

# TPS56x210, 4.5-V to 17-V Input, 2-A, 3-A Synchronous Step-Down Voltage Regulator In 8-Pin SOT-23

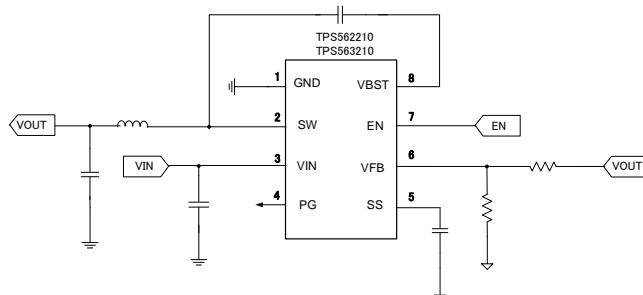
## 1 Features

- TPS562210: 2-A Converter With Integrated 133-mΩ and 80-mΩ FETs
- TPS563210: 3-A Converter With Integrated 68-mΩ and 39-mΩ FETs
- D-CAP2™ Mode Control for Fast Transient Response
- Advanced Eco-mode™ Pulse-skip
- Input Voltage Range: 4.5 V to 17 V
- Output Voltage Range: 0.76 V to 7 V
- 650-kHz Switching Frequency
- Low Shutdown Current Less than 10 µA
- 1% Feedback Voltage Accuracy (25°C)
- Startup from Pre-Biased Output Voltage
- Cycle By Cycle Over-current Limit
- Hiccup-mode Under Voltage Protection
- Non-latch OVP, UVLO and TSD Protections
- Adjustable Soft Start
- Power Good Output

## 2 Applications

- Digital TV Power Supply
- High Definition Blu-ray Disc™ Players
- Networking Home Terminal
- Digital Set Top Box (STB)

## 4 Simplified Schematic



## 3 Description

The TPS562210 and TPS563210 are simple, easy-to-use, 2 A, 3 A synchronous step-down converters in 8 pin SOT-23 package.

The devices are optimized to operate with minimum external component counts and also optimized to achieve low standby current.

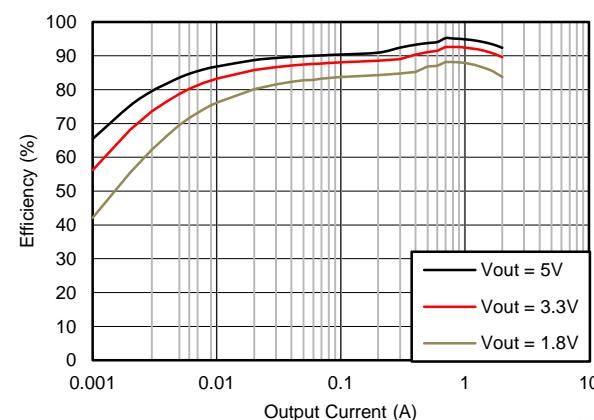
These switch mode power supply (SMPS) devices employ D-CAP2™ mode control providing a fast transient response and supporting both low equivalent series resistance (ESR) output capacitors such as specialty polymer and ultra-low ESR ceramic capacitors with no external compensation components.

The devices operate in Advanced Eco-mode™, which maintains high efficiency during light load operation. The TPS562210 and TPS563210 are available in a 8-pin 1.6 × 2.9 (mm) SOT (DDF) package, and specified from –40°C to 85°C of ambient temperature.

### Device Information<sup>(1)</sup>

ORDER NUMBER	PACKAGE	BODY SIZE (NOM)
TPS562210DDFT	DDF(8)	1.60 mm × 2.90 mm
TPS562210DDFR		
TPS563210DDFT		
TPS563210DDFR		

(1) For all available packages, see the orderable addendum at the end of the datasheet.



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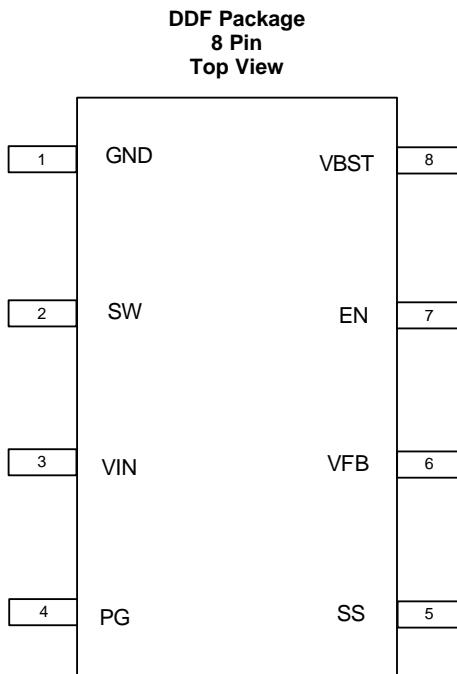
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## 5 Revision History

### Changes from Original (February 2015) to Revision A

		Page
•	Changed the <i>Thermal Information</i> values for TPS563210.	4
•	Changed the $V_{FBTH}$ values in the <i>Electrical Characteristics</i> From: MIN = 757, MAX = 773 To: MIN = 758, MAX = 772	5
•	Changed $I_{VFB}$ spec UNIT from "mA" to "μA".	5
•	Changed $T_{HiccupOn}$ in the <i>Electrical Characteristics</i> From TYP = 1 ms To: TYP = 1 cycle	5
•	Changed $T_{HiccupOff}$ in the <i>Electrical Characteristics</i> From TYP = 1.7 ms To: TYP = 7 cycles	5
•	Changed $V_{out} = 5V$ to $V_{out} = 1.8V$ in <i>Figure 6</i>	7
•	Changed column heading $C8 + C9$ (μF) To: $C6 + C7 + C8$ (μF) in <i>Table 2</i>	15
•	Changed column heading $C8 + C9$ (μF) To: $C6 + C7 + C8$ (μF) in <i>Table 4</i>	19

