

## TPS4030x 3V 至 20V 输入、电压模式、同步降压控制器

### 1 特性

- 输入电压范围为 3V 至 20V
- 300kHz (TPS40303)、600kHz (TPS40304) 和 1.2MHz (TPS40305) 开关频率
- 高侧和低侧 FET  $R_{DS(on)}$  电流检测
- 可编程热补偿 OCP 电平
- 可编程软启动
- 600mV、1% 基准电压
- 电压前馈补偿
- 支持预偏置输出
- 扩频频谱
- 145°C 的热关断保护限制
- 10 引脚 3mm × 3mm VSON 封装，散热垫具有接地连接
- 使用 TPS4030x 并借助 [WEBENCH® Power Designer](#) 创建定制设计方案

### 2 应用

- 负载点 (POL) 模块
- 打印机
- 数字电视
- 电信
- USB Type-C 墙壁插座

### 3 说明

TPS4030x 是成本优化的同步降压控制器系列产品，可在 3V 至 20V 输入电压下运行。此控制器实现了一种电压模式控制架构，具有输入电压前馈补偿功能，可对输入电压变化做出即时响应。固定开关频率为 300KHz、600KHz 或 1.2MHz。

在开关频率部分添加了扩频频谱 (FSS) 特性，显著降低了峰值 EMI 噪声，使其更容易符合 EMI 标准。

TPS4030x 具有多种用户可编程功能，包括软启动、过流保护 (OCP) 电平以及环路补偿。

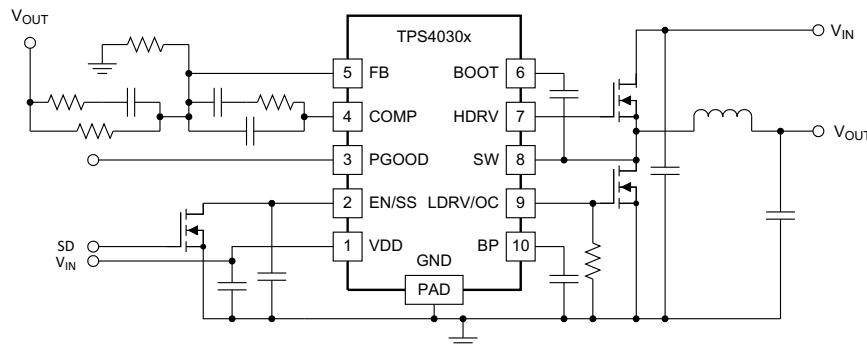
OCP 电平可以通过从 LDRV 引脚连接到电路接地的单个外部电阻器进行编程。在初始通电过程中，TPS4030x 将进入校准环节，测量 LDRV 引脚电压，并设置内部 OCP 电压电平。在工作期间，器件可在通电时通过将已编程 OCP 电压电平与低侧 FET 上的压降进行比较来确定是否发生过流情况。之后，TPS4030x 会进入关断和重启周期，直到故障消除为止。

#### 器件信息(1)

器件型号	封装	封装尺寸 (标称值)
TPS40303	VSON (10)	3.00mm × 3.00mm
TPS40304		
TPS40305		

(1) 如需了解所有可用封装，请参阅数据表末尾的可订购产品附录。

#### 简化应用示意图



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## 目录

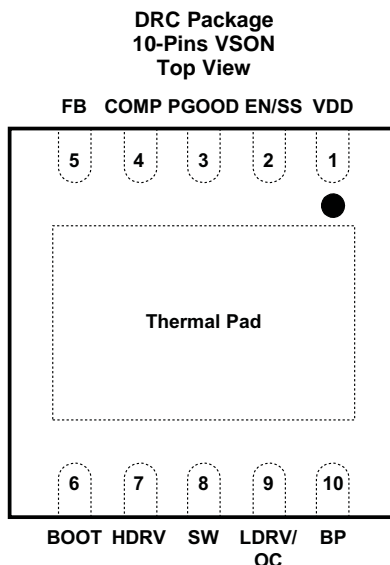
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## 4 修订历史记录

注：之前版本的页码可能与当前版本有所不同。

<b>Changes from Revision C (January 2018) to Revision D</b>		<b>Page</b>
• 已更改 更改了 SEO 的数据表标题 .....	1	
• 已添加 将“USB Type-C 墙壁插座”添加到 <a href="#">应用</a> ；添加了 WEBENCH 链接 .....	1	
• Deleted redundant <i>Dissipation Ratings</i> table .....	4	
<b>Changes from Revision B (May 2015) to Revision C</b>		<b>Page</b>
• 已添加 在 TPS40303 TI 设计中添加了顶部导航图标 .....	1	
• 已删除 从 <a href="#">器件和文档支持</a> 中删除了相关器件表 .....	32	
<b>Changes from Revision A (August 2012) to Revision B</b>		<b>Page</b>
• 已添加 添加了引脚配置和功能 部分、ESD 额定值表、特性 说明 部分、器件功能模式、应用和实施 部分、电源相关建议 部分、布局 部分、器件和文档支持 部分以及机械、封装和可订购信息 部分 .....	1	
<b>Changes from Original (November 2009) to Revision A</b>		<b>Page</b>
• Changed minimum controllable pulse width max value from 100 to 70 .....	5	

## 5 Pin Configuration and Functions



### Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
BOOT	6	I	Gate drive voltage for the high-side N-channel MOSFET. A 0.1- $\mu$ F capacitor (typical) must be connected between this pin and SW. For low input voltage operation, an external schottky diode from BP to BOOT is recommended to maximize the gate drive voltage for the high-side.
BP	10	O	Output bypass for the internal regulator. Connect a low ESR bypass ceramic capacitor of 1 $\mu$ F or greater from this pin to GND.
COMP	4	O	Output of the error amplifier and connection node for loop feedback components.
EN/SS	2	I	Logic level input which starts or stops the controller via an external user command. Letting this pin float turns the controller on. Pulling this pin low disables the controller. This is also the soft-start programming pin. A capacitor connected from this pin to GND programs the soft-start time. The capacitor is charged with an internal current source of 10 $\mu$ A. The resulting voltage ramp of this pin is also used as a second non-inverting input to the error amplifier after a 0.8 V (typical) level shift downwards. Output regulation is controlled by the internal level shifted voltage ramp until that voltage reaches the internal reference voltage of 600 mV – the voltage ramp of this pin reaches 1.4 V (typical). Optionally, a 267-k $\Omega$ resistor from this pin to BP enables the FSS feature.
FB	5	I	Inverting input to the error amplifier. In normal operation, the voltage on this pin is equal to the internal reference voltage.
HDRV	7	O	Bootstrapped gate drive output for the high-side N-channel MOSFET.
LDRV/OC	9	O	Gate drive output for the low-side synchronous rectifier N-channel MOSFET. A resistor from this pin to GND is also used to determine the voltage level for OCP. An internal current source of 10 $\mu$ A flows through the resistor during initial calibration and that sets up the voltage trip point used for OCP.
PGOOD	3	O	Open-drain power good output.
SW	8	O	Sense line for the adaptive anti-cross conduction circuitry. Serves as common connection for the flying high-side FET driver.
VDD	1	I	Power input to the controller. Bypass VDD to GND with a low ESR ceramic capacitor of at least 1- $\mu$ F close to the device.
GND	Thermal Pad	—	Ground connection to the controller. This is also the thermal pad used to conduct heat from the device. This connection serves a twofold purpose. The first is to provide an electrical ground connection for the device. The second is to provide a low thermal impedance path from the device die to the PCB. This pad should be tied externally to a ground plane.

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

	MIN	MAX	UNIT
VDD	-0.3	22	V
SW	-3	27	V
SW (< 100-ns pulse width, 10 $\mu$ J)		-5	V
BOOT	-0.3	30	V
HDRV	-5	30	V
BOOT-SW, HDRV-SW (differential from BOOT or HDRV to SW)	-0.3	7	V
COMP, PGOOD, FB, BP, LDRV, EN/SS	-0.3	7	V
Operating junction temperature, T <sub>J</sub>	-40	145	°C
Storage temperature, T <sub>stg</sub>	-55	150	°C

- (1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other condition beyond those included under [Recommended Operating Conditions](#) is not implied. Exposure to absolute-maximum-rated conditions for extended periods of time may affect device reliability.

### 6.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub> Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
	Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.  
 (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

		MIN	NOM	MAX	UNIT
VDD	Input voltage	3		20	V
T <sub>J</sub>	Operating junction temperature	-40		125	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TPS4030x	UNIT
		DRC (VSON)	
		10 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	44.3	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	56.1	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	19.2	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	0.7	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	19.4	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	5.5	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

## 6.5 Electrical Characteristics

 $T_J = -40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ ,  $V_{DD} = 12\text{ V}$ , all parameters at zero power dissipation (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
<b>VOLTAGE REFERENCE</b>							
$V_{FB}$	FB input voltage	$T_J = 25^{\circ}\text{C}$ , $3\text{ V} < V_{DD} < 20\text{ V}$	597	600	603	mV	
		$-40^{\circ}\text{C} < T_J < 125^{\circ}\text{C}$ , $3\text{ V} < V_{DD} < 20\text{ V}$	594	600	606		
<b>INPUT SUPPLY</b>							
$V_{DD}$	Input supply voltage range		3		20	V	
$I_{DDSD}$	Shutdown supply current	$V_{EN/SS} < 0.2\text{ V}$		70	100	$\mu\text{A}$	
$I_{DDQ}$	Quiescent, nonswitching	Let EN/SS float, $V_{FB} = 1\text{ V}$		2.5	3.5	mA	
<b>ENABLE/SOFT START</b>							
$V_{IH}$	High-level input voltage, EN/SS		0.55	0.7	1	V	
$V_{IL}$	Low-level input voltage, EN/SS		0.27	0.3	0.33	V	
$I_{SS}$	Soft-start source current		8	10	12	$\mu\text{A}$	
$V_{SS}$	Soft-start voltage level		0.4	0.8	1.3	V	
<b>BP REGULATOR</b>							
$V_{BP}$	Output voltage	$I_{BP} = 10\text{ mA}$	6.2	6.5	6.8	V	
$V_{DO}$	Regulator dropout voltage, $V_{DD} - V_{BP}$	$I_{BP} = 25\text{ mA}$ , $V_{DD} = 3\text{ V}$		70	110	mV	
<b>OSCILLATOR</b>							
$f_{SW}$	PWM frequency	TPS40303	$3\text{ V} < V_{DD} < 20\text{ V}$	270	300	330	kHz
		TPS40304		540	600	660	
		TPS40305		1.02	1.20	1.38	
$V_{RAMP}^{(1)}$	Ramp amplitude		$V_{DD}/6.6$	$V_{DD}/6$	$V_{DD}/5.4$	V	
$f_{SWFSS}$	Frequency spread-spectrum frequency deviation		12%			$f_{sw}$	
$f_{MOD}$	Modulation frequency			25		kHz	
<b>PWM</b>							
$D_{MAX}^{(1)}$	Maximum duty cycle	TPS40303	$V_{FB} = 0\text{ V}$ , $3\text{ V} < V_{DD} < 20\text{ V}$	90%			
		TPS40304		90%			
		TPS40305		85%			
$t_{ON(min)}^{(1)}$	Minimum controllable pulse width				70	ns	
$t_{DEAD}$	Output driver dead time	HDRV off to LDRV on	5	25	35	ns	
		LDRV off to HDRV on	5	25	30		
<b>ERROR AMPLIFIER</b>							
$G_{BWP}^{(1)}$	Gain bandwidth product		10	24		MHz	
$A_{OL}^{(1)}$	Open loop gain		60			dB	
$I_{IB}$	Input bias current (current out of FB pin)	$V_{FB} = 0.6\text{ V}$			75	nA	
$I_{EAOP}$	Output source current	$V_{FB} = 0\text{ V}$	2			mA	
$I_{EAOM}$	Output sink current	$V_{FB} = 1\text{ V}$	2				
<b>PGOOD</b>							
$V_{OV}$	Feedback upper voltage limit for PGOOD		655	675	700	mV	
$V_{UV}$	Feedback lower voltage limit for PGOOD		500	525	550		
$V_{PGD-HYST}$	PGOOD hysteresis voltage at FB			25	40		
$R_{PGD}$	PGOOD pulldown resistance	$V_{FB} = 0\text{ V}$ , $I_{FB} = 5\text{ mA}$		30	70	$\Omega$	
$I_{PGDLK}$	PGOOD leakage current	$550\text{ mV} < V_{FB} < 655\text{ mV}$ , $V_{PGOOD} = 5\text{ V}$		10	20	$\mu\text{A}$	

(1) Ensured by design. Not production tested.

**Electrical Characteristics (continued)**
 $T_J = -40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ ,  $V_{DD} = 12\text{ V}$ , all parameters at zero power dissipation (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OUTPUT DRIVERS</b>						
$R_{HDHI}$	High-side driver pullup resistance	$V_{BOOT} - V_{SW} = 5\text{ V}$ , $I_{HDRV} = -100\text{ mA}$	0.8	1.5	2.5	$\Omega$
$R_{HDLO}$	High-side driver pulldown resistance	$V_{BOOT} - V_{SW} = 5\text{ V}$ , $I_{HDRV} = 100\text{ mA}$	0.5	1	2.2	$\Omega$
$R_{LDHI}$	Low-side driver pullup resistance	$I_{LDRV} = -100\text{ mA}$	0.8	1.5	2.5	$\Omega$
$R_{LDLO}$	Low-side driver pulldown resistance	$I_{LDRV} = 100\text{ mA}$	0.35	0.6	1.2	$\Omega$
$t_{HRISE}^{(1)}$	High-side driver rise time	$C_{LOAD} = 5\text{ nF}$		15		ns
$t_{HFALL}^{(1)}$	High-side driver fall time			12		ns
$t_{LRISE}^{(1)}$	Low-side driver rise time			15		ns
$t_{LFALL}^{(1)}$	Low-side driver fall time			10		ns
<b>OVERCURRENT PROTECTION</b>						
$t_{PSSC(min)}^{(1)}$	Minimum pulse time during short circuit			250		ns
$t_{BLNKH}^{(1)}$	Switch leading-edge blanking pulse time			150		ns
$V_{OCH}$	OC threshold for high-side FET	$T_J = 25^{\circ}\text{C}$	360	450	580	mV
$I_{OCSET}$	OCSET current source	$T_J = 25^{\circ}\text{C}$	9.5	10	10.5	$\mu\text{A}$
$V_{LD-CLAMP}$	Maximum clamp voltage at LDRV		260	340	400	mV
$V_{OCLOS}$	OC comparator offset voltage for low-side FET	$T_J = 25^{\circ}\text{C}$	-8		8	mV
$V_{OCLPRO}^{(1)}$	Programmable OC range for low-side FET	$T_J = 25^{\circ}\text{C}$	12		300	mV
$V_{THTC}^{(1)}$	OC threshold temperature coefficient (both high-side and low-side)			3000		ppm
$t_{OFF}$	OC retry cycles on EN/SS pin			4		Cycle
<b>BOOT DIODE</b>						
$V_{DFWD}$	Bootstrap diode forward voltage	$I_{BOOT} = 5\text{ mA}$		0.8		V
<b>THERMAL SHUTDOWN</b>						
$T_{JSD}^{(1)}$	Junction shutdown temperature			145		$^{\circ}\text{C}$
$T_{JSDH}^{(1)}$	Hysteresis			20		$^{\circ}\text{C}$

