

High **VOLT** Interactive

Where power supply design meets collaboration

Gate Driver Design – from Basics to Details

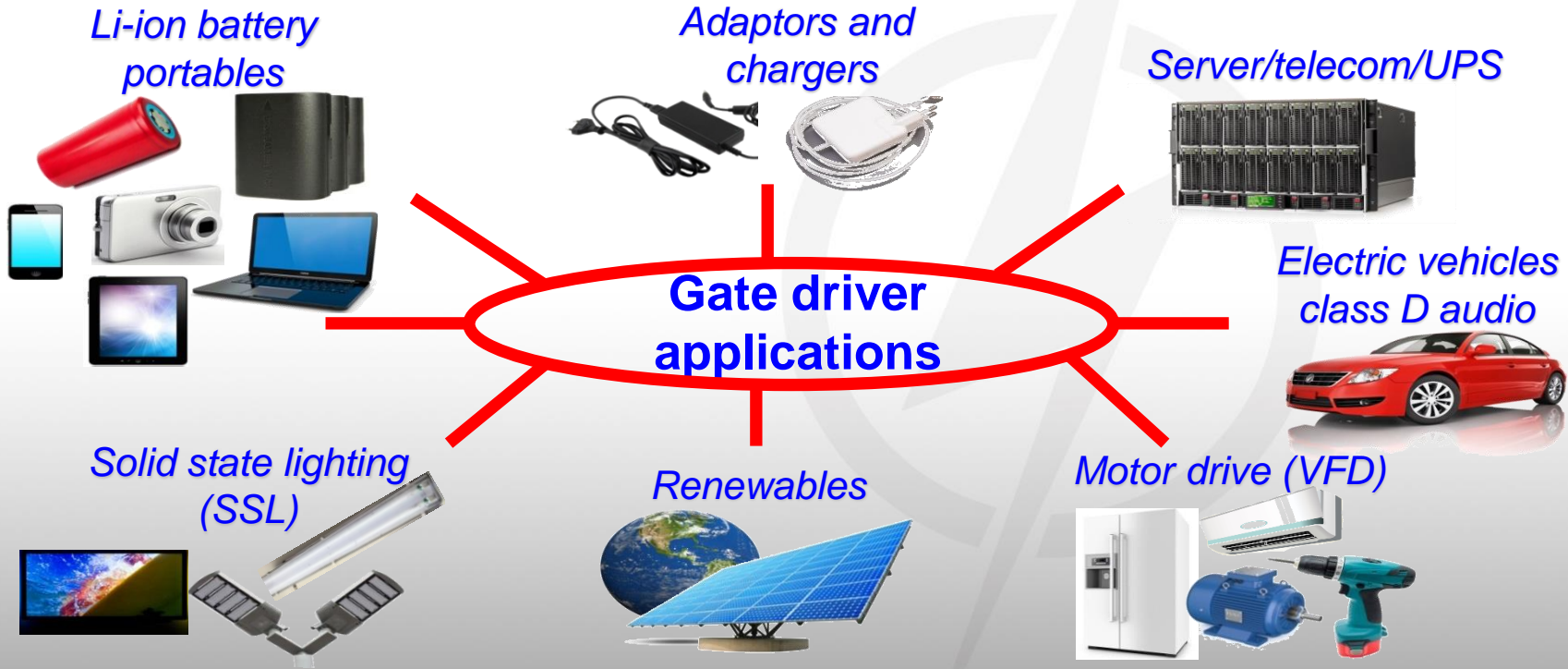
Wei Zhang

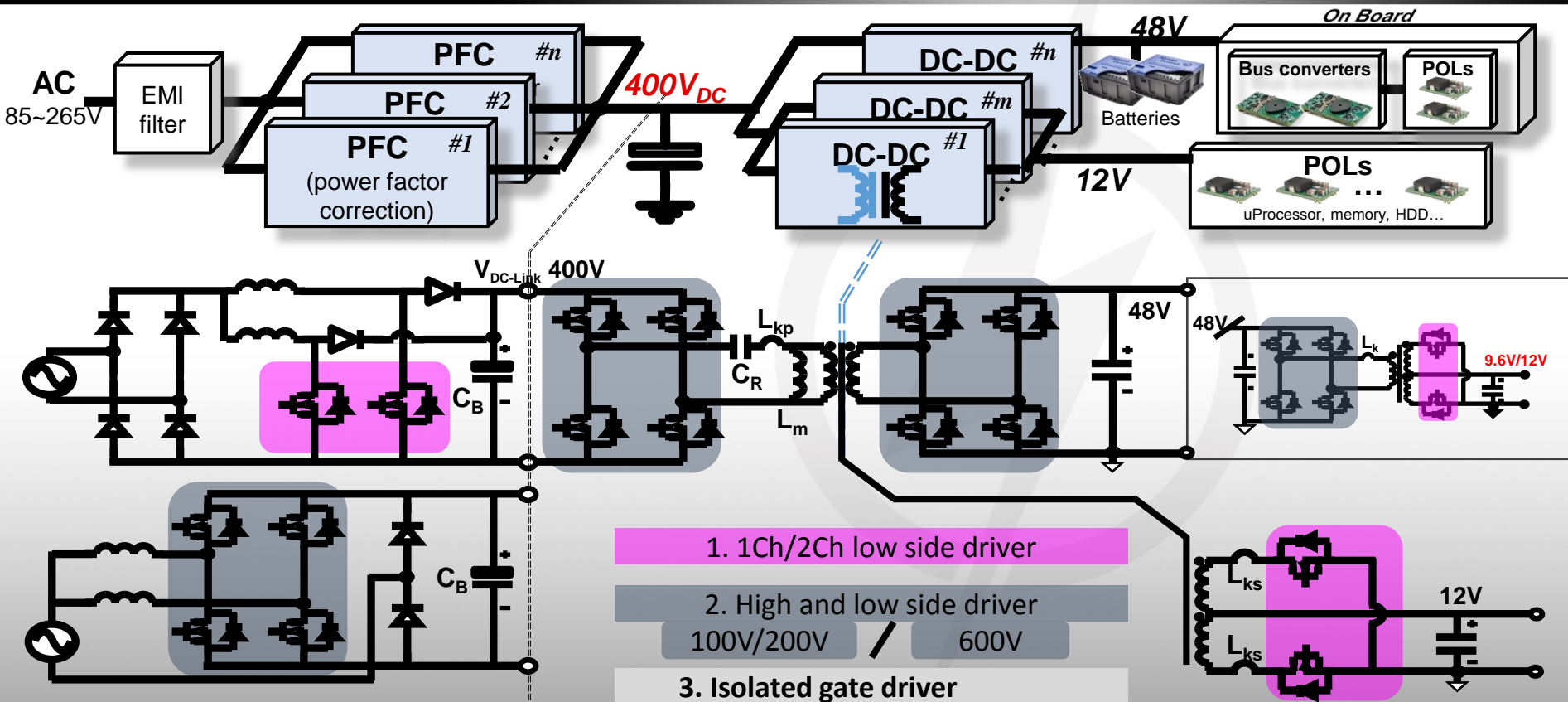
What will I get out of this session?

❑ **PURPOSES:**

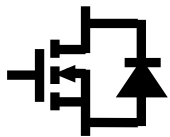
- What is the difference: low side, high and low side driver, and isolated gate driver?
- How to maximize the gate driver performance – from basic to details
 - Parasitics in the gate driver
 - Hard/soft switching
 - High dv/dt and di/dt
 - Isolated gate driver
- Part numbers mentioned:
 - Low side: UCC2751x, UCC2752x, UCC27x24
 - H-/L- Side: UCC2771x, UCC272xx
 - Isolated: UCC2152x, UCC2122x UCC53xx
- Reference designs mentioned:
 - TIDA-01160, TIDA-01159
- Relevant end equipment:
 - EV/HEV, UPS, telecom, servers, solar, motor drive

Where are gate driver ICs used?

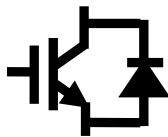




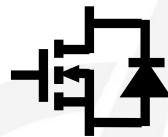
Si-MOSFET



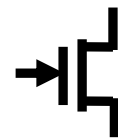
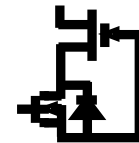
IGBT



SiC-MOSFET



GaN



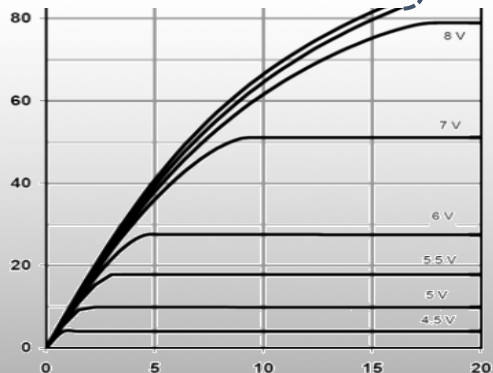
Nom-ON

Nom-OFF

Voltage ratings	20~650V	≥650V	≥650V	≤650V	
Optimal V_{GS}	0~15V	-10~15V	-5~20V	-5~10V	-4~6V
Max.limit	(±20V)	(±20V)	(-10~25V)	(±18V)	(-10~7V)

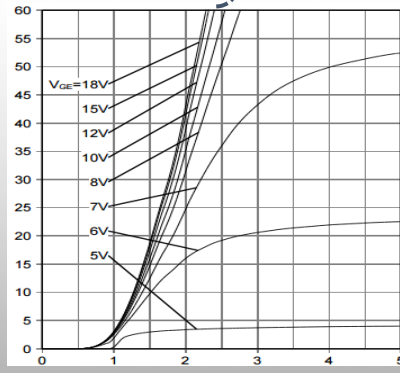
Si-MOSFET

10V

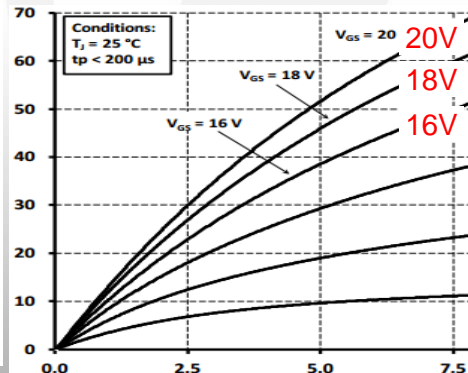


IGBT

12V

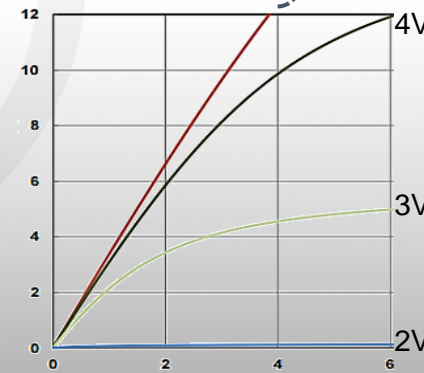


SiC-MOSFET

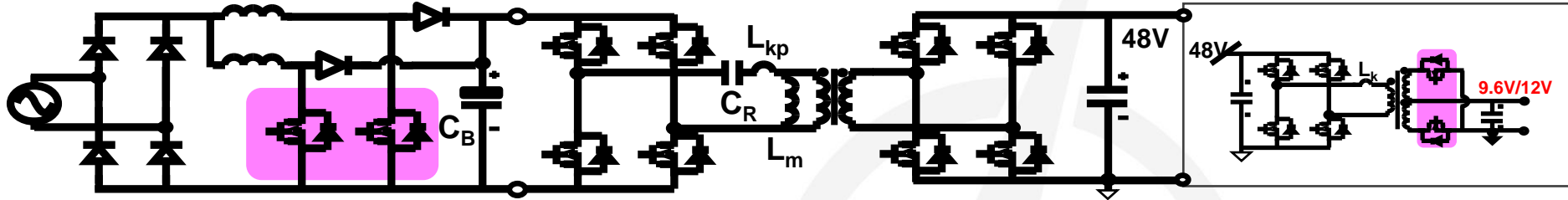


GaN

5V



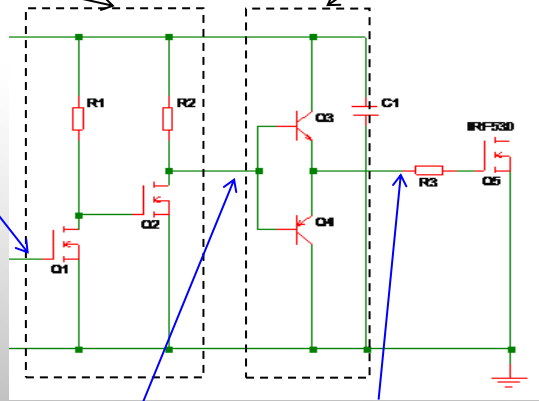
- I-V curves are from datasheets of Infineon, Fairchild, ST, CREE, EPC



