V} \le \text{V}_{\text{ID}} \le -0.05 \text{ V}$   $0.05 \text{ V} \le \text{V}_{\text{ID}} \le 2.4 \text{ V}$  

 Type 2
  $-2.4 \text{ V} \le \text{V}_{\text{ID}} \le 0.05 \text{ V}$   $0.15 \text{ V} \le \text{V}_{\text{ID}} \le 2.4 \text{ V}$ 

表 7. Receiver Input Voltage Threshold Requirements

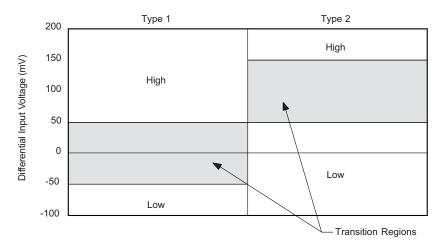


图 19. Expanded Graph of Receiver Differential Input Voltage Showing Transition Region

#### 9.2.3.8 Receiver Output Signal

Receiver outputs comply with LVTTL output voltage standards when the supply voltage is within the range of 3 V to 3.6 V.

#### 9.2.3.9 Interconnecting Media

The physical communication channel between the driver and the receiver may be any balanced paired metal conductors meeting the requirements of the M-LVDS standard, the key points which will be included here. This media may be a twisted pair, twinax, flat ribbon cable, or PCB traces.

The nominal characteristic impedance of the interconnect should be between 100  $\Omega$  and 120  $\Omega$  with variation no more than 10% (90  $\Omega$  to 132  $\Omega$ ).



#### 9.2.3.10 PCB Transmission Lines

As per SNLA187, 20 depicts several transmission line structures commonly used in printed-circuit boards (PCBs). Each structure consists of a signal line and a return path with uniform cross-section along its length. A microstrip is a signal trace on the top (or bottom) layer, separated by a dielectric layer from its return path in a ground or power plane. A stripline is a signal trace in the inner layer, with a dielectric layer in between a ground plane above and below the signal trace. The dimensions of the structure along with the dielectric material properties determine the characteristic impedance of the transmission line (also called controlled-impedance transmission line).

When two signal lines are placed close by, they form a pair of coupled transmission lines. 20 shows examples of edge-coupled microstrips, and edge-coupled or broad-side-coupled striplines. When excited by differential signals, the coupled transmission line is referred to as a differential pair. The characteristic impedance of each line is called odd-mode impedance. The sum of the odd-mode impedances of each line is the differential impedance of the differential pair. In addition to the trace dimensions and dielectric material properties, the spacing between the two traces determines the mutual coupling and impacts the differential impedance. When the two lines are immediately adjacent; for example, if S is less than 2 x W, the differential pair is called a tightly-coupled differential pair. To maintain constant differential impedance along the length, it is important to keep the trace width and spacing uniform along the length, as well as maintain good symmetry between the two lines.

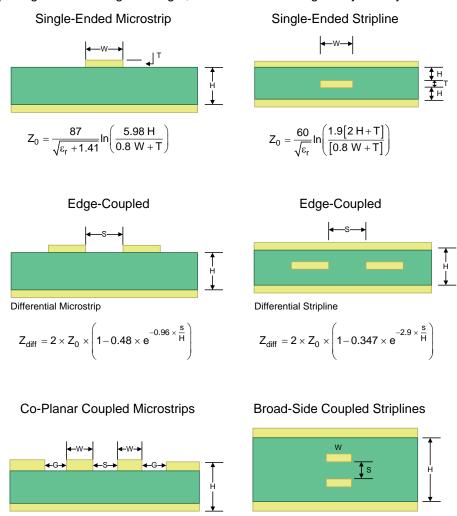
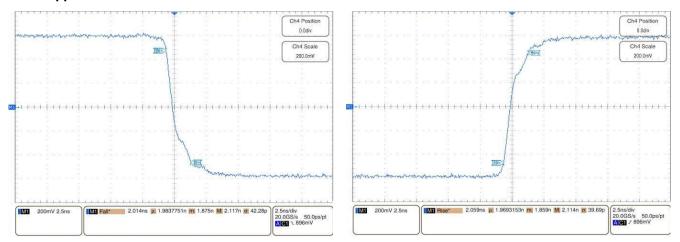