## 6.6 Typical Characteristics

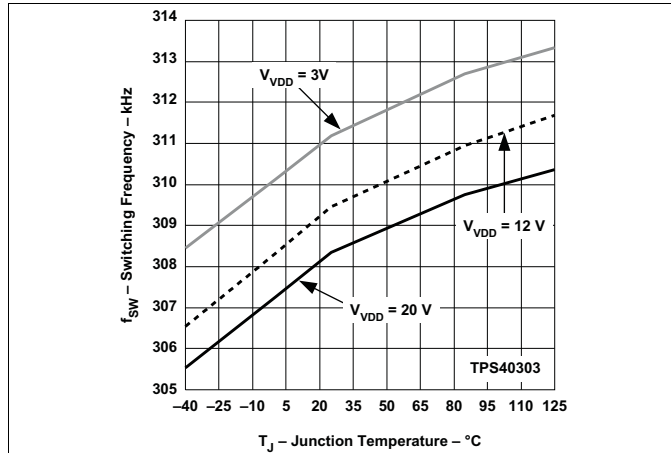


Figure 1. Switching Frequency vs Junction Temperature

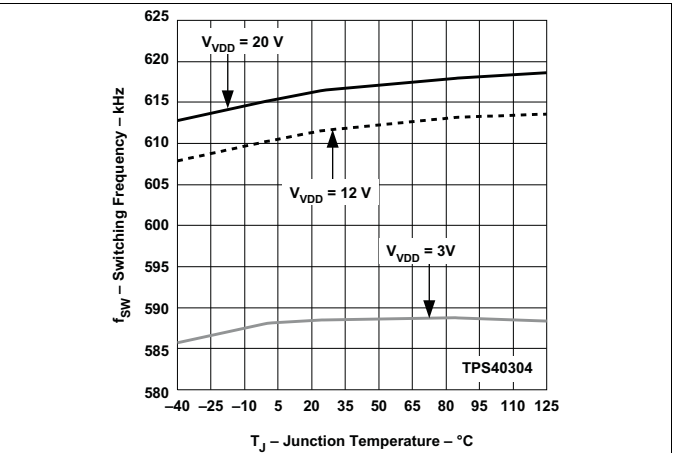


Figure 2. Switching Frequency vs Junction Temperature

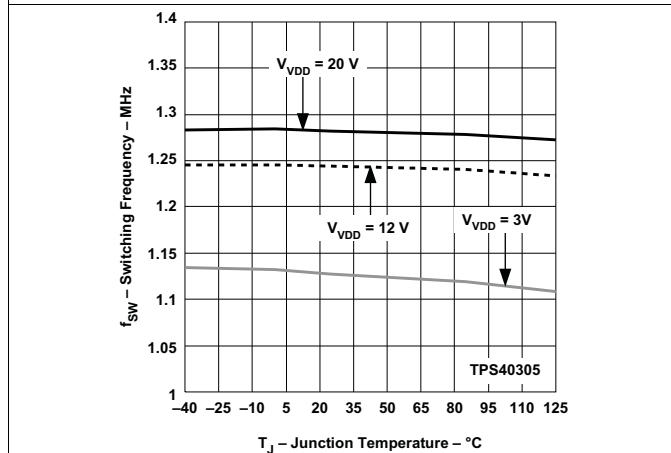


Figure 3. Switching Frequency vs Junction Temperature

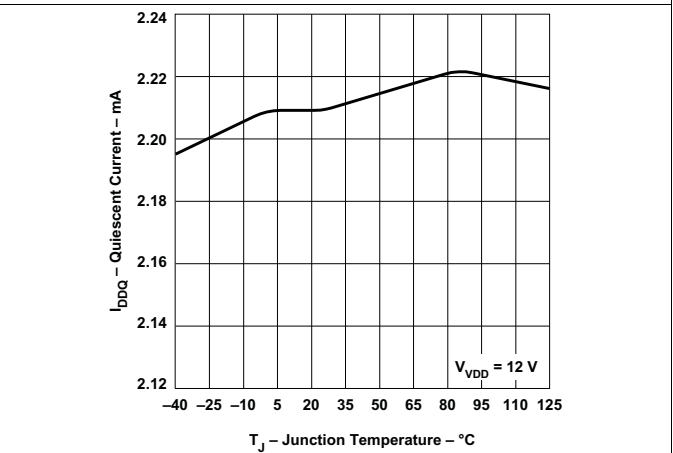


Figure 4. Quiescent Current vs Junction Temperature

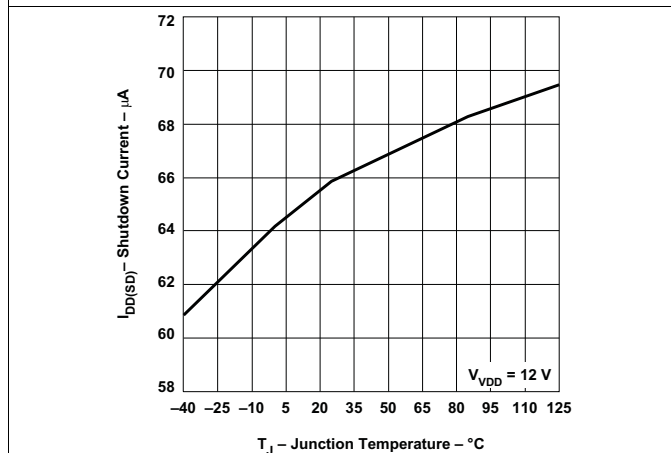


Figure 5. Shutdown Current vs Junction Temperature

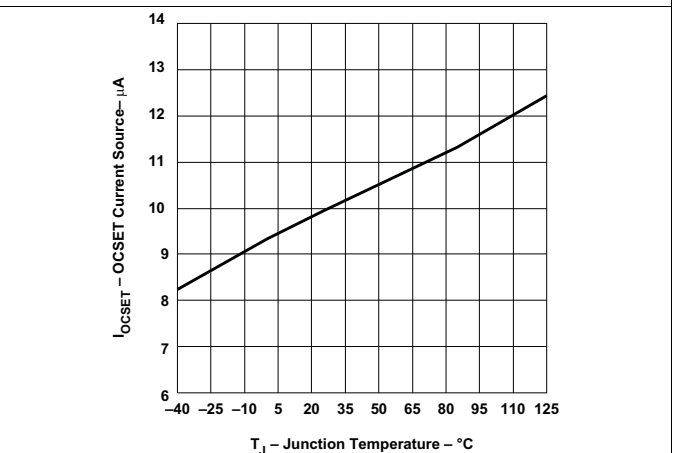


Figure 6. OCSET Current Source vs Junction Temperature

Typical Characteristics (continued)

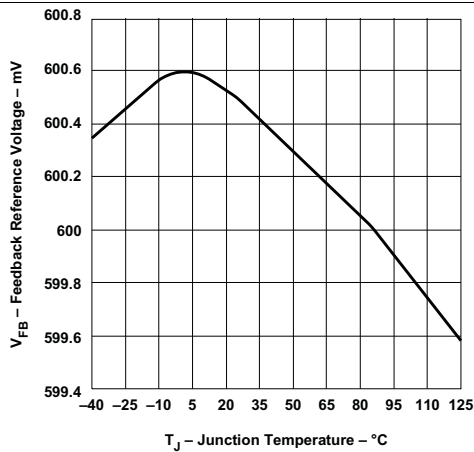


Figure 7. Feedback Reference Voltage vs Junction Temperature

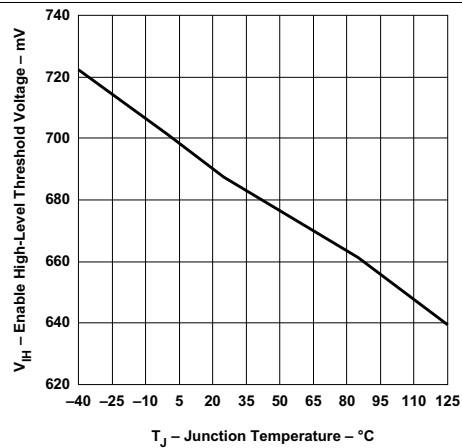


Figure 8. Enable High-Level Threshold Voltage vs Junction Temperature

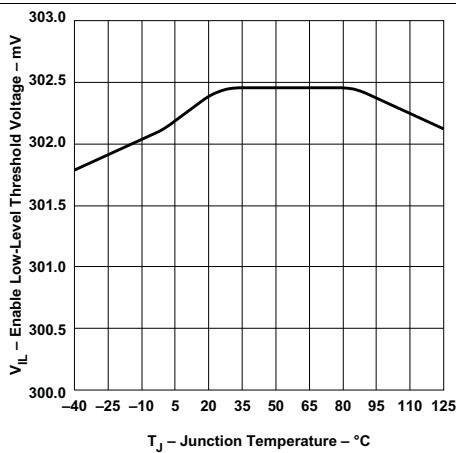


Figure 9. Enable Low-Level Threshold Voltage vs Junction Temperature

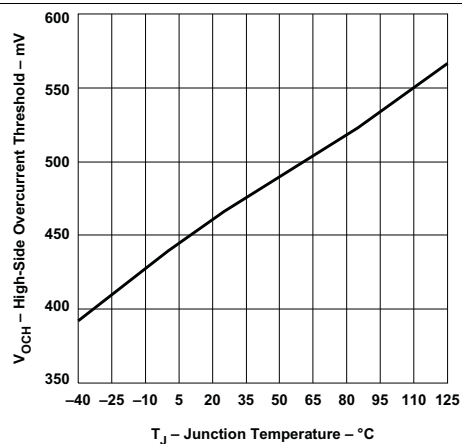


Figure 10. High-Side Overcurrent Threshold vs Junction Temperature

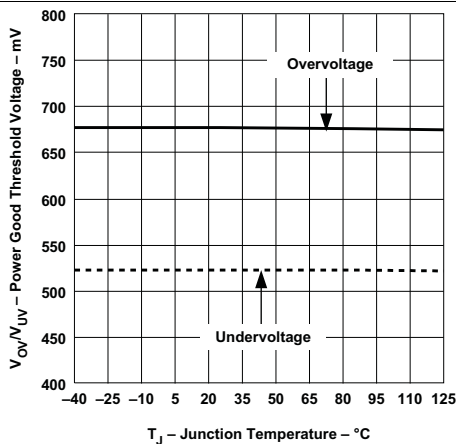


Figure 11. Power Good Threshold Voltage vs Junction Temperature

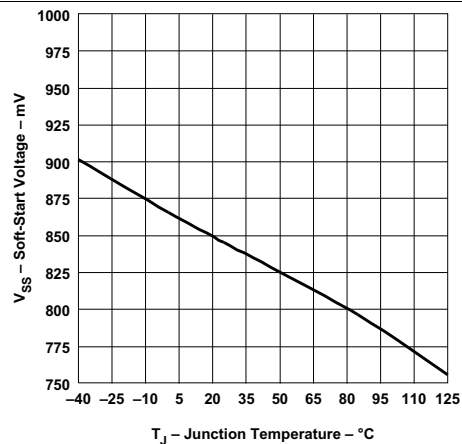


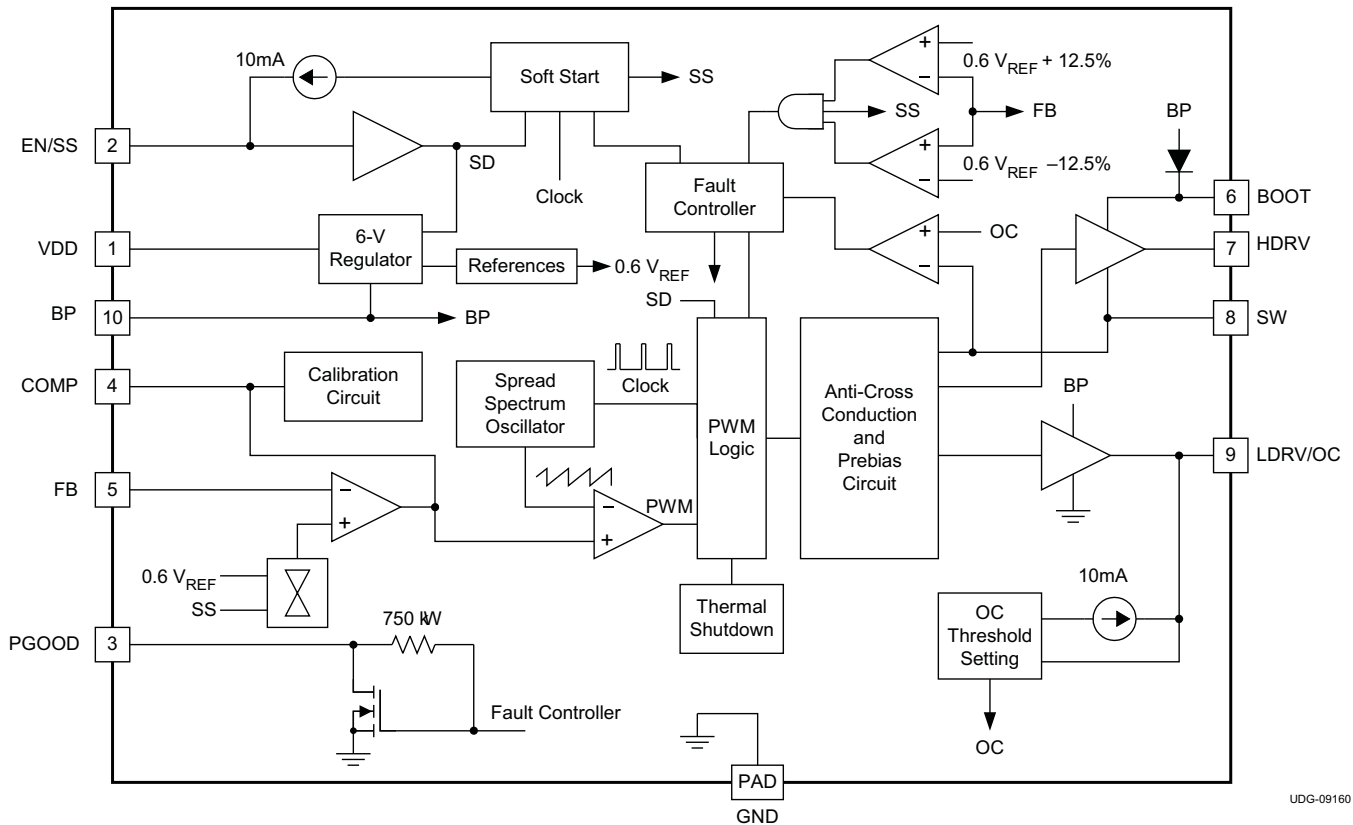
Figure 12. Soft-Start Voltage vs Junction Temperature

## 7 Detailed Description

### 7.1 Overview

The TPS4030x is a family of cost-optimized synchronous buck controllers providing high-end features to construct high-performance DC–DC converters. Prebias capability eliminates concerns about damaging sensitive loads during start-up. Programmable overcurrent protection levels and hiccup overcurrent fault recovery maximize design flexibility and minimize power dissipation in the event of a prolonged output short. The Frequency Spread Spectrum (FSS) feature reduces peak EMI noise by spreading the initial energy of each harmonic along a frequency band, thus giving a wider spectrum with lower amplitudes.

### 7.2 Functional Block Diagram



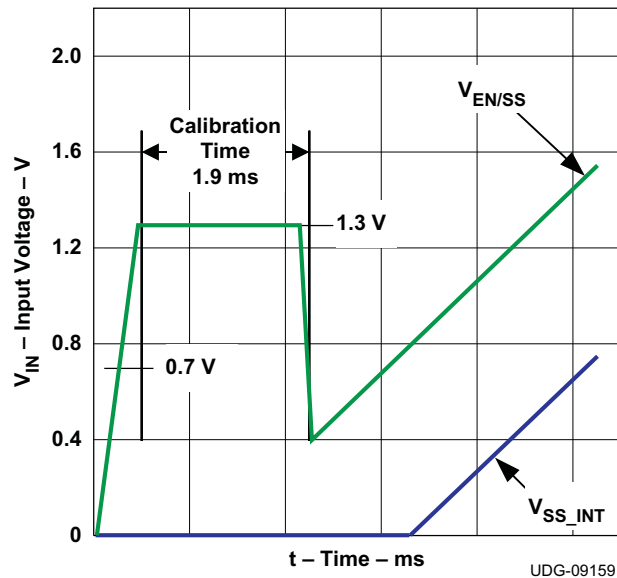
### 7.3 Feature Description

#### 7.3.1 Voltage Reference

The 600-mV band gap cell is internally connected to the noninverting input of the error amplifier. The reference voltage is trimmed with the error amplifier in a unity gain configuration to remove amplifier offset from the final regulation voltage. The 1% tolerance on the reference voltage allows the user to design a very accurate power supply.