Level shift circuit + NPN/PNP totem pole

3.3V/5V
PWM signal from
microcontroller or
DSP

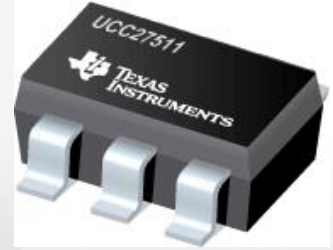
Micro/DSP



Level shifted
12V signal

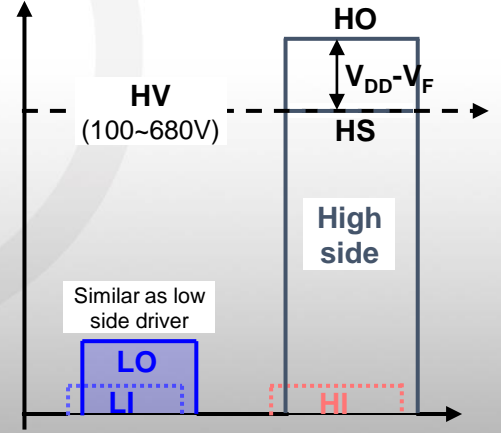
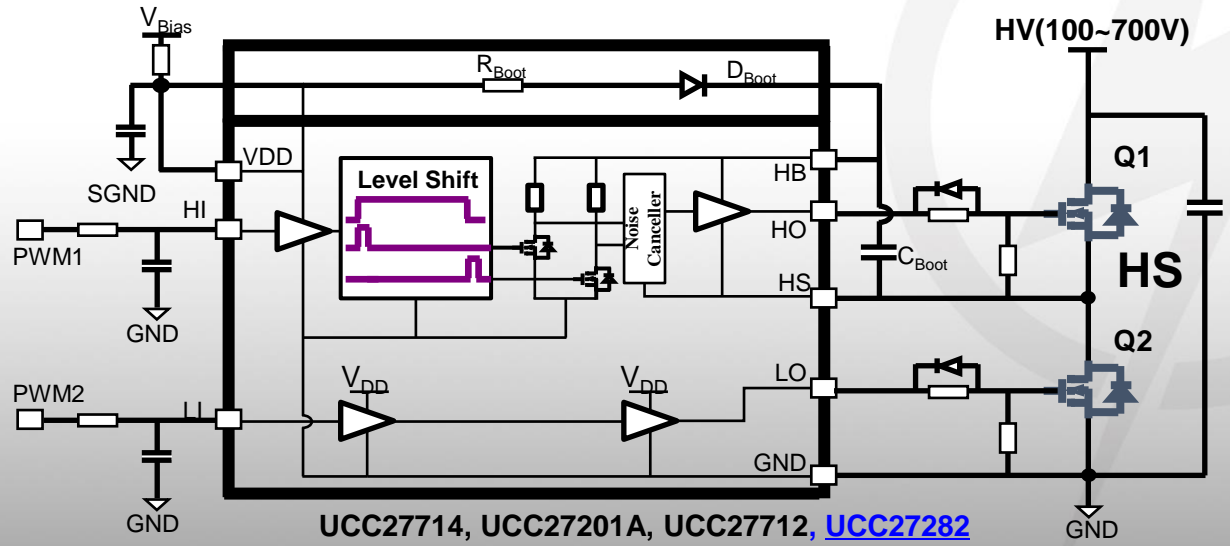
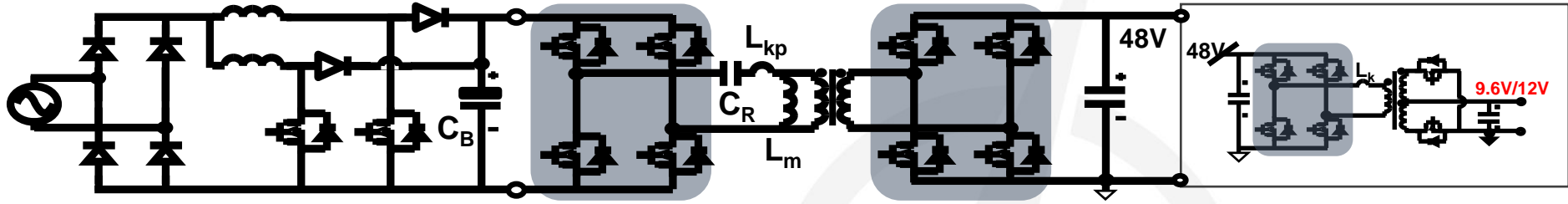
12V with high peak
source/sink current

Now

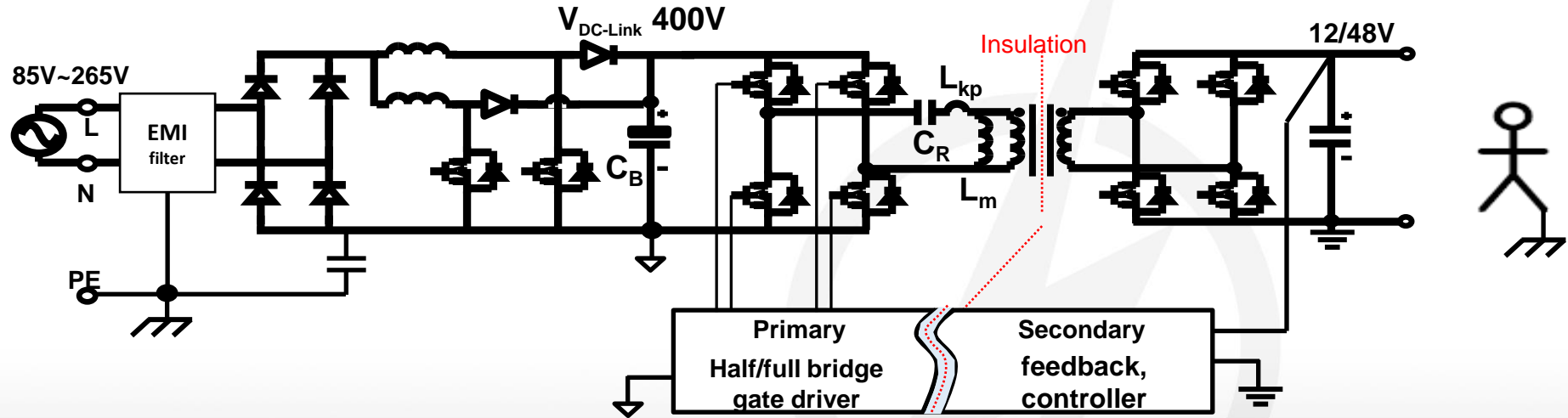


- Reduces BOM component count
- Reduces PCB space
- Protects from spurious signals during power up (such as UVLO)
- Improves reliability

High **VOLT** Interactive How does a Half-Bridge Driver Operate?



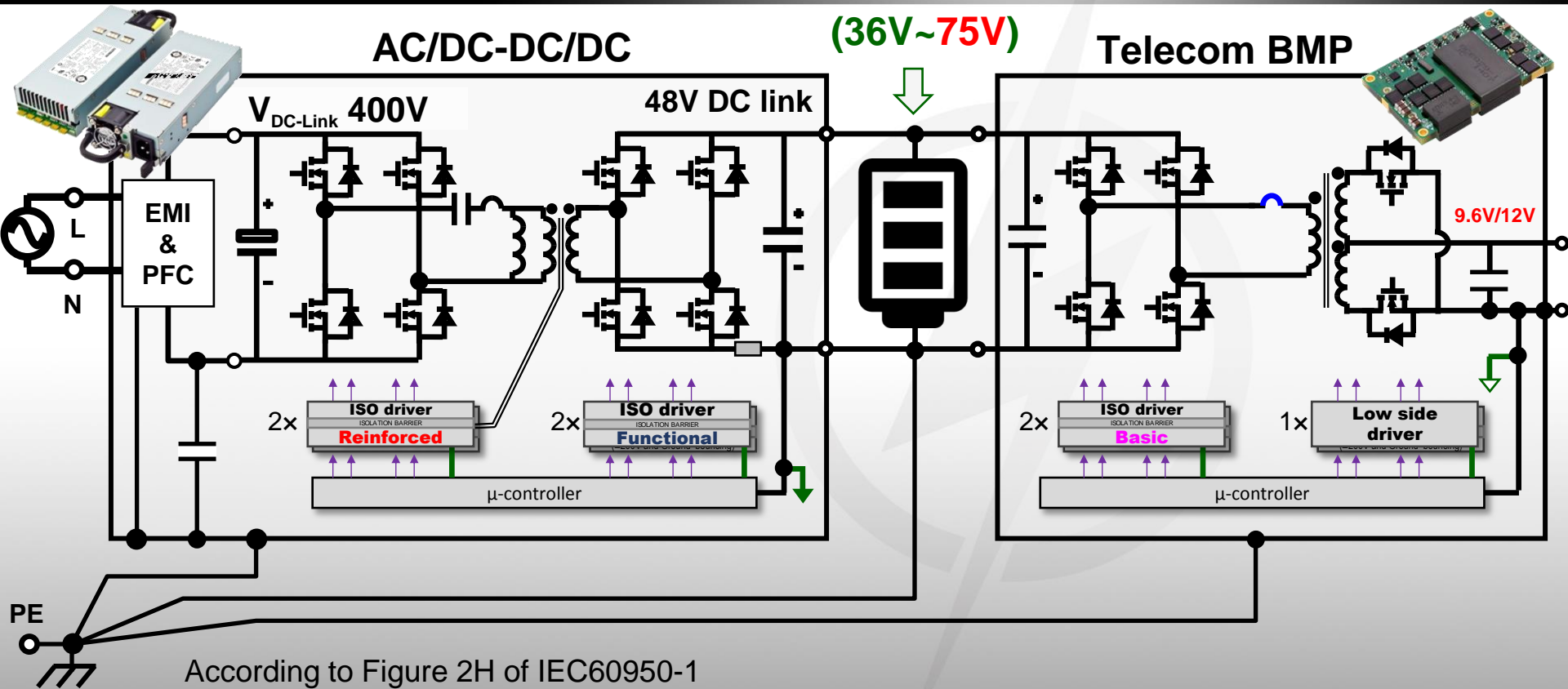
UCC27714, UCC27201A, UCC27712, [UCC27282](#)