## 6 Pin Configuration and Functions



### Pin Functions

PIN		DESCRIPTION
NAME	NO.	
GND	1	Ground pin Source terminal of low-side power NFET as well as the ground terminal for controller circuit. Connect sensitive VFB to this GND at a single point.
SW	2	Switch node connection between high-side NFET and low-side NFET.
VIN	3	Input voltage supply pin. The drain terminal of high-side power NFET.
PG	4	Power good open drain output
SS	5	Soft-start control. An external capacitor should be connected to GND.
VFB	6	Converter feedback input. Connect to output voltage with feedback resistor divider.
EN	7	Enable input control. Active high and must be pulled up to enable the device.
VBST	8	Supply input for the high-side NFET gate drive circuit. Connect 0.1 $\mu$ F capacitor between VBST and SW pins.

## 7 Specifications

### 7.1 Absolute Maximum Ratings

$T_J = -40^{\circ}\text{C}$  to  $150^{\circ}\text{C}$  (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
Input voltage range	VIN, EN	-0.3	19	V
	VBST	-0.3	25	V
	VBST (10 ns transient)	-0.3	27.5	V
	VBST (vs SW)	-0.3	6.5	V
	VFB, PG	-0.3	6.5	V
	SS	-0.3	5.5	V
	SW	-2	19	V
	SW (10 ns transient)	-3.5	21	V
Operating junction temperature, $T_J$		-40	150	$^{\circ}\text{C}$
Storage temperature, $T_{\text{stg}}$		-55	150	$^{\circ}\text{C}$

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 7.2 ESD Ratings

			VALUE	UNIT
$V_{(\text{ESD})}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	$\pm 2000$	V
		Charged device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	$\pm 500$	V

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 7.3 Recommended Operating Conditions

$T_J = -40^{\circ}\text{C}$  to  $150^{\circ}\text{C}$  (unless otherwise noted)

		MIN	MAX	UNIT
$V_{\text{IN}}$	Supply input voltage range	4.5	17	V
$V_I$	VBST	-0.1	23	V
	VBST (10 ns transient)	-0.1	26	V
	VBST(vs SW)	-0.1	6	V
	EN	-0.1	17	V
	VFB, pg	-0.1	5.5	V
	SS	-0.1	5	V
	SW	-1.8	17	V
	SW (10 ns transient)	-3.5	20	V
$T_A$	Operating free-air temperature	-40	85	$^{\circ}\text{C}$

### 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>	TPS562210	TPS563210	UNIT
	DDF (8 PINS)		
$R_{\theta JA}$	Junction-to-ambient thermal resistance	106.1	$^{\circ}\text{C/W}$
$R_{\theta JC(\text{top})}$	Junction-to-case (top) thermal resistance	49.1	$^{\circ}\text{C/W}$
$R_{\theta JB}$	Junction-to-board thermal resistance	10.9	$^{\circ}\text{C/W}$
$\Psi_{JT}$	Junction-to-top characterization parameter	8.6	$^{\circ}\text{C/W}$
$\Psi_{JB}$	Junction-to-board characterization parameter	10.8	$^{\circ}\text{C/W}$

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).

## 7.5 Electrical Characteristics

over operating free-air temperature range,  $V_{IN} = 12\text{ V}$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>SUPPLY CURRENT</b>						
$I_{VIN}$	Operating – non-switching supply current	$V_{IN}$ current, $T_A = 25^\circ\text{C}$ , $EN = 5\text{V}$ , $V_{FB} = 0.8\text{ V}$	190	290		$\mu\text{A}$
$I_{VINSND}$	Shutdown supply current	$V_{IN}$ current, $T_A = 25^\circ\text{C}$ , $EN = 0\text{ V}$	3.0	10		$\mu\text{A}$
<b>LOGIC THRESHOLD</b>						
$V_{ENH}$	EN high-level input voltage	EN	1.6			V
$V_{ENL}$	EN low-level input voltage	EN		0.6		V
$R_{EN}$	EN pin resistance to GND	$V_{EN} = 12\text{ V}$	225	450	900	$\text{k}\Omega$
<b><math>V_{FB}</math> VOLTAGE AND DISCHARGE RESISTANCE</b>						
$V_{FBTH}$	$V_{FB}$ threshold voltage TPS562210	$T_A = 25^\circ\text{C}$ , $V_O = 1.05\text{ V}$ , $I_O = 10\text{ mA}$ , Eco-mode™ operation	772			mV
	$V_{FB}$ threshold voltage TPS562210 and TPS563210	$T_A = 25^\circ\text{C}$ , $V_O = 1.05\text{ V}$	758	765	772	mV
		$T_A = 0^\circ\text{C}$ to $85^\circ\text{C}$ , $V_O = 1.05\text{ V}^{(1)}$	753		777	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ , $V_O = 1.05\text{ V}^{(1)}$	751		779	
$I_{VFB}$	$V_{FB}$ input current	$V_{FB} = 0.8\text{ V}$ , $T_A = 25^\circ\text{C}$	0	$\pm 0.1$		$\mu\text{A}$
<b>MOSFET</b>						
$R_{DS(on)h}$	High side switch resistance	$T_A = 25^\circ\text{C}$ , $V_{BST} - SW = 5.5\text{ V}$ , TPS562210	133			$\text{m}\Omega$
		$T_A = 25^\circ\text{C}$ , $V_{BST} - SW = 5.5\text{ V}$ , TPS563210	68			
$R_{DS(on)l}$	Low side switch resistance	$T_A = 25^\circ\text{C}$ , TPS562210	80			$\text{m}\Omega$
		$T_A = 25^\circ\text{C}$ , TPS563210	39			
<b>CURRENT LIMIT</b>						
$I_{ocl}$	Current limit <sup>(1)</sup>	DC current, $V_{OUT} = 1.05\text{V}$ , $L_1 = 2.2\text{ }\mu\text{H}$ , TPS562210	2.5	3.2	4.3	A
		DC current, $V_{OUT} = 1.05\text{V}$ , $L_1 = 1.5\text{ }\mu\text{H}$ , TPS563210	3.5	4.2	5.3	
<b>THERMAL SHUTDOWN</b>						
$T_{SDN}$	Thermal shutdown threshold <sup>(1)</sup>	Shutdown temperature	155			°C
		Hysteresis	35			
<b>SOFT START</b>						
$I_{ss}$	SS charge current	$V_{ss} = 0.5\text{ V}$	4.2	6	7.8	$\mu\text{s}$
	SS discharge current	$V_{ss} = 0.5\text{ V}$ , $EN = L$	0.75	1.3		$\text{mA}$
<b>POWER GOOD</b>						
$V_{THPG}$	PG threshold	VFB rising (Good)	85%	90%	95%	
		VFB falling (Fault)		85%		
IPG	PG sink current	PG = 0.5 V	0.5	1		$\text{mA}$
<b>OUTPUT UNDERVOLTAGE AND OVERVOLTAGE PROTECTION</b>						
$V_{OVP}$	Output OVP threshold	OVP Detect	$125\% \times V_{fbth}$			
$V_{UVP}$	Output UVP threshold	Hiccup detect	$65\% \times V_{fbth}$			
$T_{HiccupOn}$	Hiccup Power On Time	Relative to soft start time	1			cycle
$T_{HiccupOff}$	Hiccup Power Off Time	Relative to soft start time	7			cycles
<b>UVLO</b>						
UVLO	UVLO threshold	Wake up VIN voltage	3.45	3.75	4.05	V
		Hysteresis VIN voltage	0.13	0.32	0.55	