#### 7.3.2 Enable Functionality, Start-Up Sequence and Timing

After input power is applied, an internal current source of 40  $\mu\text{A}$  starts to charge up the soft-start capacitor connected from EN/SS to GND. When the voltage across that capacitor increases to 0.7 V, it enables the internal BP regulator followed by a calibration. The total calibration time is about 1.9 ms. See [Figure 13](#). During the calibration, the device performs in the following way. It disables the LDRV drive and injects an internal 10- $\mu\text{A}$  current source to the resistor connected from LDRV to GND. The voltage developed across that resistor is then sampled and latched internally as the OCP trip level until one cycles the input or toggles the EN/SS.

**Feature Description (continued)**

**Figure 13. Start-Up Sequence and Timing**

The voltage at EN/SS is internally clamped to 1.3 V before and/or during calibration to minimize the discharging time once calibration. The discharging current is from an internal current source of 140  $\mu$ A and it pulls the voltage down to 0.4 V. The discharging current then initiates the soft-start by charging up the capacitor using an internal current source of 10  $\mu$ A. The resulting voltage ramp on this pin is used as a second noninverting input to the error amplifier after an 800 mV (typical) downward level-shift; therefore, actual soft-start does not occur until the voltage at this pin reaches 800 mV.

If EN/SS is left floating, the controller starts automatically. EN/SS must be pulled down to less than 270 mV to ensure that the chip is in shutdown mode.

**7.3.3 Soft-Start Time**

The soft-start time of the TPS4030x is user programmable by selecting a single capacitor. The EN/SS pin sources 10  $\mu$ A to charge this capacitor. The actual output ramp-up time is the amount of time that it takes for the 10  $\mu$ A to charge the capacitor through a 600-mV range. There is some initial lag due to calibration and an offset (800 mV) from the actual EN/SS pin voltage to the voltage applied to the error amplifier.

The soft-start is done in a closed-loop fashion, meaning that the error amplifier controls the output voltage at all times during the soft-start period and the feedback loop is never open as occurs in duty cycle limit soft-start schemes. The error amplifier has two non-inverting inputs, one connected to the 600-mV reference voltage, and the other connected to the offset EN/SS pin voltage. The lower of these two voltages is what the error amplifier controls the FB pin. As the voltage on the EN/SS pin ramps up past approximately 1.4 V (800-mV offset voltage plus the 600 mV reference voltage), the 600-mV reference voltage becomes the dominant input and the converter has reached its final regulation voltage.

The capacitor required for a given soft-start ramp time for the output voltage is given by [Equation 1](#).

$$C_{SS} = \left( \frac{I_{SS}}{V_{FB}} \right) \times t_{SS}$$

where

- $C_{SS}$  is the required capacitance on the EN/SS pin. (F)
- $I_{SS}$  is the soft-start source current (10  $\mu$ A).
- $V_{FB}$  is the feedback reference voltage (0.6 V).
- $t_{SS}$  is the desired soft-start ramp time (s).

(1)

## Feature Description (continued)

### 7.3.4 Oscillator and Frequency Spread Spectrum (FSS)

The oscillator frequency is internally fixed. The TPS40303 operating frequency is 300 kHz, the TPS40304 operating frequency is 600 kHz, and the TPS40305 operating frequency is 1.2 MHz.

Connecting a resistor with a value of 267 kΩ ±10% from BP to EN/SS enables the FSS feature. When the FSS is enabled, it spreads the internal oscillator frequency over a minimum 12% window using a 25-kHz modulation frequency with triangular profile. By modulating the switching frequency, side-bands are created. The emission power of the fundamental switching frequency and its harmonics is distributed into smaller pieces scattered around many sideband frequencies. The effect significantly reduces the peak EMI noise and makes it much easier for the resultant emission spectrum to pass EMI regulations.

### 7.3.5 Overcurrent Protection

Programmable OCP level at LDRV is from 6 mV to 150 mV at room temperature with 3000 ppm temperature coefficient to help compensate for changes in the low-side FET channel resistance as temperature increases. With a scale factor of 2, the actual trip point across the low-side FET is in the range of 12 mV to 300 mV. The accuracy of the internal current source is ±5%. Overall offset voltage, including the offset voltage of the internal comparator and the amplifier for scale factor of 2, is limited to ±8 mV.

Maximum clamp voltage at LDRV is 340 mV to avoid turning on the low-side FET during calibration and in a prebiased condition. The maximum clamp voltage is fixed and it does not change with temperature. If the voltage drop across R<sub>OCSET</sub> reaches the 340-mV maximum clamp voltage during calibration (no R<sub>OCSET</sub> resistor included), it disables OC protection. Once disabled, there is no low-side or high-side current sensing.

OCP level at HDRV is fixed at 450 mV with 3000-ppm temperature coefficient to help compensate for changes in the high-side FET channel resistance as temperature increases. OCP at HDRV provides pulse-by-pulse current limiting.

OCP sensing at LDRV is a true inductor valley current detection, using sample and hold. [Equation 2](#) can be used to calculate R<sub>OCSET</sub>:

$$R_{OCSET} = \left( \frac{\left( I_{OUT(max)} - \left( \frac{I_{P-P}}{2} \right) \right) \times R_{DS(on)} - V_{OCLOS}}{2 \times I_{OCSET}} \right)$$

where

- I<sub>OCSET</sub> is the internal current source.
- V<sub>OCLOS</sub> is the overall offset voltage.
- I<sub>P-P</sub> is the peak-to-peak inductor current.
- R<sub>DS(on)</sub> is the drain to source ON-resistance of the low-side FET.
- I<sub>OUT(max)</sub> is the trip point for OCP.
- R<sub>OCSET</sub> is the resistor used for setting the OCP level. (2)

To avoid overcurrent tripping in normal operating load range, calculate R<sub>OCSET</sub> using the equation above with:

- The maximum R<sub>DS(ON)</sub> at room temperature
- The lower limit of V<sub>OCLOS</sub> (–8 mV) and the lower limit of I<sub>OCSET</sub> (9.5 μA) from the *Electrical Characteristics* table.
- The peak-to-peak inductor current I<sub>P-P</sub> at minimum input voltage

Overcurrent is sensed across both the low-side FET and the high-side FET. If the voltage drop across either FET exceeds the OC threshold, a count increments one count. If no OC is detected on either FET, the fault counter decrements by one count. If three OC pulses are summed, a fault condition is declared which cycles the soft-start function in a hiccup mode. Hiccup mode consists of four dummy soft-start timeouts followed by a real one if overcurrent condition is encountered during normal operation, or five dummy soft-start timeouts followed by a real one if overcurrent condition occurs from the beginning during start. This cycle continues indefinitely until the fault condition is removed.

## Feature Description (continued)

### 7.3.6 Drivers

The drivers for the external high-side and low-side MOSFETs can drive a gate-to-source voltage of  $V_{BP}$ . The LDRV driver for the low-side MOSFET switches between BP and GND, while the HDRV driver for the high-side MOSFET is referenced to SW and switches between BOOT and SW. The drivers have nonoverlapping timing that is governed by an adaptive delay circuit to minimize body diode conduction in the synchronous rectifier.

### 7.3.7 Prebias Start-Up

The TPS4030x contains a circuit to prevent current from being pulled from the output during start-up in the condition the output is prebiased. There are no PWM pulses until the internal soft-start voltage rises above the error amplifier input (FB pin), if the output is prebiased. Once the soft-start voltage exceeds the error amplifier input, the controller slowly initiates synchronous rectification by starting the synchronous rectifier with a narrow on time. The controller then increments that on time on a cycle-by-cycle basis until it coincides with the time dictated by  $(1-D)$ , where D is the duty cycle of the converter. This approach prevents the sinking of current from a prebiased output, and ensures the output voltage start-up and ramp to regulation is smooth and controlled.

### 7.3.8 Power Good

The TPS4030x provides an indication that output is good for the converter. This is an open-drain signal and pulls low when any condition exists that would indicate that the output of the supply might be out of regulation. These conditions include the following:

- $V_{FB}$  is more than  $\pm 12.5\%$  from nominal.
- Soft-start is active.
- A short-circuit condition has been detected.

---

#### NOTE

When there is no power to the device, PGOOD is not able to pull close to GND if an auxiliary supply is used for the power good indication. In this case, a built-in resistor connected from drain to gate on the PGOOD pulldown device makes the PGOOD pin look approximately like a diode to GND.

---

### 7.3.9 Thermal Shutdown

If the junction temperature of the device reaches the thermal shutdown limit of  $145^{\circ}\text{C}$ , the PWM and the oscillator are turned off and HDRV and LDRV are driven low. When the junction cools to the required level ( $125^{\circ}\text{C}$  typical), the PWM initiates soft-start as during a normal power-up cycle.

## 7.4 Device Functional Modes

### 7.4.1 Modes of Operation

#### 7.4.1.1 UVLO

In UVLO, VDD is less than UVLO\_ON, the BP6 regulator is off, and the HDRV and LDRV are held low by internal passive discharge resistors.

#### 7.4.1.2 Disable

Disable is forced by holding SS/EN below 0.4 V. In disable, the BP6 regulator is off, and both HDRV and LDRV are held low by passive discharge resistors.

#### 7.4.1.3 Calibration

Each enable of the TPS4030X3/4/5 devices requires a calibration which lasts approximately 2 ms. During calibration the TPS40303/4/5 devices LDRV and HDRV are held off by their respective pulldown drivers while the device configures as detailed in [Enable Functionality, Start-Up Sequence and Timing](#).

#### 7.4.1.4 Converting

When calibration completes, the TPS40303/4/5 devices ramp their reference voltage as described in [Soft-Start Time](#), and the states of the LDRV and HDRV drivers are dictated by the COMP pin to regulate the FB pin equal to the internal reference.

## 8 Application and Implementation

### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

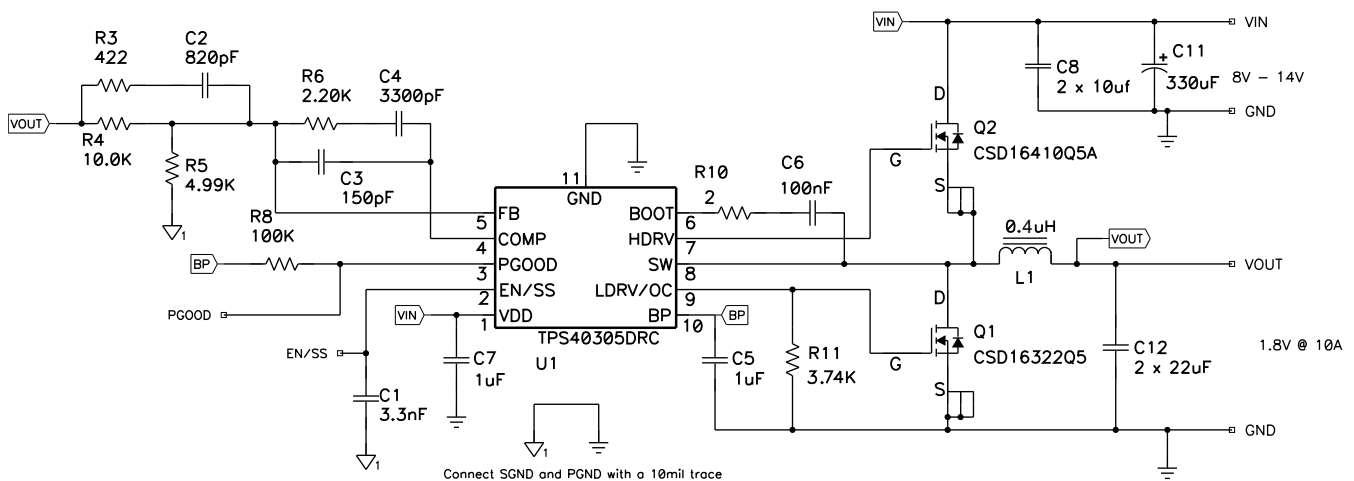
### 8.1 Application Information

The TPS4030x is a family of cost-optimized synchronous buck controllers providing high-end features to construct high-performance DC-DC converters. Prebias capability eliminates concerns about damaging sensitive loads during start-up. Programmable overcurrent protection levels and hiccup overcurrent fault recovery maximize design flexibility and minimize power dissipation in the event of a prolonged output short. Frequency Spread Spectrum (FSS) feature reduces peak EMI noise by spreading the initial energy of each harmonic along a frequency band, thus giving a wider spectrum with lower amplitudes.

### 8.2 Typical Applications

#### 8.2.1 Using the TPS40305 for a 12-V to 1.8-V Point-of-Load Synchronous Buck Regulator

Figure 14 shows 12-V to 1.8-V at 10-A synchronous buck application using the TPS40305 switching at 1200 kHz.



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Figure 14. TPS40305 Design Example Schematic

## Typical Applications (continued)

### 8.2.1.1 Design Requirements

For this example, follow the design parameters listed in [Table 1](#).

**Table 1. Design Example Electrical Characteristics**

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$V_{IN}$	Input voltage		8		14	V
$V_{IN(ripple)}$	Input ripple	$I_{OUT} = 10\text{ A}$			0.6	V
$V_{OUT}$	Output voltage	$0\text{ A} \leq I_{OUT} \leq 10\text{ A}$	1.764	1.800	1.836	V
	Line regulation	$8\text{ V} \leq V_{IN} \leq 14\text{ V}$			0.5%	
	Load regulation	$0\text{ A} \leq I_{OUT} \leq 10\text{ A}$			0.5%	
$V_{RIPPLE}$	Output ripple	$I_{OUT} = 10\text{ A}$			36	mV
$V_{OVER}$	Output overshoot	$I_{OUT}$ falling from 7 A to 3 A		100		mV
$V_{UNDER}$	Output undershoot	$I_{OUT}$ rising from 3 A to 7 A		100		mV
$I_{OUT}$	Output current	$4.5\text{ V} \leq V_{IN} \leq 5.5\text{ V}$	0		10	A
$t_{SS}$	Soft-start time	$V_{IN} = 12\text{ V}$		1.5		ms
$I_{SCP}$	Short-circuit current trip point		13	15		A
$f_{SW}$	Switching frequency			1200		kHz
	Size			1		in <sup>2</sup>

The bill of materials for this application is shown in [Table 2](#). The efficiency, line, and load regulation from boards built using this design are shown in [Figure 14](#). Gerber files and additional application information are available from the factory.

