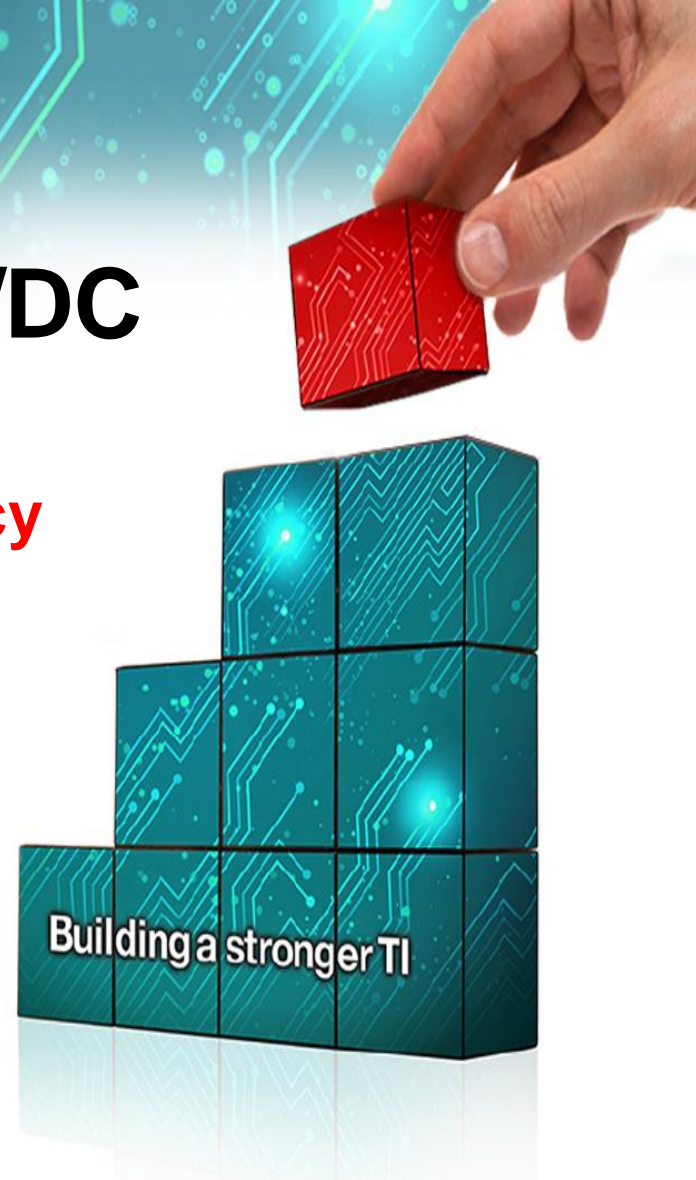


4V-16V/40A Stackable DC/DC Converter TPS543C20

Internal Compensation Fixed Frequency Converter



Contents

- TPS543C20/B20 Overview
- Integrated Stacked High Current MOSFETs
- Efficiency and Thermal performance
- 2-Phase Stackable Configuration
- Control scheme and loop stability
- Transient performance and Body breaking feature
- Design configuration
- Vout Regulation
- Protection Features

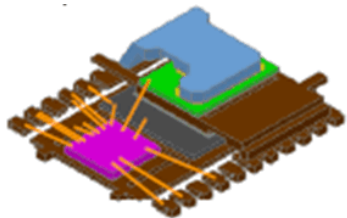
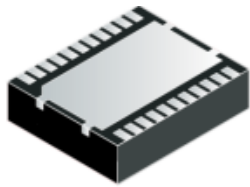
TPS543C20 Stackable DC/DC Converter

Features

- Stackable DC/DC Converter
- Output Voltage Range 0.6V to 5.5V
- ACM Fixed Frequency with CLK Sync
- Fully Differential Remote Voltage Sense
- Fsw: 300KHz to 2MHz (1Ph)
300KHz to 1MHz (2--Ph)
- 10 Vref choices: 0.6V to 1.1V
- 10 SS choices: 0.5, 1, 2, 4, 5, 8, 12, 16, 24, 32ms
- High accuracy Over Current Limit (Hiccup Ilim)
- Asynchronous Pulse Injection (API)/ Body Braking Features
- 5x7x1.5mm, 0.5mm pitch 40Ld Stacked Clip QFN
- Stackable DC/DC Converter

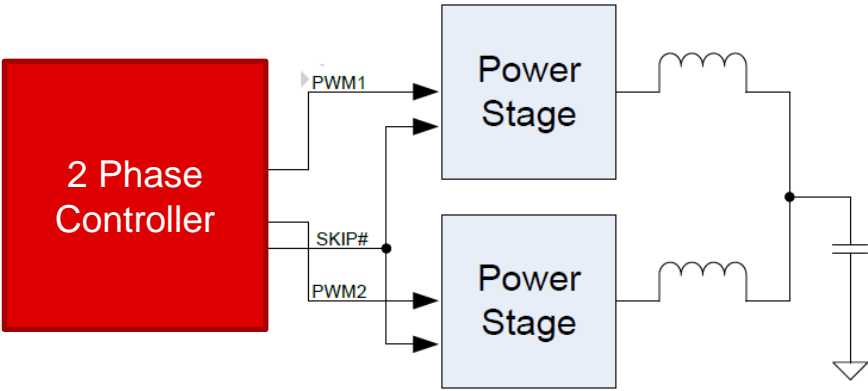
Benefits

- Power ASICs and System Rails
- No External Compensation
- +/-0.5% 1Vref accuracy over temp
- Easy to optimize for efficiency and BOM size
- Flexible Design for multiple Vouts
- Flexible Design for startup timing option
- +/-10% Ilim Accuracy over temp & process
- Option to better manage undershoot/overshoot
- High density & Easy Layout w/ single GND pad

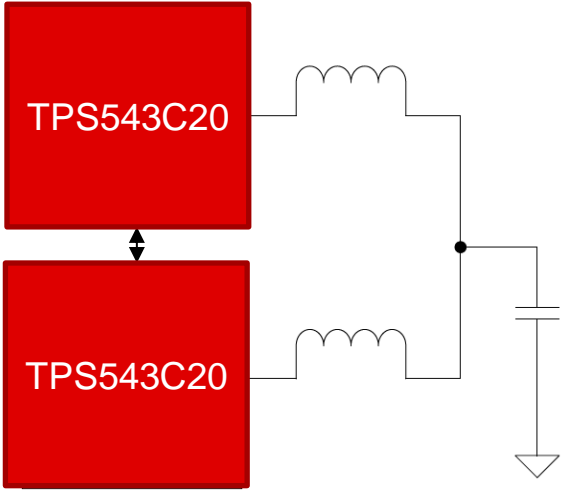


2-Phase Stackable: 2x the output current

Traditional 2-Phase DC/DC

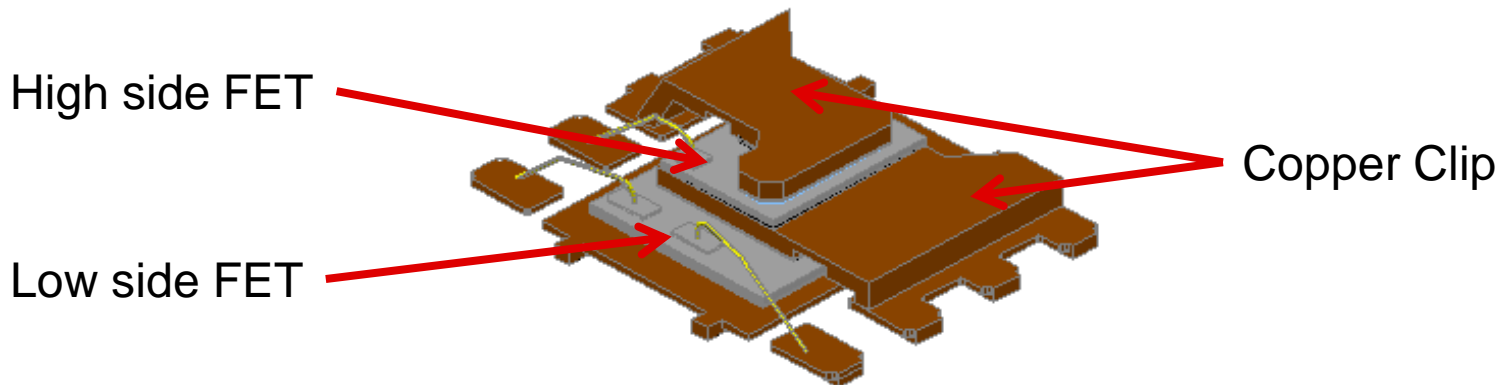


Advanced 2-Phase stackable DC/DC

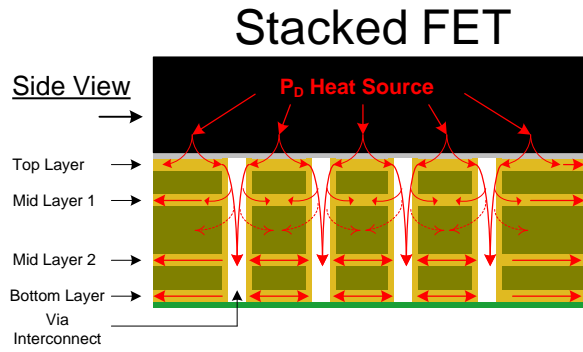


Integrated Stacked High Current MOSFETs

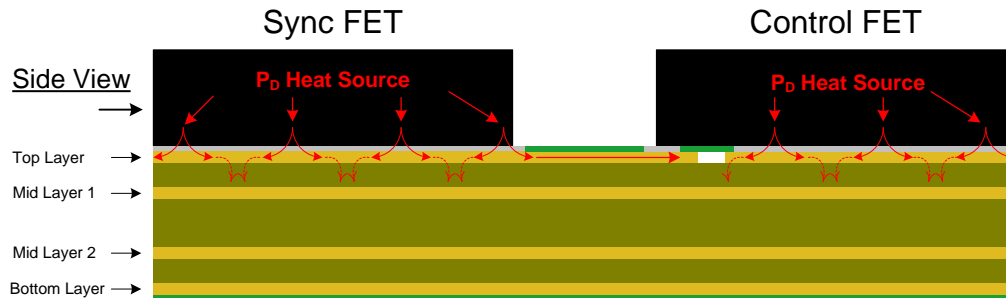
Device	Output Current	Vin Range	Rdson	Stackable
TPS543C20	40A	4V to 16V	UF: 3mΩ LF: 0.9mΩ Included Clip metal 20V FET	Yes-2PH
TPS543B20	25A	4V to 19V	UF: 4.1mΩ LF: 1.9mΩ Included Clip metal 25V FET	No



Grounded Thermal Advantage



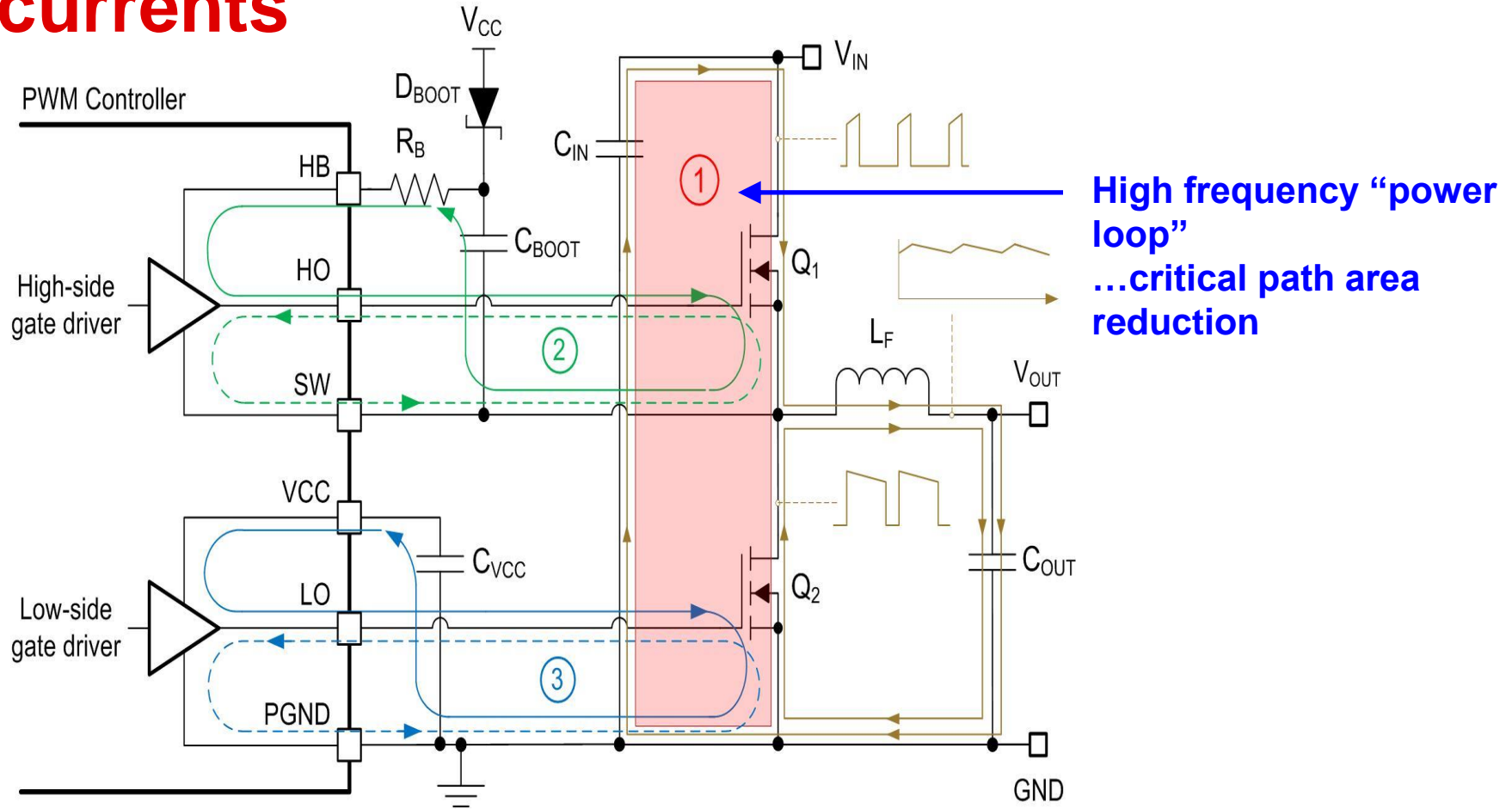
Abundant GND layers typical in all systems. PCB surface area helps dissipate heat.