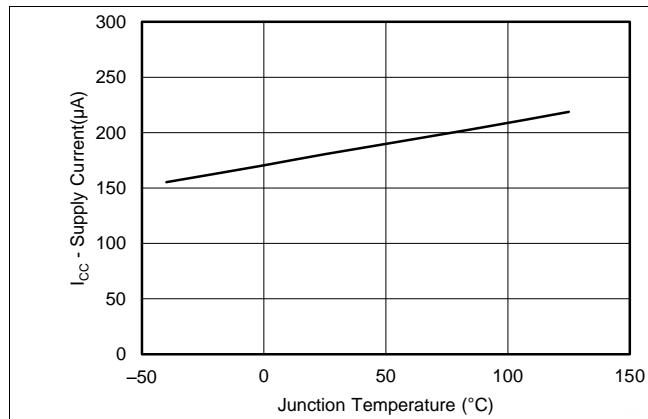
(1) Not production tested.

## 7.6 Timing Requirements

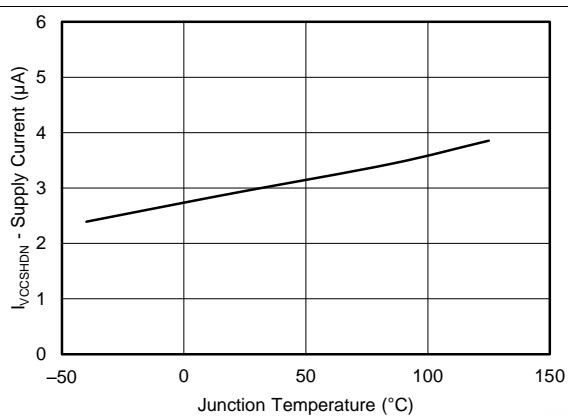
			MIN	TYP	MAX	UNIT
<b>ON-TIME TIMER CONTROL</b>						
$t_{ON}$	On time	$V_{IN} = 12 \text{ V}$ , $V_O = 1.05 \text{ V}$		150		ns
$t_{OFF(MIN)}$	Minimum off time	$T_A = 25^\circ\text{C}$ , $V_{FB} = 0.5 \text{ V}$		260	310	ns

## 7.7 Typical Characteristics: TPS562210

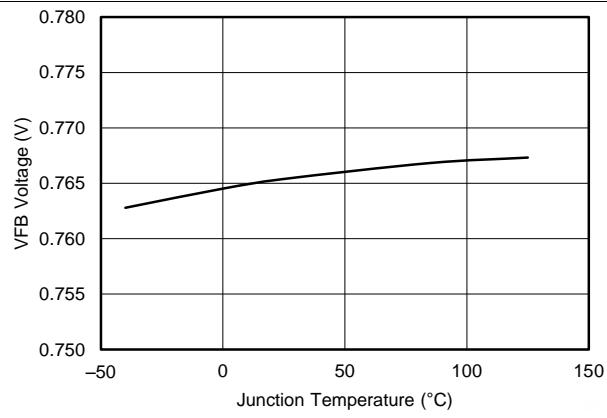
$V_{IN} = 12\text{ V}$  (unless otherwise noted)



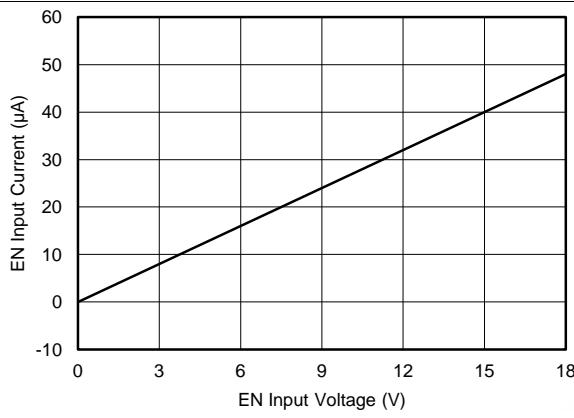
**Figure 1. Supply Current vs Junction Temperature**