图 20. Controlled-Impedance Transmission Lines



# 9.2.4 Application Curves



$$V_{CC} = 3.3 \text{ V}$$
  $T_A = 25^{\circ}\text{C}$ 

图 21. Driver Fall Time

$$V_{CC} = 3.3 \text{ V}$$
  $T_A = 25^{\circ}\text{C}$ 

图 22. Driver Rise Time



### 10 Power Supply Recommendations

The M-LVDS driver and receivers in this data sheet are designed to operate from a single power supply. Both drivers and receivers operate with supply voltages in the range of 3 V to 3.6 V. In a typical application, a driver and a receiver may be on separate boards, or even separate equipment. In these cases, separate supplies would be used at each location. The expected ground potential difference between the driver power supply and the receiver power supply would be less than ±1 V. Board level and local device level bypass capacitance should be used and are covered Supply Bypass Capacitance.

#### 11 Layout

#### 11.1 Layout Guidelines

#### 11.1.1 Microstrip vs. Stripline Topologies

As per SLLD009, printed-circuit boards usually offer designers two transmission line options: Microstrip and stripline. Microstrips are traces on the outer layer of a PCB, as shown in 23.

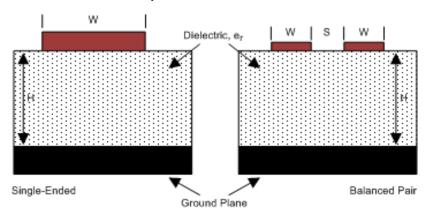


图 23. Microstrip Topology

On the other hand, striplines are traces between two ground planes. Striplines are less prone to emissions and susceptibility problems because the reference planes effectively shield the embedded traces. However, from the standpoint of high-speed transmission, juxtaposing two planes creates additional capacitance. TI recommends routing M-LVDS signals on microstrip transmission lines if possible. The PCB traces allow designers to specify the necessary tolerances for  $Z_O$  based on the overall noise budget and reflection allowances. Footnotes 1<sup>(1)</sup>, 2<sup>(2)</sup>, and 3<sup>(3)</sup> provide formulas for  $Z_O$  and  $t_{PD}$  for differential and single-ended traces. (1) (2) (3)

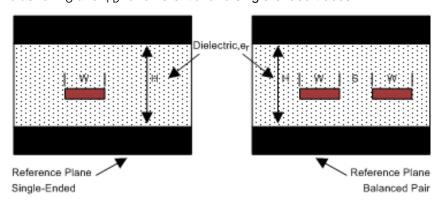


图 24. Stripline Topology

- (1) Howard Johnson & Martin Graham.1993. High Speed Digital Design A Handbook of Black Magic. Prentice Hall PRT. ISBN number 013395724
- (2) Mark I. Montrose. 1996. Printed Circuit Board Design Techniques for EMC Compliance. IEEE Press. ISBN number 0780311310.
- (3) Clyde F. Coombs, Jr. Ed, Printed Circuits Handbook, McGraw Hill, ISBN number 0070127549.



# Layout Guidelines (接下页)

#### 11.1.2 Dielectric Type and Board Construction

The speeds at which signals travel across the board dictates the choice of dielectric. FR-4, or equivalent, usually provides adequate performance for use with M-LVDS signals. If rise or fall times of TTL/CMOS signals are less than 500 ps, empirical results indicate that a material with a dielectric constant near 3.4, such as Rogers<sup>™</sup> 4350 or Nelco N4000-13 is better suited. Once the designer chooses the dielectric, there are several parameters pertaining to the board construction that can affect performance. The following set of guidelines were developed experimentally through several designs involving M-LVDS devices:

- Copper weight: 15 g or 1/2 oz start, plated to 30 g or 1 oz
- All exposed circuitry should be solder-plated (60/40) to 7.62 μm or 0.0003 in (minimum).
- Copper plating should be 25.4 μm or 0.001 in (minimum) in plated-through-holes.
- · Solder mask over bare copper with solder hot-air leveling

#### 11.1.3 Recommended Stack Layout

Following the choice of dielectrics and design specifications, you must decide how many levels to use in the stack. To reduce the TTL/CMOS to M-LVDS crosstalk, it is a good practice to have at least two separate signal planes as shown in 图 25.