Discrete & DrMOS solutions create localized hot spots!
DrMOS is Like Co-Packaged /Smaller Discrete Design

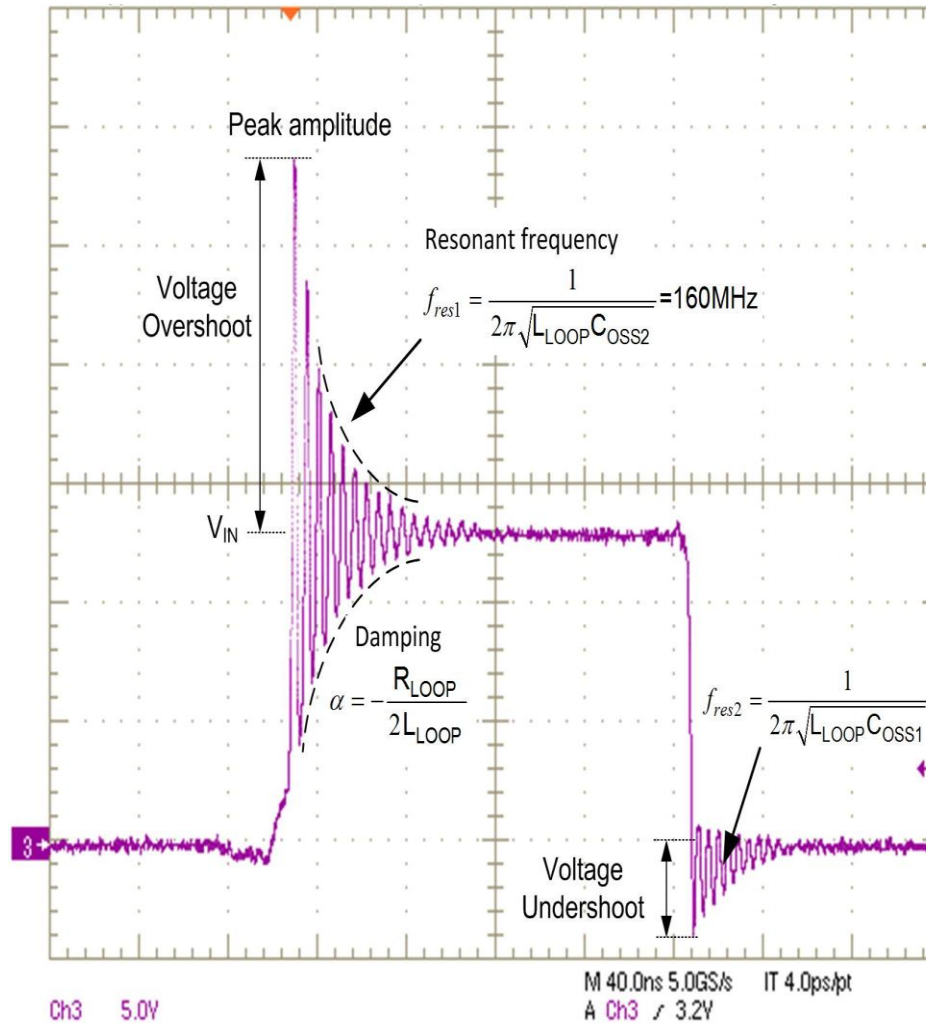
TI Can Use Ground Planes to Dissipate Heat More Effectively and Run Cooler Even if there is Similar Power Loss

Identify critical loops with high di/dt currents

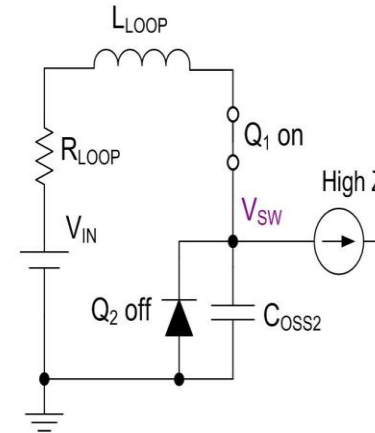


In translating a converter schematic to a board layout, it's essential to pinpoint the high slew-rate current (**high di/dt**) loops to recognize the layout-induced **parasitic or stray inductances** that cause excessive **noise, overshoot, ringing and ground bounce**

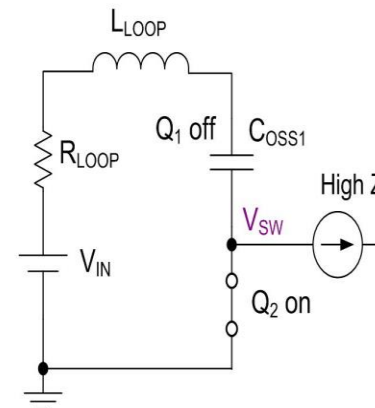
Equivalent RLC circuits for SW node ringing – buck



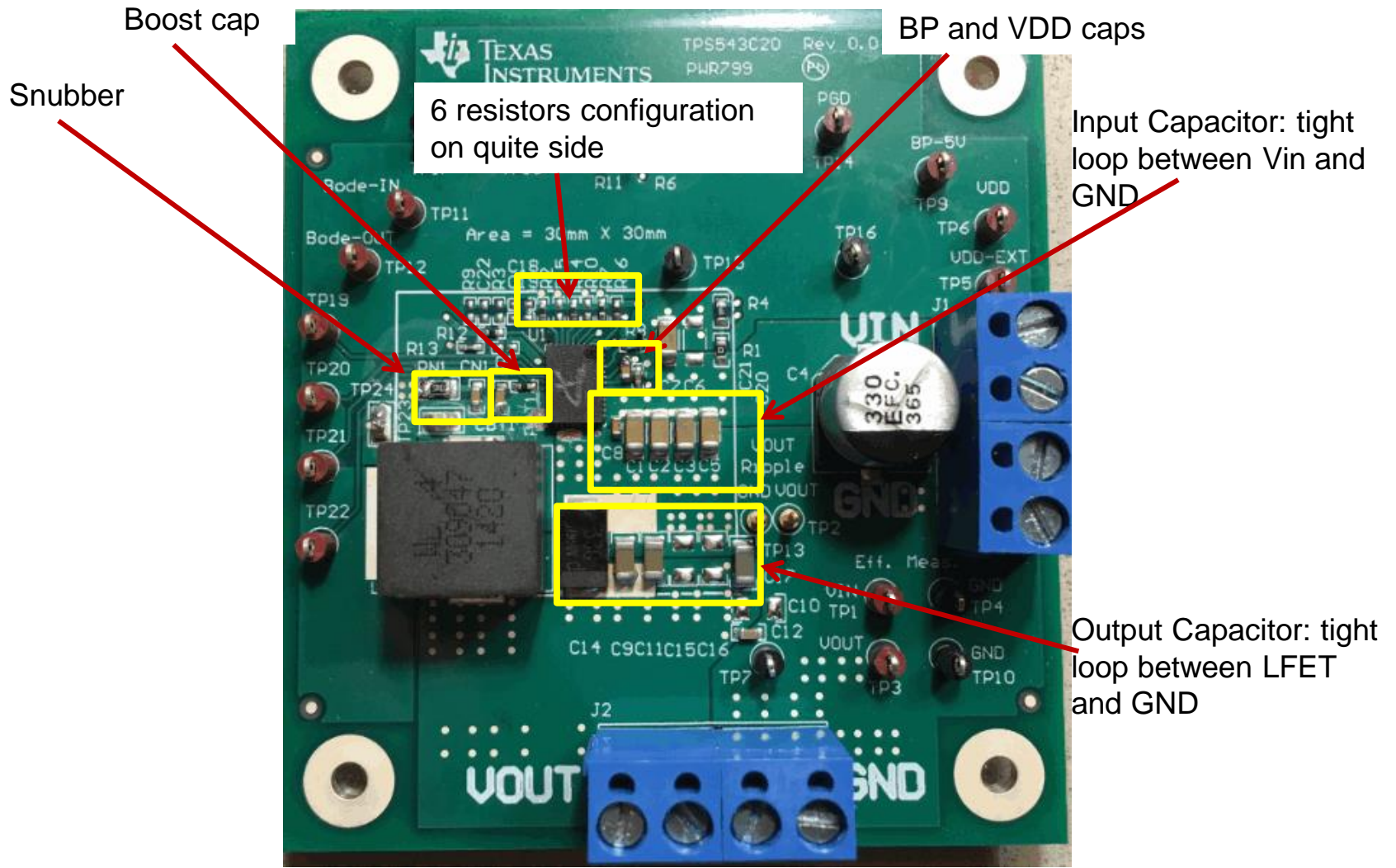
Equivalent RLC circuit after Q_1 turns ON



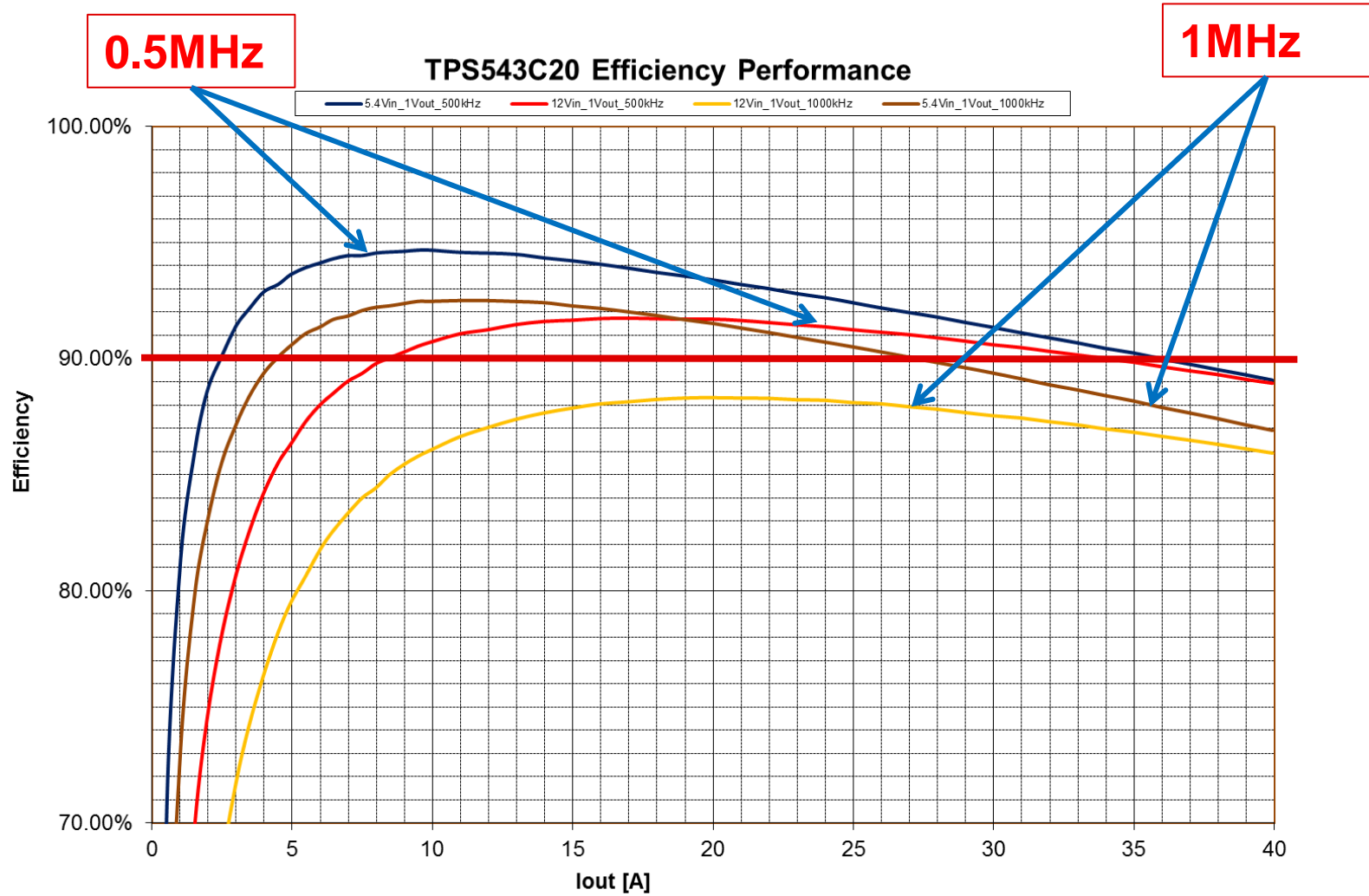
Equivalent RLC circuit after Q_1 turns OFF