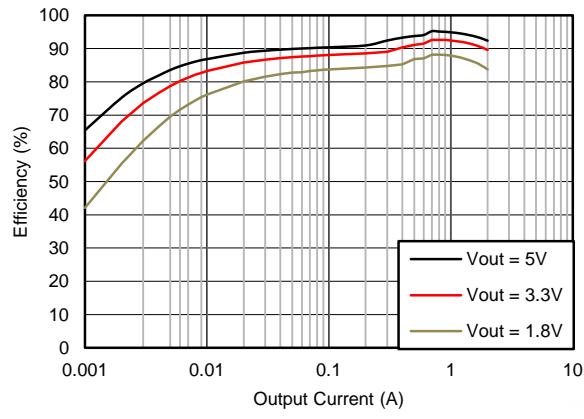
**Figure 2. VIN Shutdown Current vs Junction Temperature**



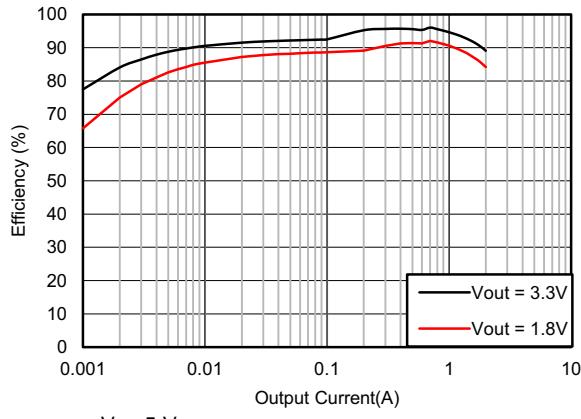
**Figure 3. VFB Voltage vs Junction Temperature**



**Figure 4. EN Current vs EN Voltage**



**Figure 5. Efficiency vs Output Current**



**Figure 6. Efficiency vs Output Current**

### Typical Characteristics: TPS562210 (continued)

$V_{IN} = 12\text{ V}$  (unless otherwise noted)

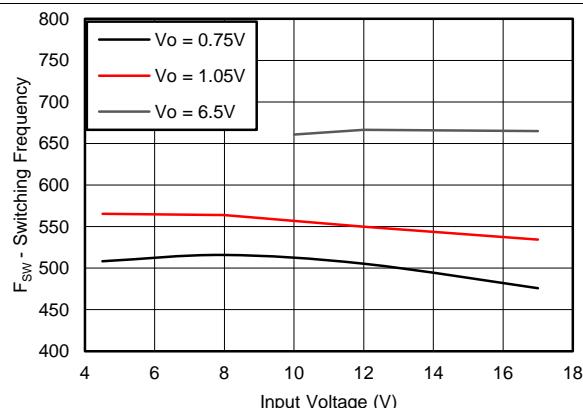


Figure 7. Switching Frequency vs Input Voltage

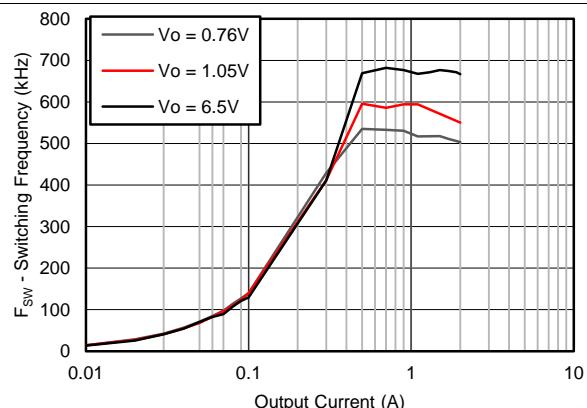
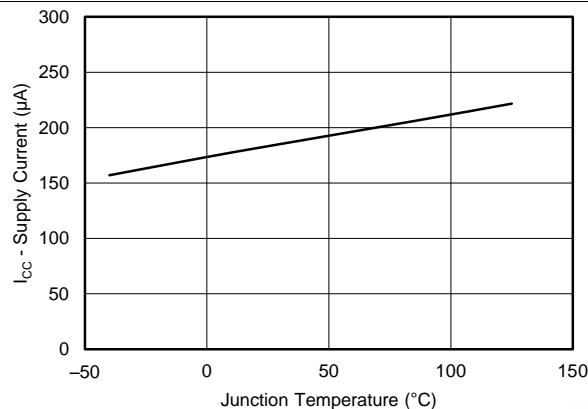


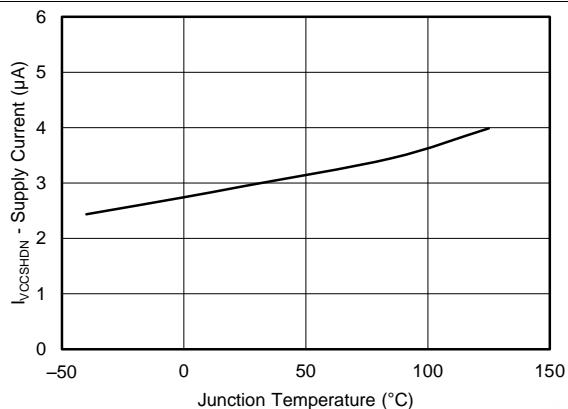
Figure 8. Switching Frequency vs Output Current