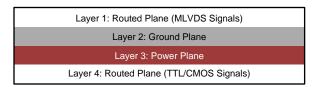


图 25. Four-Layer PCB Board

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The separation between layers 2 and 3 should be 127  $\mu m$  (0.005 in). By keeping the power and ground planes tightly coupled, the increased capacitance acts as a bypass for transients.

One of the most common stack configurations is the six-layer board, as shown in \begin{align\*} \begin{align\*} 26.

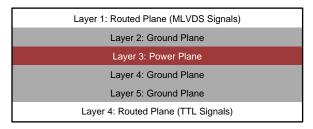


图 26. Six-Layer PCB Board

In this particular configuration, it is possible to isolate each signal layer from the power plane by at least one ground plane. The result is improved signal integrity; however, fabrication is more expensive. Using the 6-layer board is preferable, because it offers the layout designer more flexibility in varying the distance between signal layers and referenced planes, in addition to ensuring reference to a ground plane for signal layers 1 and 6.

#### 11.1.4 Separation Between Traces

The separation between traces depends on several factors; however, the amount of coupling that can be tolerated usually dictates the actual separation. Low noise coupling requires close coupling between the differential pair of an M-LVDS link to benefit from the electromagnetic field cancellation. The traces should be  $100-\Omega$  differential and thus coupled in the manner that best fits this requirement. In addition, differential pairs should have the same electrical length to ensure that they are balanced, thus minimizing problems with skew and signal reflection.



#### Layout Guidelines (接下页)

In the case of two adjacent single-ended traces, one should use the 3-W rule, which stipulates that the distance between two traces must be greater than two times the width of a single trace, or three times its width measured from trace center to trace center. This increased separation effectively reduces the potential for crosstalk. The same rule should be applied to the separation between adjacent M-LVDS differential pairs, whether the traces are edge-coupled or broad-side-coupled.

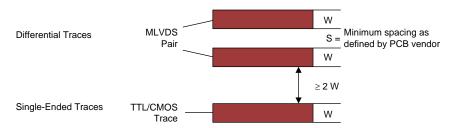


图 27. 3-W Rule for Single-Ended and Differential Traces (Top View)

You should exercise caution when using autorouters, because they do not always account for all factors affecting crosstalk and signal reflection. For instance, it is best to avoid sharp 90° turns to prevent discontinuities in the signal path. Using successive 45° turns tends to minimize reflections.

#### 11.1.5 Crosstalk and Ground Bounce Minimization

To reduce crosstalk, it is important to provide a return path to high-frequency currents that is as close as possible to its originating trace. A ground plane usually achieves this. Because the returning currents always choose the path of lowest inductance, they are most likely to return directly under the original trace, thus minimizing crosstalk. Lowering the area of the current loop lowers the potential for crosstalk. Traces kept as short as possible with an uninterrupted ground plane running beneath them emit the minimum amount of electromagnetic field strength. Discontinuities in the ground plane increase the return path inductance and should be avoided.

#### 11.1.6 Decoupling

Each power or ground lead of a high-speed device should be connected to the PCB through a low inductance path. For best results, one or more vias are used to connect a power or ground pin to the nearby plane. Ideally, via placement is immediately adjacent to the pin to avoid adding trace inductance. Placing a power plane closer to the top of the board reduces the effective via length and its associated inductance.