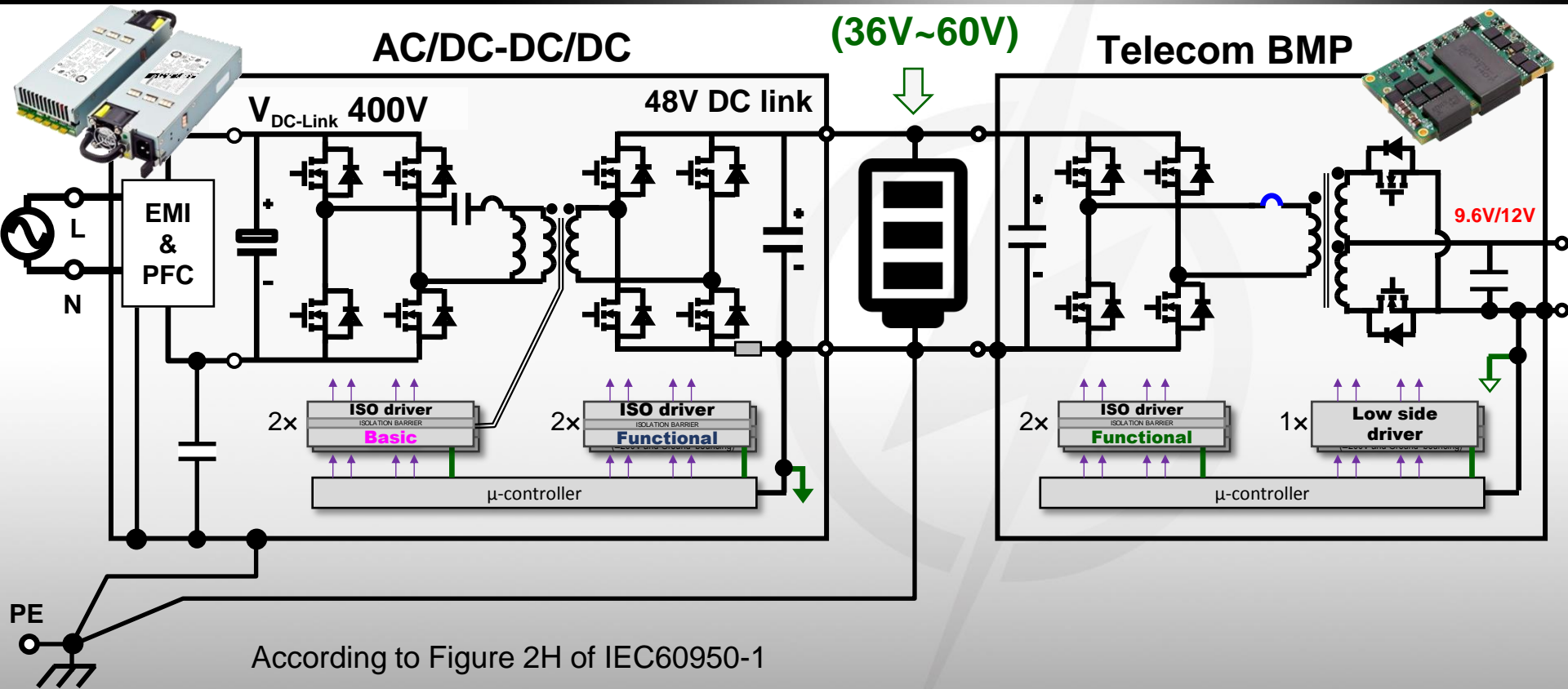
IEC 60950-1 ed. 2.0, Table 5B

Working voltage V, peak or DC	Test voltage for electric strength based on peak working voltage		
	Functional insulation (V_{RMS})	Basic insulation (V_{RMS})	Reinforced insulation (V_{RMS})
≤ 210	1000	1000	1500
≤ 420	1500	1500	3000

Isolation	Definition
<u>Functional</u>	Insulation that is necessary only for the <u>correct functioning</u> of the equipment
<u>Basic</u>	Insulation to provide <u>basic protection against electric shock</u>
Supplementary	Independent insulation applied in addition to BASIC insulation in order to reduce the risk of electric shock in the event of a failure of the BASIC insulation
Double	Insulation comprising both BASIC insulation and SUPPLEMENTARY insulation
<u>Reinforced</u>	<u>Single insulation system</u> that provides a degree of protection against electric shock equivalent to DOUBLE insulation under the conditions specified in this standard

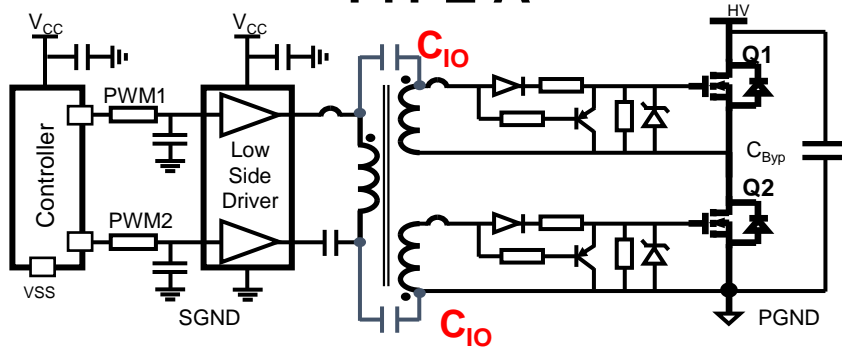


According to Figure 2H of IEC60950-1

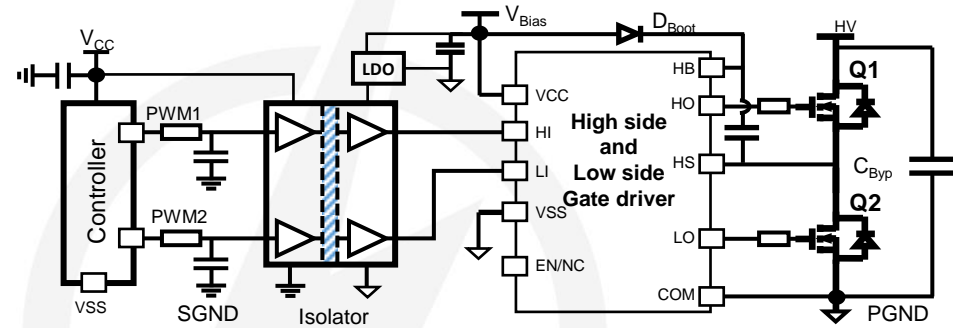


According to Figure 2H of IEC60950-1

TYPE A

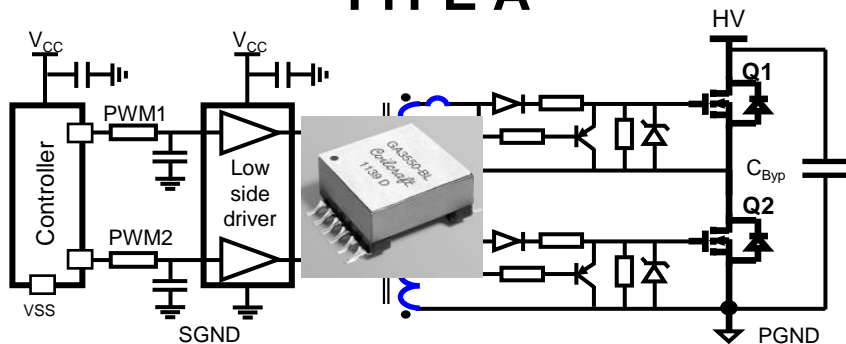


TYPE B

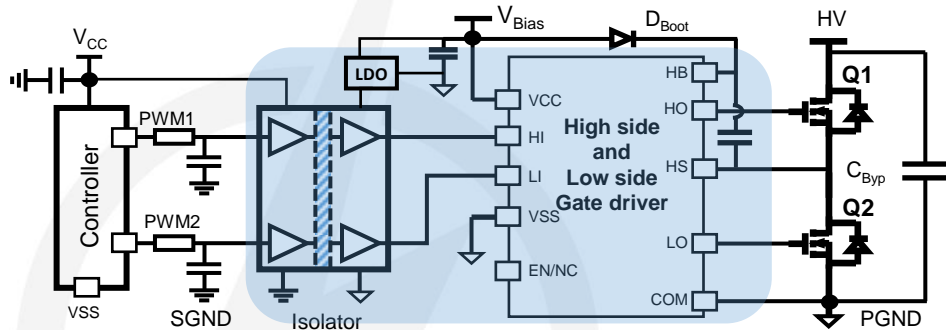


	Type A	Type B
T_{Prop}	≈20ns	≈100ns
Bias power	NO	Yes
C_{IO}	≥10pF	<1pF
Parasitics	Large (L_{LK})	Very small
Overshoot	Large	Small
Size	Bulky	Small

TYPE A



TYPE B



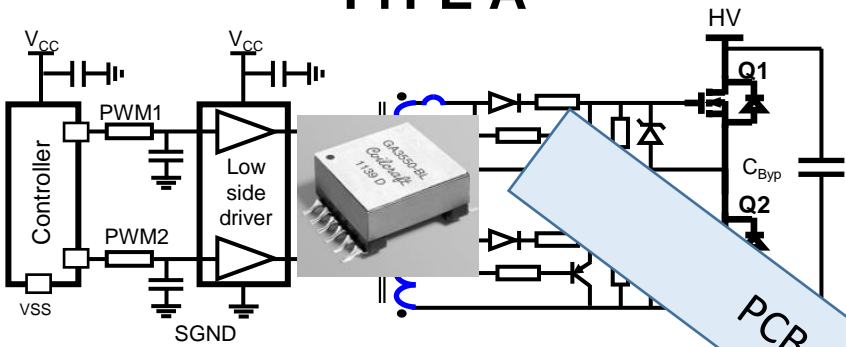
TYPE C: ISO driver

- ❖ CMTI > 100V/ns
- ❖ 5kVrms reinforced isolation
- ❖ T_{Prop} : 19ns typ.
- ❖ Match./ $T_{PWD} < 5ns$
- ❖ **110mm²**

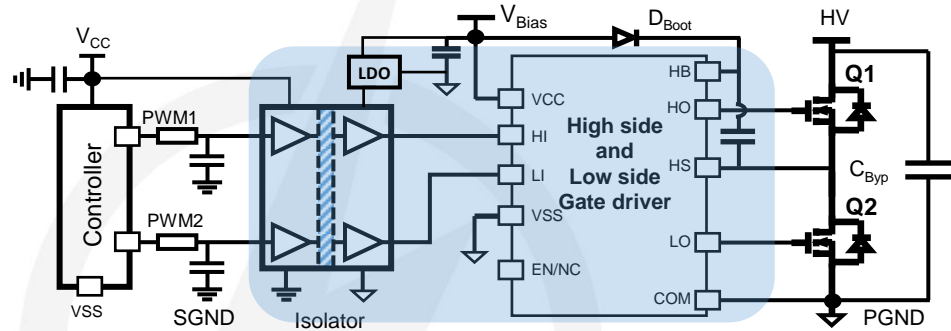
		W (mm)	L (mm)	H (mm)	Area (mm ²)	Vol (mm ³)
Type A	UCC27324	5	6.2	1.75	31	54.25
	GA3550-BL	17.4	24.13	10	420	4200
				SUM	451	4254

Type B	ISO7520C	10.5	10.6	2.65	111.3	295
	UCC27714	8.75	6.2	1.75	54.25	95
	MURS360	8.1	6.1	2.4	49.41	119
				SUM	215	509

TYPE A



TYPE B



PCB area reduction – 76%

TYPE C: ISO driver

- ❖ CMTI > 100V/ns
- ❖ 5kVrms reinforced isolation

τ_{fall}: 19ns typ.

