

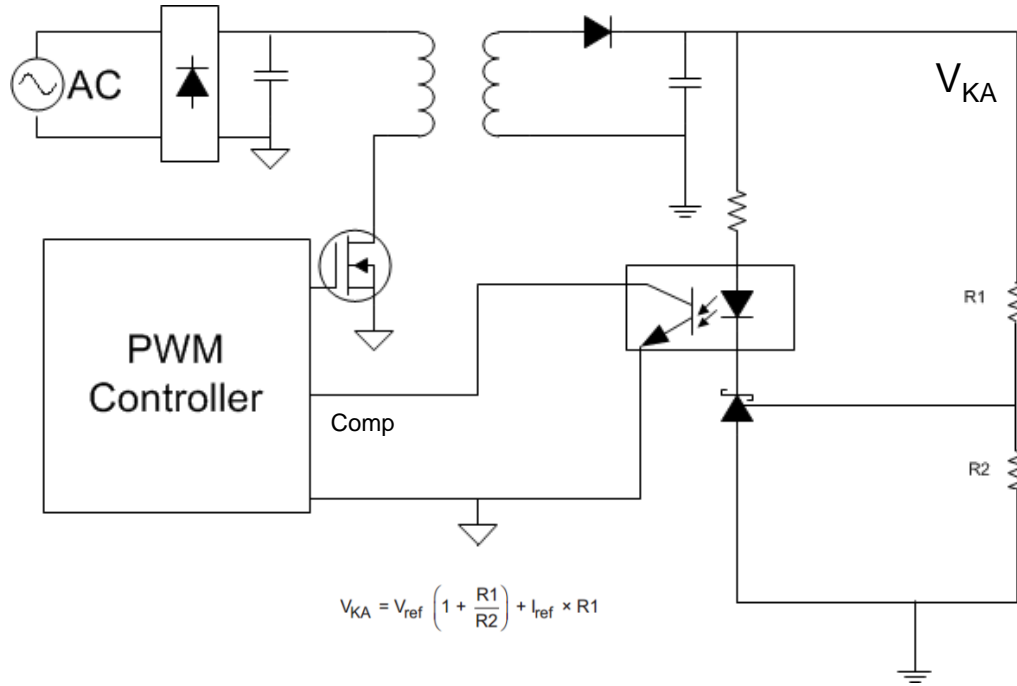
Shunt Reference Considerations for Flyback Converters with Optocoupler Feedback

A Voltage Reference Deep Dive

Agenda

- Why do I need a shunt voltage reference in flyback systems with optocoupler feedback?
- Feedback process example
- Importance of lower I_{ref} and I_{ref} delta
- Importance of lower $I_{\text{l(dev)}}$ and $I_{\text{l(dev)}}$ delta
- Total system accuracy calculations
- Stand by power (Class VI) standards

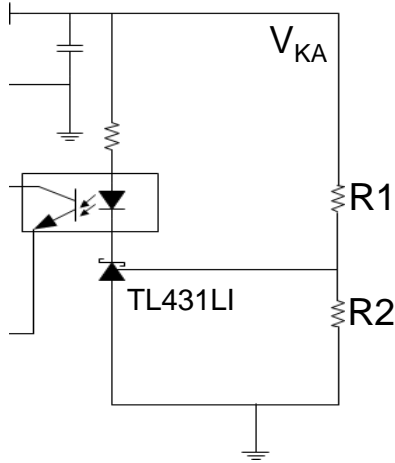
AC/DC Flyback systems with optocoupler feedback



- Secondary side regulation
- Drives optocoupler as a current controller
- Senses output voltage and feeds information back via optocoupler

Output voltage (V_{ka}) error due to discrete resistor choices

$$V_{ka} = (V_{ref}) * \left(1 + \frac{R1}{R2}\right) + (I_{ref} * R1)$$



For $V_{ka} = 5V$ and $R1 = 10K\Omega$:

- $R2 = 10.1K\Omega$ for $I_{ref} = 4\mu A$
- $R2 = 10.01K\Omega$ for $I_{ref} = 0.4\mu A$

Part	I_{ref} Max
TL431	4 μA
TL431LI	0.4 μA

Standard Resistor Values: 9.1K Ω , 10K Ω , 11K Ω

$$\text{Error in } V_{ka} = I_{ref} * R1$$

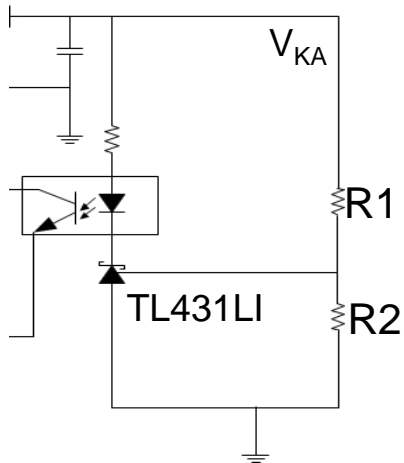
TL431 Error = $I_{ref} * R1 = 4\mu A * 10K\Omega = 40mV$ (0.8% of a 5V system)

TL431LI Error = $I_{ref} * R1 = 0.4\mu A * 10K\Omega = 4mV$ (0.08% of a 5V system)

Importance of lower I_{ref} delta

Error $V_{ka} = I_{ref} * R1$

For $R1 = 10K\Omega$, Error V_{ka} is calculated as:



- Industry standard TL431: Part-to-part variation (ΔI_{ref}) is 2uA**

		Typ		Max	
I_{ref}	Reference input current	See Figure 21	$I_{KA} = 10 \text{ mA}, R1 = 10 \text{ k}\Omega, R2 = \infty$	2	4 μA

TL431 $\Delta I_{ref} = 4\mu\text{A} - 2\mu\text{A} = 2\mu\text{A}$

Error $V_{ka} = \Delta I_{ref} * R1 = 2\mu\text{A} * 10K\Omega = 20\text{mV}$

- TL431LI: Part-to-part variation (ΔI_{ref}) is only 0.2uA**

		Typ		Max	
I_{ref}	Reference Input Current	See Figure 15	$I_{KA} = 1 \text{ mA}, R1 = 10\text{k}\Omega, R2 = \infty$	0.2	0.4 μA

TL431LI, $\Delta I_{ref} = 0.4\mu\text{A} - 0.2\mu\text{A} = 0.2\mu\text{A}$

Error $V_{ka} = \Delta I_{ref} * R1 = 0.2\mu\text{A} * 10K\Omega = 2\text{mV}$

Initial accuracy improvement with lower $I_{I(dev)}$

Error $V_{ka} = I_{ref} * R1$ $I_{I(dev)}$ is I_{ref} over full operating temperature (-40°C to 125°C)

Industry standard TL431:

$$I_{I(dev)} \text{ Error } V_{ka} = I_{I(dev)} * R1 = 1.2\mu A * 10K\Omega = 12mV$$

(0.24% of a 5V system)

$$\Delta I_{I(dev)} \quad \Delta I_{I(dev)} = 1.2\mu A - 0.4\mu A = 0.8\mu A$$

$$\text{Error } V_{ka} = \Delta I_{I(dev)} * R1 = 0.8\mu A * 10K\Omega = 8mV$$

$I_{I(dev)}$	Deviation of reference input current over full temperature range ⁽¹⁾	See Figure 21	$I_{KA} = 10 \text{ mA}, R1 = 10 \text{ k}\Omega, R2 = \infty$	Typ Max		
				0.4	1.2	μA

TL431LI:

$$I_{I(dev)} \text{ Error } V_{ka} = I_{I(dev)} * R1 = 0.3\mu A * 10K\Omega = 3mV$$