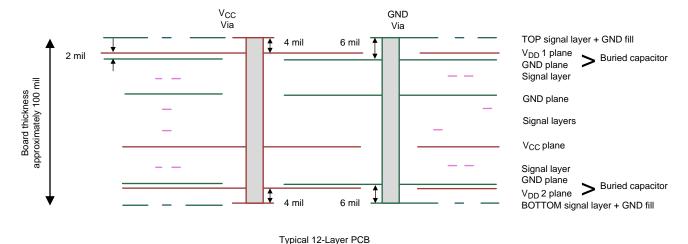


图 28. Low Inductance, High-Capacitance Power Connection



#### Layout Guidelines (接下页)

Bypass capacitors should be placed close to  $V_{DD}$  pins. They can be placed conveniently near the corners or underneath the package to minimize the loop area. This extends the useful frequency range of the added capacitance. Small-physical-size capacitors, such as 0402, 0201, or X7R surface-mount capacitors should be used to minimize body inductance of capacitors. Each bypass capacitor is connected to the power and ground plane through vias tangent to the pads of the capacitor as shown in 29 29(a).

An X7R surface-mount capacitor of size 0402 has about 0.5 nH of body inductance. At frequencies above 30 MHz or so, X7R capacitors behave as low-impedance inductors. To extend the operating frequency range to a few hundred MHz, an array of different capacitor values like 100 pF, 1 nF, 0.03 μF, and 0.1 μF are commonly used in parallel. The most effective bypass capacitor can be built using sandwiched layers of power and ground at a separation of 2 to 3 mils. With a 2-mil FR4 dielectric, there is approximately 500 pF per square inch of PCB. Many high-speed devices provide a low-inductance GND connection on the backside of the package. This center pad must be connected to a ground plane through an array of vias. The via array reduces the effective inductance to ground and enhances the thermal performance of the small Surface Mount Technology (SMT) package. Placing vias around the perimeter of the pad connection ensures proper heat spreading and the lowest possible die temperature. Placing high-performance devices on opposing sides of the PCB using two GND planes (as shown in 🛭 20) creates multiple paths for heat transfer. Often thermal PCB issues are the result of one device adding heat to another, resulting in a very high local temperature. Multiple paths for heat transfer minimize this possibility. In many cases the GND pad makes the optimal decoupling layout impossible to achieve due to insufficient pad-to-pad spacing as shown in 8 29(b). When this occurs, placing the decoupling capacitor on the backside of the board keeps the extra inductance to a minimum. It is important to place the V<sub>DD</sub> via as close to the device pin as possible while still allowing for sufficient solder mask coverage. If the via is left open, solder may flow from the pad and into the via barrel. This will result in a poor solder connection.



图 29. Typical Decoupling Capacitor Layouts

#### 11.2 Layout Example

At least two or three times the width of an individual trace should separate single-ended traces and differential pairs to minimize the potential for crosstalk. Single-ended traces that run in parallel for less than the wavelength of the rise or fall times usually have negligible crosstalk. Increase the spacing between signal paths for long parallel runs to reduce crosstalk. Boards with limited real estate can benefit from the staggered trace layout, as shown in 30.

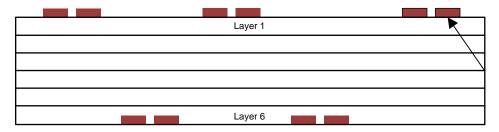


图 30. Staggered Trace Layout



#### Layout Example (接下页)

This configuration lays out alternating signal traces on different layers; thus, the horizontal separation between traces can be less than 2 or 3 times the width of individual traces. To ensure continuity in the ground signal path, TI recommends having an adjacent ground via for every signal via, as shown in ₹31. Note that vias create additional capacitance. For example, a typical via has a lumped capacitance effect of 1/2 pF to 1 pF in FR4.

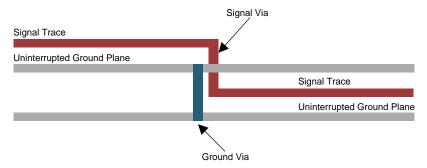


图 31. Ground Via Location (Side View)

Short and low-impedance connection of the device ground pins to the PCB ground plane reduces ground bounce. Holes and cutouts in the ground planes can adversely affect current return paths if they create discontinuities that increase returning current loop areas.

To minimize EMI problems, TI recommends avoiding discontinuities below a trace (for example, holes, slits, and so on) and keeping traces as short as possible. Zoning the board wisely by placing all similar functions in the same area, as opposed to mixing them together, helps reduce susceptibility issues.