**Table 2. Design Example List of Materials**

REFERENCE DESIGNATOR	QTY	VALUE	DESCRIPTION	SIZE	PART NUMBER	MFR
C1	1	3.3 nF	Capacitor, Ceramic, 10 V, X7R, 20%	0603	Std	Std
C2	1	820 pF	Capacitor, Ceramic, 25 V, X7R, 10%	0603	Std	Std
C3	1	150 pF	Capacitor, Ceramic, 25 V, X7R, 10%	0603	Std	Std
C4	1	3300 pF	Capacitor, Ceramic, 25 V, X7R, 10%	0603	Std	Std
C5	1	1.0 $\mu$ F	Capacitor, Ceramic, 10 V, X7R, 20%	0805	Std	Std
C6	1	100 nF	Capacitor, Ceramic, 16 V, X7R, 20%	0603	Std	Std
C7	1	1 $\mu$ F	Capacitor, Ceramic, 25 V, X7R, 20%	0805	Std	Std
C8	2	10 $\mu$ f	Capacitor, Ceramic, 25 V, X7R, 10%	1210	Std	Std
C11	1	330 $\mu$ F	Capacitor, Aluminum, 25 V, $\pm$ 20%, 160 m $\Omega$	0.328 x 0.390 inch	EEVFK1E331P	Panasonic
C12	2	22 $\mu$ F	Capacitor, Ceramic, 6.3 V, X5R, 20%	0805	Std	Std
L1	1	0.32 $\mu$ H	Inductor, SMT, 17 A	0.268 x 0.268 inch	PG0083.401	Pulse
Q1	1		MOSFET, N-Channel, 25 V, 97 A, 4.6 m $\Omega$	QFN-8 POWER	CSD16322Q5	TI
Q2	1		MOSFET, N-Channel, 25 V, 59 A, 9.6 m $\Omega$	QFN-8 POWER	CSD16410Q5A	TI
R3	1	422 $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
R4	1	10.0 k $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
R5	1	4.99 k $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
R6	1	2.20 k $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
R8	1	100 k $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
R10	1	2 $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
R11	1	3.74 k $\Omega$	Resistor, Chip, 1/16W, 1%	0603	Std	Std
U1	1		IC, 3-V to 20-V sync. 1.2-MHz Buck controller	DRC10	TPS40305DRC	TI

## 8.2.1.2 Detailed Design Procedure

### 8.2.1.2.1 Custom Design With WEBENCH® Tools

[Click here](#) to create a custom design using the TPS4030x device with the WEBENCH® Power Designer.

1. Start by entering the input voltage ( $V_{IN}$ ), output voltage ( $V_{OUT}$ ), and output current ( $I_{OUT}$ ) requirements.
2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at [www.ti.com/WEBENCH](http://www.ti.com/WEBENCH).

### 8.2.1.2.2 Selecting the Switching Frequency

To achieve the small size for this design, the TPS40305, with  $f_{SW} = 1200$  kHz, is selected for minimal external component size.

### 8.2.1.2.3 Inductor Selection (L1)

Synchronous buck power inductors are typically sized for approximately 30% peak-to-peak ripple current ( $I_{RIPPLE}$ )

Given this target ripple current, the required inductor size can be calculated in [Equation 3](#).

$$L \approx \frac{V_{IN(max)} - V_{OUT}}{0.3 \times I_{OUT}} \times \frac{V_{OUT}}{V_{IN(max)}} \times \frac{1}{f_{SW}} = \frac{14\text{ V} - 1.8\text{ V}}{0.3 \times 10\text{ A}} \times \frac{1.8\text{ V}}{14\text{ V}} \times \frac{1}{1200\text{ kHz}} = 471\text{ nH} \quad (3)$$

Selecting a standard 400-nH inductor value, solve for  $I_{RIPPLE} = 3.5$  A

The RMS current through the inductor is approximated by [Equation 4](#).

$$I_{L(rms)} = \sqrt{I_{L(avg)}^2 + \frac{1}{12} I_{RIPPLE}^2} = \sqrt{I_{OUT}^2 + \frac{1}{12} I_{RIPPLE}^2} = \sqrt{10^2 + \frac{1}{12} 3.5^2} = 10.05\text{ A} \quad (4)$$

### 8.2.1.2.4 Output Capacitor Selection (C12)

The selection of the output capacitor is typically driven by the output transient response. [Equation 5](#) and [Equation 6](#) overestimate the voltage deviation to account for delays in the loop bandwidth and can be used to determine the required output capacitance.

$$V_{OVER} < \frac{I_{TRAN}}{C_{OUT}} \times \Delta T = \frac{I_{TRAN}}{C_{OUT}} \times \frac{I_{TRAN} \times L}{V_{OUT}} = \frac{I_{TRAN}^2 \times L}{V_{OUT} \times C_{OUT}} \quad (5)$$

$$V_{UNDER} < \frac{I_{TRAN}}{C_{OUT}} \times \Delta T = \frac{I_{TRAN}}{C_{OUT}} \times \frac{I_{TRAN} \times L}{V_{IN} - V_{OUT}} = \frac{I_{TRAN}^2 \times L}{(V_{IN} - V_{OUT}) \times C_{OUT}} \quad (6)$$

If  $V_{IN(min)} > 2 \times V_{OUT}$ , use overshoot ([Equation 5](#)) to calculate minimum output capacitance. If  $V_{IN(min)} < 2 \times V_{OUT}$ , use undershoot ([Equation 6](#)) to calculate minimum output capacitance.

$$C_{OUT(min)} = \frac{I_{TRAN(max)}^2 \times L}{(V_{OUT}) \times V_{OVER}} = \frac{4^2 \times 400\text{ nH}}{1.8 \times 100\text{ mV}} = 35\text{ }\mu\text{F} \quad (7)$$

With a minimum capacitance, the maximum allowable ESR is determined by the maximum ripple voltage and is approximated by [Equation 8](#).

$$ESR_{MAX} = \frac{V_{RIPPLE(total)} - V_{RIPPLE(cap)}}{I_{RIPPLE}} = \frac{V_{RIPPLE(total)} - \left( \frac{I_{RIPPLE}}{8 \times C_{OUT} \times f_{SW}} \right)}{I_{RIPPLE}}$$

$$= \frac{36\text{mV} - \left( \frac{3.5\text{A}}{8 \times 35\mu\text{F} \times 1200\text{kHz}} \right)}{3.5\text{A}} = 7\text{m}\Omega \quad (8)$$

Two 0805, 22- $\mu\text{F}$ , 6.3-V, X5R ceramic capacitors are selected to provide more than 35  $\mu\text{F}$  of minimum capacitance and less than 7 m $\Omega$  of ESR (2.5 m $\Omega$  each).

#### 8.2.1.2.5 Peak Current Rating of Inductor

With output capacitance, it is possible to calculate the charge current during start-up and determine the minimum saturation current rating for the inductor. The start-up charging current is approximated by [Equation 9](#).

$$I_{CHARGE} = \frac{V_{OUT} \times C_{OUT}}{t_{SS}} = \frac{1.8\text{V} \times 2 \times 22\mu\text{F}}{1.5\text{ms}} = 0.053\text{A} \quad (9)$$

$$I_{L(peak)} = I_{OUT(max)} + \frac{1}{2}I_{RIPPLE} + I_{CHARGE} = 10\text{A} + \frac{1}{2} \times 3.5\text{A} + 0.053\text{A} = 11.8\text{A} \quad (10)$$

**Table 3. Inductor Requirements**

SYMBOL	PARAMETER	VALUE	UNIT
L	Inductance	400	nH
$I_{L(rms)}$	RMS current (thermal rating)	10.05	A
$I_{L(peak)}$	Peak current (saturation rating)	11.8	A

A PG0083.401, 400-nH inductor is selected for its small size, low DCR (3.0 m $\Omega$ ) and high-current handling capability (17-A thermal, 27-A saturation).

#### 8.2.1.2.6 Input Capacitor Selection (C8)

The input voltage ripple is divided between capacitance and ESR. For this design  $V_{RIPPLE(cap)} = 150\text{mV}$  and  $V_{RIPPLE(esr)} = 150\text{mV}$ . The minimum capacitance and maximum ESR are estimated by [Equation 11](#).

$$C_{IN(min)} = \frac{I_{LOAD} \times V_{OUT}}{V_{RIPPLE(cap)} \times V_{IN} \times f_{SW}} = \frac{10 \times 1.8\text{V}}{150\text{mV} \times 8\text{V} \times 1200\text{kHz}} = 12.5\mu\text{F} \quad (11)$$

$$ESR_{MAX} = \frac{V_{RIPPLE(esr)}}{I_{LOAD} + \frac{1}{2}I_{RIPPLE}} = \frac{150\text{mV}}{11.75\text{A}} = 12.7\text{m}\Omega \quad (12)$$

The RMS current in the input capacitors is estimated by [Equation 13](#).

$$I_{RMS(cin)} = I_{LOAD} \times \sqrt{D \times (1 - D)} = 10\text{A} \times \sqrt{0.225 \times (1 - 0.225)} = 4.17\text{A}_{RMS} \quad (13)$$

Two 1210, 10- $\mu\text{F}$ , 25-V, X5R ceramic capacitors with approximately 2-m $\Omega$  of ESR and a 2.5-A RMS current rating each are selected. Higher voltage capacitors are selected to minimize capacitance loss at the DC bias voltage to ensure the capacitors allow sufficient capacitance at the working voltage.

#### 8.2.1.2.7 MOSFET Switch Selection (Q1 and Q2)

Reviewing available TI NexFET MOSFETs using TI's NexFET MOSFET selection tool, the CSD16410Q5A and CSD16322Q5 5-mm  $\times$  6-mm MOSFETs are selected.

These two FETs have maximum total gate charges of 5 nC and 10 nC, respectively, which draws 18 mA at 1.2 MHz from the BP regulator, less than its 50 mA minimum rating.

### 8.2.1.2.8 Bootstrap Capacitor (C6)

To ensure proper charging of the high-side FET gate, limit the ripple voltage on the boost capacitor to less than 50 mV.

$$C_{\text{BOOST}} = 20 \times Q_{G2} = 20 \times 5 \text{ nC} = 100 \text{ nF} \quad (14)$$

### 8.2.1.2.9 VDD Bypass Capacitor (C7)

Per the TPS40305 [Electrical Characteristics](#) specifications, select a 1.0- $\mu\text{F}$  X5R or better ceramic bypass capacitor for VDD.

### 8.2.1.2.10 BP Bypass Capacitor (C5)

As listed in the [Electrical Characteristics](#), a minimum of 1.0- $\mu\text{F}$  ceramic capacitance is required to stabilize the BP regulator. To limit regulator noise to less than 10 mV, the value of the bypass capacitor is calculated in [Equation 15](#).

$$C_{\text{BP}} = 100 \times \text{MAX}(Q_{G1}, Q_{G2}) \quad (15)$$

Because Q1 is larger than Q2, and the total gate charge of Q1 is 10 nC, a BP capacitor of 1.0  $\mu\text{F}$  is calculated. A standard value of 1.0  $\mu\text{F}$  is selected to limit noise on the BP regulator.

### 8.2.1.2.11 Short-Circuit Protection (R11)

The TPS40305 uses the negative drop across the low-side FET at the end of the OFF time to measure the inductor current. Allowing for 30% over maximum load and 20% rise in  $R_{\text{DS(on)Q1}}$  for self-heating, the voltage drop across the low-side FET at current limit is given by [Equation 16](#).

$$V_{\text{OC}} = (1.3 \times I_{\text{LOAD}} - \frac{1}{2} I_{\text{RIPPLE}}) \times 1.2 \times R_{\text{DS(on)Q1}} = (1.3 \times 10 \text{ A} - \frac{1}{2} 3.5 \text{ A}) \times 1.2 \times 4.6 \text{ m}\Omega = 62.1 \text{ mV} \quad (16)$$

The TPS40305 internal temperature coefficient helps compensate for the  $R_{\text{DS(on)}}$  temperature coefficient of the MOSFET, so the current limit programming resistor is selected by [Equation 17](#).

$$R_{\text{CS}} = \frac{V_{\text{OC}} - V_{\text{OCLOS(min)}}}{2 \times I_{\text{OCSET(min)}}} = \frac{62.1 \text{ mV} - (-8 \text{ mV})}{2 \times 9.5 \text{ mA}} = 3.69 \text{ k}\Omega \approx 3.74 \text{ k}\Omega \quad (17)$$

### 8.2.1.2.12 Feedback Divider (R4, R5)

The TPS40305 controller uses a full operational amplifier with an internally fixed 0.600-V reference. R4 is selected between 10 k $\Omega$  and 50 k $\Omega$  for a balance of feedback current and noise immunity. With R4 set to 10 k $\Omega$ , The output voltage is programmed with a resistor divider given by [Equation 18](#).

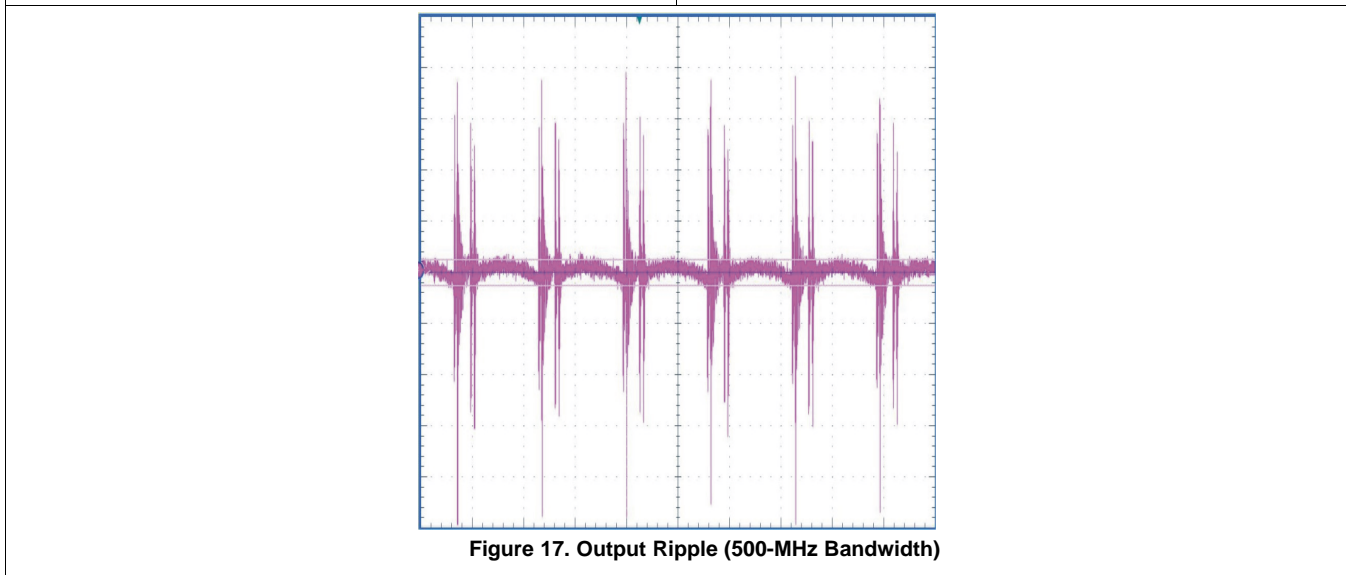
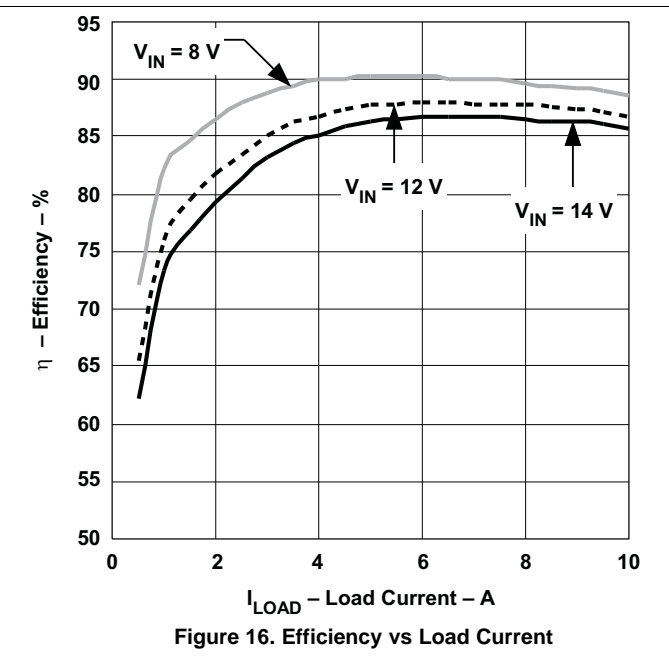
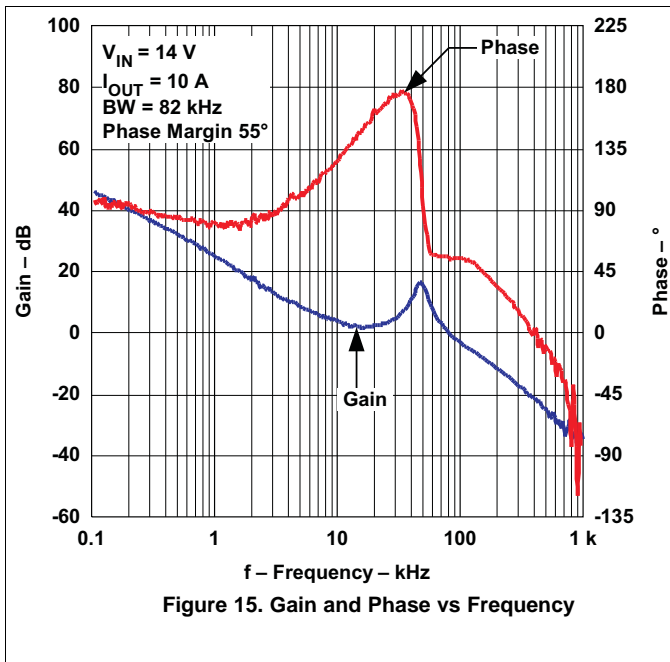
$$R5 = \frac{V_{\text{FB}} \times R4}{V_{\text{OUT}} - V_{\text{FB}}} = \frac{0.600 \text{ V} \times 10.0 \text{ k}\Omega}{1.8 \text{ V} - 0.600 \text{ V}} = 5.0 \text{ k}\Omega \approx 4.99 \text{ k}\Omega \quad (18)$$

### 8.2.1.2.13 Compensation: (C2, C3, C4, R3, R6)

Using the TPS40k Loop Stability Tool for 100-kHz bandwidth and 60° phase margin with a R4 value of 10.0 k $\Omega$ , the following values are returned.