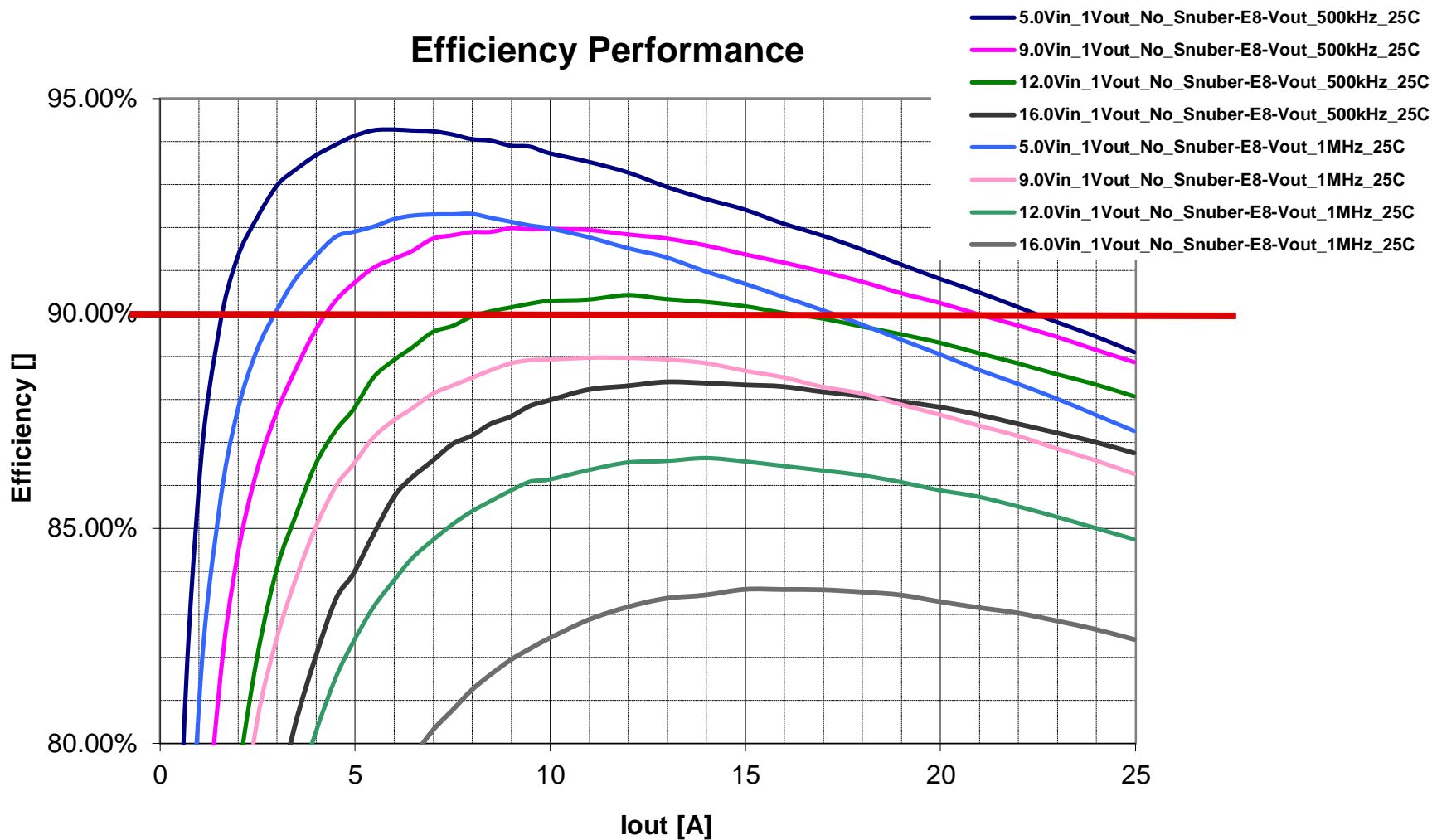
Total Solution Area: 30 x 30mm



TPS543C20 Efficiency: 1Vout@ 5.4-12Vin



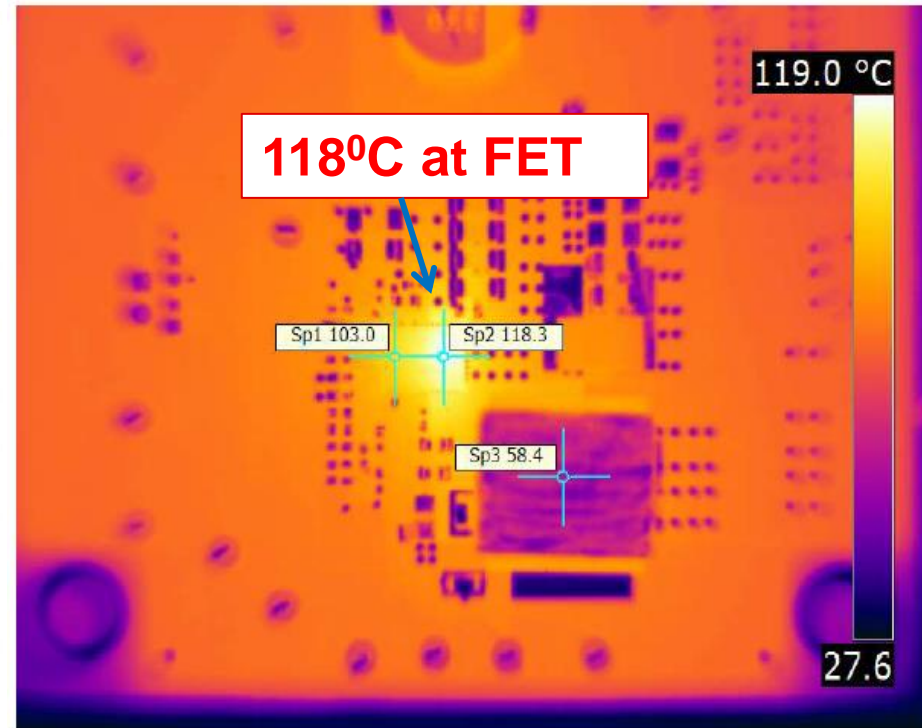
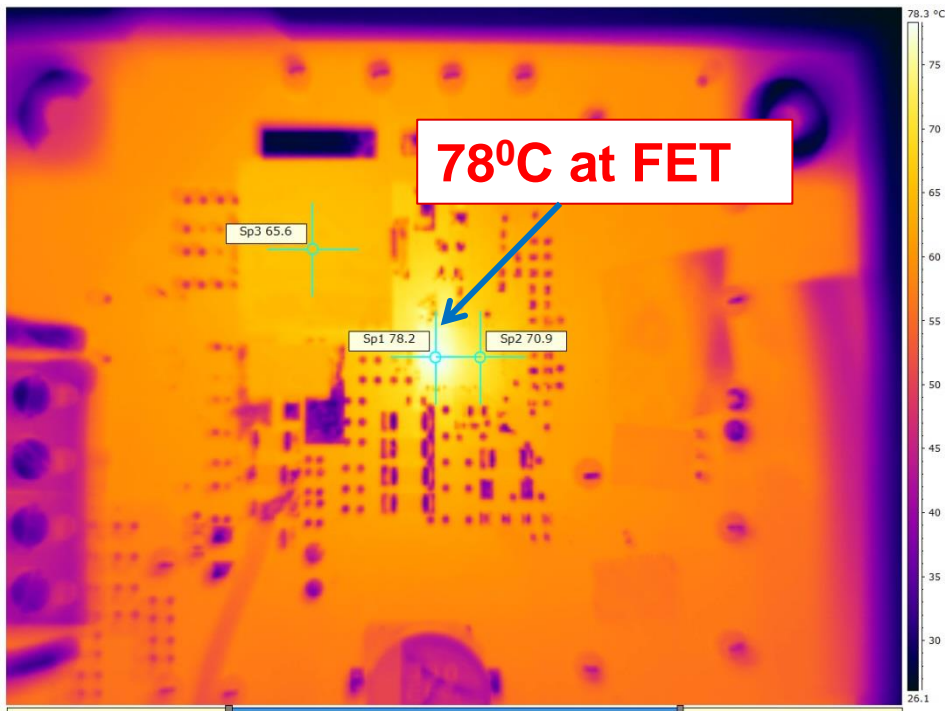
TPS543B20 Efficiency: 1Vout@ 5.0-16Vin with Fsw at 0.5MHz and 1MHz



TPS543C20 Thermal Performance

IOUT = 40A

IOUT = 40A



VIN = 12V, Vout=0.9V, Fsw=500kHz,

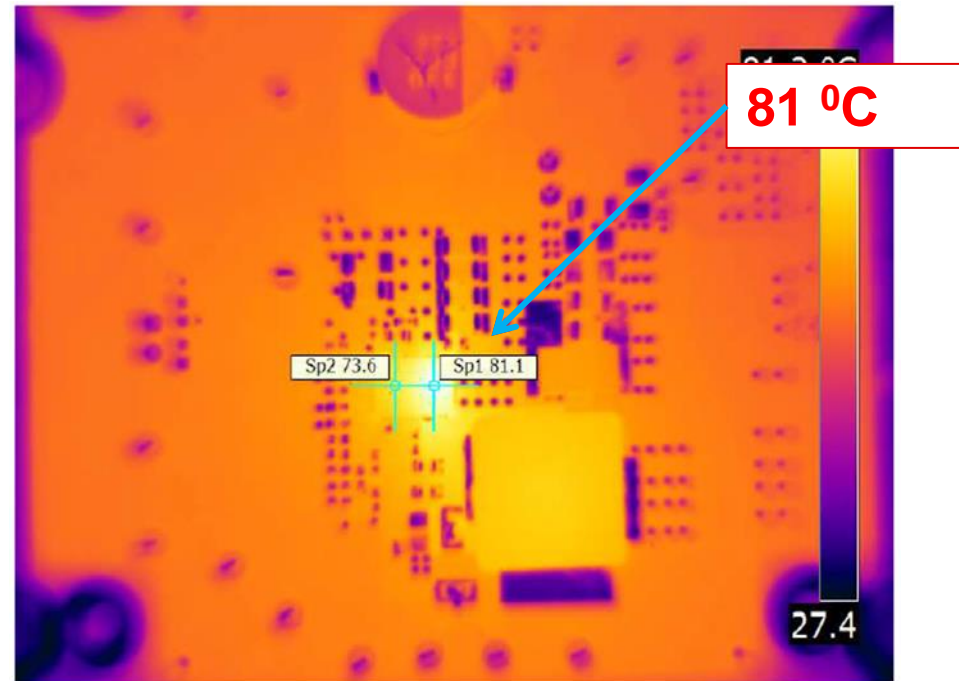
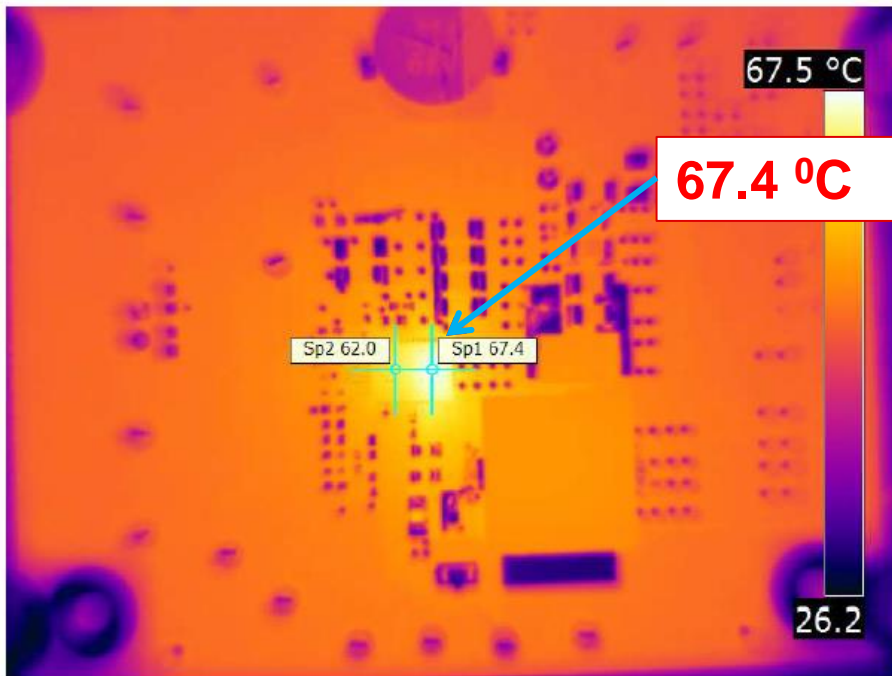
VIN = 12V, Vout=5V, Fsw=500kHz,