## 7.8 Typical Characteristics: TPS563210

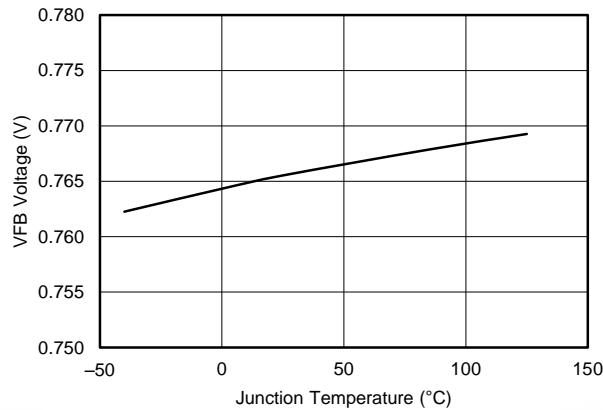
$V_{IN} = 12V$  (unless otherwise noted)



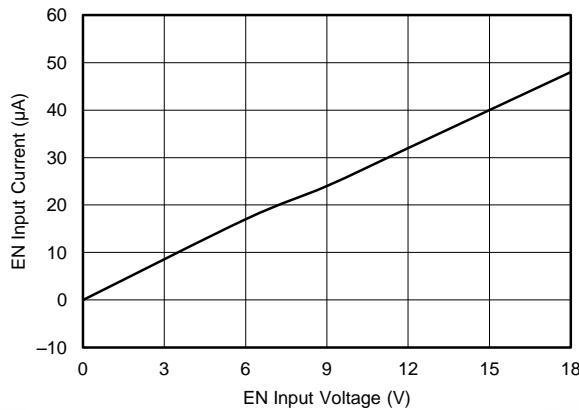
**Figure 9. Supply Current vs Junction Temperature**



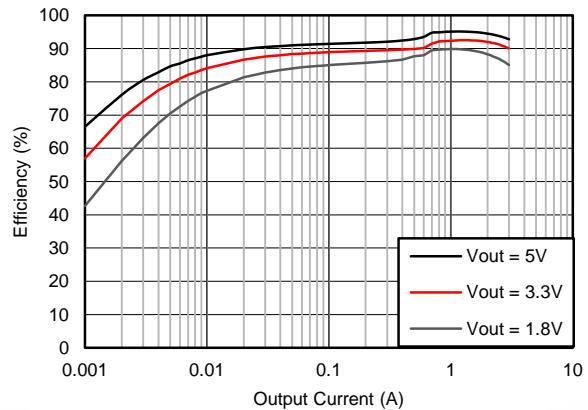
**Figure 10. VIN Shutdown Current vs Junction Temperature**



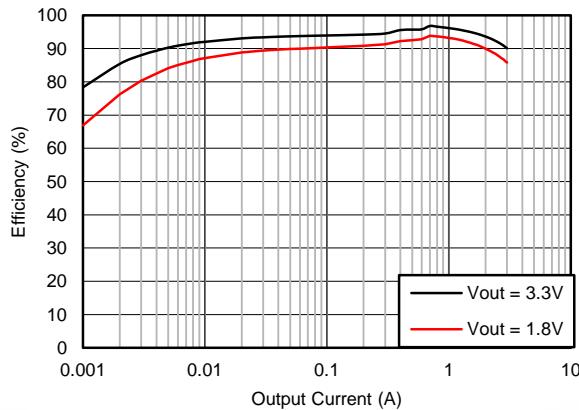
**Figure 11. VFB Voltage vs Junction Temperature**



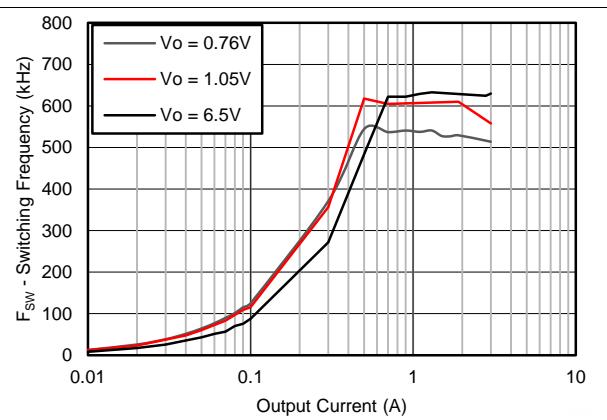
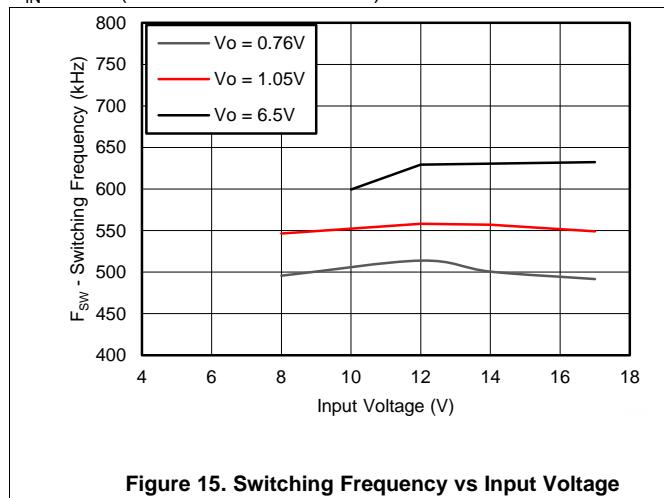
**Figure 12. EN Current vs EN Voltage**



**Figure 13. Efficiency vs Output Current**



**Figure 14. Efficiency vs Output Current**

**Typical Characteristics: TPS563210 (continued)**
 $V_{IN} = 12V$  (unless otherwise noted)


## 8 Detailed Description

### 8.1 Overview

The TPS562210 and TPS563210 are 2-A, 3-A synchronous step-down converters. The proprietary D-CAP2™ mode control supports low ESR output capacitors such as specialty polymer capacitors and multi-layer ceramic capacitors without complex external compensation circuits. The fast transient response of D-CAP2™ mode control can reduce the output capacitance required to meet a specific level of performance.