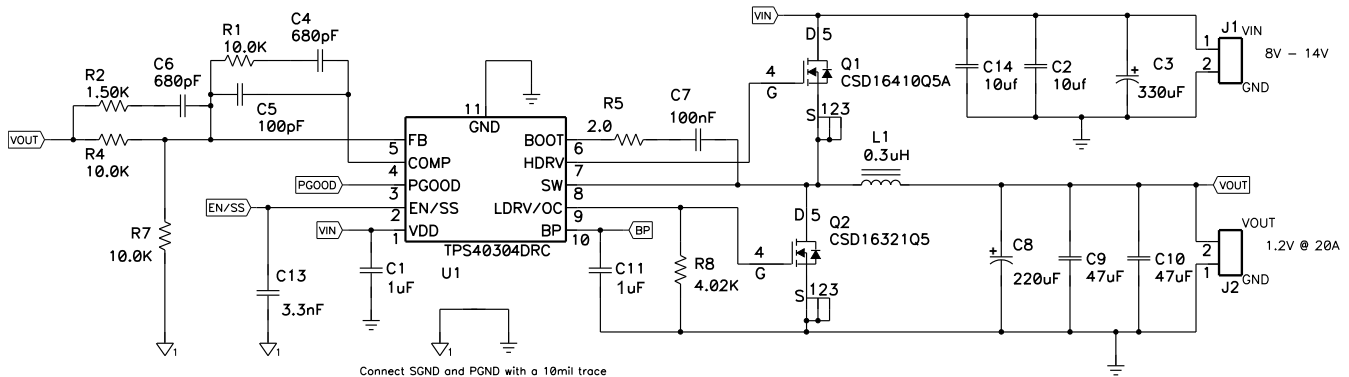
- C2 = C\_1 = 820 pF
- C3 = C\_3 = 150 pF
- C4 = C\_2 = 3300 pF
- R3 = R\_2 = 422  $\Omega$
- R6 = R\_3 = 2.20 k $\Omega$

8.2.1.3 Application Curves



### 8.2.2 A High-Current, Low-Voltage Design Using the TPS40304

For this 20-A, 12-V to 1.2-V design, the 600-kHz TPS40304 was selected for a balance between small size and high efficiency.



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Figure 18. TPS40304 Design Example Schematic

#### 8.2.2.1 Design Requirements

For this example, follow the design parameters listed in Table 4.

Table 4. Design Example Electrical Characteristics

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
V <sub>IN</sub>	Input voltage		8		14	V
V <sub>IN</sub> ripple	Input ripple	I <sub>OUT</sub> = 20 A			0.5	V
V <sub>OUT</sub>	Output voltage	0 A ≤ I <sub>OUT</sub> ≤ 20 A	1.164	1.200	1.236	V
	Line regulation	8 V ≤ V <sub>IN</sub> ≤ 14 V			0.5%	
	Load regulation	0 A ≤ I <sub>OUT</sub> ≤ 20 A			0.5%	
V <sub>RIPPLE</sub>	Output ripple	I <sub>OUT</sub> = 20 A			36	mV
V <sub>OVER</sub>	Output overshoot	5 A ≤ I <sub>OUT</sub> ≤ 15 A		100		mV
V <sub>UNDER</sub>	Output undershoot	5 A ≤ I <sub>OUT</sub> ≤ 15 A		100		mV
I <sub>OUT</sub>	Output current	8 V ≤ V <sub>IN</sub> ≤ 14 V	0		20	A
t <sub>SS</sub>	Soft-start time	V <sub>IN</sub> = 12 V		1.5		ms
I <sub>SCP</sub>	Short-circuit current trip point		26			A
f <sub>SW</sub>	Switching frequency			600		kHz
	Size				1.5	in <sup>2</sup>

#### 8.2.2.2 Detailed Design Procedure

##### 8.2.2.2.1 Selecting the Switching Frequency

To achieve the small size for this design the TPS40304, with f<sub>SW</sub> = 600 kHz, is selected for minimal external component size.

##### 8.2.2.2.2 Inductor Selection (L1)

Synchronous buck power inductors are typically sized for approximately 30% peak-to-peak ripple current (I<sub>RIPPLE</sub>)

Given this target ripple current, the required inductor size can be calculated in Equation 19.

$$L \approx \frac{V_{IN(max)} - V_{OUT}}{0.3 \times I_{OUT}} \times \frac{V_{OUT}}{V_{IN(max)}} \times \frac{1}{F_{SW}} = \frac{14V - 1.2V}{0.3 \times 20A} \times \frac{1.2V}{14V} \times \frac{1}{600kHz} = 305nH \quad (19)$$

Selecting a standard 300-nH inductor value, solve for I<sub>RIPPLE</sub> = 6 A

The RMS current through the inductor is approximated by [Equation 20](#).

$$I_{L_{rms}} = \sqrt{I_{L_{avg}}^2 + \frac{1}{12} I_{RIPPLE}^2} = \sqrt{I_{OUT}^2 + \frac{1}{12} I_{RIPPLE}^2} = \sqrt{20^2 + \frac{1}{12} 6^2} = 20.07 \text{ A} \quad (20)$$

### 8.2.2.2.3 Output Capacitor Selection (C12)

The selection of the output capacitor is typically driven by the output transient response. [Equation 21](#) and [Equation 22](#) overestimate the voltage deviation to account for delays in the loop bandwidth and can be used to determine the required output capacitance.

$$V_{OVER} < \frac{I_{TRAN}}{C_{OUT}} \times \Delta T = \frac{I_{TRAN}}{C_{OUT}} \times \frac{I_{TRAN} \times L}{V_{OUT}} = \frac{I_{TRAN}^2 \times L}{V_{OUT} \times C_{OUT}} \quad (21)$$

$$V_{UNDER} < \frac{I_{TRAN}}{C_{OUT}} \times \Delta T = \frac{I_{TRAN}}{C_{OUT}} \times \frac{I_{TRAN} \times L}{V_{IN} - V_{OUT}} = \frac{I_{TRAN}^2 \times L}{(V_{IN} - V_{OUT}) \times C_{OUT}} \quad (22)$$

If  $V_{IN(min)} > 2 \times V_{OUT}$ , use overshoot ([Equation 21](#)) to calculate minimum output capacitance. If  $V_{IN(min)} < 2 \times V_{OUT}$ , use undershoot ([Equation 22](#)) to calculate minimum output capacitance.

$$C_{OUT(MIN)} = \frac{I_{TRAN(MAX)}^2 \times L}{(V_{OUT}) \times V_{OVER}} = \frac{10^2 \times 300\text{nH}}{1.2 \times 100\text{mV}} = 250\mu\text{F} \quad (23)$$

With a minimum capacitance, the maximum allowable ESR is determined by the maximum ripple voltage and is approximated by [Equation 24](#).

$$ESR_{max} = \frac{V_{RIPPLE(Total)} - V_{RIPPLE(CAP)}}{I_{RIPPLE}} = \frac{V_{RIPPLE(total)} - \left( \frac{I_{RIPPLE}}{8 \times C_{OUT} \times F_{SW}} \right)}{I_{RIPPLE}} = \frac{36\text{mV} - \left( \frac{6\text{A}}{8 \times 250\mu\text{F} \times 600\text{kHz}} \right)}{6\text{A}} = 5.2\text{m}\Omega \quad (24)$$

Two 47- $\mu\text{F}$  and one 220- $\mu\text{F}$  capacitors are selected to provide more than 250  $\mu\text{F}$  of minimum capacitance and 5.2  $\text{m}\Omega$  of ESR.

### 8.2.2.2.4 Peak Current Rating of Inductor

With output capacitance, it is possible to calculate the charge current during start-up and determine the minimum saturation current rating for the inductor. The start-up charging current is approximated by [Equation 25](#).

$$I_{CHARGE} = \frac{V_{OUT} \times C_{OUT}}{T_{SS}} = \frac{1.2 \text{ V}(2 \times 47 \mu\text{F} + 220 \mu\text{F})}{1.5 \text{ ms}} = 0.251 \text{ A} \quad (25)$$

$$I_{L\_PEAK} = I_{OUT(max)} + \frac{1}{2} I_{RIPPLE} + I_{CHARGE} = 20 \text{ A} + \frac{1}{2} \times 6 \text{ A} + 0.2512 \text{ A} = 23.25 \text{ A} \quad (26)$$

**Table 5. Inductor Requirements**

PARAMETER		VALUE	UNIT
L	Inductance	300	nH
$I_{L(rms)}$	RMS current (thermal rating)	20.07	A
$I_{L(peak)}$	Peak current (saturation rating)	23.25	A

### 8.2.2.2.5 Input Capacitor Selection (C8)

The input voltage ripple is divided between capacitance and ESR. For this design  $V_{\text{RIPPLE}(\text{cap})} = 150 \text{ mV}$  and  $V_{\text{RIPPLE}(\text{esr})} = 150 \text{ mV}$ . The minimum capacitance and maximum ESR are estimated by Equation 27.

$$C_{\text{IN}(\text{min})} = \frac{I_{\text{LOAD}} \times V_{\text{OUT}}}{V_{\text{RIPPLE}(\text{CAP})} \times V_{\text{IN}} \times F_{\text{SW}}} = \frac{20 \times 1.2\text{V}}{150\text{mV} \times 8\text{V} \times 600\text{kHz}} = 33.3\mu\text{F} \quad (27)$$

$$\text{ESR}_{\text{MAX}} = \frac{V_{\text{RIPPLE}(\text{ESR})}}{I_{\text{LOAD}} + \frac{1}{2}I_{\text{RIPPLE}}} = \frac{150 \text{ mV}}{23\text{A}} = 6.5 \text{ m}\Omega \quad (28)$$

The RMS current in the input capacitors is estimated by Equation 29.

$$I_{\text{RMS\_CIN}} = I_{\text{LOAD}} \times \sqrt{D \times (1-D)} = 20 \text{ A} \times \sqrt{0.15 \times (1-0.15)} = 7.14 \text{ Arms} \quad (29)$$

Three 1210, 10- $\mu\text{F}$ , 25-V, X5R ceramic capacitors are selected. Higher voltage capacitors are selected to minimize capacitance loss at the DC bias voltage to ensure the capacitors allow sufficient capacitance at the working voltage.

### 8.2.2.2.6 MOSFET Switch Selection (Q1 and Q2)

Reviewing available TI NexFET MOSFETs using the TI NexFET MOSFET selection tool, the CSD16410Q5A and CSD16321Q5 5-mm  $\times$  6-mm MOSFETs are selected.

These two FETs have maximum total gate charges of 5 nC and 10 nC, respectively.

### 8.2.2.2.7 Bootstrap Capacitor (C6)

To ensure proper charging of the high-side FET gate, limit the ripple voltage on the boost capacitor to less than 50 mV.

$$C_{\text{Boost}} = 20 \times Q_{\text{G1}} = 20 \times 5 \text{ nC} = 100 \text{ nF} \quad (30)$$

### 8.2.2.2.8 VDD Bypass Capacitor (C7)

Per the TPS40304 data sheet, select a 1.0- $\mu\text{F}$  X5R or better ceramic bypass capacitor for VDD.

### 8.2.2.2.9 BP Bypass Capacitor (C5)

Per the TPS40304 data sheet, a minimum 1.0- $\mu\text{F}$  ceramic capacitance is required to stabilize the BP regulator. To limit regulator noise to less than 10 mV, the value of the bypass capacitor is calculated in Equation 31.

$$C_{\text{BP}} = 100 \times \text{MAX}(Q_{\text{G1}}, Q_{\text{G2}}) \quad (31)$$

Because Q2 is larger than Q1, and the total gate charge of Q2 is 10 nC, a BP capacitor of 1.0  $\mu\text{F}$  is calculated. A standard value of 1.0  $\mu\text{F}$  is selected to limit noise on the BP regulator.

### 8.2.2.2.10 Short-Circuit Protection (R11)

The TPS40304 uses the negative drop across the low-side FET at the end of the OFF time to measure the inductor current. Allowing for 30% over maximum load and 20% rise in  $R_{\text{DS}(\text{on})\text{Q1}}$  for self-heating, the voltage drop across the low-side FET at current limit is given by Equation 32.

$$V_{\text{OC}} = (1.3 \times I_{\text{LOAD}} - \frac{1}{2}I_{\text{ripple}}) \times 1.2 \times R_{\text{DS}(\text{on})\text{Q2}} = (1.3 \times 20 \text{ A} - \frac{1}{2} 6 \text{ A}) \times 1.2 \times 4.6 \text{ m}\Omega = 127 \text{ mV} \quad (32)$$

The TPS40304 internal temperature coefficient helps compensate for the MOSFET  $R_{\text{DS}(\text{on})}$  temperature coefficient, so the current limit programming resistor is selected by Equation 33.

$$R_{\text{CS}} = \frac{V_{\text{OC}} - V_{\text{OCL}(\text{min})}}{2 \times I_{\text{OCSET}(\text{min})}} = \frac{127 \text{ mV} - (-8 \text{ mV})}{2 \times 9.5 \mu\text{A}} = 7.1 \text{ k}\Omega \quad (33)$$

**8.2.2.2.11 Feedback Divider (R4, R5)**

The TPS40304 controller uses a full operational amplifier with an internally fixed 0.6-V reference. R4 is selected between 10 k $\Omega$  and 50 k $\Omega$  for a balance of feedback current and noise immunity. With R4 set to 10 k $\Omega$ , The output voltage is programmed with a resistor divider given by [Equation 34](#).