Thermal Equilibrium: 10 mins

TPS543B20 Thermal Performance

IOUT = 25A

IOUT = 25A



VIN = 12V, Vout=1V, fsw=500kHz

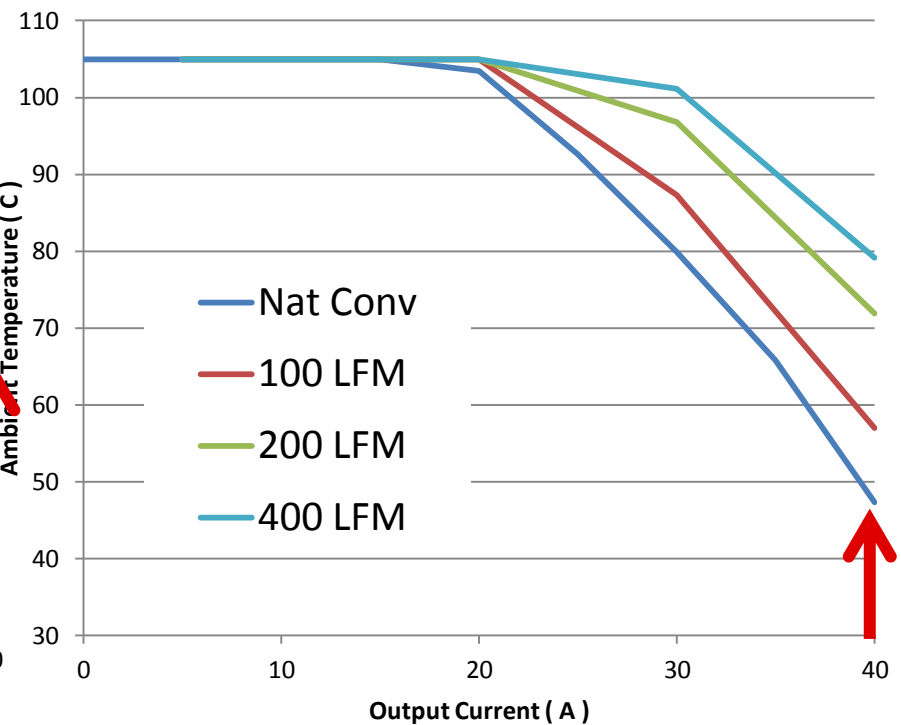
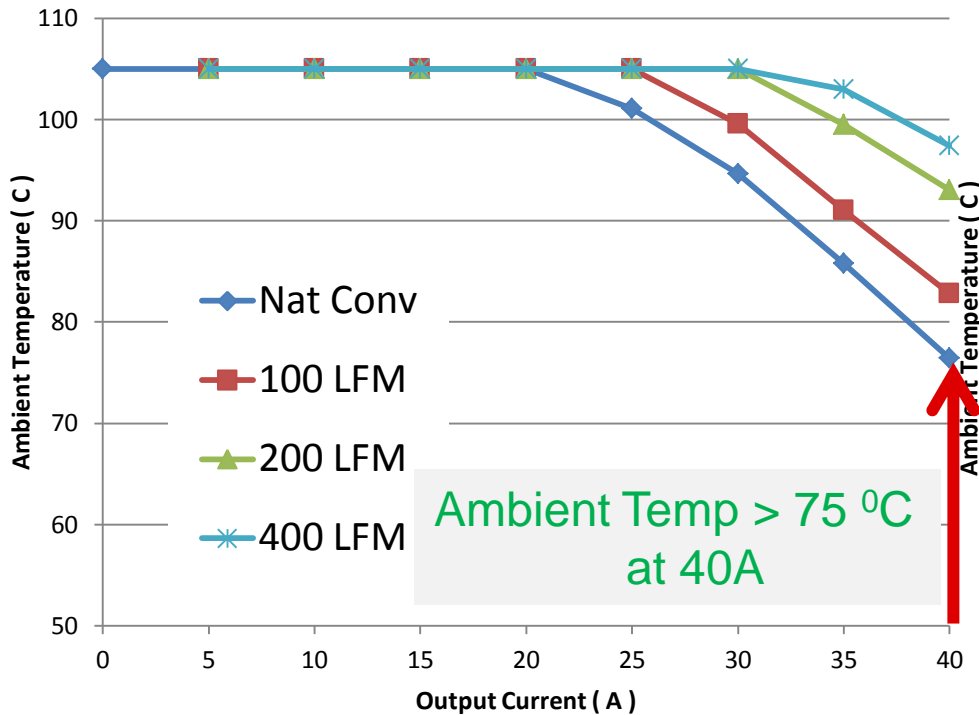
VIN = 12V, Vout=5V, fsw=500kHz

Thermal Equilibrium: 10 mins

Safe Operating Area: TPS543C20

TPS543C20 SOA: 12Vin, 1.0Vout, 500kHz

TPS543C20 SOA: 12Vin, 5.0Vout, 500kHz

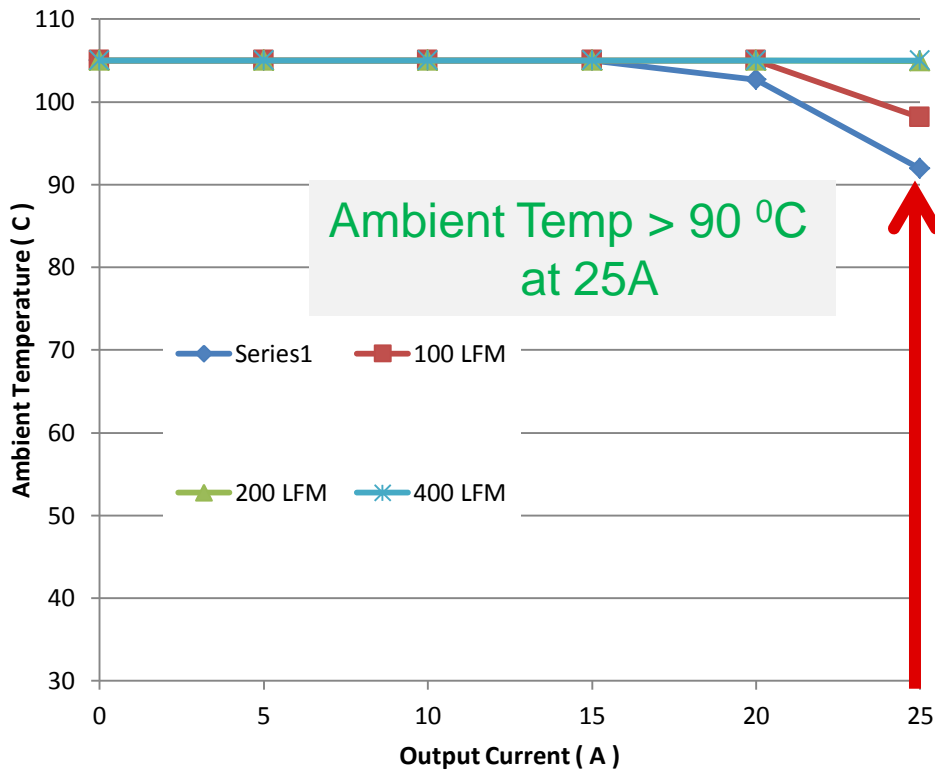


Note: The $T_j = 125\text{ }^\circ\text{C}$ for all data point
For more information of SOA:
<http://www.ti.com/lit/an/slva766/slva766.pdf>

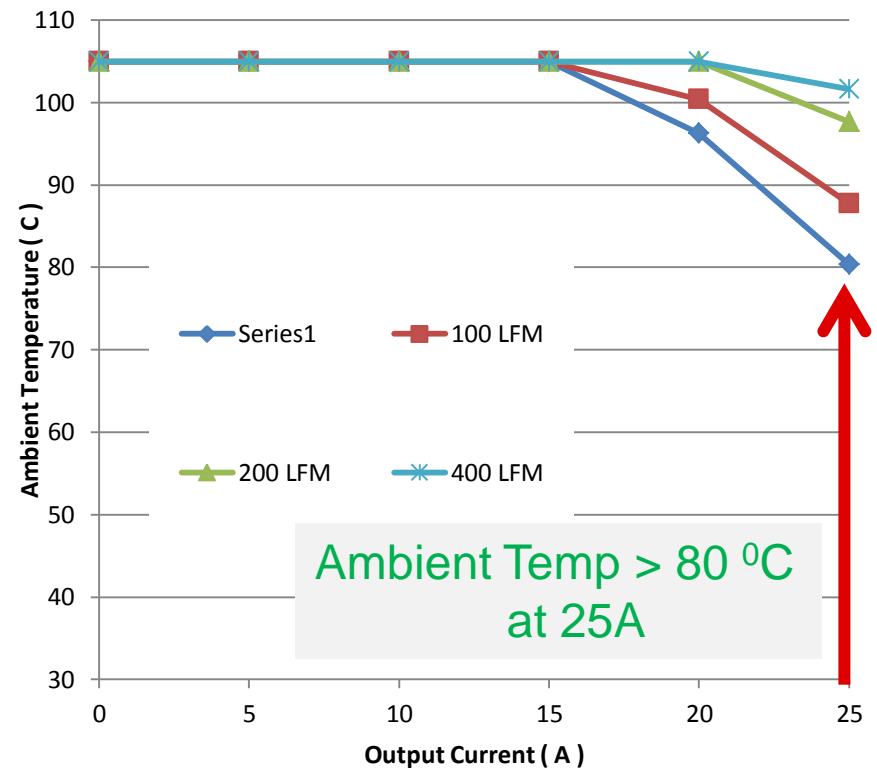
Ambient Temp > 47 °C
at 40A

Safe Operating Area: TPS543B20

TPS543B20 SOA: 12Vin, 1.0Vout, 500kHz

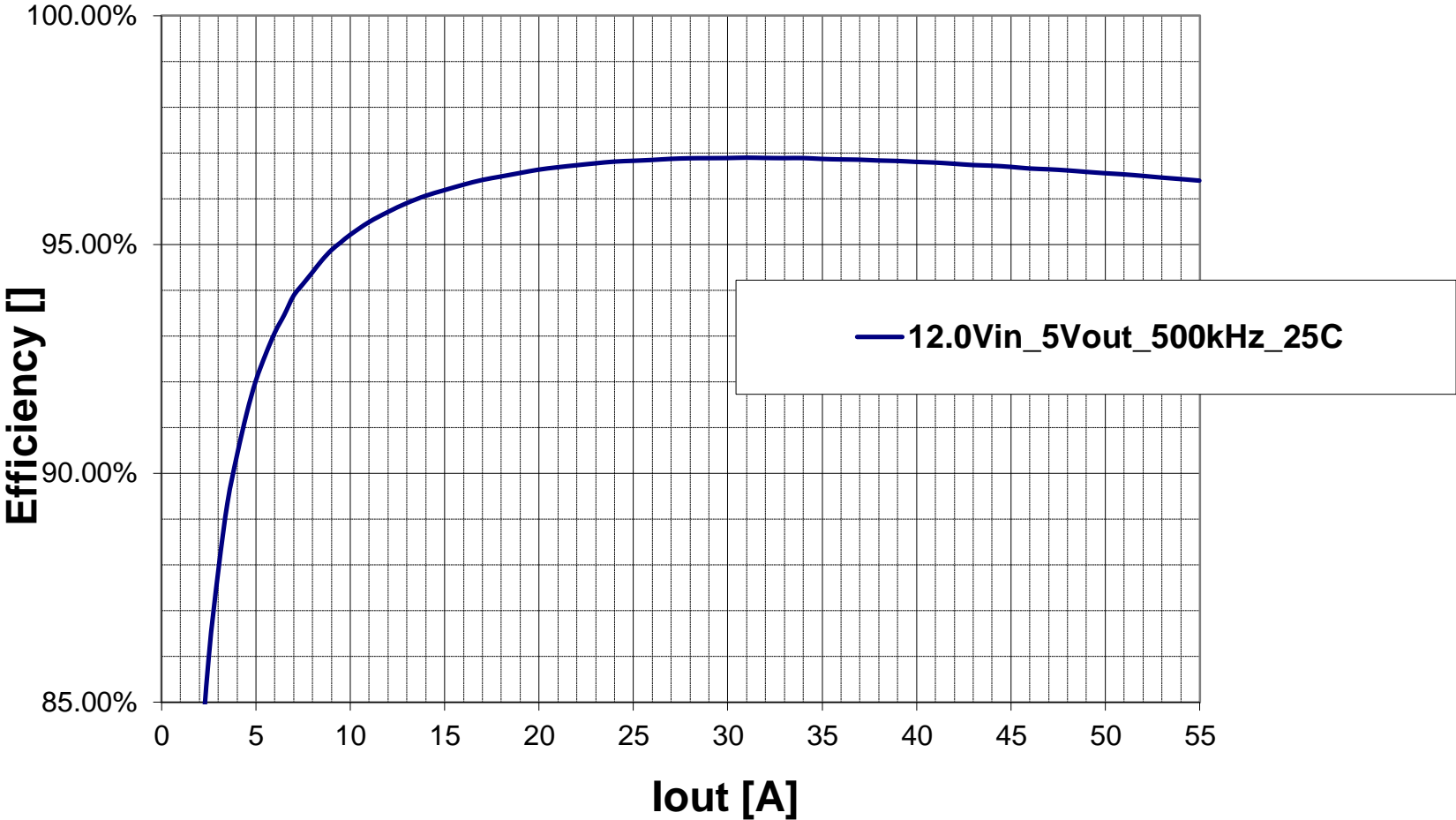


TPS543B20 SOA: 12Vin, 5.0Vout, 500kHz



2-Phase Stackable Efficiency: 275Watts Output

Efficiency Performance



2-Phase Stackable Thermal: 275Watts Output

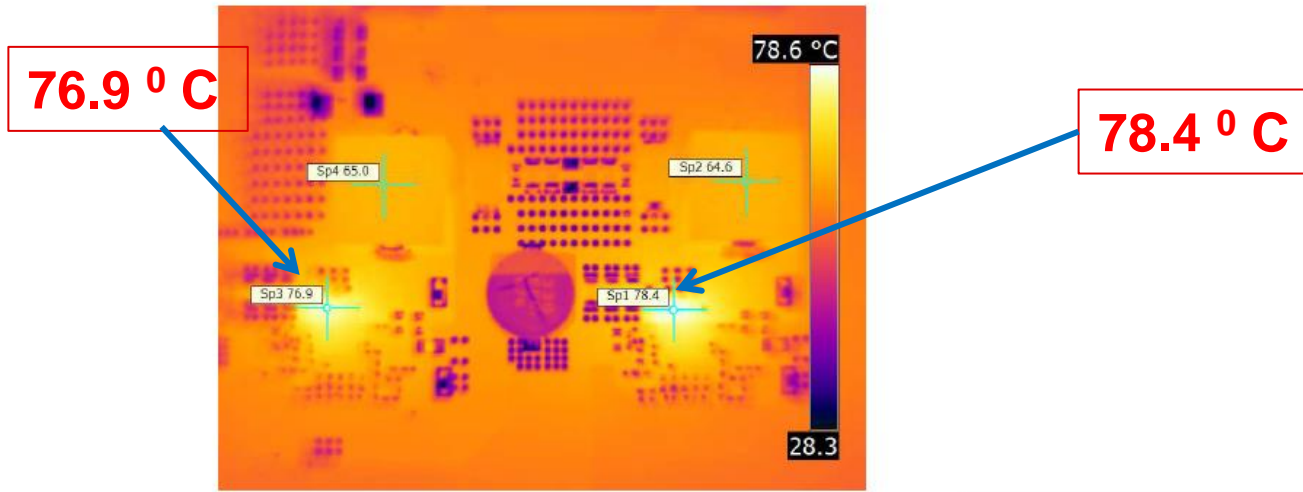


Image and Object Parameters

Camera Model	FLIR T300
Image Date	11/9/2016 11:35:06 PM
Image Name	IR_0208.jpg
Emissivity	0.95
Reflected apparent temperature	20.0 °C
Object Distance	1.0 ft