### 8.2 Functional Block Diagram

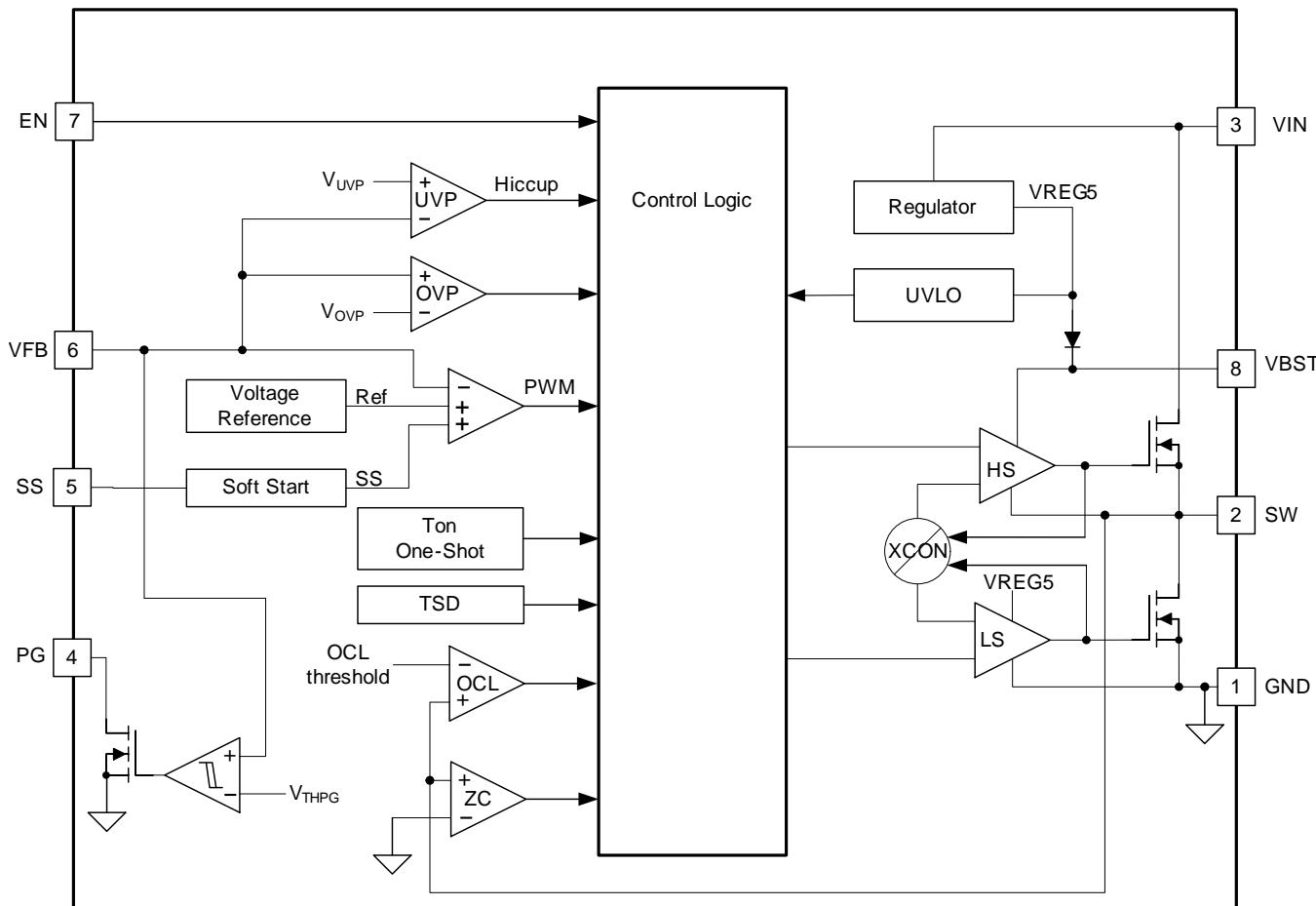


Figure 17. TPS562210

### 8.3 Feature Description

#### 8.3.1 The Adaptive On-Time Control and PWM Operation

The main control loop of the TPS562210 and TPS563210 are adaptive on-time pulse width modulation (PWM) controller that supports a proprietary D-CAP2™ mode control. The D-CAP2™ mode control combines adaptive on-time control with an internal compensation circuit for pseudo-fixed frequency and low external component count configuration with both low ESR and ceramic output capacitors. It is stable even with virtually no ripple at the output.

## Feature Description (continued)

At the beginning of each cycle, the high-side MOSFET is turned on. This MOSFET is turned off after internal one shot timer expires. This one shot duration is set proportional to the converter input voltage,  $V_{IN}$ , and inversely proportional to the output voltage,  $V_{O}$ , to maintain a pseudo-fixed frequency over the input voltage range, hence it is called adaptive on-time control. The one-shot timer is reset and the high-side MOSFET is turned on again when the feedback voltage falls below the reference voltage. An internal ramp is added to reference voltage to simulate output ripple, eliminating the need for ESR induced output ripple from D-CAP2™ mode control.

### 8.3.2 Soft Start and Pre-Biased Soft Start

The TPS562210 and TPS563210 have adjustable soft-start. When the EN pin becomes high, the SS charge current ( $I_{SS}$ ) begins charging the capacitor which is connected from the SS pin to GND ( $C_{SS}$ ). Smooth control of the output voltage is maintained during start up. The equation for the soft start time,  $T_{SS}$  is shown in [Equation 1](#).

$$T_{SS}(\text{ms}) = \frac{C_{SS} \times V_{FBTH} \times 1.1}{I_{SS}} \quad (1)$$

where  $V_{FBTH}$  is 0.765V and  $I_{SS}$  is 6 $\mu$ A.