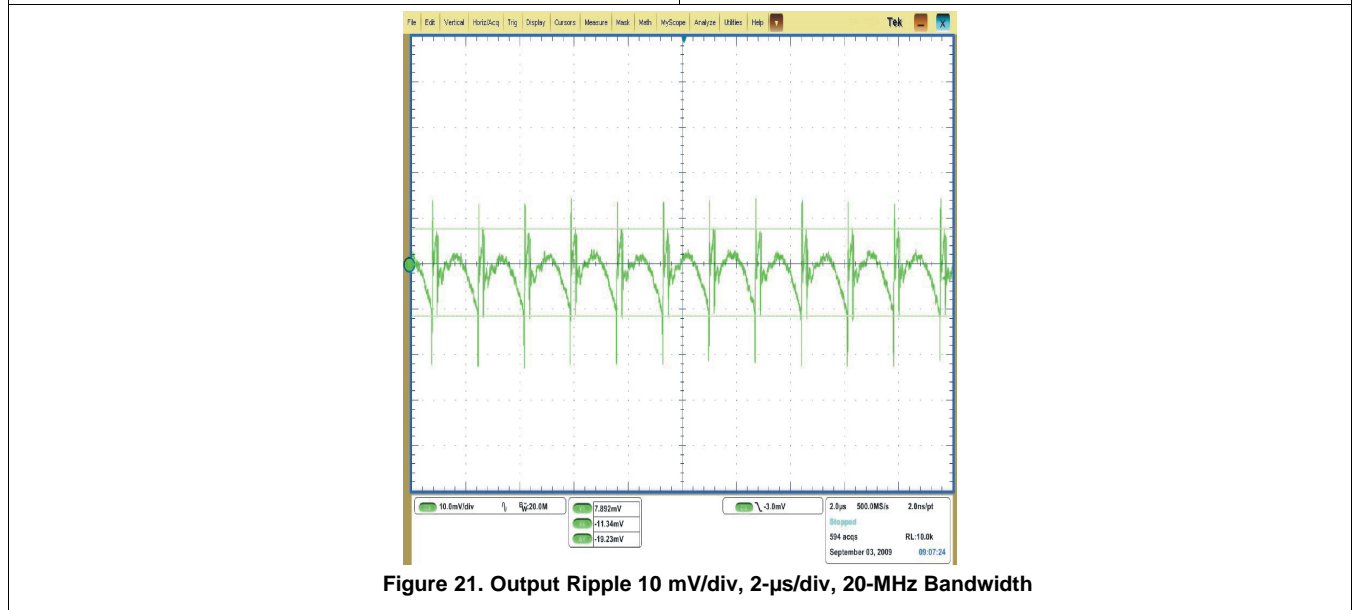
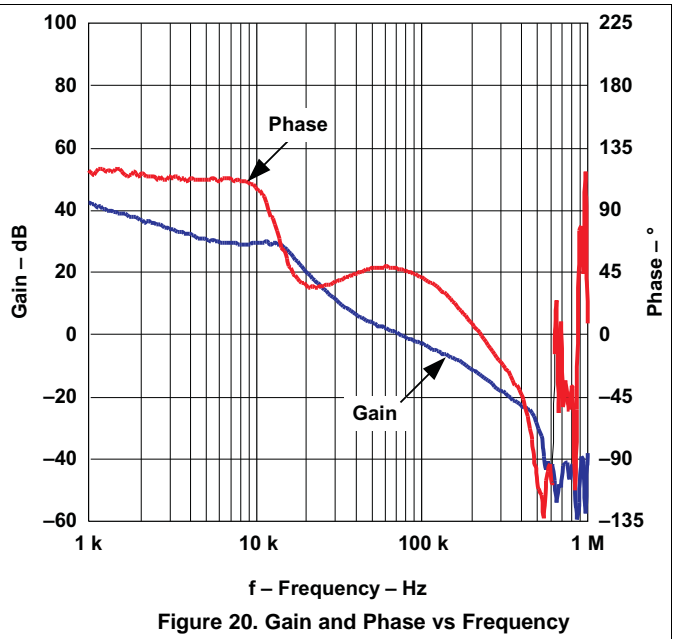
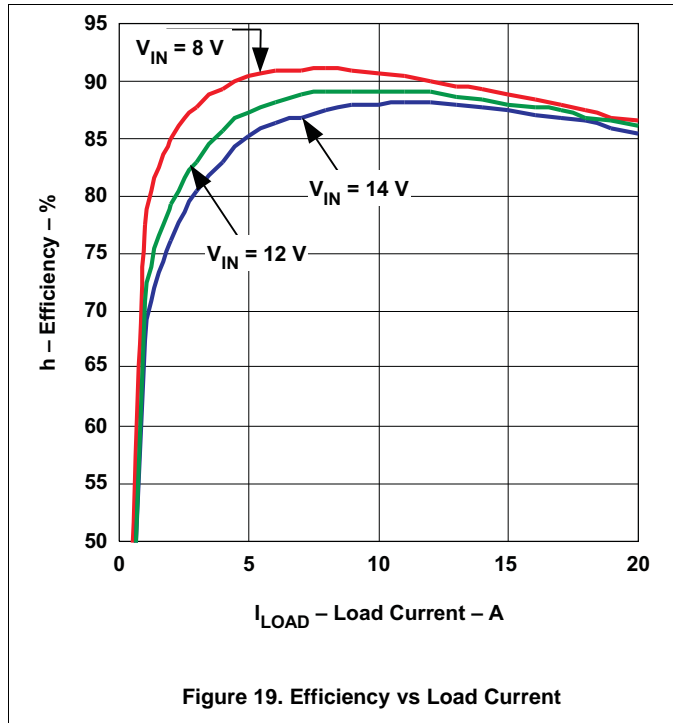
$$R7 = \frac{V_{FB} \times R4}{V_{OUT} - V_{FB}} = \frac{0.600 \text{ V} \times 10.0 \text{ k}\Omega}{1.2 \text{ V} - 0.600 \text{ V}} = 10 \text{ k}\Omega \quad (34)$$

**8.2.2.2.12 Compensation: (C2, C3, C4, R3, R6)**

Using the TPS40k Loop Stability Tool for 100-kHz bandwidth and 60° phase margin with a R4 value of 10.0 k $\Omega$ , the following values are returned.

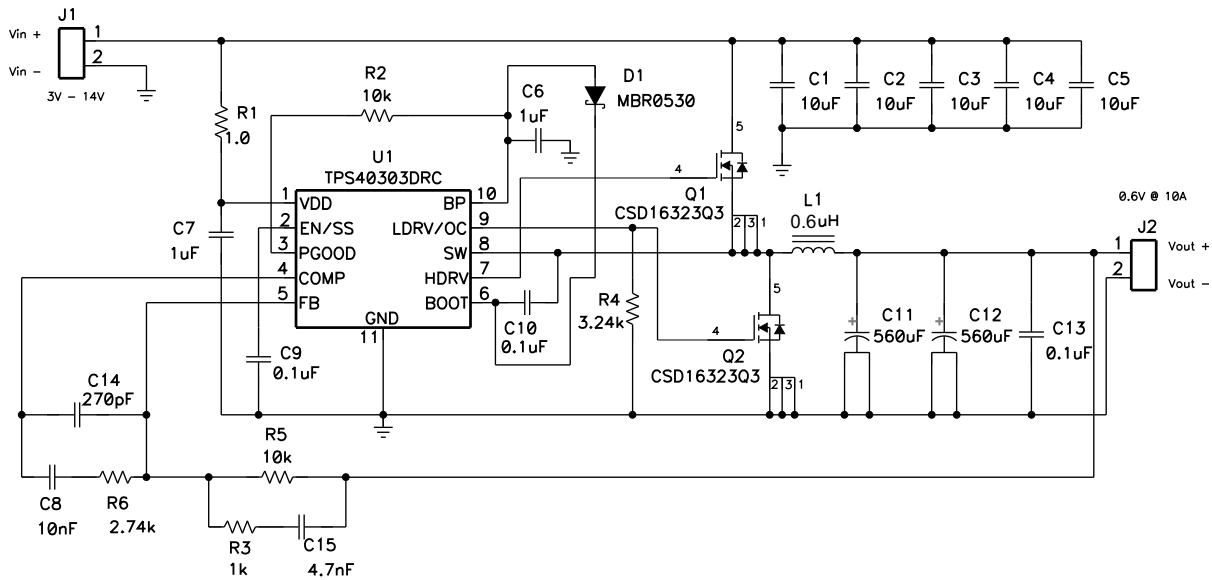
- C4 = 680 pF
- C5 = 100 pF
- C6 = 680 pF
- R1 = 10 k $\Omega$
- R2 = 1.5 k $\Omega$

8.2.2.3 Application Curves



### 8.2.3 A Synchronous Buck Application Using the TPS40303

Figure 22 shows a 3.3-V/5-V/12-V to 0.6-V at 10-A synchronous buck application using the TPS40303 switching at 300 kHz.



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Figure 22. TPS40303 Design Example Schematic

#### 8.2.3.1 Design Requirements

For this example, follow the design parameters listed in Table 6.

Table 6. Design Example Electrical Characteristics

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
$V_{IN}$	Input voltage	3.3		14	V	
$V_{INripple}$	Input ripple			0.6	V	
$V_{OUT}$	Output voltage	0 A $\leq I_{OUT} \leq$ 10 A	0.582	0.6	0.618	V
	Line regulation			0.5%		
	Load regulation			0.5%		
$V_{RIPPLE}$	Output ripple			12	mV	
$V_{OVER}$	Output overshoot		100		mV	
$V_{UNDER}$	Output undershoot		100		mV	
$I_{OUT}$	Output current		0	10	A	
$t_{SS}$	Soft-start time		1.5		ms	
$I_{SCP}$	Short-circuit current trip point		13	15	A	
	Efficiency		84%			
$f_{SW}$	Switching frequency		300		kHz	
	Size			1.5	in <sup>2</sup>	

### 8.2.3.2 Detailed Design Procedure

#### 8.2.3.2.1 Selecting the Switching Frequency

To achieve the small size for this design the TPS40303, with  $f_{SW} = 300$  kHz, is selected for minimal external component size.

#### 8.2.3.2.2 Inductor Selection (L1)

Synchronous buck power inductors are typically sized for approximately 30% peak-to-peak ripple current ( $I_{RIPPLE}$ ). Given this target ripple current, the required inductor size can be calculated in [Equation 35](#).

$$L \approx \frac{V_{IN(max)} - V_{OUT}}{0.3 \times I_{OUT}} \times \frac{V_{OUT}}{V_{IN(max)}} \times \frac{1}{F_{SW}} = \frac{14V - 0.6V}{0.3 \times 10A} \times \frac{0.6V}{14V} \times \frac{1}{300kHz} = 638nH \quad (35)$$

Selecting a standard 600-nH inductor value, solve for  $I_{RIPPLE} = 3.2$  A

The RMS current through the inductor is approximated by [Equation 36](#).

$$I_{Lrms} = \sqrt{I_{Lavg}^2 + \frac{1}{12} I_{RIPPLE}^2} = \sqrt{I_{OUT}^2 + \frac{1}{12} I_{RIPPLE}^2} = \sqrt{10^2 + \frac{1}{12} 3.2^2} = 10.04A \quad (36)$$

#### 8.2.3.2.3 Output Capacitor Selection (C12)

The selection of the output capacitor is typically driven by the output transient response. [Equation 37](#) and [Equation 38](#) overestimate the voltage deviation to account for delays in the loop bandwidth and can be used to determine the required output capacitance.

$$V_{OVER} < \frac{I_{TRAN}}{C_{OUT}} \times \Delta T = \frac{I_{TRAN}}{C_{OUT}} \times \frac{I_{TRAN} \times L}{V_{OUT}} = \frac{I_{TRAN}^2 \times L}{V_{OUT} \times C_{OUT}} \quad (37)$$

$$V_{UNDER} < \frac{I_{TRAN}}{C_{OUT}} \times \Delta T = \frac{I_{TRAN}}{C_{OUT}} \times \frac{I_{TRAN} \times L}{V_{IN} - V_{OUT}} = \frac{I_{TRAN}^2 \times L}{(V_{IN} - V_{OUT}) \times C_{OUT}} \quad (38)$$

If  $V_{IN(min)} > 2 \times V_{OUT}$ , use overshoot ([Equation 37](#)) to calculate minimum output capacitance. If  $V_{IN(min)} < 2 \times V_{OUT}$ , use undershoot ([Equation 38](#)) to calculate minimum output capacitance.

$$C_{OUT(MIN)} = \frac{I_{TRAN(MAX)}^2 \times L}{(V_{OUT}) \times V_{OVER}} = \frac{4^2 \times 600 \text{ nH}}{0.6 \times 100 \text{ mV}} = 160 \mu F \quad (39)$$

With a minimum capacitance, the maximum allowable ESR is determined by the maximum ripple voltage and is approximated by [Equation 40](#).

$$ESR_{max} = \frac{V_{RIPPLE(Total)} - V_{RIPPLE(CAP)}}{I_{RIPPLE}} = \frac{V_{RIPPLE(total)} - \left( \frac{I_{RIPPLE}}{8 \times C_{OUT} \times F_{SW}} \right)}{I_{RIPPLE}} = \frac{36 \text{ mV} - \left( \frac{3.2 \text{ A}}{8 \times 160 \mu F \times 300 \text{ kHz}} \right)}{3.2 \text{ A}} = 8.6 \text{ m}\Omega \quad (40)$$

Two 560- $\mu$ F capacitors are selected to provide more than 160- $\mu$ F of minimum capacitance and less than 8.6 m $\Omega$  of ESR.

### 8.2.3.2.4 Peak Current Rating of Inductor

With output capacitance, it is possible to calculate the charge current during start-up and determine the minimum saturation current rating for the inductor. The start-up charging current is approximated by [Equation 41](#).

$$I_{\text{CHARGE}} = \frac{V_{\text{OUT}} \times C_{\text{OUT}}}{T_{\text{SS}}} = \frac{0.6 \text{ V}(2 \times 560 \mu\text{F})}{1.5 \text{ ms}} = 0.448 \text{ A} \quad (41)$$

$$I_{\text{L\_PEAK}} = I_{\text{OUT(max)}} + \frac{1}{2}I_{\text{RIPPLE}} + I_{\text{CHARGE}} = 10\text{A} + \frac{1}{2} \times 3.2\text{A} + 0.448\text{A} = 12.05\text{A} \quad (42)$$

**Table 7. Inductor Requirements**

PARAMETER		VALUE	UNIT
L	Inductance	600	nH
$I_{\text{L(rms)}}$	RMS current (thermal rating)	10.04	A
$I_{\text{L(peak)}}$	Peak current (saturation rating)	12.05	A

### 8.2.3.2.5 Input Capacitor Selection (C8)

The input voltage ripple is divided between capacitance and ESR. For this design  $V_{\text{RIPPLE(cap)}} = 150 \text{ mV}$  and  $V_{\text{RIPPLE(esr)}} = 150 \text{ mV}$ . The minimum capacitance and maximum ESR are estimated by [Equation 43](#).

$$C_{\text{IN(min)}} = \frac{I_{\text{LOAD}} \times V_{\text{OUT}}}{V_{\text{RIPPLE(CAP)}} \times V_{\text{IN}} \times F_{\text{SW}}} = \frac{10 \times 0.6 \text{ V}}{150 \text{ mV} \times 3.3 \text{ V} \times 300 \text{ kHz}} = 40.4 \mu\text{F} \quad (43)$$

$$\text{ESR}_{\text{MAX}} = \frac{V_{\text{RIPPLE(ESR)}}}{I_{\text{LOAD}} + \frac{1}{2}I_{\text{RIPPLE}}} = \frac{150 \text{ mV}}{11.6 \text{ A}} = 13 \text{ m}\Omega \quad (44)$$

The RMS current in the input capacitors is estimated by [Equation 45](#).

$$I_{\text{RMS\_CIN}} = I_{\text{LOAD}} \times \sqrt{D \times (1-D)} = 10 \text{ A} \times \sqrt{0.2 \times (1-0.2)} = 4 \text{ Arms} \quad (45)$$

Five 1210, 10- $\mu\text{F}$ , 25-V, X5R ceramic capacitors with approximately 2-m $\Omega$  of ESR and a 2.5-A RMS current rating each are selected. Higher voltage capacitors are selected to minimize capacitance loss at the DC bias voltage to ensure the capacitors allow sufficient capacitance at the working voltage.