τ_{rise}: < 5ns

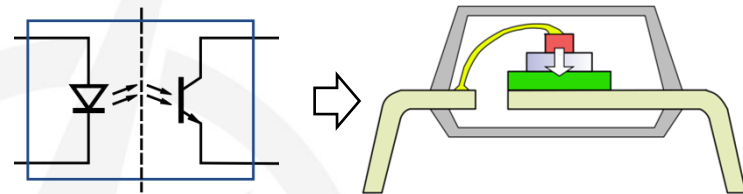
❖ 110%

		W (mm)	L (mm)	H (mm)	Area (mm ²)	
Type A	UCC27324	5	6.2	1.75	31	54
	GA3550-BL	17.4	24.13	10	420	4200
					SUM	451
						4254

Type B	ISO7520C	10.5	10.6	2.65	111.3	295
	UCC27714	8.75	6.2	1.75	54.25	95
	MURS360	8.1	6.1	2.4	49.41	119
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						509

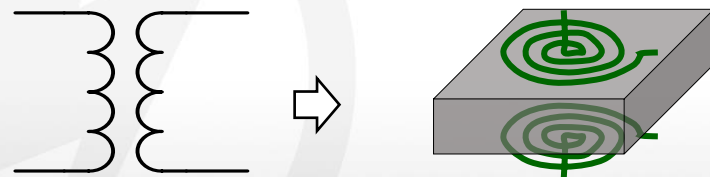
- A) Optocoupler

- Signal transfer between two isolated circuits using light – LED + phototransistor, ~1970s



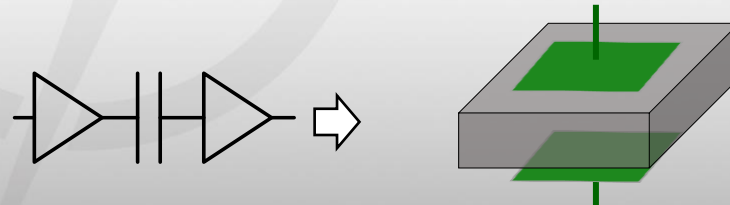
- B) Transformer

- Integrated micro-transformer and electronic circuitry, ~2001

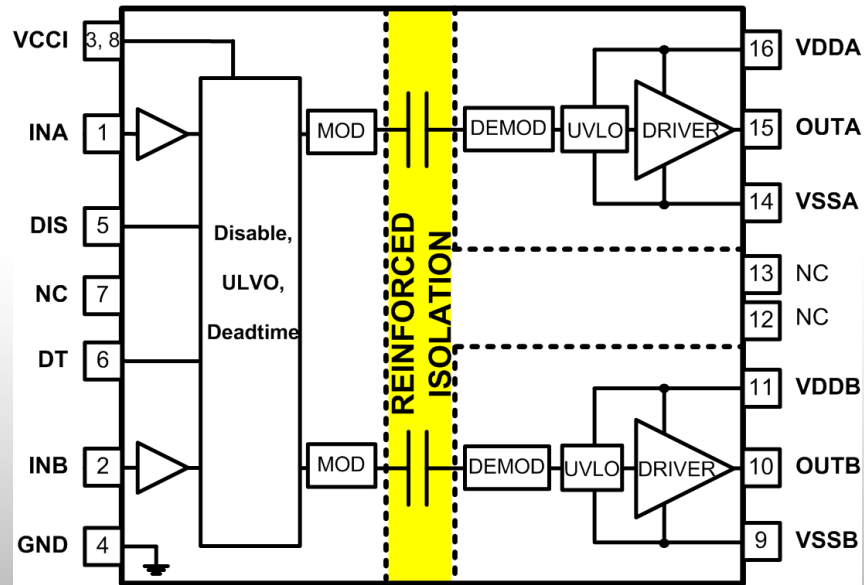


- C) Capacitor

- Signal transmission through capacitive isolation with on-off-keying (OOK) modulation, ~2004



UCC2122x, UCC2x520: 2-ch. Isolated Gate Driver



- 6A/4A sink/source
- 19ns propagation delay
- >100V/ns
- Up to 3~18V wide input range and 6.5~30V wide output voltage range
- Programmable overlap, and interlock/delay time from 0ns~5 μ s
- Output fail safe low with active pull down
- UVLO options: 5V, 8V, 12V
- 3.0kV, 5.7kV basic / reinforced isolation
- Pin-2-pin compatible to industry standard
- UL, VDE, CQC certified

UCC53xx single ch. isolated gate driver

Miller clamp:

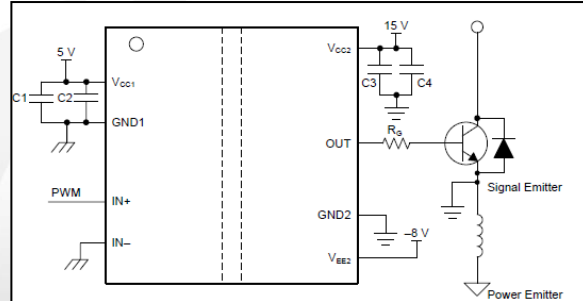
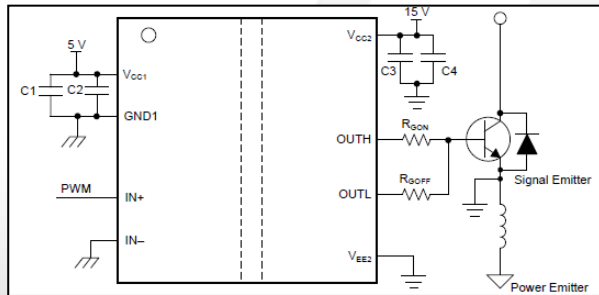
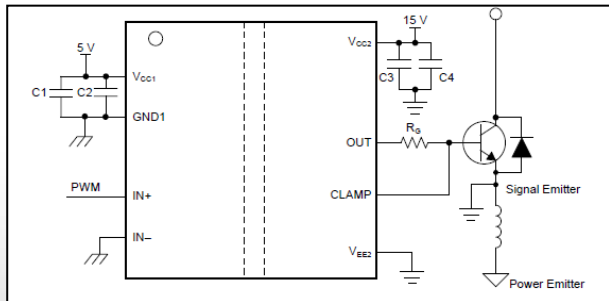
3-kV – UCC5310M and UCC5350M
5-kV – UCC5310M

Split output:

3-kV – UCC5320S, UCC5350SB, UCC5390S
5-kV – UCC5320S

Emitter – UVLO control:

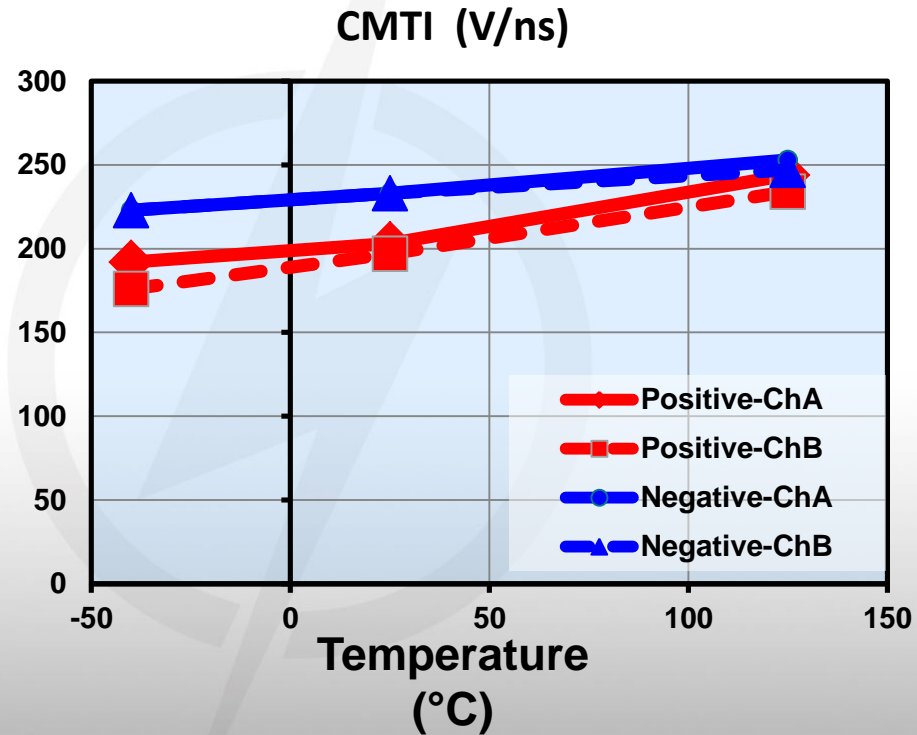
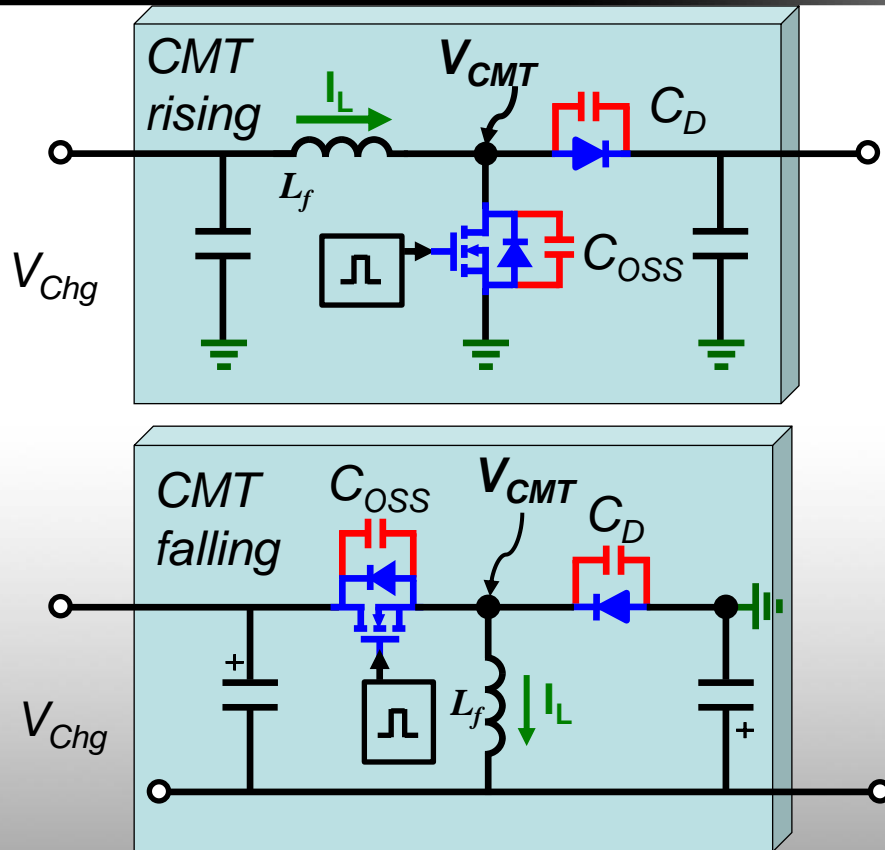
3-kV – UCC5320E and UCC5390E
5-kV – UCC5390E

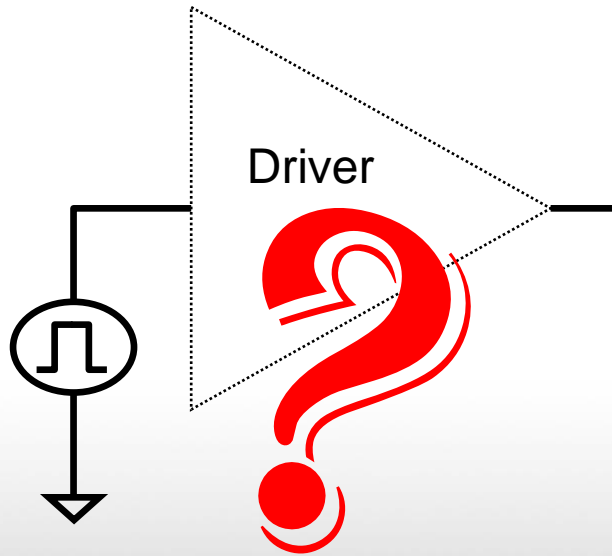


- Features active Miller clamping which prevents false turn-on of the power transistors induced by the Miller current
- Tie clamp pin to gate of FET

- Two outputs OUTH and OUTL can be used to separately control rise and fall times of power transistor
- Rise and fall times are controlled by series resistors: R_{GON} and R_{GOFF}

- UVLO protection by monitoring the voltage between the V_{CC2} and GND2 pins to prevent the power transistors from operating in a saturation region