Text Comments

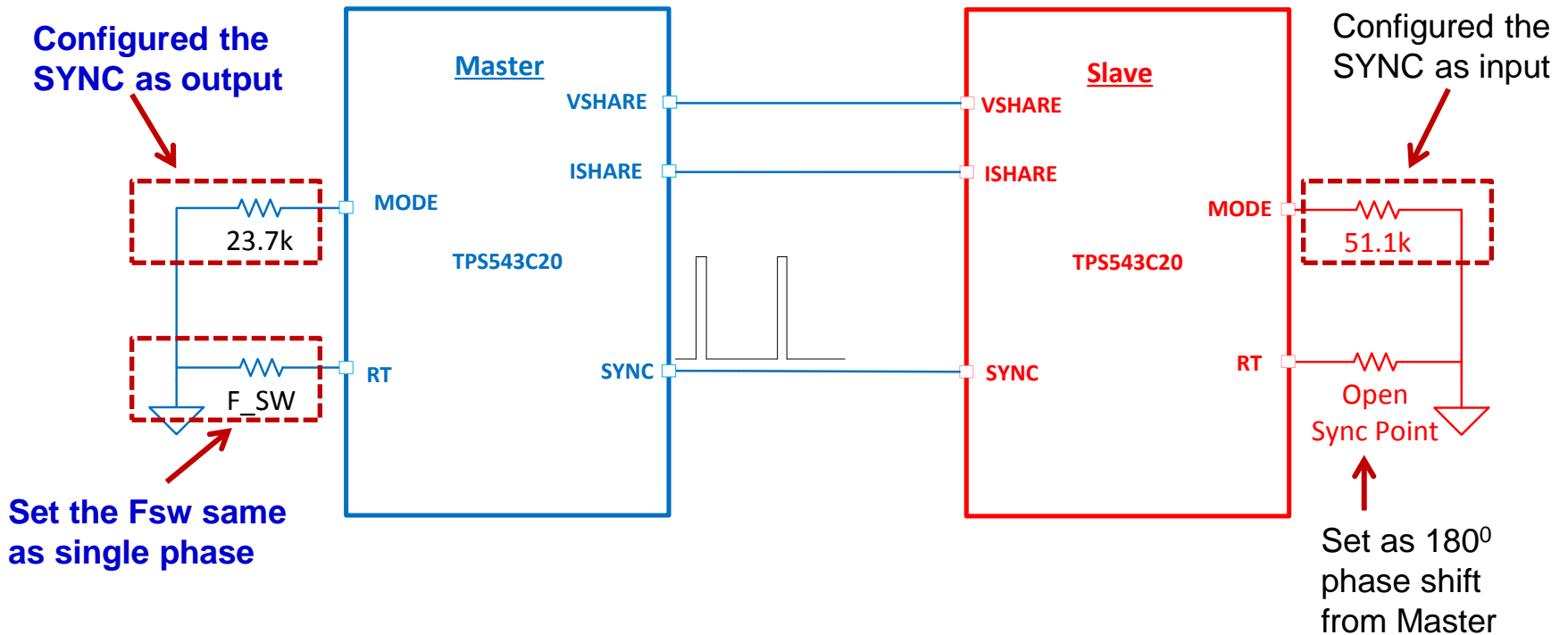
Sp1=IC1	78.4C
Sp2=Inductor1	64.6C
Sp3=IC2	76.9C
Sp4=Inductor2	65C

Description

Vin=12V, Vout=5V, Iout=55A, Fsw=500kHz, Ta=room

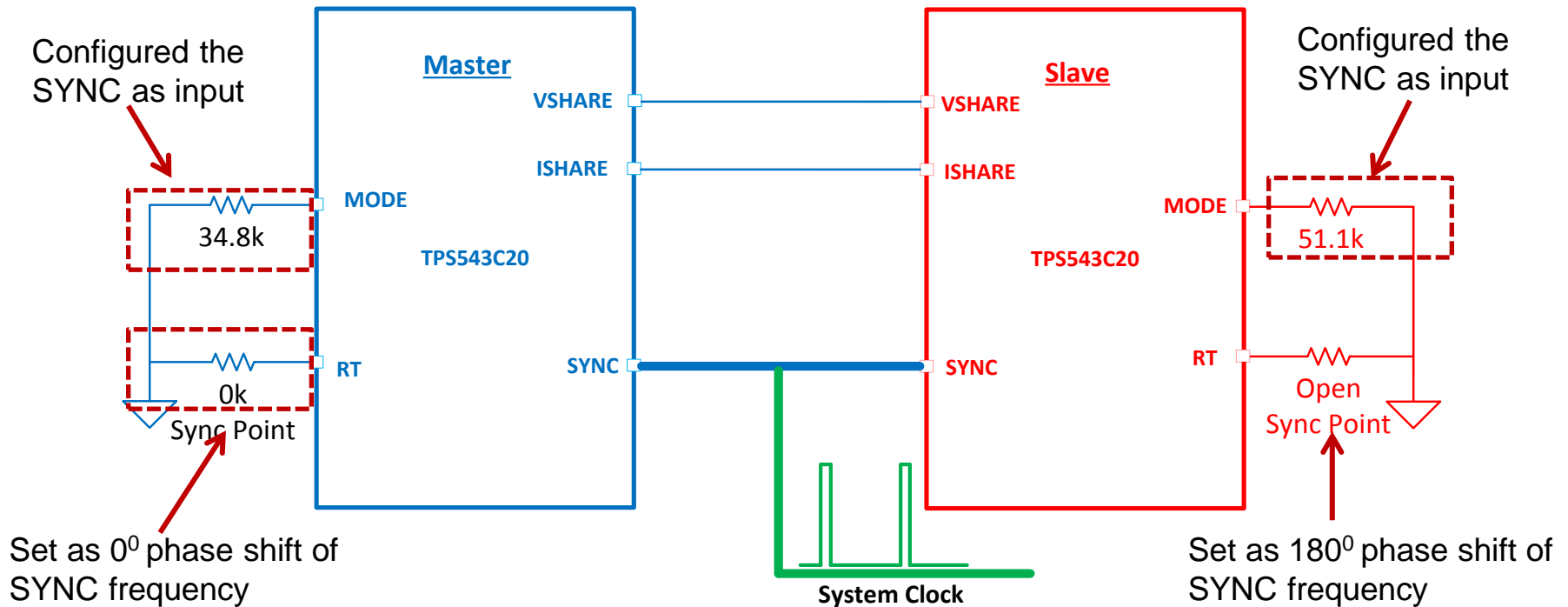
Stackable Operation 1:

- Direct SYNC, VSHARE and ISHARE connections between Master and Slave.
- Switching frequency is set by RT pin of Master, and pass to slave through SYNC pin. SYNC pin of master will be configured as sync out by it's MODE pin.
- Slave receives clock from SYNC pin. It's RT pin determines the sync point for clock phase shift.

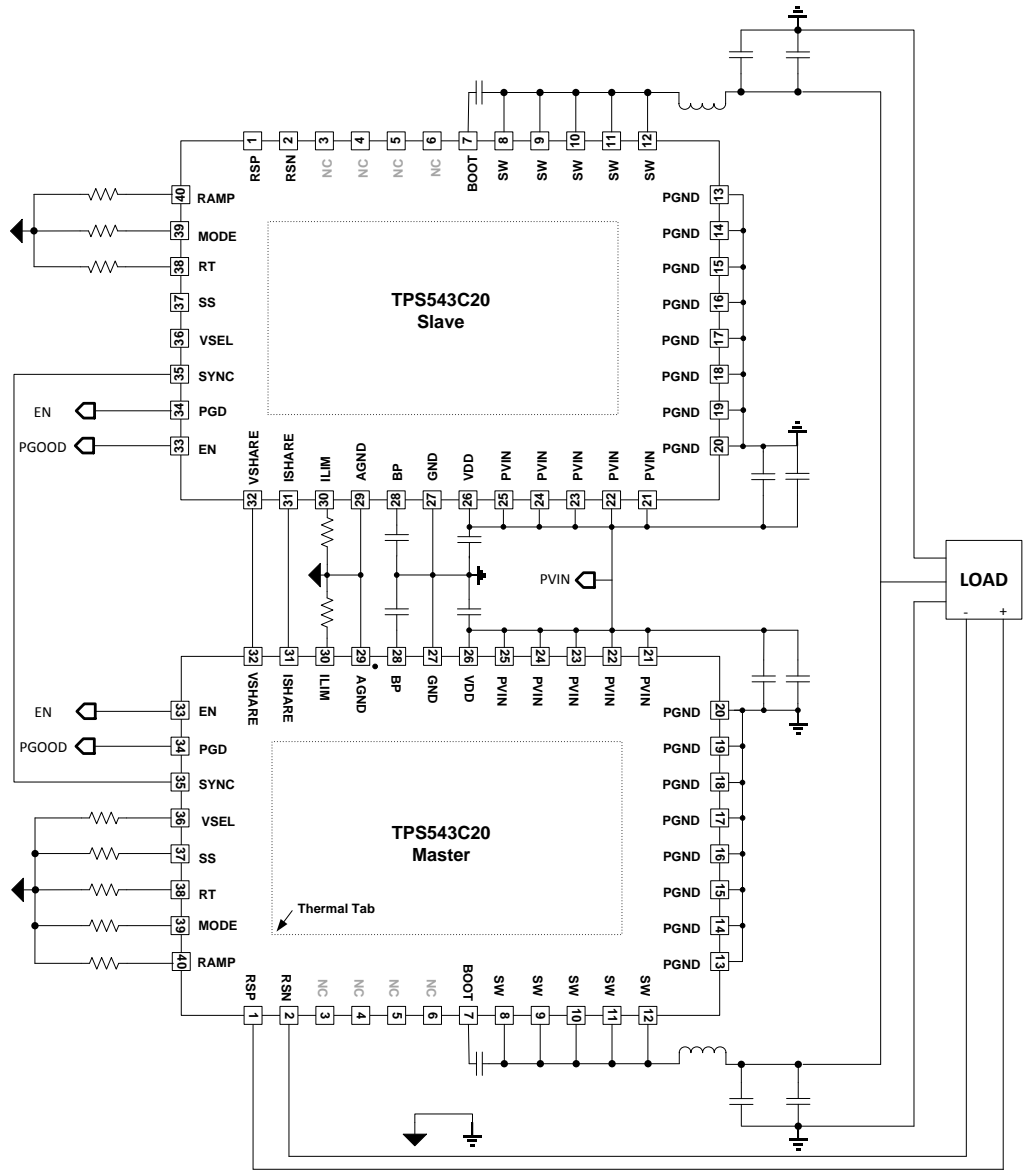


Stackable Operation 2

- Direct connection between external clock and SYNC pin of Master and Slave.
- Direct VSHARE and ISHARE connections between Master and Slave.
- SYNC pin of master will be configured as sync in by it's MODE pin.
- Master and Slave receive external system clock from SYNC pin. Their RT pin determine the sync point for clock phase shift.

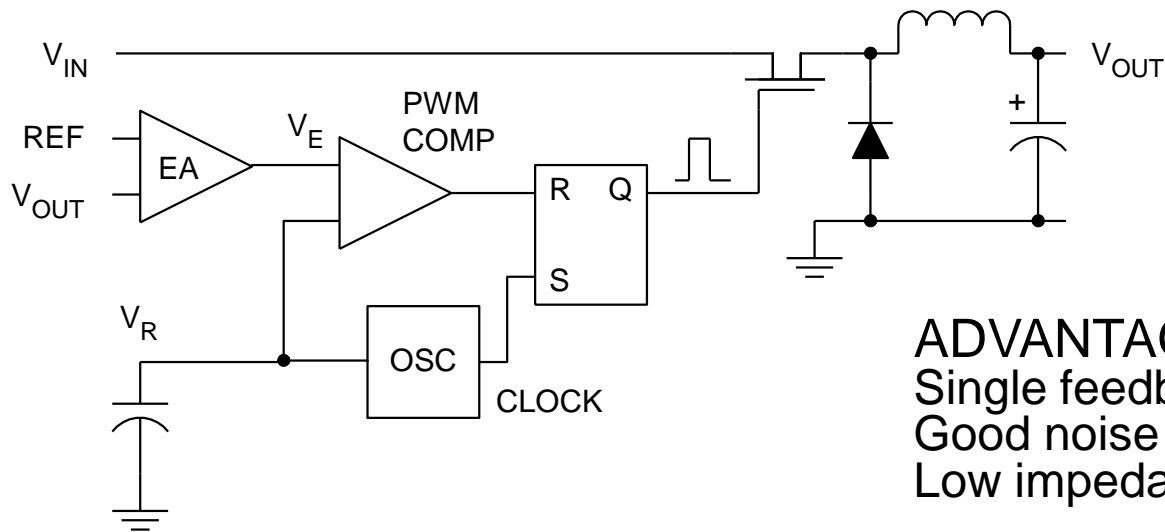


2-Phase Stackable DC/DC schematic



Control Loop Topologies

Voltage Mode

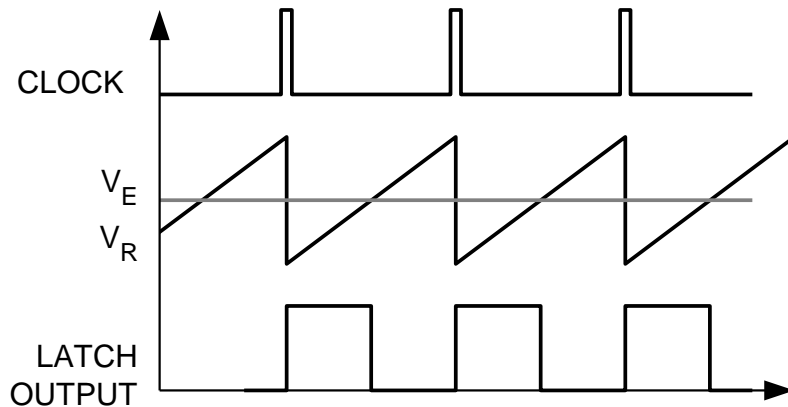


ADVANTAGES

- Single feedback loop
- Good noise margin
- Low impedance output

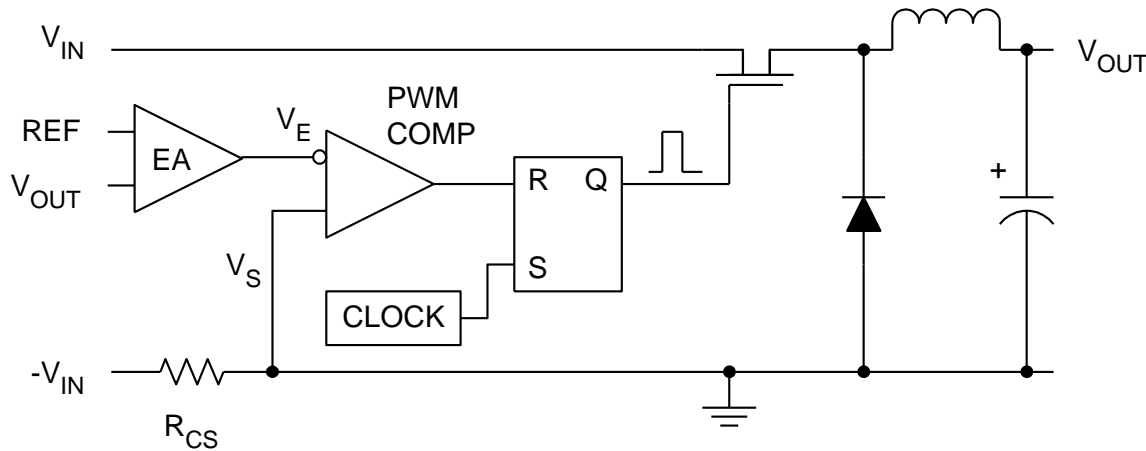
DISADVANTAGES

- Slow dynamic response
- Double-pole compensation
- Output caps affect comp
- V_{IN} affects loop gain