#### 12 器件和文档支持

#### 12.1 接收文档更新通知

如需接收文档更新通知,请访问 www.ti.com.cn 网站上的器件产品文件夹。点击右上角的*提醒我* (Alert me) 注册后,即可每周定期收到已更改的产品信息。有关更改的详细信息,请查阅已修订文档中包含的修订历史记录。

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#### 12.5 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

#### 13 机械、封装和可订购信息

以下页中包括机械、封装和可订购信息。这些信息是针对指定器件可提供的最新数据。这些数据会在无通知且不对本文档进行修订的情况下发生改变。欲获得该数据表的浏览器版本,请查阅左侧的导航栏。

www.ti.com 10-Nov-2025

#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
SN65MLVD204BD	Active	Production	SOIC (D)   8	75   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	MF204B
SN65MLVD204BD.B	Active	Production	SOIC (D)   8	75   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	MF204B
SN65MLVD204BDR	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	MF204B
SN65MLVD204BDR.B	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	MF204B
SN65MLVD204BRUMR	Active	Production	WQFN (RUM)   16	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	MLVD 204B
SN65MLVD204BRUMR.B	Active	Production	WQFN (RUM)   16	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	MLVD 204B
SN65MLVD204BRUMT	Active	Production	WQFN (RUM)   16	250   SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	MLVD 204B
SN65MLVD204BRUMT.B	Active	Production	WQFN (RUM)   16	250   SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	MLVD 204B

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

<sup>(2)</sup> Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.



# **PACKAGE OPTION ADDENDUM**

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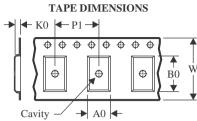
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#### TAPE AND REEL INFORMATION

# REEL DIMENSIONS Reel Diameter Reel Width (W1)



A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
SN65MLVD204BDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
SN65MLVD204BRUMR	WQFN	RUM	16	3000	330.0	12.4	4.25	4.25	1.15	8.0	12.0	Q2
SN65MLVD204BRUMT	WQFN	RUM	16	250	180.0	12.4	4.25	4.25	1.15	8.0	12.0	Q2



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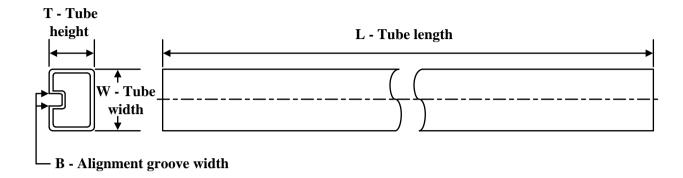
#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
SN65MLVD204BDR	SOIC	D	8	2500	353.0	353.0	32.0
SN65MLVD204BRUMR	WQFN	RUM	16	3000	367.0	367.0	35.0
SN65MLVD204BRUMT	WQFN	RUM	16	250	210.0	185.0	35.0

# **PACKAGE MATERIALS INFORMATION**

www.ti.com 23-May-2025

#### **TUBE**



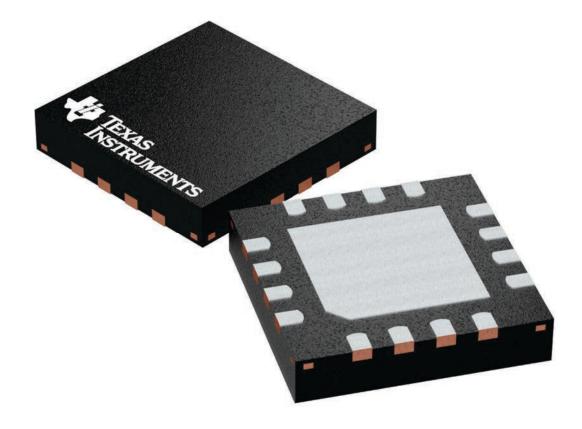
#### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
SN65MLVD204BD	D	SOIC	8	75	507	8	3940	4.32
SN65MLVD204BD.B	D	SOIC	8	75	507	8	3940	4.32