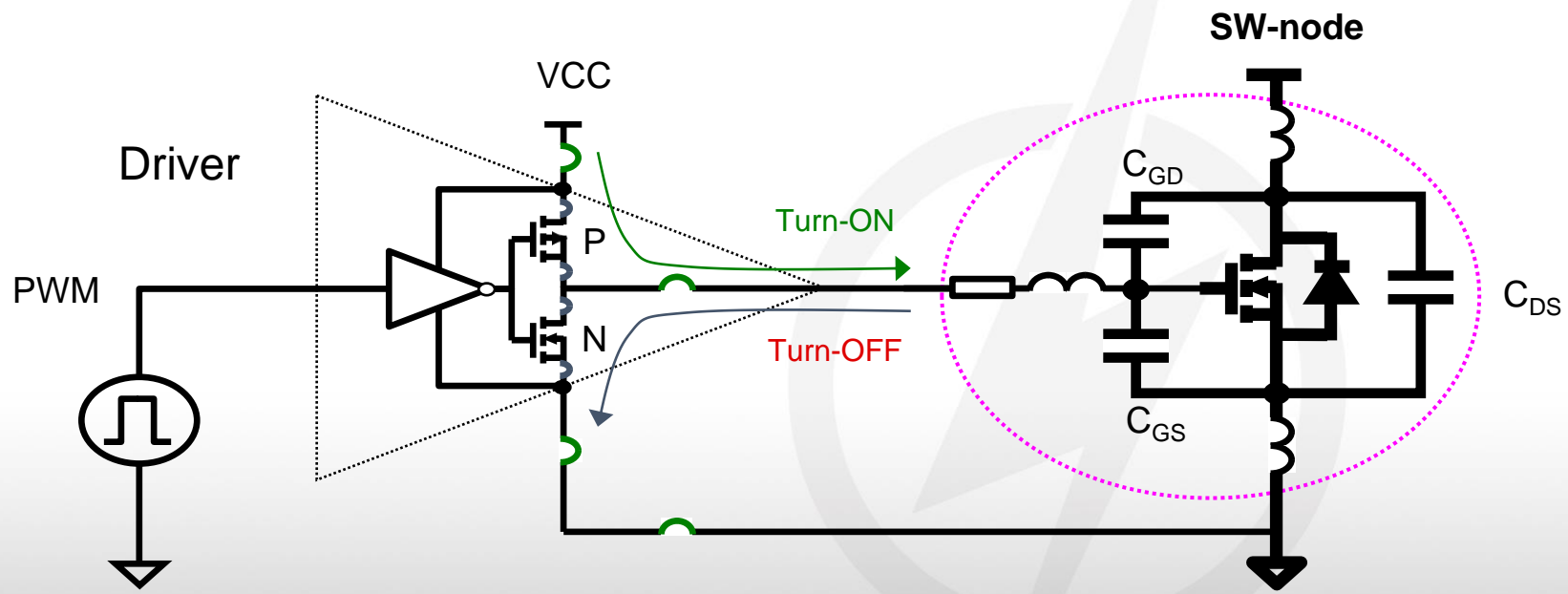




1. Parasitics in gate driver?
2. Gate driver soft/hard switching difference?
3. Strong gate driver and MOSFET nonlinear C_{oss} ?
4. Common mode transient immunity(CMTI), dv/dt and di/dt through parasitics L and C?
5. How to separate power ground noise by PCB layout?
6. Power supply for isolated gate driver in UPS, server and Telecom system
7. TIDA and experimental waveforms

Gate driver deep dive

Very critical role in converter efficiency and reliability

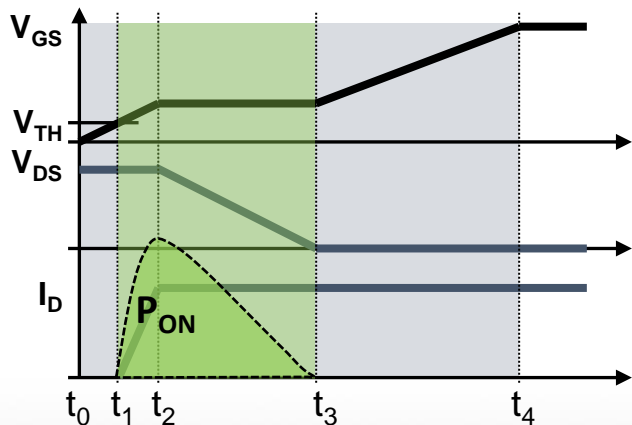


$$C_{ISS} = C_{GS} + C_{GD}$$

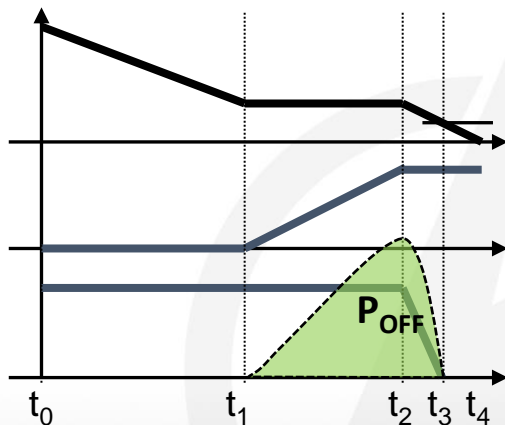
$$C_{RSS} = C_{GD}$$

$$C_{OSS} = C_{GD} + C_{DS}$$

Turn-ON



Turn-OFF

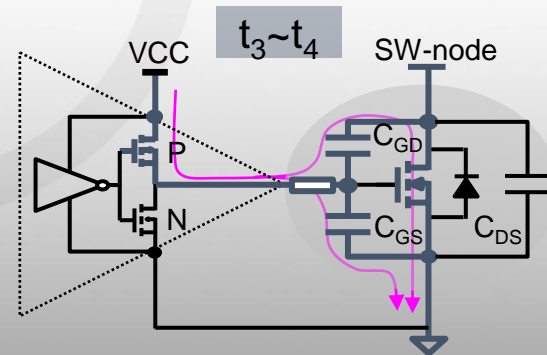
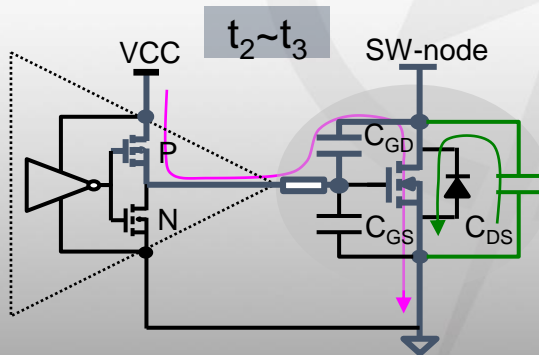
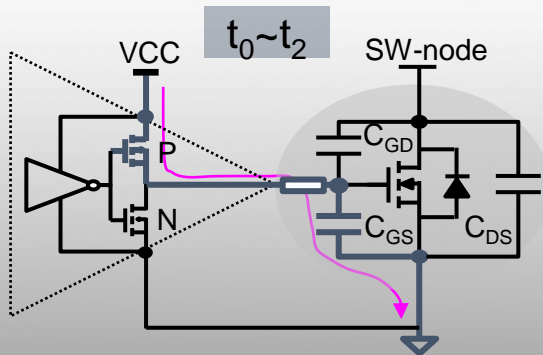


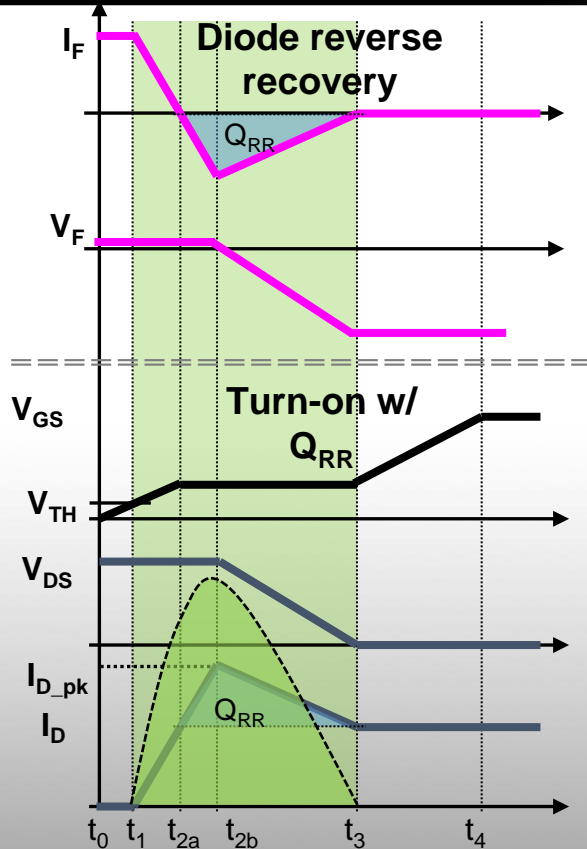
Switching on loss

$$\int_{t_1}^{t_3} V_{DS}(t) \cdot I_D(t) dt + E_{OSS}$$

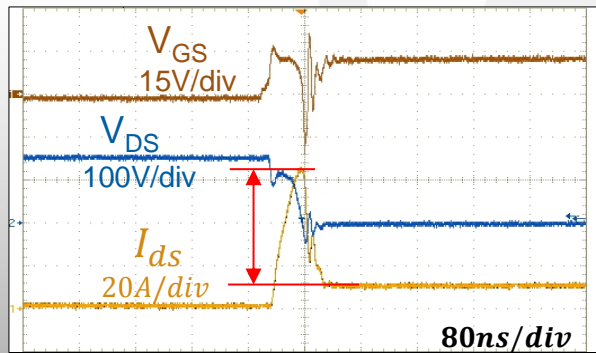
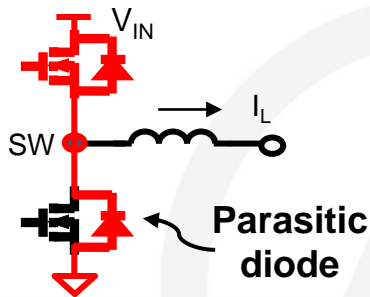
$$t_{1\sim3} \propto \frac{1}{I_{Drv}}$$

Stronger driver \rightarrow lower switching loss

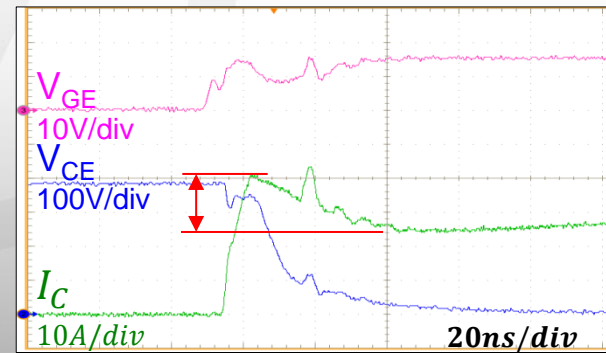
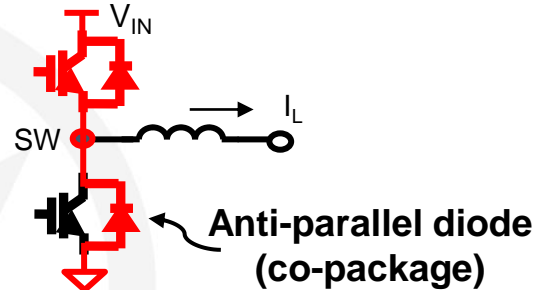