Control Loop Topologies

Current - Mode

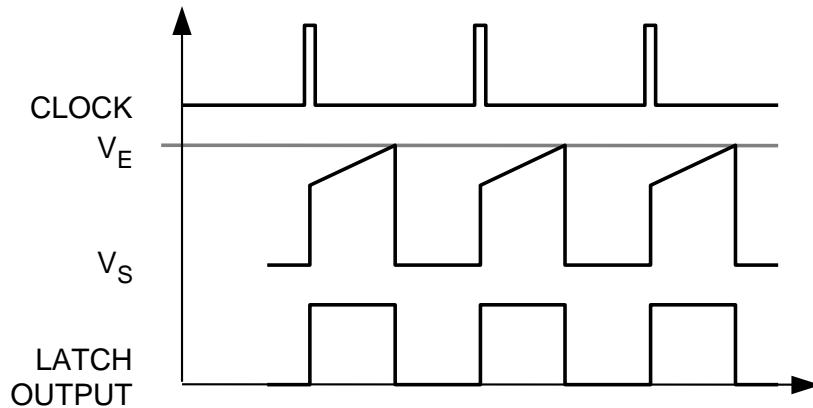


ADVANTAGES

- Fast response to input voltage changes
- Single-pole compensation
- Inherent current limiting
- Parallelability with load sharing

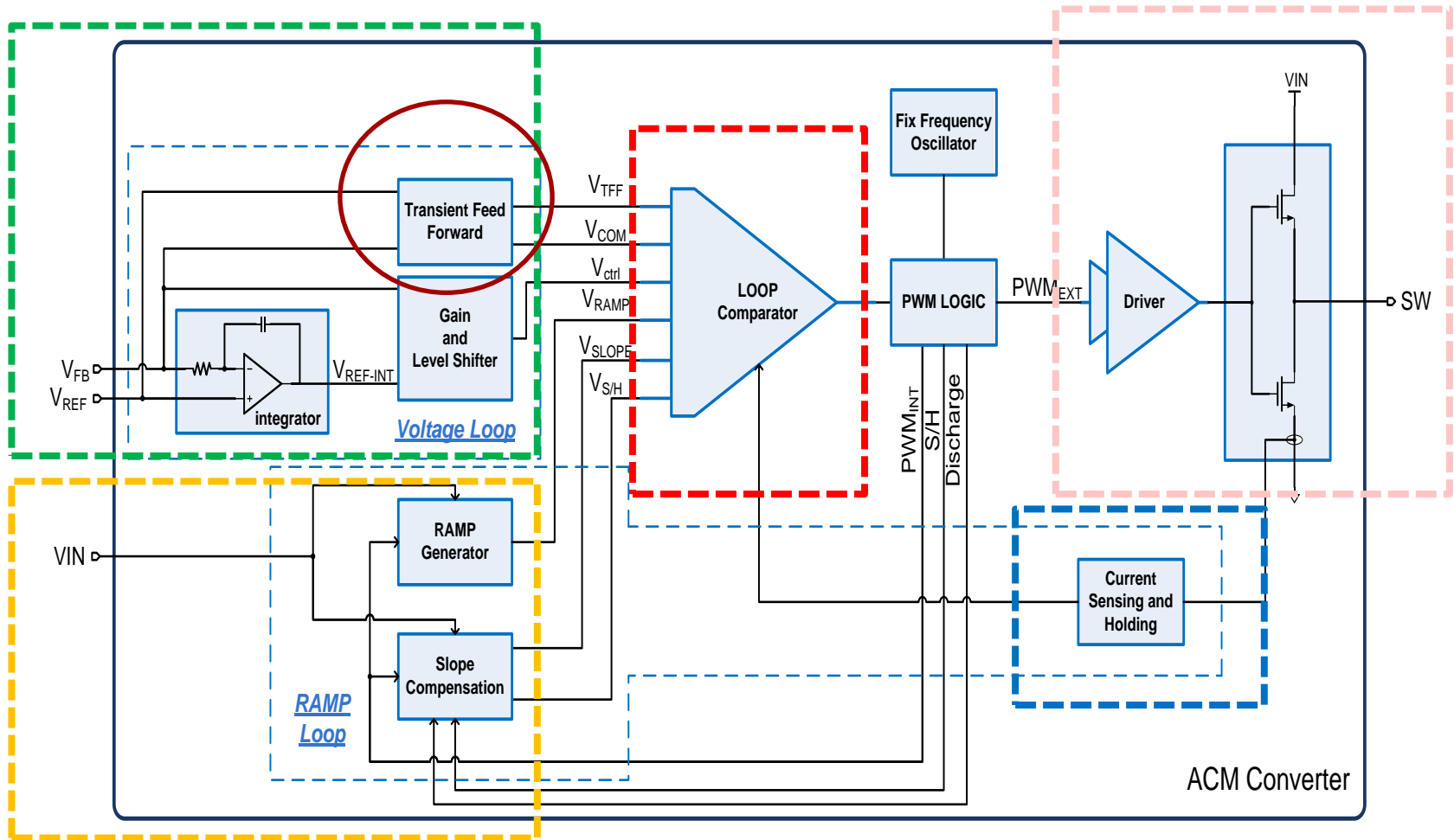
DISADVANTAGES

- Noise sensitivity to current spikes
- Two feedback loops
- Need for slope compensation
- Current limit "tail"



ACM(Advanced Current Mode)-True Fixed Frequency with Internal Compensation

- Inside the converter



Advanced DART Control

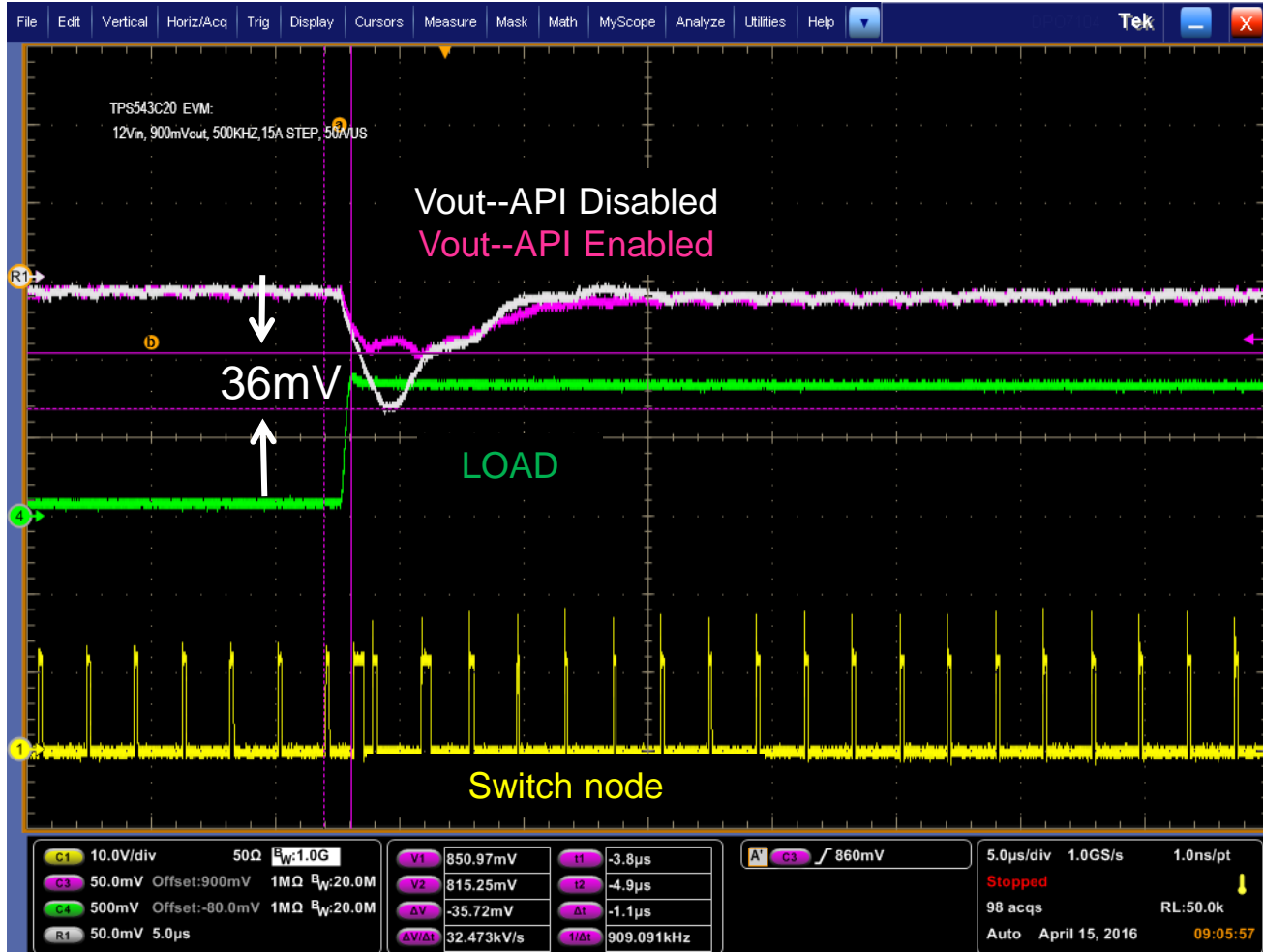
DART : Directly Amplified Ripple Tracking control topology

- TPS543C20 is a true fixed-frequency, non-comp IFET converter
 - Fast loop response
 - Wide LC stability range
 - High Signal to noise ratio. Good jitter performance
 - Ease of design
- DART Control can achieve
 - True fixed frequency modulator
 - No external compensation needed, ease of design
 - One resistor to GND for control loop optimization
 - “Constant phase” for over a decade
 - Wide stability range to support large design parameter variation
 - Supports very high frequency, low duty operation with small Jitter