4 x 4, 0.65 mm pitch

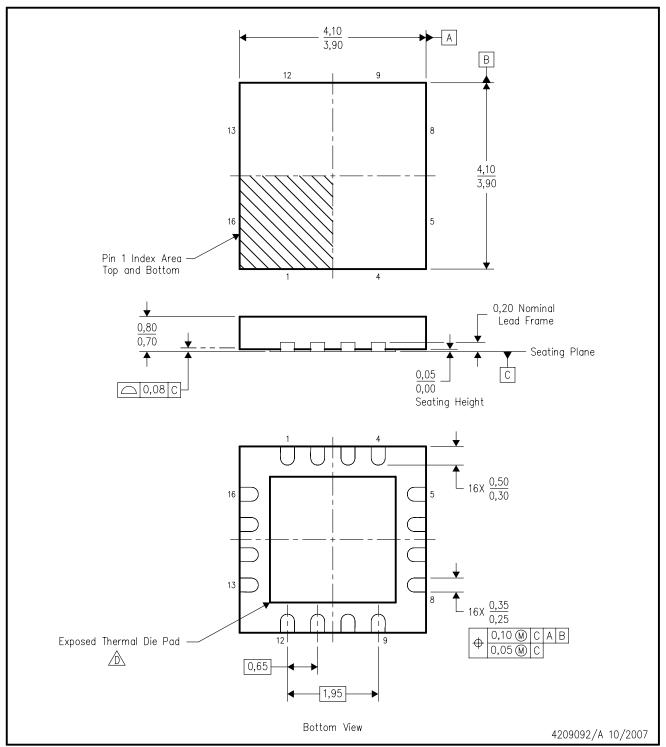
PLASTIC QUAD FLATPACK - NO LEAD

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



# RUM (S-PQFP-N16)

# PLASTIC QUAD FLATPACK



NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

- B. This drawing is subject to change without notice.
- C. QFN (Quad Flatpack No-Lead) package configuration.

The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.

E. Package complies to JEDEC MO-220 variation WGGC-3.



4209093-2/F 09/15

# RUM (S-PWQFN-N16)

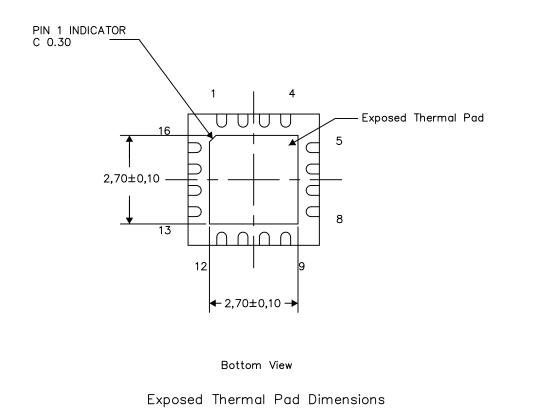
#### PLASTIC QUAD FLATPACK NO-LEAD

#### THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

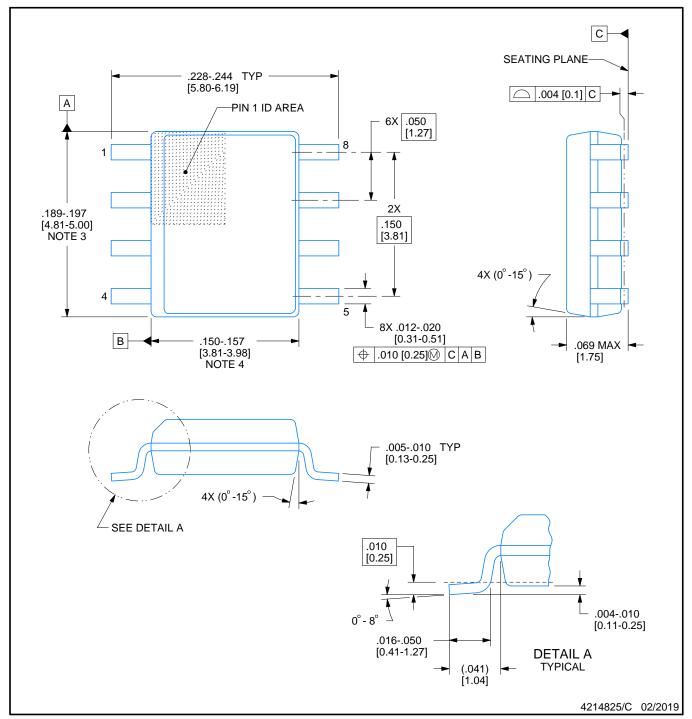
The exposed thermal pad dimensions for this package are shown in the following illustration.