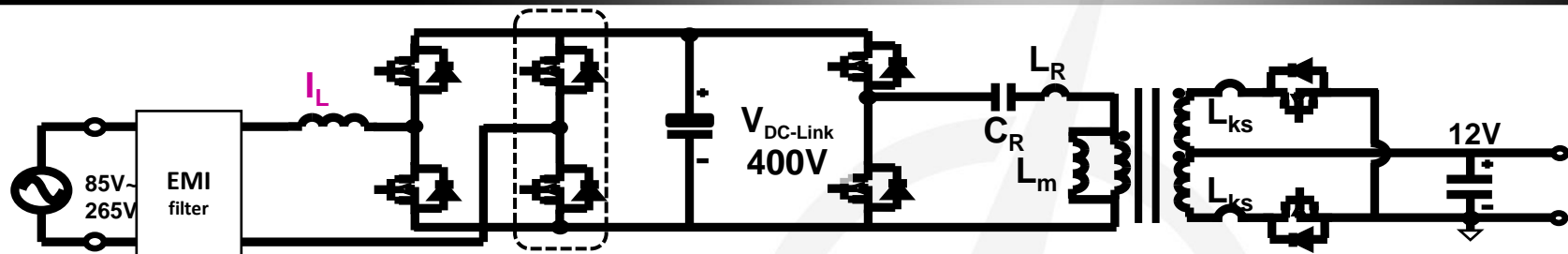


SJ-MOSFET

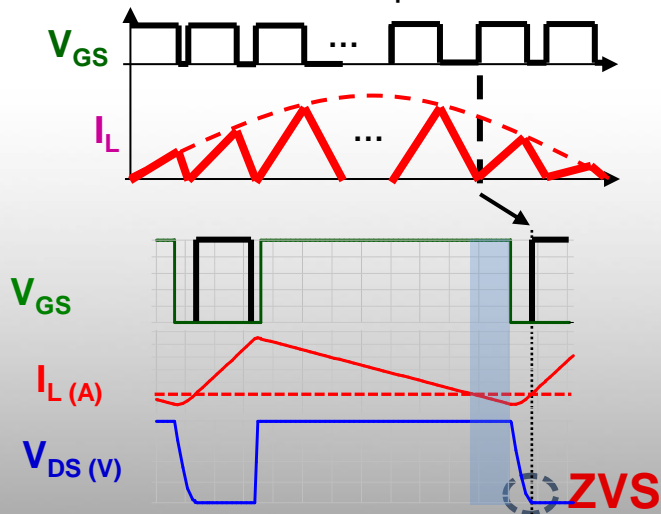


IGBT

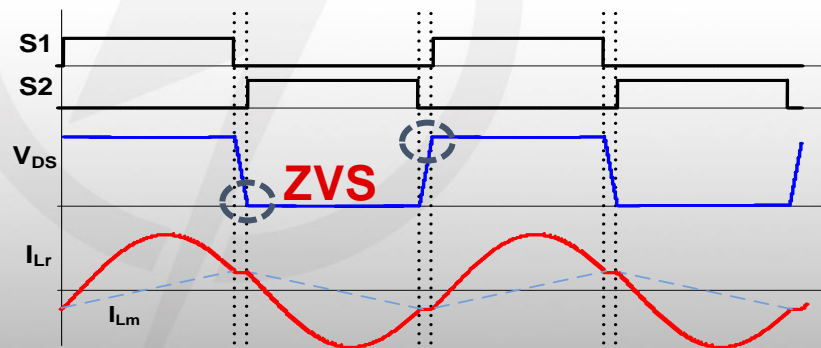


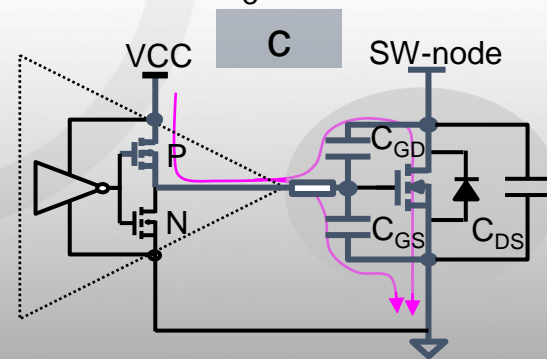
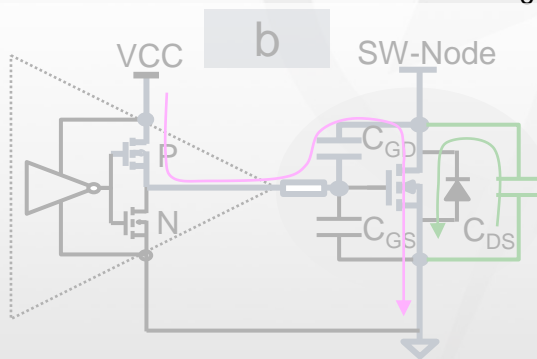
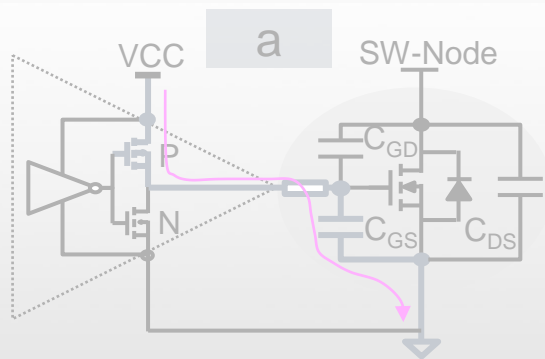
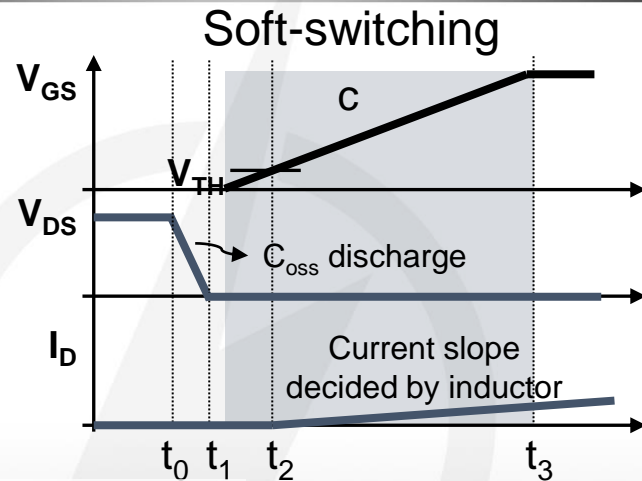
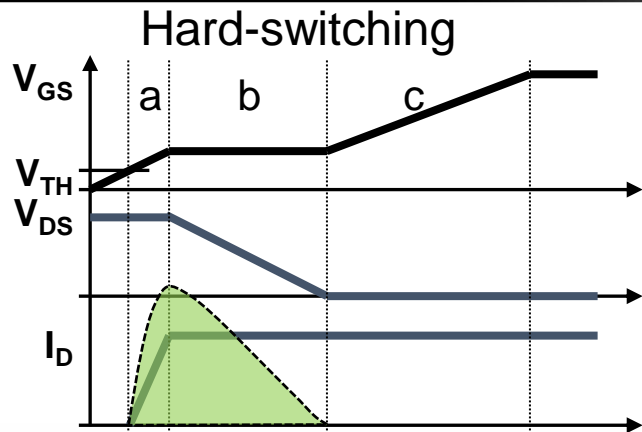


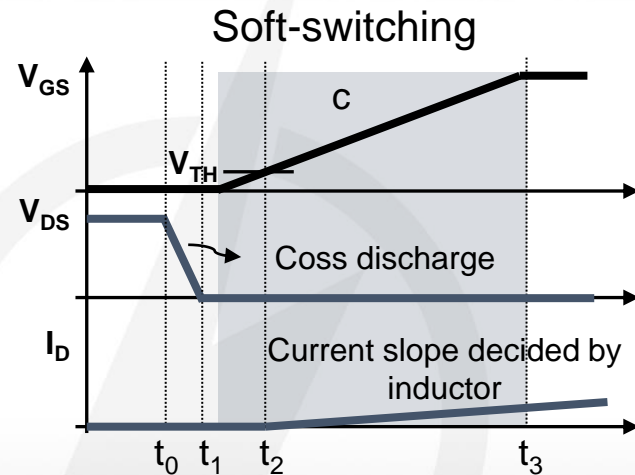
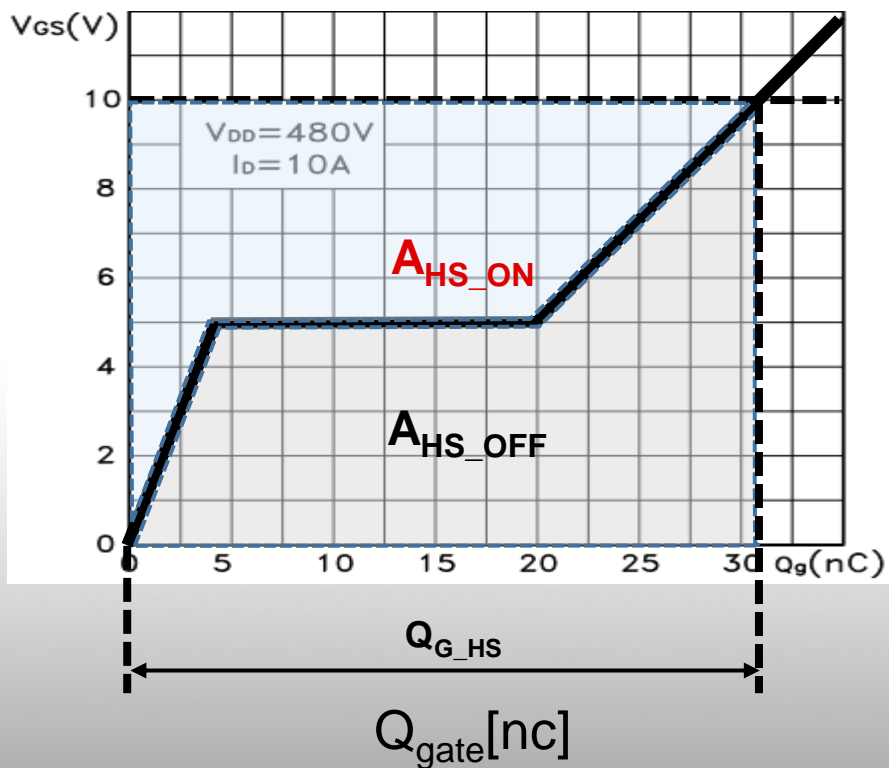
CRM totem pole PFC



LLC converter + center-tap rectifier

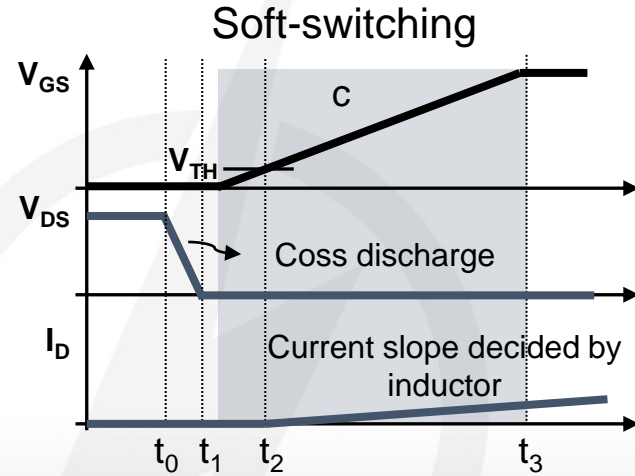
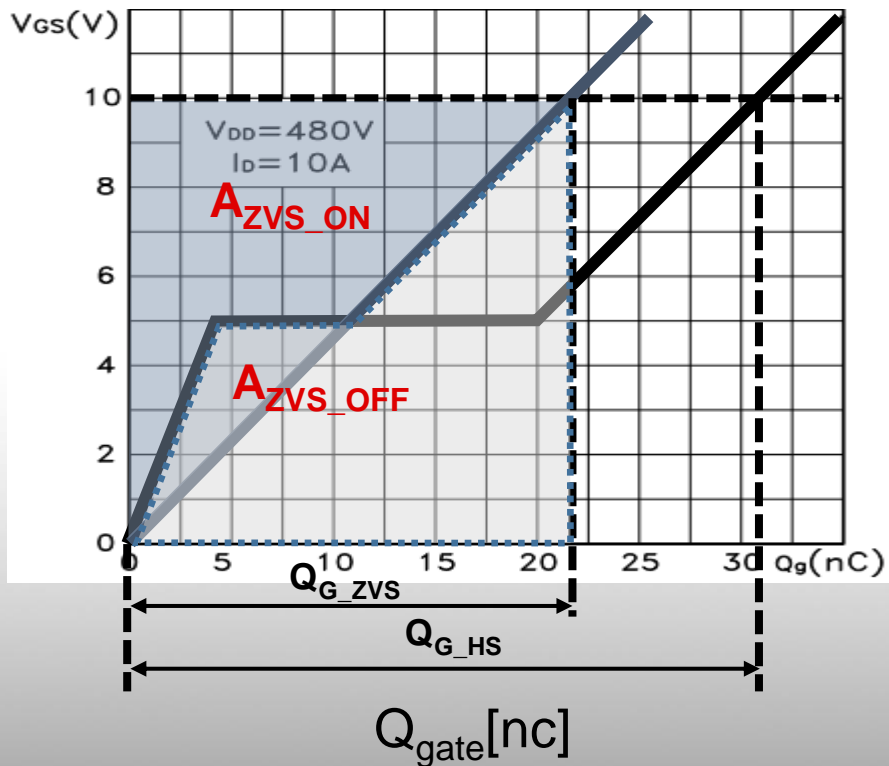