Fast Transient Response and No External Compensation with DART Control

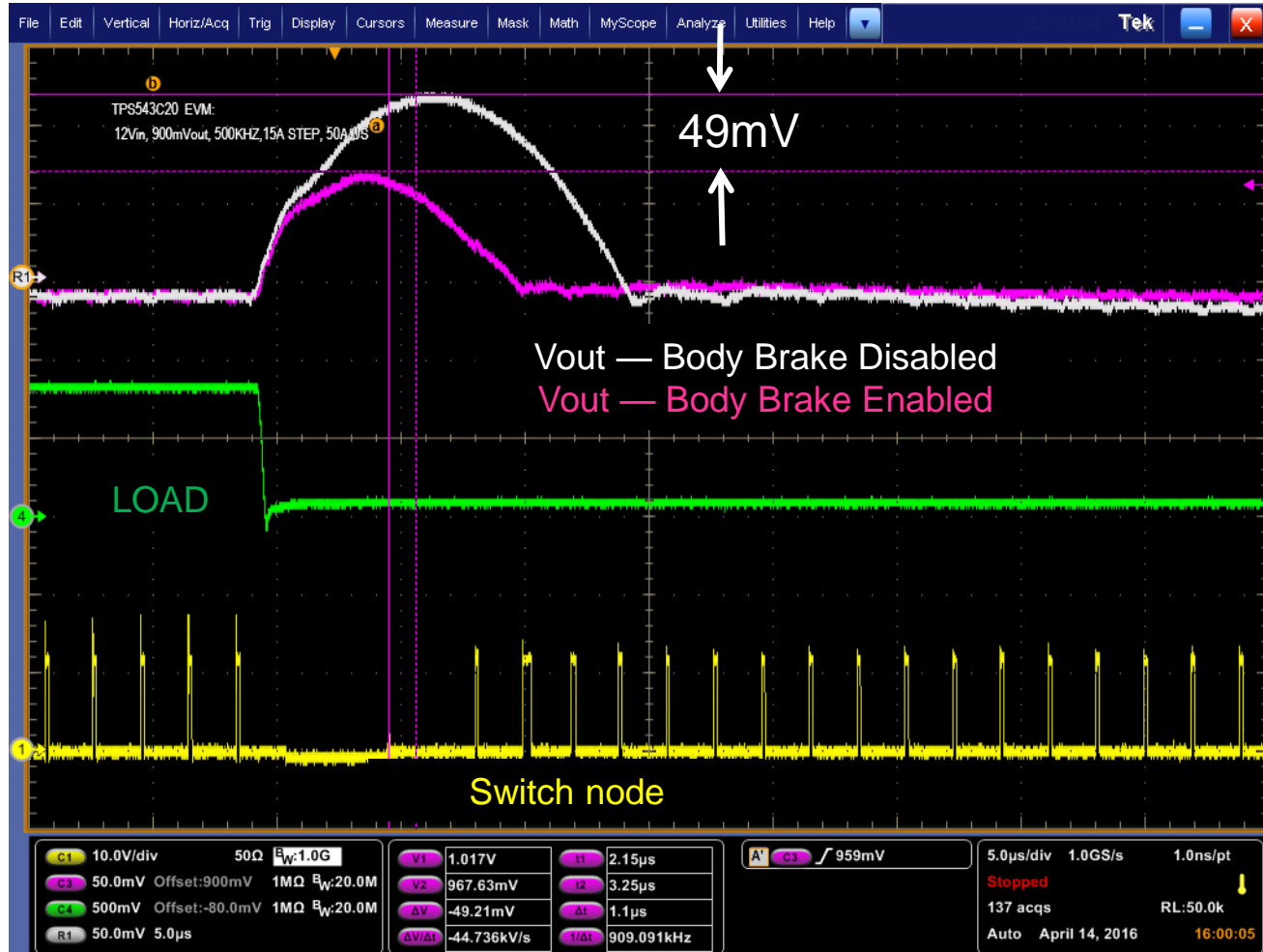
API - Asynchronous Pulse Injection

Further Reducing Transient Undershoot



Body Brake

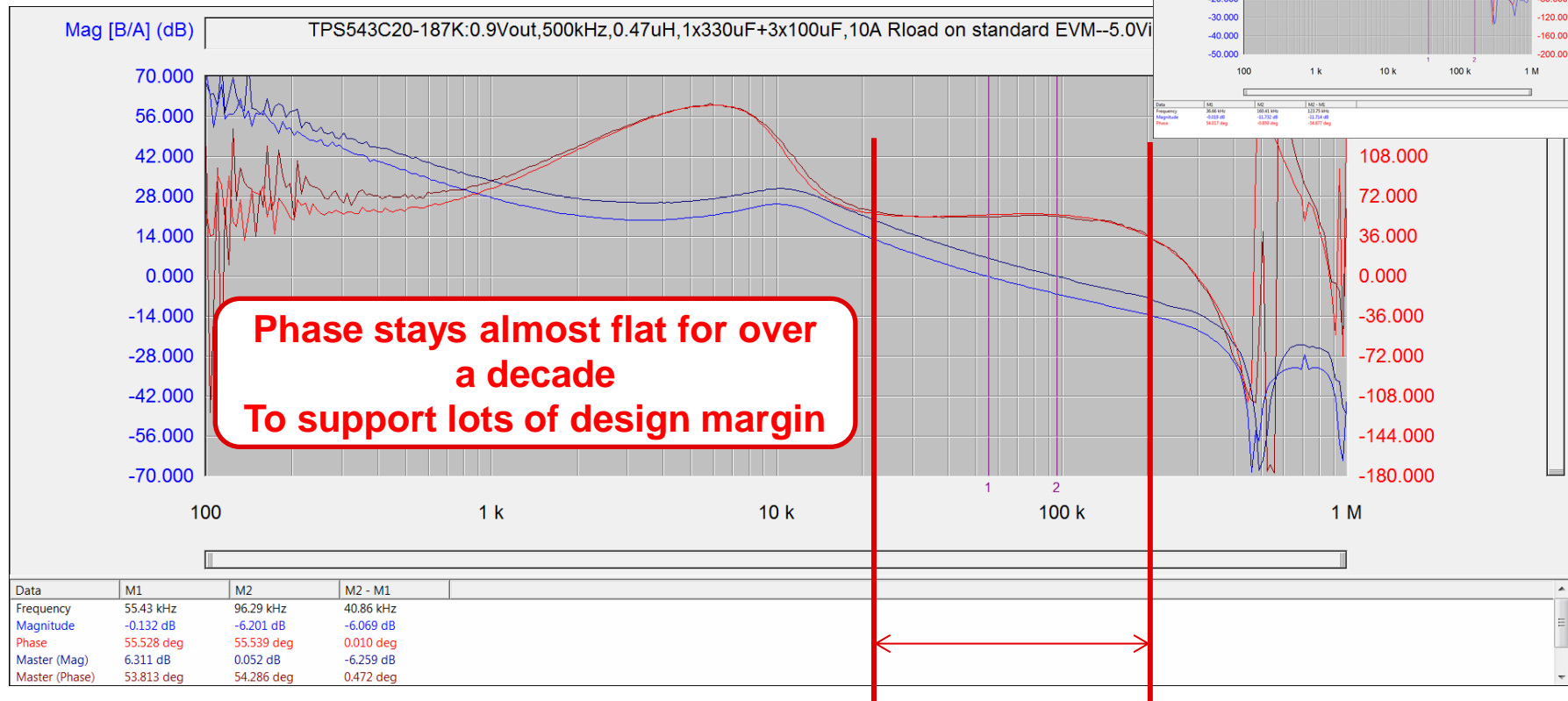
Further Reducing Transient Undershoot



ACM Constant Phase Character

VM control

0.9V, 500kHz, 10A Load and $V_{in} = 5V$ vs. $12V$



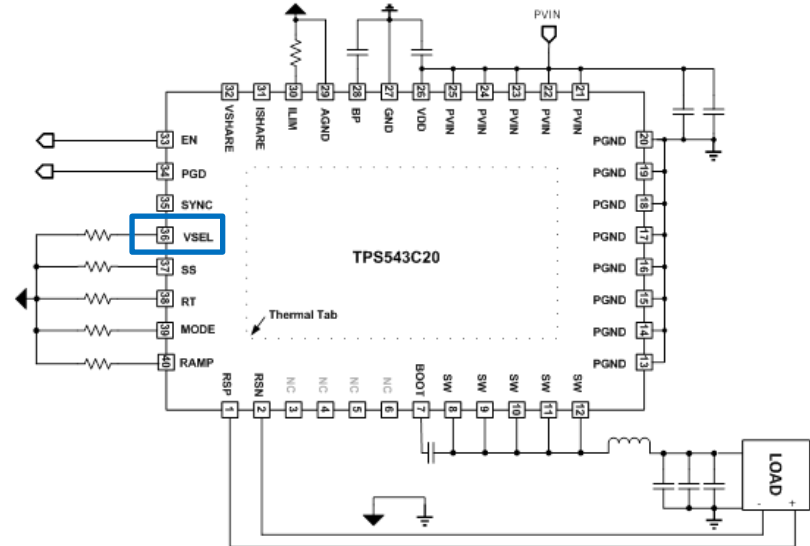
Single Phase Configuration—6 Pins to Setup: Reference voltage or Vout

VSEL pin (36): Set the Vref and RSP/RSN directly to Vout < 1.1V

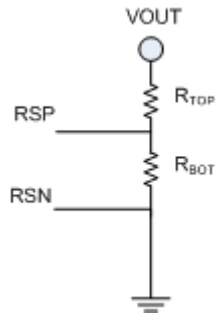
Table 2. VSEL Pin Configuration

DEFAULT Vref (V)	RESISTOR VALUE (k Ω) ⁽¹⁾
0.6	0
0.7	8.66
0.75	15.4
0.8	23.7
0.85	34.8
0.9	51.1
0.95	78.7
1.0	OPEN
1.05	121
1.1	187

(1) The E48 series resistors with no worse than 1% tolerance are recommended



VSEL pin (36): Set the Vref and RSP/RSN directly to resistor divider Vout > 1.1V



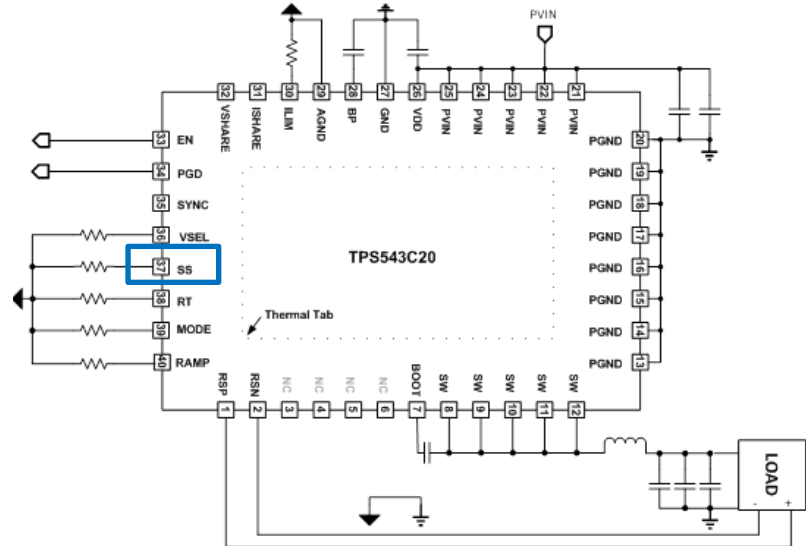
Single Phase Configuration—6 Pins to Setup: Soft-Start

SS pin (37): 10 options to choose from table 1.

Table 1. SS Pin Configuration

SS TIME (ms)	RESISTOR VALUE (k Ω) ⁽¹⁾
0.5	0
1	8.66
2	15.4
5	23.7
4	OPEN
8	34.8
12	51.1
16	78.7
24	121
32	187

(1) The E48 series resistors with no more than 1% tolerance are recommended.



Single Phase Configuration—6 Pins to Setup: Switching Frequency

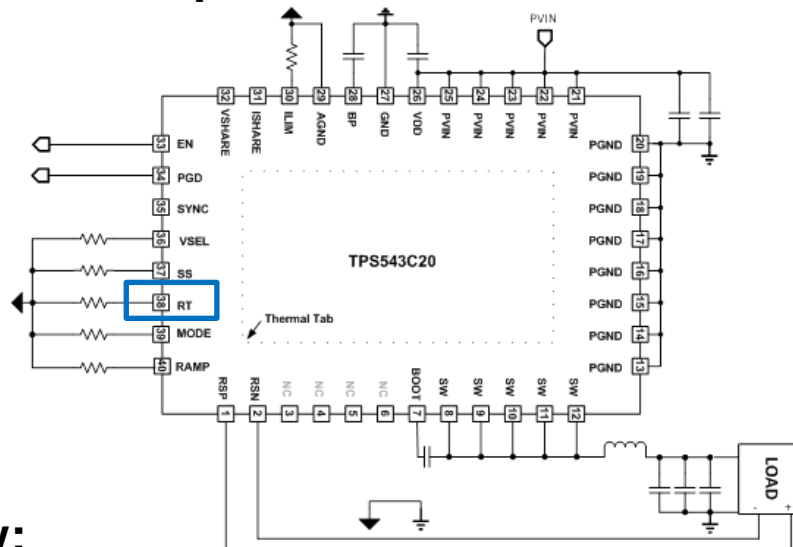
RT pin (38): 300kHz to 2MHz calculation from equation 1.

Resistor R_{RT} sets the continuous switching frequency selection by

$$R_{RT} = \frac{20 \times 10^9}{f_{SW}} - \frac{f_{SW} \times 2}{2000}$$

where

- R is the resistor from RT pin to GND, in Ω
- f_{SW} is the desired switching frequency, in Hz



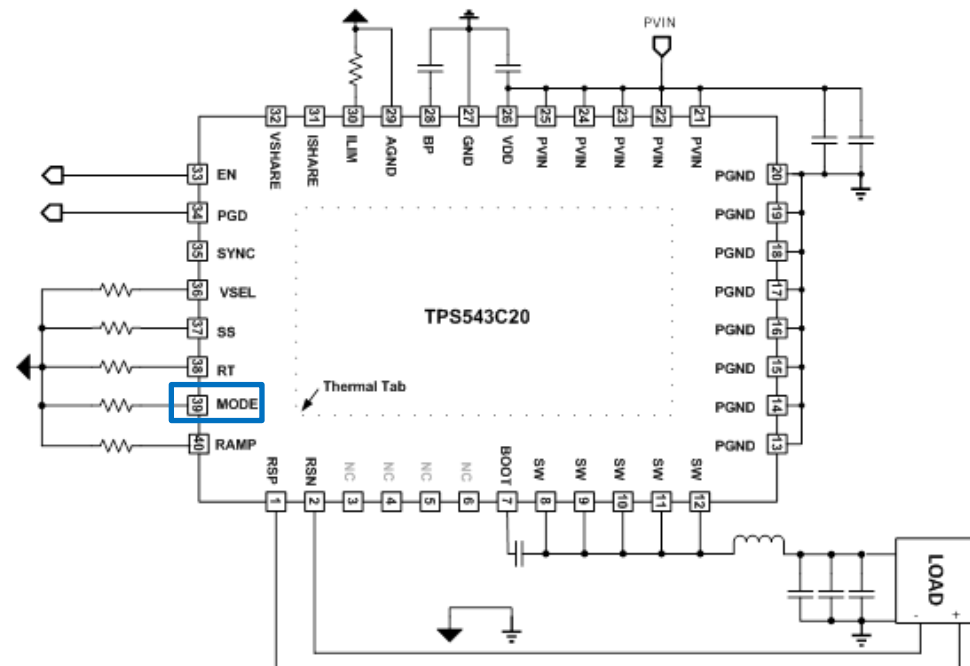
Or use values below for standard Fsw:

SWITCHING FREQUENCY		$V_{RSN}-V_{GND} = 1.00 \text{ V}$	1.0	1.0
F_{SW}	V_O switching frequency Max frequency for multi-phase is 1MHz	$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 66.5 \text{ k}\Omega$	300	kHz
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 48.7 \text{ k}\Omega$	400	
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 39.2 \text{ k}\Omega$	500	
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 28.0 \text{ k}\Omega$	700	
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 22.6 \text{ k}\Omega$	850	
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 19.1 \text{ k}\Omega$	1000	
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 15.4 \text{ k}\Omega$	1200	
		$V_{IN} = 12 \text{ V}, V_{VO} = 1.0 \text{ V}, RT = 8.06 \text{ k}\Omega$	2000	

Single Phase Configuration—6 Pins to Setup: API/BB Selection Options

MODE pin (39): 6 options to choose

API/BB	Resistor Value—Pin 39
Both Off	Open
API=On; BB = Off	15.4K Ω
Both ON at 1x	121K, API = 15mV, BB=30mV
Both ON at 2x	187K, API = 25mV, BB=30mV
Both ON at 3x	8.66K, API = 35mV, BB=30mV
Both ON at 4x	78.7K, API = 45mV, BB=30mV



- When API enables, the RSP/RSN has high pass filter (2.5pF and 2.5M Ω). If the threshold is passing this frequency, API will be active.