NOTES: All linear dimensions are in millimeters



SMALL OUTLINE INTEGRATED CIRCUIT

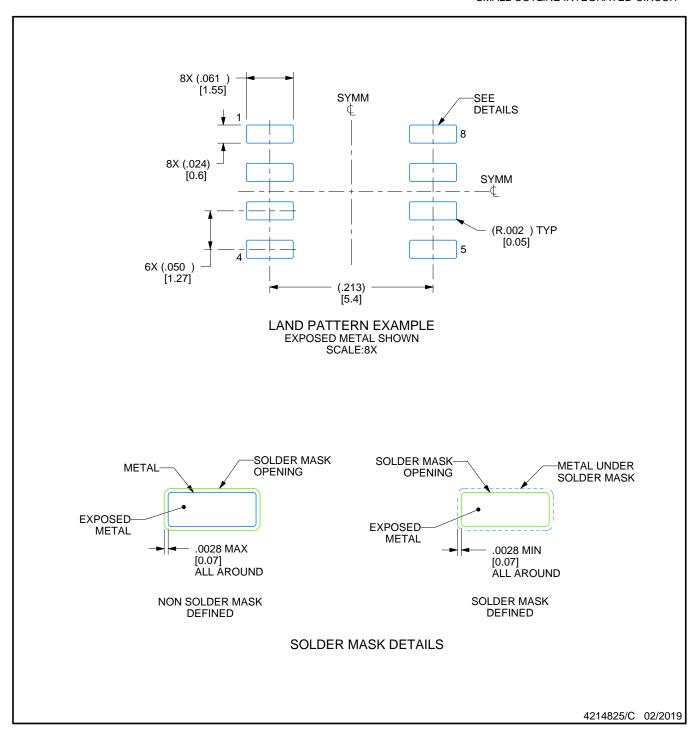


#### NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



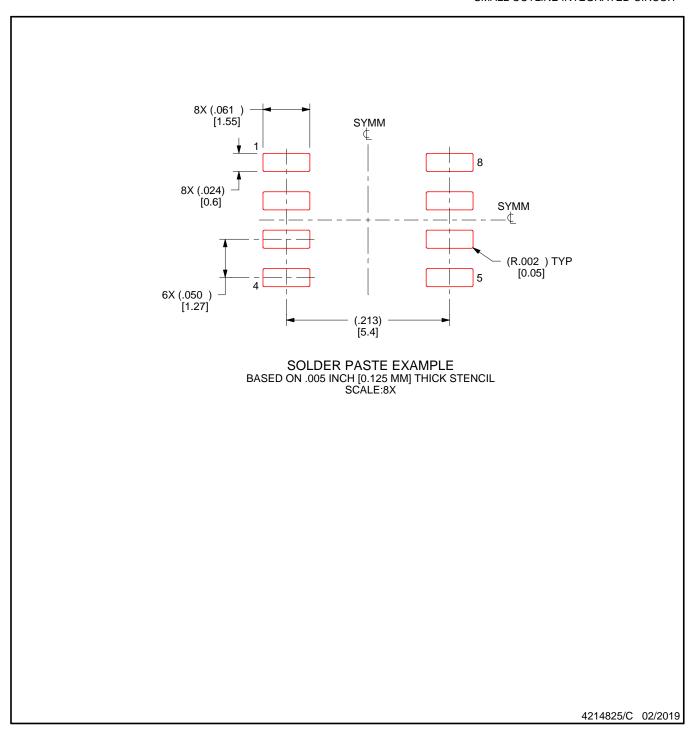
NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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