$$E_{G_HS} = A_{HS_ON} + A_{HS_OFF} = V_{GS} \cdot Q_{G_HS}$$

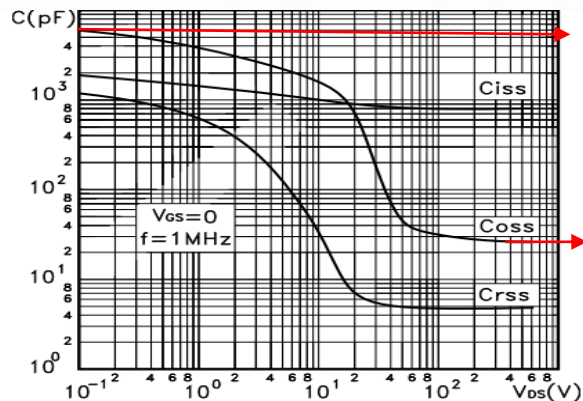
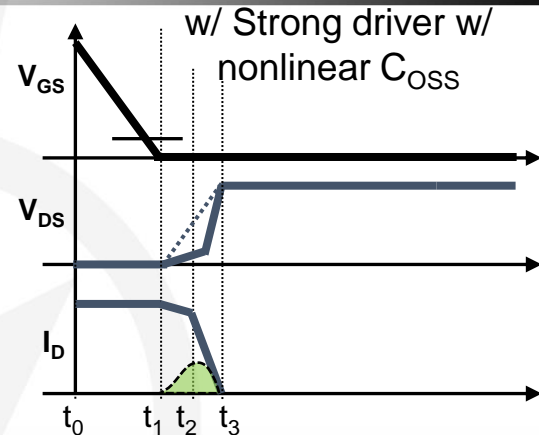
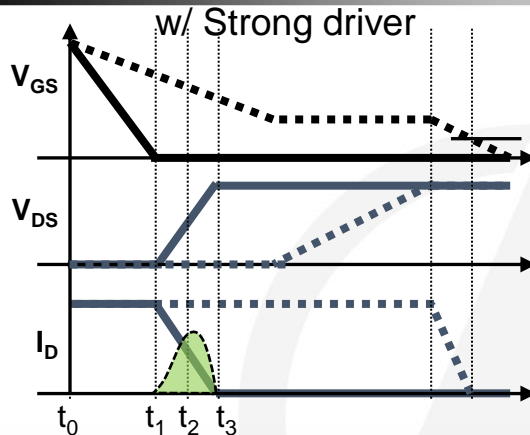
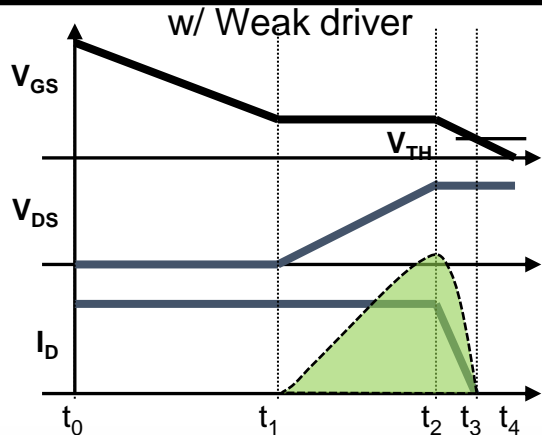
$$P_{GateDrv} = E_G \cdot f_{SW}$$



$$E_{G_HS} = A_{HS_ON} + A_{HS_OFF} = V_{GS} \cdot Q_{G_HS}$$

$$E_{G_ZVS} = A_{ZVS_ON} + A_{ZVS_OFF} \approx V_{GS} \cdot Q_{G_ZVS}$$

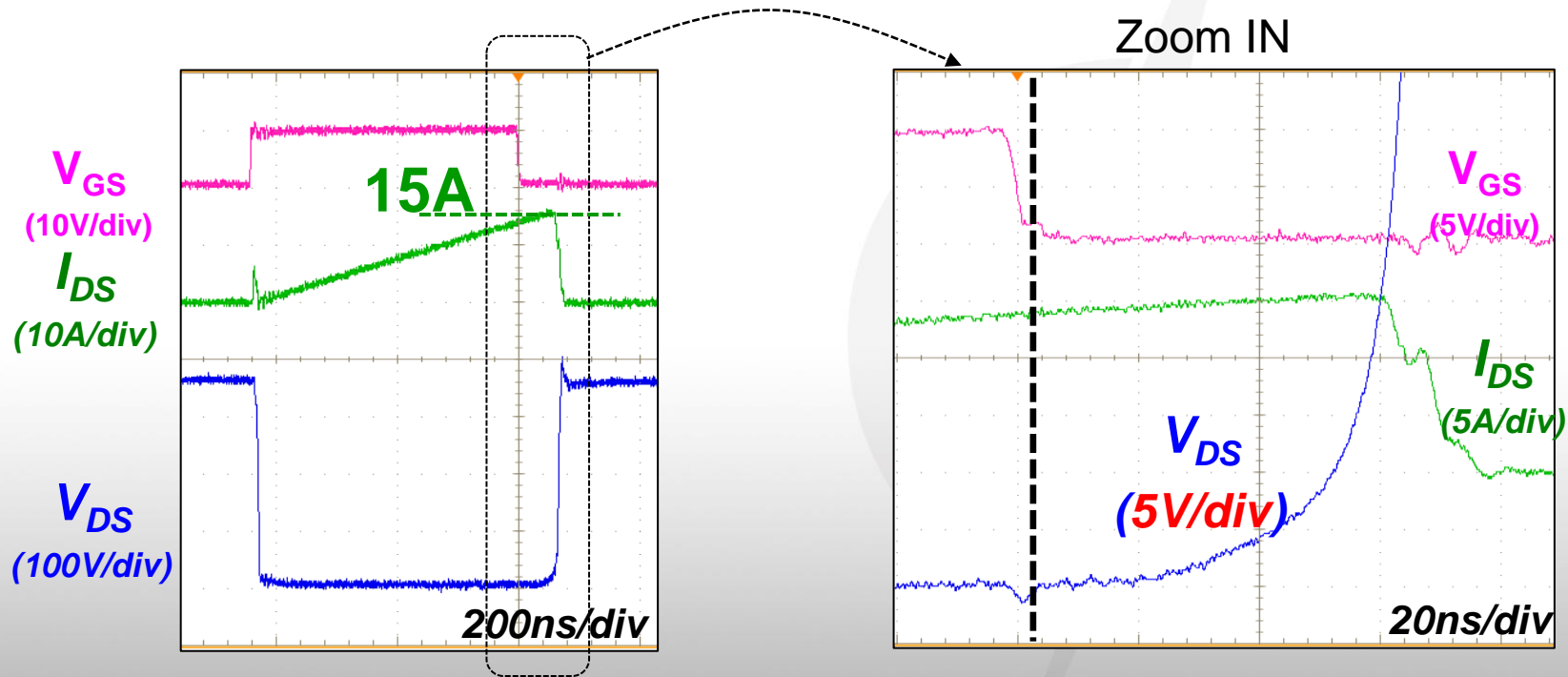
$$P_{GateDrv} = E_G \cdot f_{sw}$$

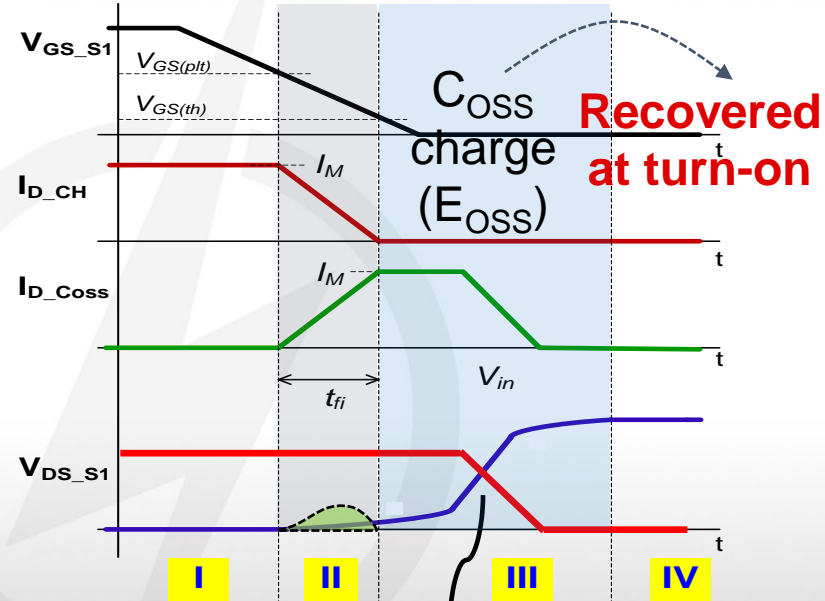
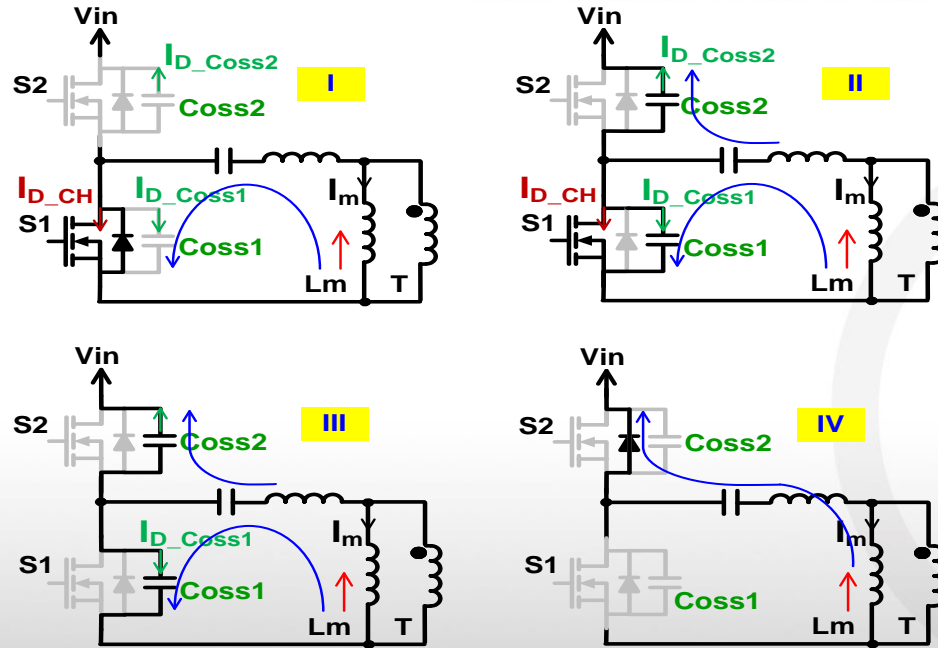


$C_{OSS}(0V)$
 $=6nF$

$C_{OSS}(400V)$
 $<30pF$

- Switching behavior is not controlled by gate current, but by C_{OSS} and load current
- Large C_{OSS} at low voltage performs as natural snubber
- Small C_{OSS} at high voltage shortens V-I overlap
- Fast dv/dt and di/dt , other bad things