- **1x stands for most sensitive and 4x stands for least sensitive**

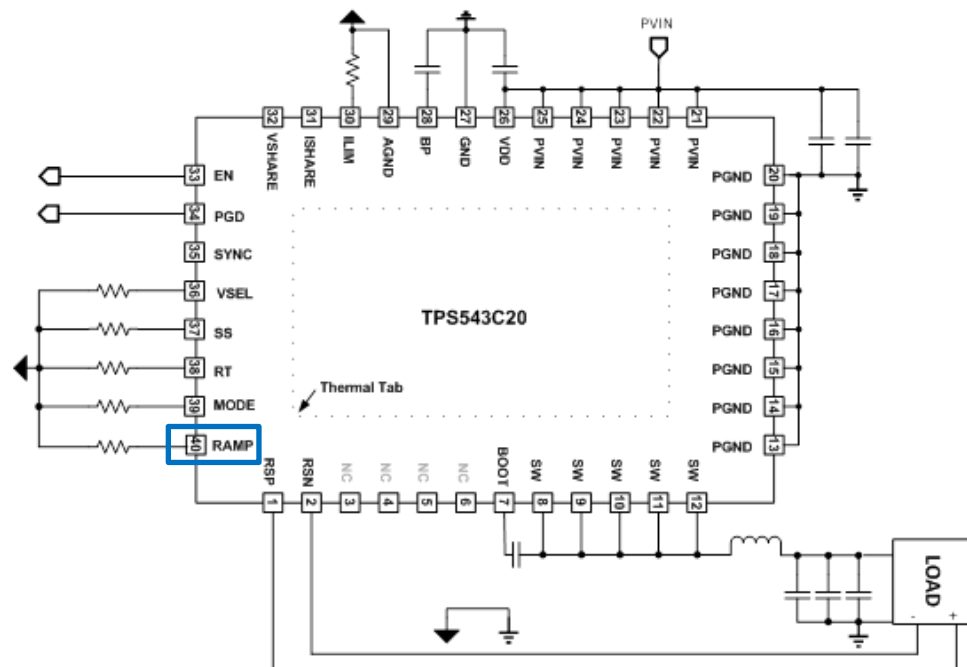
Single Phase Configuration—6 Pins to Setup: RAMP Selection Options

RAMP pin (40): 10 options to choose

Table 3. RAMP Pin-strapping Selection

C_{RAMP} (pF)	RESISTOR VALUE (k Ω) ⁽¹⁾
1	0
1.42	8.66
1.94	15.4
2.58	23.7
3.43	34.8
4.57	51.1
6.23	78.7
8.91	121
14.1	187
29.1	Open

(1) The E48 series resistors with tolerance of 1% or less are recommended.



TPS543C20 is defined to be ease-of-use, for most applications, we recommend ramp resistor to be 187 k Ω to achieve the optimized jitter and loop response. For detailed design procedure please see the WEBENCH® Power Designer.

Single Phase Configuration—6 Pins to Setup: OCP setup

ILIM pin (30): OCP detects near peak inductor

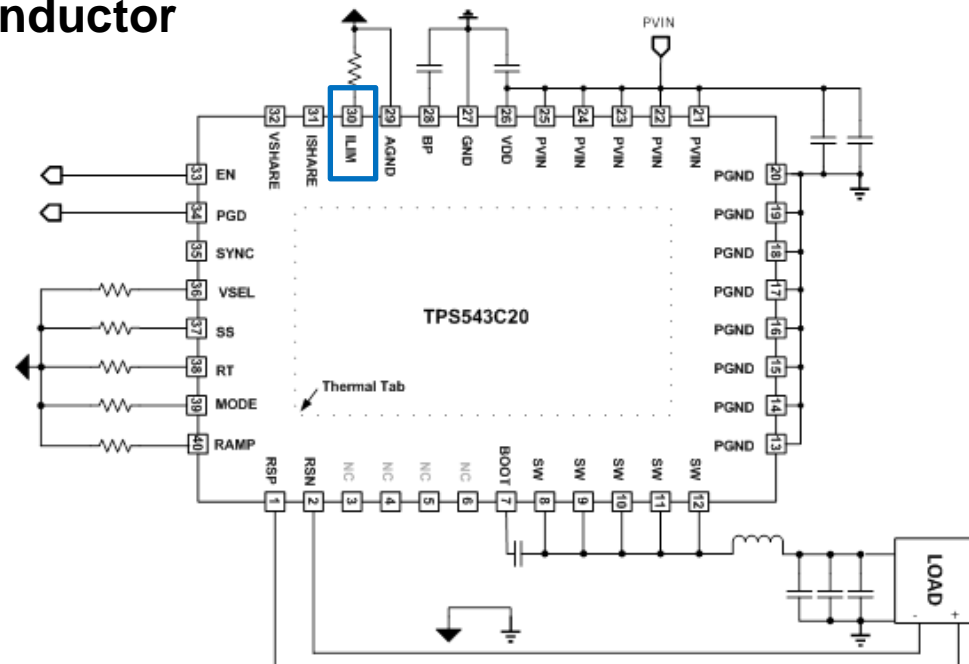
$$I_{OCP} = \frac{V_{ILIM}}{16 \times R_{DS(on)}} - \frac{I_{IND(ripple)}}{2}$$

$$= \frac{V_{ILIM}}{16 \times R_{DS(on)}} - \frac{1}{2 \times L \times f_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}}$$

where

- $R_{DS(on)}$ is the on-resistance of the low-side MOSFET.

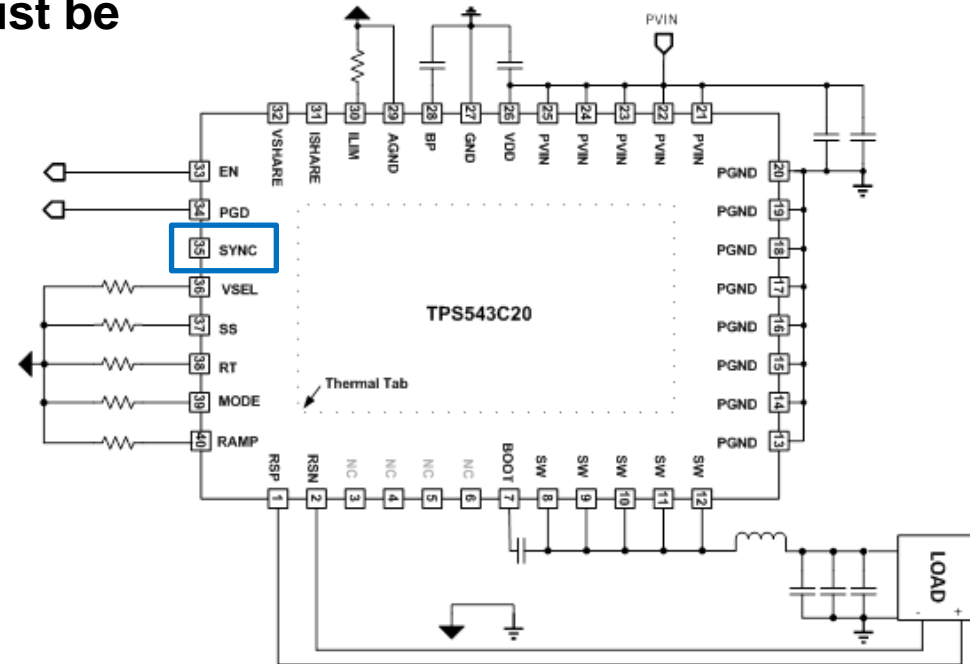
$\frac{1}{2}$ of Inductor
Current Ripple



Use $R_{dson} = 0.62m\Omega$ for above equation due to die sense

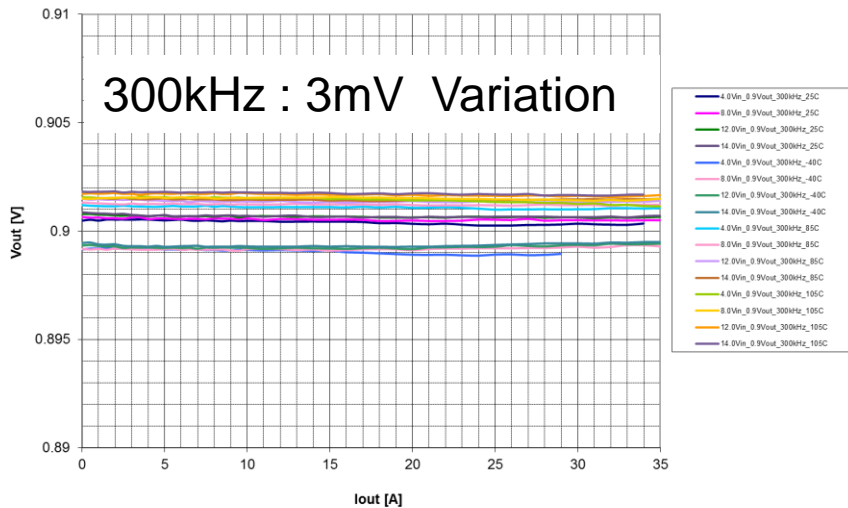
SYNC in Single Phase Configuration

SYNC pin (35): External frequency must be higher or equal to RT setting

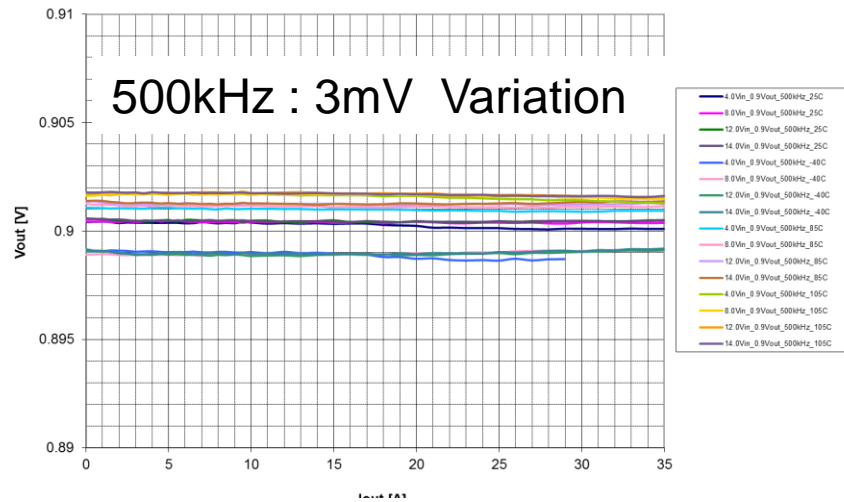


TPS543C20 VOUT Regulation: 4Vin-14Vin, -40C to 105C

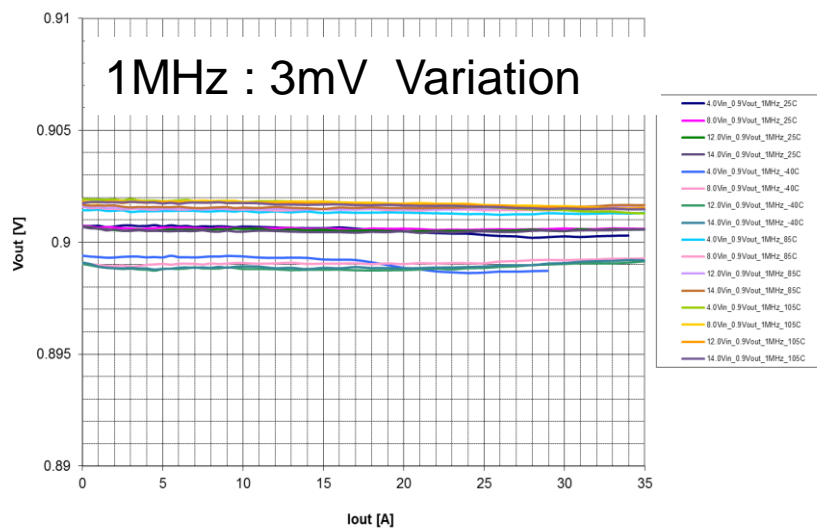
Load Regulation Performance



Load Regulation Performance



Load Regulation Performance



Private

Fault Protection

- Input Voltage UVLO
 - 3.8V UVLO for Vbias and VIN
- UV Protection
 - 83% of reference voltage
- OV Protection
 - 117% of reference voltage
- Over Current protection
 - Fixed HS OCP and programmable LS OCP
- Hiccup for OV, UV, OC

Summary

- Advanced Control Scheme
 - TPS43C20 is a true fixed-frequency, non-comp IFET converter
 - Fast transient response
 - Wide LC stability range with “**Constant Phase**” Character
 - Ease of design
 - Supports very high frequency, low duty operation
- Advanced Integrated MOSFET
 - Very low (sub-m Ω) Rdson, high efficiency performance
 - TPS543C20:~3.0/0.9m Ω
 - TPS543B20:~4.1/1.9m Ω
- Full of Feature sets
 - True remote sense.
 - Sync capability, sync IN/OUT
 - Very tight OC accuracy (+/-10%)
 - API/Body brake function to help transient
 - **2-phase Stackable. Good design flexibility**
- Other:
 - 40A/25A versions in same package
 - Low bias voltage support (down to 4V)

Thank you !

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