### 8.2.3.2.6 MOSFET Switch Selection (Q1 and Q2)

Reviewing available TI NexFET MOSFETs using the TI NexFET MOSFET selection tool, the CSD16323Q3 and CSD16323Q3 5-mm  $\times$  6-mm MOSFETs are selected. These two FETs have maximum total gate charges of 8.4 nC.

### 8.2.3.2.7 Bootstrap Capacitor (C6)

To ensure proper charging of the high-side FET gate, limit the ripple voltage on the boost capacitor to less than 50 mV.

$$C_{\text{Boost}} = 20 \times Q_{\text{G1}} = 20 \times 8.4 \text{ nC} = 100 \text{ nF} \quad (46)$$

### 8.2.3.2.8 VDD Bypass Capacitor (C7)

Per the TPS40305 [Electrical Characteristics](#) specifications, select a 1.0-μF X5R or better ceramic bypass capacitor for VDD.

### 8.2.3.2.9 BP Bypass Capacitor (C5)

Per the TPS40303 data sheet, a minimum 1.0-μF ceramic capacitance is required to stabilize the BP regulator. To limit regulator noise to less than 10 mV, the value of the bypass capacitor is calculated in [Equation 47](#).

$$C_{BP} = 100 \times \text{MAX}(Q_{G1}, Q_{G2}) \quad (47)$$

Because both Q1 and Q2's are the same, total gate charge is 8.4 nC, a BP capacitor of 0.84 μF is calculated. A standard value of 1.0 μF is selected to limit noise on the BP regulator.

### 8.2.3.2.10 Short-Circuit Protection (R11)

The TPS40305 uses the negative drop across the low-side FET at the end of the OFF time to measure the inductor current. Allowing for 30% over maximum load and 20% rise in  $R_{DS(on)Q1}$  for self-heating, the voltage drop across the low-side FET at current limit is given by [Equation 48](#).

$$V_{OC} = (1.3 \times I_{LOAD} - \frac{1}{2} I_{ripple}) \times 1.2 \times R_{DSONQ2} = (1.3 \times 10A - \frac{1}{2} 3.2A) \times 1.2 \times 4.4m\Omega = 60mV \quad (48)$$

The TPS40305 internal temperature coefficient helps compensate for the MOSFET's  $R_{DS(on)}$  temperature coefficient, so the current limit programming resistor is selected by [Equation 49](#).

$$R_{CS} = \frac{V_{OC} - V_{OCLOS(min)}}{2 \times I_{OCSET(min)}} = \frac{60mV - (-8mV)}{2 \times 9.5\mu A} = 3.6k\Omega \quad (49)$$

### 8.2.3.2.11 Feedback Divider (R4, R5)

The TPS40305 controller uses a full operational amplifier with an internally fixed 0.600-V reference. R5 is selected between 10 kΩ and 50 kΩ for a balance of feedback current and noise immunity. With R5 set to 10 kΩ, the output voltage is programmed with a resistor divider given by [Equation 50](#). Because the feedback voltage is equal to output voltage, low-side voltage divider resistor is not needed.

$$R_{Lowside} = \frac{V_{FB} \times R5}{V_{OUT} - V_{FB}} \quad (50)$$

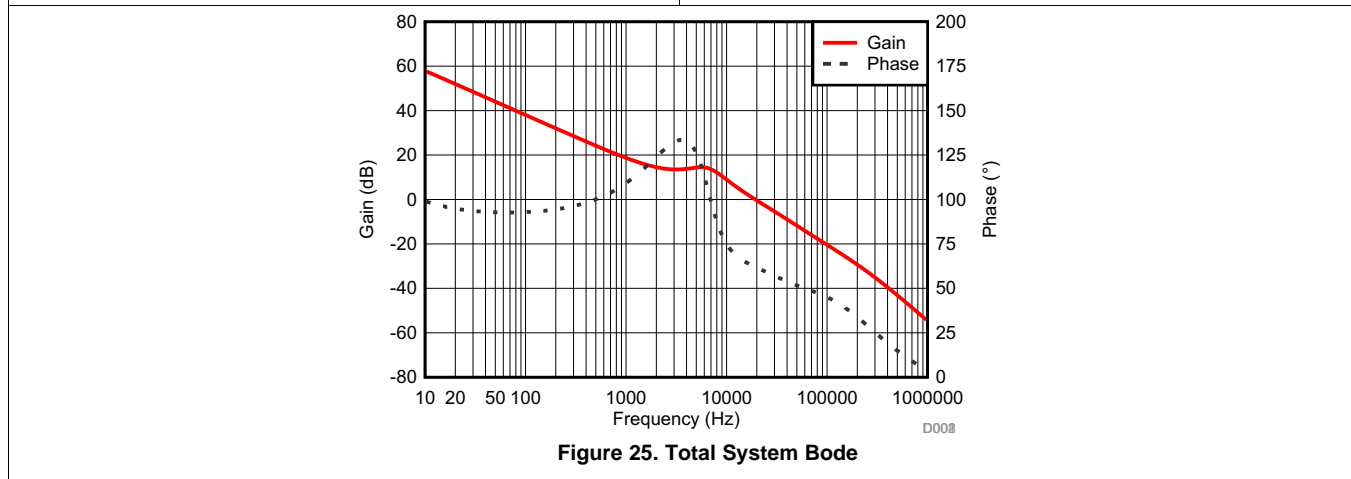
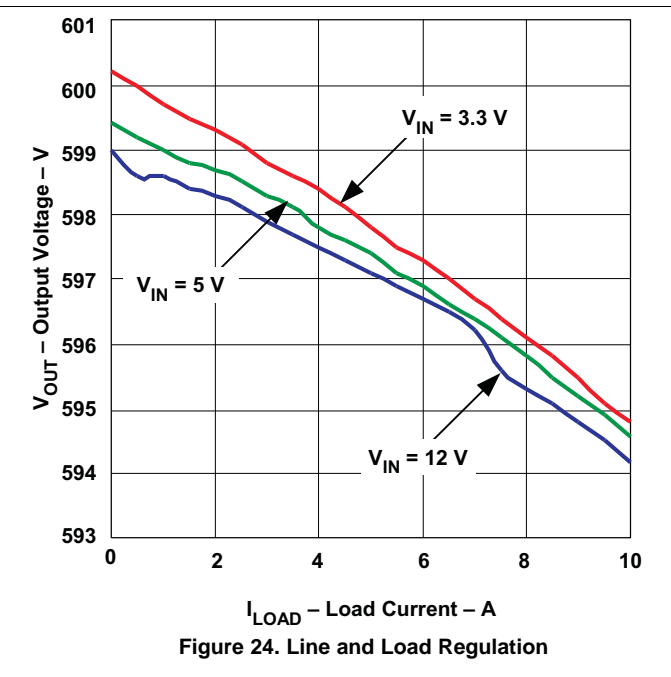
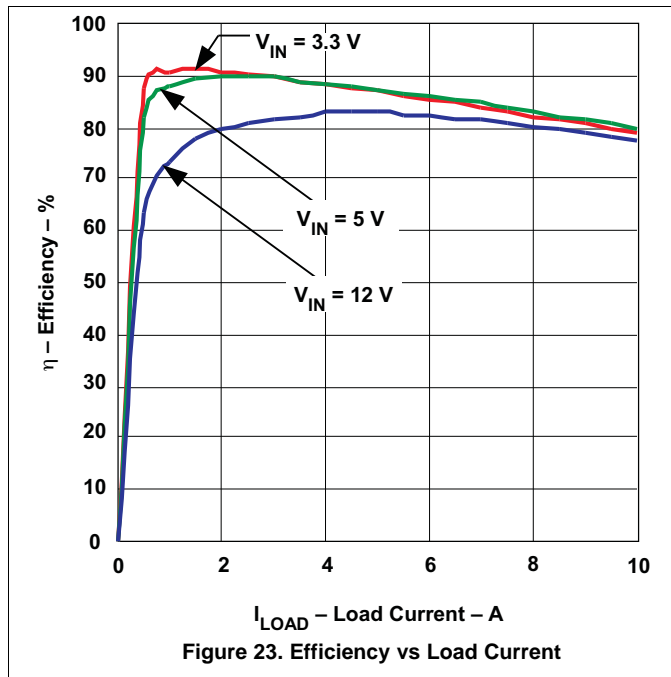
### 8.2.3.2.12 Compensation: (C2, C3, C4, R3, R6)

Using the TPS40k Loop Stability Tool for 100-kHz bandwidth and 60° phase margin with a R5 value of 10 kΩ, the following values are returned.

- C8 = 10 nF
- C14 = 270 pF
- C15 = 4.7 nF
- R6 = 2.74 kΩ
- R3 = 1 kΩ

### 8.2.3.3 Application Curves

A typical efficiency graph for this design example using the TPS40303 is shown in Figure 23. The typical line and load regulation this design example using the TPS40303 is shown in Figure 24



## 9 Power Supply Recommendations

These devices are designed to operate from an input voltage supply between 3 V and 20 V. This input supply should remain within the input voltage supply range. This supply must be well regulated.

## 10 Layout

### 10.1 Layout Guidelines

- For MOSFET or Power Block Layout, follow the layout recommendations provided for the MOSFET or Power Block selected.
- Connect VDD to VIN as close as possible to the drain connection of the high-side FET to avoid introducing additional drop which could trigger short-circuit protection.
- Place VDD and BP to GND capacitors within 2 mm of the device and connected to the Thermal Pad (GND).
- The FB to GND resistor should connect to the thermal tab (GND) with a minimum 10-mil wide trace.
- Place VOUT to FB resistor within 2 mm of the FB pin.
- The EN/SS-to-GND capacitor must connect to the thermal tab (GND) with a minimum 10-mil-wide trace. It may share this trace with FB to GND.
- If a BJT or MOSFET is used to disable EN/SS, place it within 5 mm of the device.
- If a COMP to GND resistor is used, place it within 5 mm of the device.
- All COMP and FB traces should be kept minimum line width and as short as possible to minimize noise coupling.
- Do not route EN/SS more than 20 mm from the device.
- If multiple layers are used, extend GND under all components connected to FB, COMP and EN/SS to reduce noise sensitivity.
- HDRV and LDRV should provide short, low inductance paths of 5 mm or less to the gates of the MOSFETs or Power Block.
- No more than 1  $\Omega$  of resistance should be placed between HDRV or LDRV and their MOSFET or Power Block gate pins.
- LDRV / OC to GND Current Limit Programming resistor may be placed on the far side of the MOSFET if necessary to ensure a short connection from LDRV to the gate of the low-side MOSFET.
- The BOOT to SW resistor and capacitor should both be placed within 4 mm of the device using a minimum of 10-mil-wide trace. The full width of the component pads are preferred for trace widths if design rules allow.
- If via must be used between the HDRV, SW and LDRV pins and their respective MOSFET or Power Block connections, use a minimum of two vias to reduce parasitic inductance
- Refer to the Land Pattern Data for the preferred layout of thermal vias within the thermal pad.
- It is recommended to extend the top-layer copper area of the thermal pad (GND) beyond the package a minimum 3 mm between pins 1 and 10 and 5 and 6 to improve thermal resistance to ambient of the device.

## 10.2 Layout Example

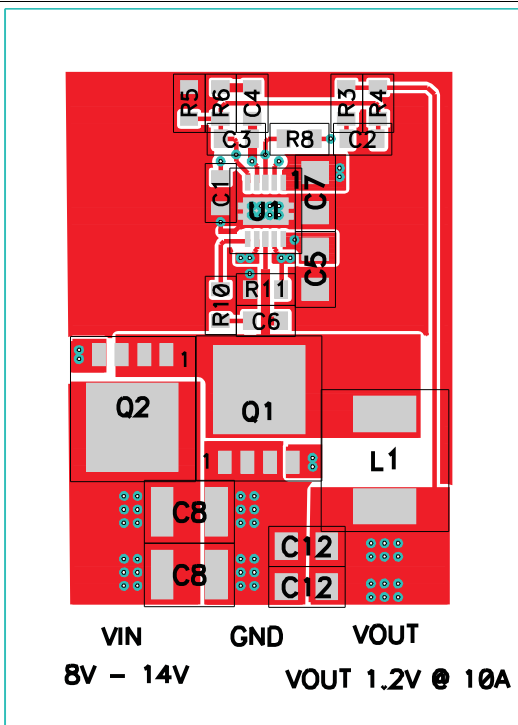


Figure 26. Top Copper With Components

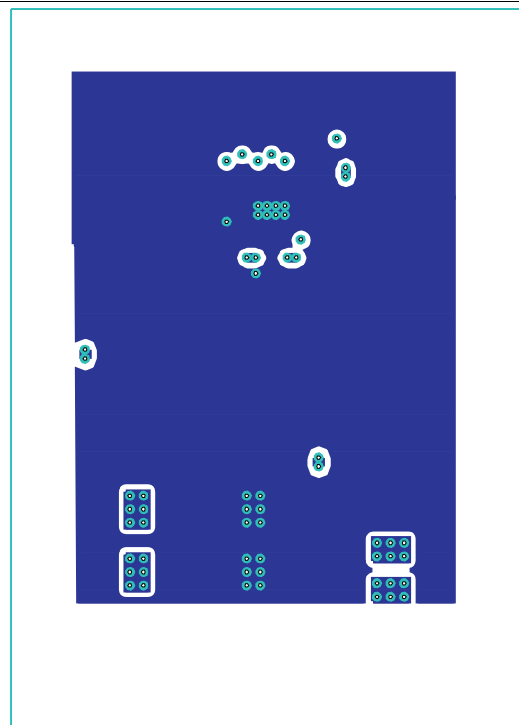


Figure 27. Top Internal Copper Layout

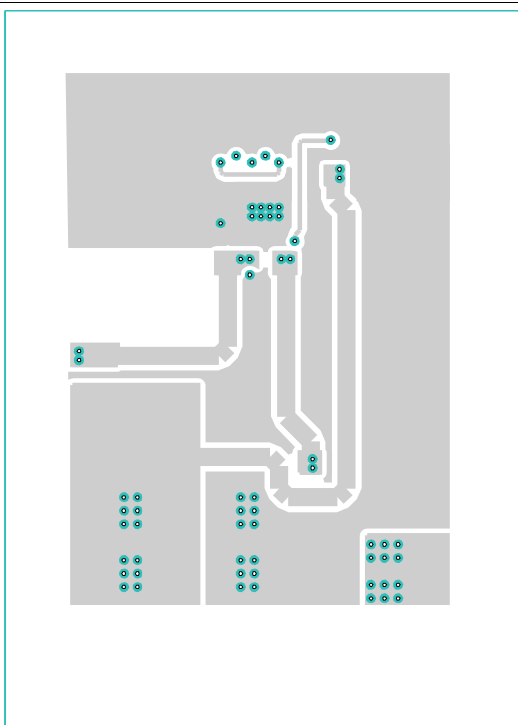


Figure 28. Bottom Internal Copper Layout

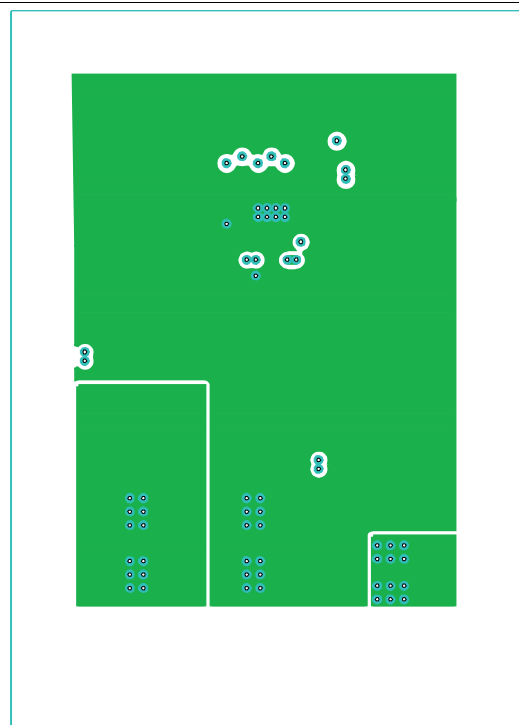


Figure 29. Bottom Copper Layer

## 11 器件和文档支持

### 11.1 器件支持

#### 11.1.1 第三方产品免责声明

TI 发布的与第三方产品或服务有关的信息，不能构成与此类产品或服务或保修的适用性有关的认可，不能构成此类产品或服务单独或与任何 TI 产品或服务一起的表示或认可。