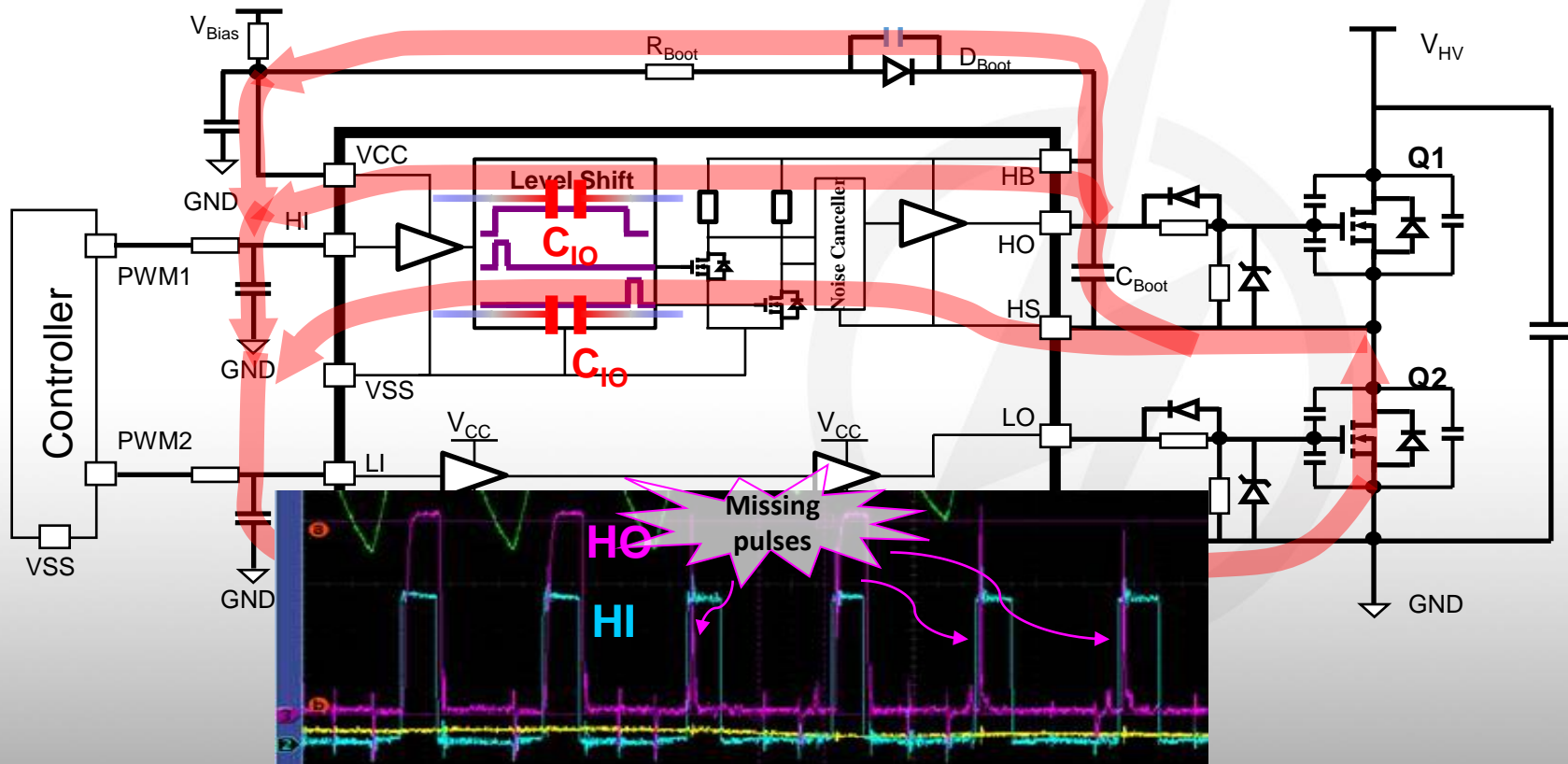


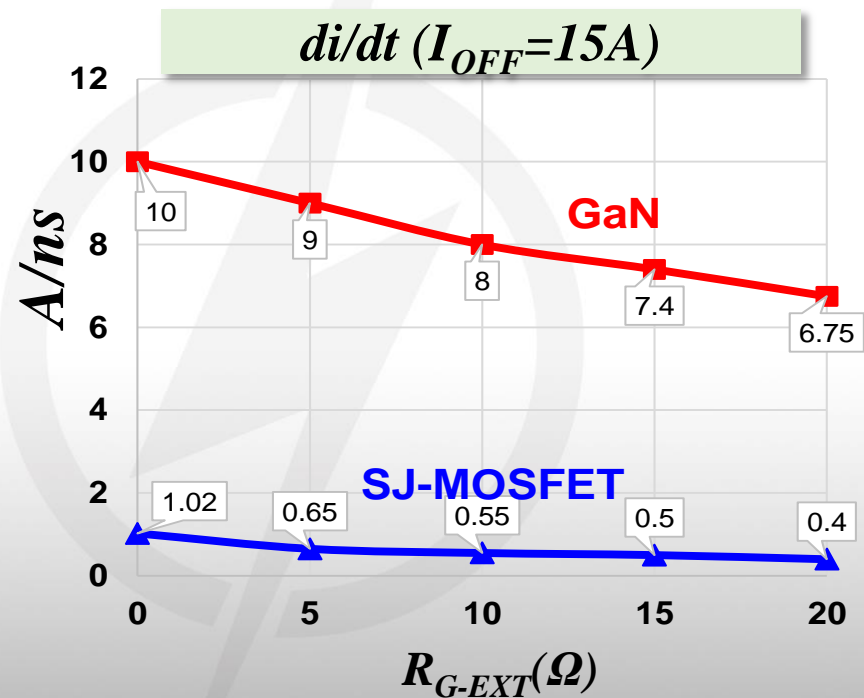
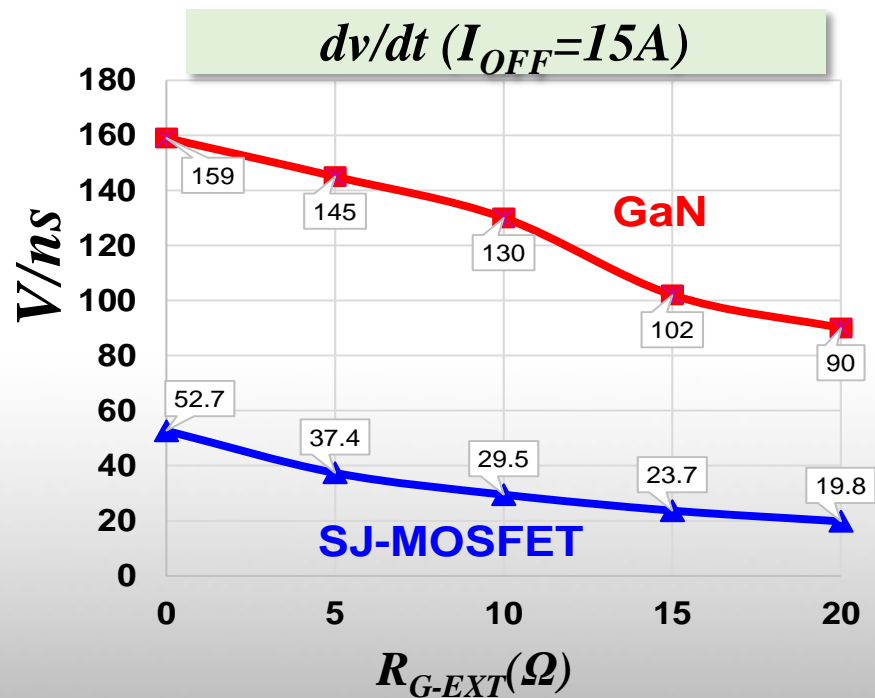


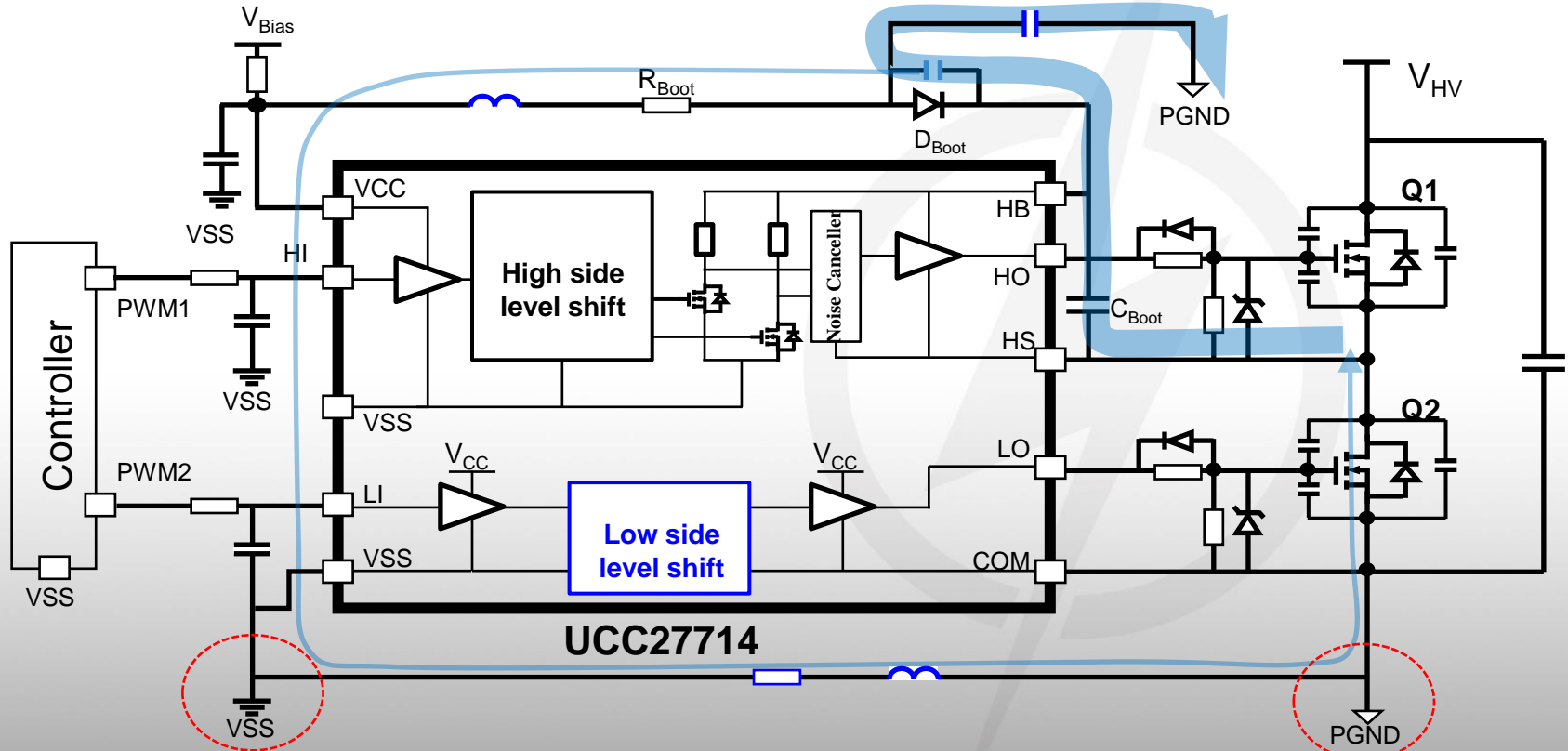
In period II, $V_{DS_S1} \ll V_{DS_S2}$; $C_{oss1} \gg C_{oss2}$

$$I_{D_Coss} = I_{D_Coss1} + I_{D_Coss2} \approx I_{D_Coss1}$$

**High
dv/dt, di/dt**







- [1] Laszlo Balogh, “Design And Application Guide For High Speed MOSFET Gate Drive Circuits”
- [2] Bob Mammano, et al., “Safety Considerations in Power Supply Design”
- [3] Ernest H. Wittenbreder, Jr., “From Control to Gate”
- [4] Fanny Bjoerk, et al., “How to make most beneficial use of the latest generation of super junction technology devices”
- [5] “An introduction to LLC resonant half-bridge converter”, AN2644, ST
- [6] Bo Yang, et al., “LLC Resonant Converter for Front End DC/DC Conversion”
- [7] Zhengyang Liu, et al., “Design and Evaluation of GaN-Based Dual-Phase Interleaved MHz Critical Mode PFC Converter”, IEEE, 2014
- [8] Wei Zhang, et al., “Gate drive design considerations for high voltage cascade GaN HEMT”, IEEE, 2014

THANK YOU