If the output capacitor is pre-biased at startup, the devices initiate switching and start ramping up only after the internal reference voltage becomes greater than the feedback voltage  $V_{FB}$ . This scheme ensures that the converters ramp up smoothly into regulation point.

### 8.3.3 Power Good

The power good output, PG is an open drain output. The power good function becomes active after 1.7 times soft-start time. When the output voltage becomes within -10% of the target value, internal comparators detect power good state and the power good signal becomes high. If the feedback voltage goes under 15% of the target value, the power good signal becomes low.

### 8.3.4 Current Protection

The output over-current limit (OCL) is implemented using a cycle-by-cycle valley detect control circuit. The switch current is monitored during the OFF state by measuring the low-side FET drain to source voltage. This voltage is proportional to the switch current. To improve accuracy, the voltage sensing is temperature compensated.

During the on time of the high-side FET switch, the switch current increases at a linear rate determined by  $V_{IN}$ ,  $V_{OUT}$ , the on-time and the output inductor value. During the on time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current  $I_{OUT}$ . If the monitored current is above the OCL level, the converter maintains low-side FET on and delays the creation of a new set pulse, even the voltage feedback loop requires one, until the current level becomes OCL level or lower. In subsequent switching cycles, the on-time is set to a fixed value and the current is monitored in the same manner. If the over current condition exists consecutive switching cycles, the internal OCL threshold is set to a lower level, reducing the available output current. When a switching cycle occurs where the switch current is not above the lower OCL threshold, the counter is reset and the OCL threshold is returned to the higher value.

There are some important considerations for this type of over-current protection. The load current is higher than the over-current threshold by one half of the peak-to-peak inductor ripple current. Also, when the current is being limited, the output voltage tends to fall as the demanded load current may be higher than the current available from the converter. This may cause the output voltage to fall. When the  $V_{FB}$  voltage falls below the UVP threshold voltage, the UVP comparator detects it. And then, the device will shut down after the UVP delay time (typically 14 $\mu$ s) and re-start after the hiccup time.

When the over current condition is removed, the output voltage returns to the regulated value.

### 8.3.5 Over Voltage Protection

TPS562210 and TPS563210 detect over voltage condition by monitoring the feedback voltage ( $V_{FB}$ ). When the feedback voltage becomes higher than 125% of the target voltage, the OVP comparator output goes high and the high-side MOSFET is turns off. This function is non-latch operation.

## Feature Description (continued)

### 8.3.6 UVLO Protection

Under voltage lock out protection (UVLO) monitors the internal regulator voltage. When the voltage is lower than UVLO threshold voltage, the device is shut off. This protection is non-latching.

### 8.3.7 Thermal Shutdown

The device monitors the temperature of itself. If the temperature exceeds the threshold value (typically 155°C), the device is shut off. This is a non-latch protection.

## 8.4 Device Functional Modes

### 8.4.1 Advanced Eco-Mode™ Control

The TPS562210 and TPS563210 are designed with Advanced Eco-mode™ to maintain high light load efficiency. As the output current decreases from heavy load condition, the inductor current is also reduced and eventually comes to point that its rippled valley touches zero level, which is the boundary between continuous conduction and discontinuous conduction modes. The rectifying MOSFET is turned off when the zero inductor current is detected. As the load current further decreases the converter runs into discontinuous conduction mode. The on-time is kept almost the same as it was in the continuous conduction mode so that it takes longer time to discharge the output capacitor with smaller load current to the level of the reference voltage. This makes the switching frequency lower, proportional to the load current, and keeps the light load efficiency high. The transition point to the light load operation  $I_{OUT(LL)}$  current can be calculated in [Equation 2](#).

$$I_{OUT(LL)} = \frac{1}{2 \times L \times f_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}} \quad (2)$$

## 9 Application and Implementation

### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

The TPS562210 and TPS563210 are typically used as step down converters, which convert a voltage from 4.5 V to 17 V to a lower voltage. Webench software is available to aid in the design and analysis of circuits.

### 9.2 Typical Application

#### 9.2.1 TPS562210 4.5-V to 17-V Input, 1.05-V output Converter

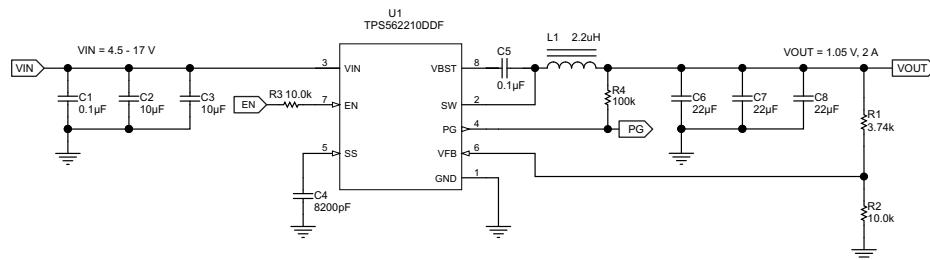


Figure 18. TPS562210 1.05V/2A Reference Design

##### 9.2.1.1 Design Requirements

For this design example, use the parameters shown in Table 1.

Table 1. Design Parameters

PARAMETER	VALUES
Input voltage range	4.5 V to 17 V
Output voltage	1.05 V
Output current	2 A
Output voltage ripple	20 mVp-p

##### 9.2.1.2 Detailed Design Procedure

###### 9.2.1.2.1 Output Voltage Resistors Selection

The output voltage is set with a resistor divider from the output node to the VFB pin. It is recommended to use 1% tolerance or better divider resistors. Start by using Equation 3 to calculate  $V_{OUT}$ .