(0.06% of a 5V system)

$$\Delta I_{I(dev)} \quad \Delta I_{I(dev)} = 0.3\mu A - 0.1\mu A = 0.2\mu A$$

$$\text{Error } V_{ka} = \Delta I_{I(dev)} * R1 = 0.2\mu A * 10K\Omega = 2mV$$

$I_{I(dev)}$	Deviation of reference input current over full temperature range ⁽¹⁾	See Figure 15	$I_{KA} = 1 \text{ mA}, R1 = 10k\Omega, R2 = \infty$	Typ Max		
				0.1	0.3	μA

Cost savings

$$\text{Error } V_{ka} = (I_{ref} + I_{I(dev)}) * R1$$

$$I_{ref} = I_{ref} \pm I_{I(dev)} \text{ over full operating temperature}$$

Let R1 = 10KΩ

Part	Resistor Accuracy	Error V_{ka}
TL431	10%	= 5.2uA * 11KΩ = 57.2 mV
	1%	= 5.2uA * 10.1KΩ = 52.5 mV
TL431LI	10%	= 0.7uA * 11KΩ = 7.7 mV
	1%	= 0.7uA * 10.1KΩ = 7.07mV

	TL431	TL431LI
Iref (μA)	4	0.4
I(dev) (μA)	1.2	0.3
Max Iref (μA)	5.2	0.7

Resistors cost saving with 10% resistors

Volume	1% SMD resistor price	10% SMD resistor price	Total cost saved per system (Two resistors)
10,000	\$0.004	\$0.002	\$0.004

Save on resistors!

Efficiency standards for under 50W power supplies

- Stricter requirements for no-load power consumption
- Adopted by Europe, China, Canada, and US
- US enforces Class VI standard

	Class IV	Class V	Class VI
No load power requirement	500mW	300mW	75mW

Class VI power supply design considerations

System requirements with no load condition:

European COC	75mW	Adapter power <49W
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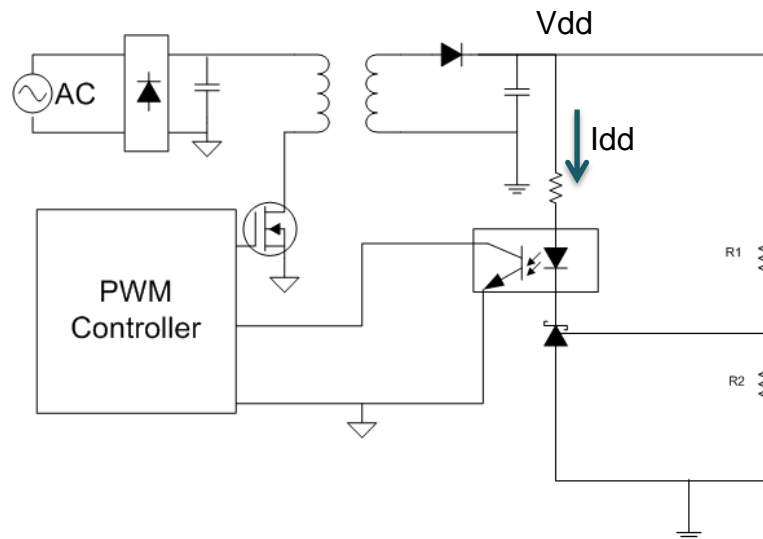
Power consumed by TL431 branch = $V_{dd} * I_{dd}$

Ex.
TL431: $V_{dd} = 20V$, $I_{dd} = 2mA$ given practical design using the **TL431** and a regular optocoupler

ATL431LI: $V_{dd} = 20V$, $I_{dd} = 200\mu A$ given practical design using the **ATL431LI** and an advanced optocoupler

230V AC input	TL431LI	*Components	ATL431LI	*Components
Power (mW)	40	40	4	40
Total (mW)	80		44	

*Components consist of: MOSFETs, controllers, etc



Thanks for Watching

- Please visit ti.com/vref