#### 11.2 使用 WEBENCH® 工具创建定制设计

请[单击此处](#)，借助 WEBENCH® 电源设计器并使用 TPS4030x 器件创建定制设计方案。

1. 首先键入输入电压 ( $V_{IN}$ )、输出电压 ( $V_{OUT}$ ) 和输出电流 ( $I_{OUT}$ ) 要求。
2. 使用优化器拨盘优化关键参数设计，如效率、封装和成本。
3. 将生成的设计与德州仪器 (TI) 的其他解决方案进行比较。

WEBENCH 电源设计器可提供定制原理图以及罗列实时价格和组件供货情况的物料清单。

在多数情况下，可执行以下操作：

- 运行电气仿真，观察重要波形以及电路性能
- 运行热性能仿真，了解电路板热性能
- 将定制原理图和布局方案导出至常用 CAD 格式
- 打印设计方案的 PDF 报告并与同事共享

有关 WEBENCH 工具的详细信息，请访问 [www.ti.com.cn/WEBENCH](http://www.ti.com.cn/WEBENCH)。

### 11.3 文档支持

#### 11.3.1 相关文章

这些参考资料、设计工具以及附加参考资料的链接（包括设计软件）均可通过 <http://power.ti.com> 获取

1. 更多 PowerPAD™ 信息可在应用简介 (SLMA002) 和 (SLMA004) 中找到。
2. 《低电压直流/直流转换器内幕揭秘》– SEM1500 主题 5 – 2002 年研讨会系列
3. 《了解开关模式电源中的降压功率级》，(SLVA057)，1999 年 3 月
4. 《设计稳定控制环路》– SEM 1400 – 2001 年研讨会系列

#### 11.4 相关链接

下表列出了快速访问链接。类别包括技术文档、支持和社区资源、工具和软件以及申请样片或购买产品的快速访问链接。

表 8. 相关链接

器件	产品文件夹	样片与购买	技术文档	工具和软件	支持和社区
TPS40303	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>
TPS40304	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>
TPS40305	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>	<a href="#">请单击此处</a>

#### 11.5 接收文档更新通知

要接收文档更新通知，请导航至 [TI.com.cn](http://TI.com.cn) 上的器件产品文件夹。请单击右上角的提醒我进行注册，即可每周接收产品信息更改摘要。有关更改的详细信息，请查看任何已修订文档中包含的修订历史记录。

#### 11.6 社区资源

下列链接提供到 TI 社区资源的连接。链接的内容由各个分销商“按照原样”提供。这些内容并不构成 TI 技术规范，并且不一定反映 TI 的观点；请参阅 TI 的《使用条款》。

**TI E2E™ 在线社区** [TI 的工程师对工程师 \(E2E\) 社区](#)。此社区的创建目的在于促进工程师之间的协作。在 [e2e.ti.com](http://e2e.ti.com) 中，您可以咨询问题、分享知识、拓展思路并与同行工程师一道帮助解决问题。

## 社区资源 (接下页)

**设计支持** *TI 参考设计支持* 可帮助您快速查找有帮助的 E2E 论坛、设计支持工具以及技术支持的联系信息。

### 11.7 商标

E2E is a trademark of Texas Instruments.

WEBENCH is a registered trademark of Texas Instruments.

All other trademarks are the property of their respective owners.

### 11.8 静电放电警告



这些装置包含有限的内置 ESD 保护。存储或装卸时，应将导线一起截短或将装置放置于导电泡棉中，以防止 MOS 门极遭受静电损伤。

### 11.9 Glossary

**SLYZ022** — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。数据如有变更，恕不另行通知，也不会对此文档进行修订。如欲获取此数据表的浏览器版本，请参阅左侧的导航。

**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">TPS40303DRCR</a>	Active	Production	VSON (DRC)   10	3000   LARGE T&R	Yes	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0303
TPS40303DRCR.A	Active	Production	VSON (DRC)   10	3000   LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	0303
<a href="#">TPS40303DRCT</a>	Active	Production	VSON (DRC)   10	250   SMALL T&R	Yes	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0303
TPS40303DRCT.A	Active	Production	VSON (DRC)   10	250   SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	0303
<a href="#">TPS40304DRCR</a>	Active	Production	VSON (DRC)   10	3000   LARGE T&R	Yes	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0304
TPS40304DRCR.A	Active	Production	VSON (DRC)   10	3000   LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	0304
<a href="#">TPS40304DRCT</a>	Active	Production	VSON (DRC)   10	250   SMALL T&R	Yes	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0304
TPS40304DRCT.A	Active	Production	VSON (DRC)   10	250   SMALL T&R	Yes	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0304
<a href="#">TPS40305DRCR</a>	Active	Production	VSON (DRC)   10	3000   LARGE T&R	Yes	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0305
TPS40305DRCR.A	Active	Production	VSON (DRC)   10	3000   LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	0305
<a href="#">TPS40305DRCT</a>	Active	Production	VSON (DRC)   10	250   SMALL T&R	Yes	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	0305
TPS40305DRCT.A	Active	Production	VSON (DRC)   10	250   SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	0305

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "-" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

**Important Information and Disclaimer:** The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS40303DRCR	VSON	DRC	10	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS40303DRCT	VSON	DRC	10	250	180.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS40304DRCR	VSON	DRC	10	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS40304DRCT	VSON	DRC	10	250	180.0	12.5	3.3	3.3	1.1	8.0	12.0	Q2
TPS40305DRCR	VSON	DRC	10	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS40305DRCT	VSON	DRC	10	250	180.0	12.5	3.3	3.3	1.1	8.0	12.0	Q2

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS40303DRCR	VSON	DRC	10	3000	353.0	353.0	32.0
TPS40303DRCT	VSON	DRC	10	250	213.0	191.0	35.0
TPS40304DRCR	VSON	DRC	10	3000	338.0	355.0	35.0
TPS40304DRCT	VSON	DRC	10	250	338.0	355.0	35.0
TPS40305DRCR	VSON	DRC	10	3000	338.0	355.0	35.0
TPS40305DRCT	VSON	DRC	10	250	338.0	355.0	35.0

## GENERIC PACKAGE VIEW

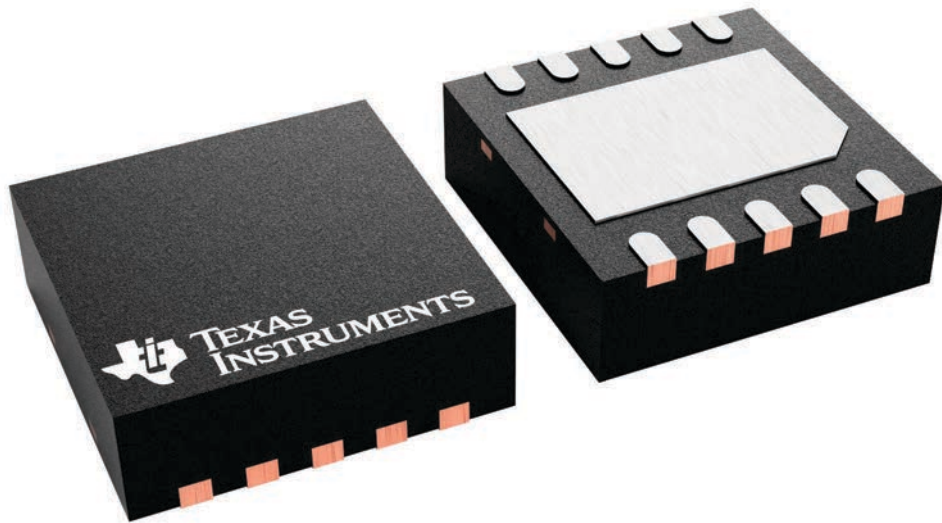
**DRC 10**

**VSON - 1 mm max height**

3 x 3, 0.5 mm pitch

PLASTIC SMALL OUTLINE - NO LEAD

This image is a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.



4226193/A

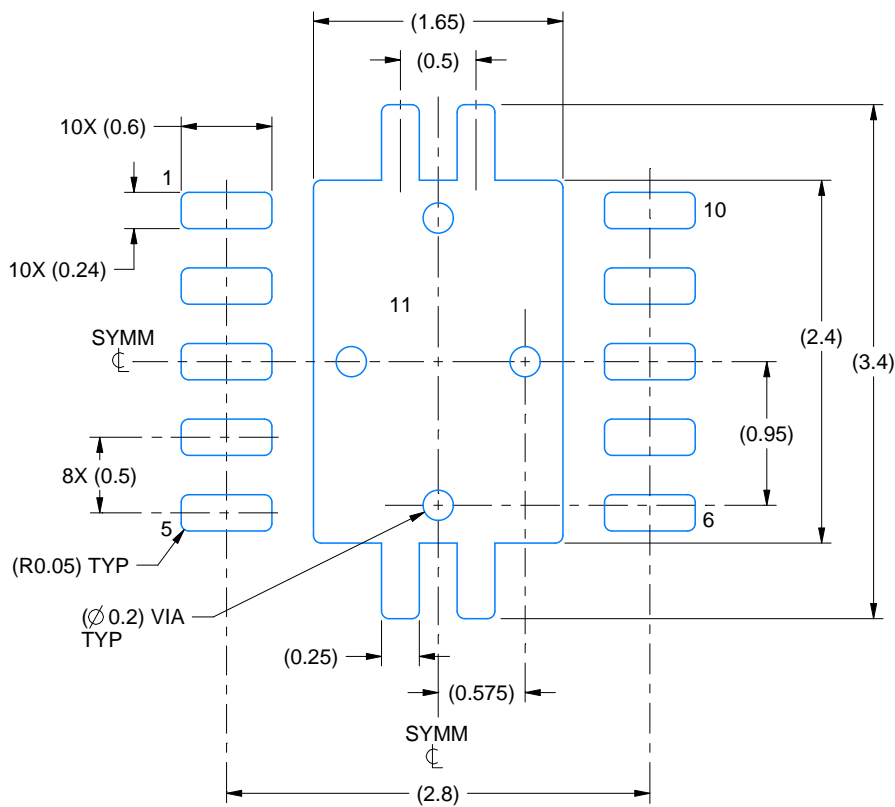


# EXAMPLE BOARD LAYOUT

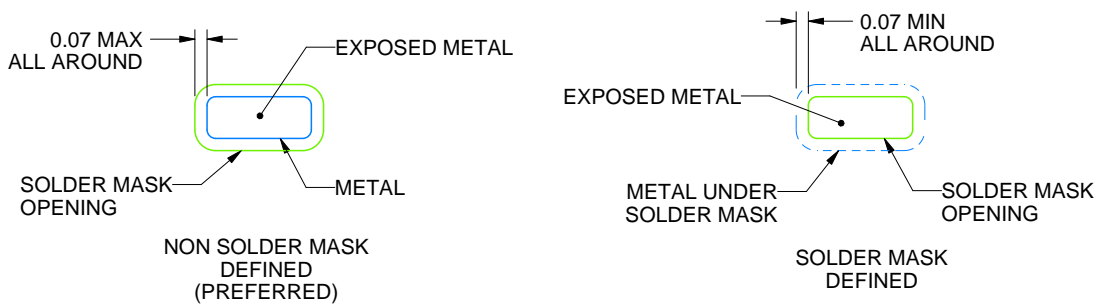
DRC0010J

VSON - 1 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:20X



SOLDER MASK DETAILS

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NOTES: (continued)

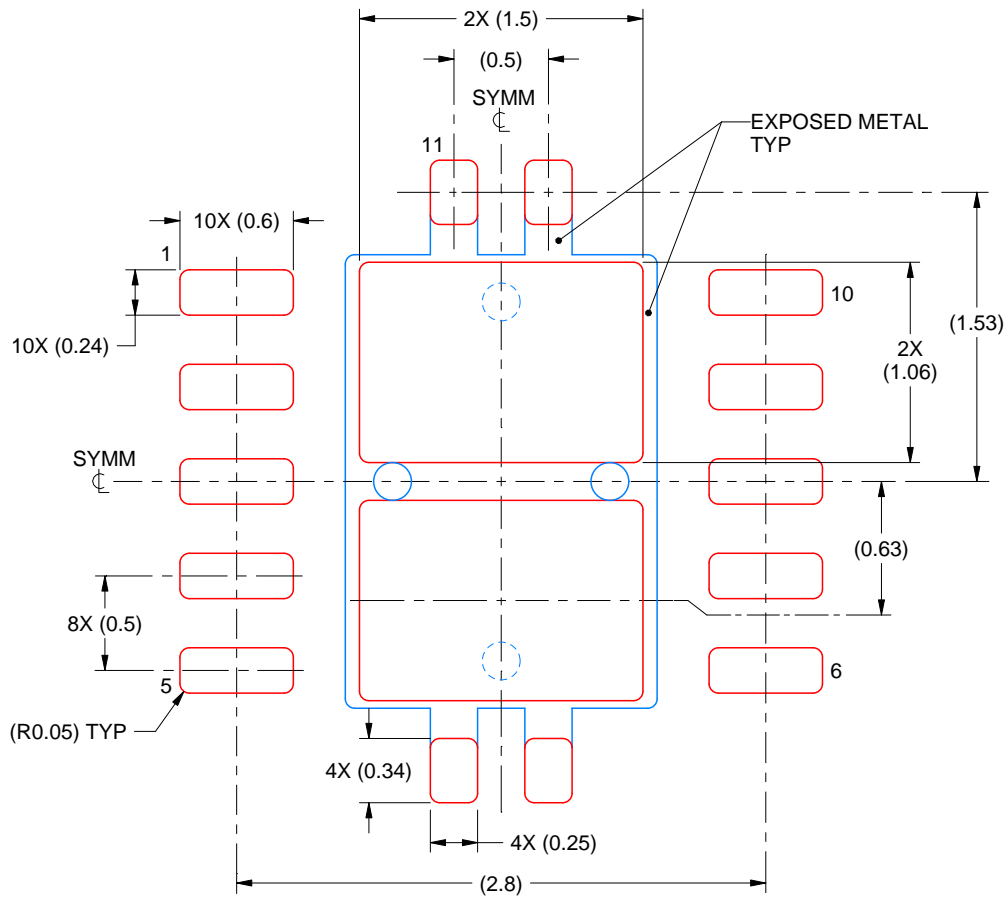
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 ([www.ti.com/lit/sluea271](http://www.ti.com/lit/sluea271)).
5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

# EXAMPLE STENCIL DESIGN

DRC0010J

VSON - 1 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 11:  
80% PRINTED SOLDER COVERAGE BY AREA  
SCALE:25X

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NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

## 重要通知和免责声明

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