To improve efficiency at light loads consider using larger value resistors, too high of resistance are more susceptible to noise and voltage errors from the VFB input current are more noticeable.

$$V_{OUT} = 0.765 \times \left( 1 + \frac{R1}{R2} \right) \quad (3)$$

###### 9.2.1.2.2 Output Filter Selection

The LC filter used as the output filter has double pole at:

$$F_P = \frac{1}{2\pi\sqrt{L_{OUT} \times C_{OUT}}} \quad (4)$$

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the device. The low frequency phase is 180 degrees. At the output filter pole frequency, the gain rolls off at a –40 dB per decade rate and the phase drops rapidly. D-CAP2™ introduces a high frequency zero that reduces the gain roll off to –20 dB per decade and increases the phase to 90 degrees one decade above the zero frequency. The inductor and capacitor for the output filter must be selected so that the double pole of [Equation 4](#) is located below the high frequency zero but close enough that the phase boost provided by the high frequency zero provides adequate phase margin for a stable circuit. To meet this requirement use the values recommended in [Table 2](#).

**Table 2. TPS562210 Recommended Component Values**

Output Voltage (V)	R2 (kΩ)	R3 (kΩ)	L1 (μH)			C6 + C7 + C8 (μF)
			MIN	TYP	MAX	
1	3.09	10.0	1.5	2.2	4.7	20 - 68
1.05	3.74	10.0	1.5	2.2	4.7	20 - 68
1.2	5.76	10.0	1.5	2.2	4.7	20 - 68
1.5	9.53	10.0	1.5	2.2	4.7	20 - 68
1.8	13.7	10.0	1.5	2.2	4.7	20 - 68
2.5	22.6	10.0	2.2	3.3	4.7	20 - 68
3.3	33.2	10.0	2.2	3.3	4.7	20 - 68
5	54.9	10.0	3.3	4.7	4.7	20 - 68
6.5	75	10.0	3.3	4.7	4.7	20 - 68

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 5](#), [Equation 6](#) and [Equation 7](#). The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current.

Use 650 kHz for  $f_{SW}$ . Make sure the chosen inductor is rated for the peak current of [Equation 6](#) and the RMS current of [Equation 7](#).

$$I_{P-P} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}} \quad (5)$$

$$I_{PEAK} = I_O + \frac{I_{P-P}}{2} \quad (6)$$

$$I_{O(RMS)} = \sqrt{I_O^2 + \frac{1}{12} I_{P-P}^2} \quad (7)$$

For this design example, the calculated peak current is 2.34 A and the calculated RMS current is 2.01 A. The inductor used is a TDK CLF7045T-2R2N with a peak current rating of 5.5 A and an RMS current rating of 4.3 A.

The capacitor value and ESR determines the amount of output voltage ripple. The TPS562210 and TPS563210 are intended for use with ceramic or other low ESR capacitors. Recommended values range from 20μF to 68μF. Use [Equation 8](#) to determine the required RMS current rating for the output capacitor.

$$I_{CO(RMS)} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{\sqrt{12} \times V_{IN} \times L_O \times f_{SW}} \quad (8)$$

For this design, two TDK C3216X5R0J226M 22 μF output capacitors are used. The typical ESR is 2 mΩ each. The calculated RMS current is 0.286A and each output capacitor is rated for 4A.

#### 9.2.1.2.3 Input Capacitor Selection

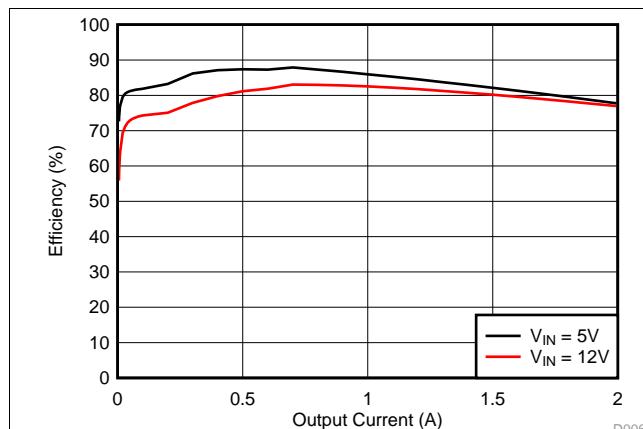
The TPS562210 and TPS563210 require an input decoupling capacitor and a bulk capacitor is needed depending on the application. A ceramic capacitor over 10 μF is recommended for the decoupling capacitor. An additional 0.1 μF capacitor (C3) from pin 3 to ground is optional to provide additional high frequency filtering. The capacitor voltage rating needs to be greater than the maximum input voltage.

#### 9.2.1.2.4 Bootstrap capacitor Selection

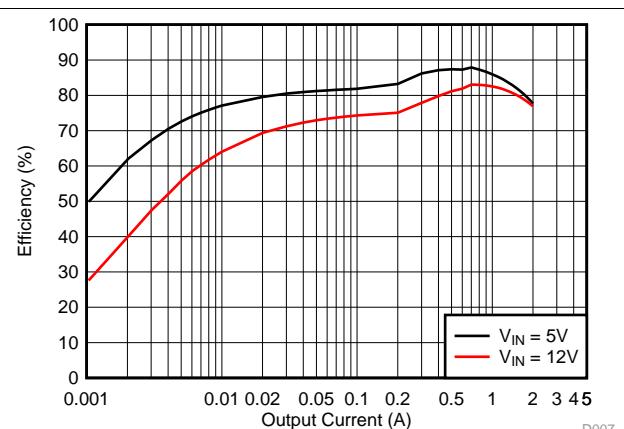
A  $0.1\mu\text{F}$  ceramic capacitor must be connected between the VBST to SW pin for proper operation. It is recommended to use a ceramic capacitor.

#### 9.2.1.3 Application Curves

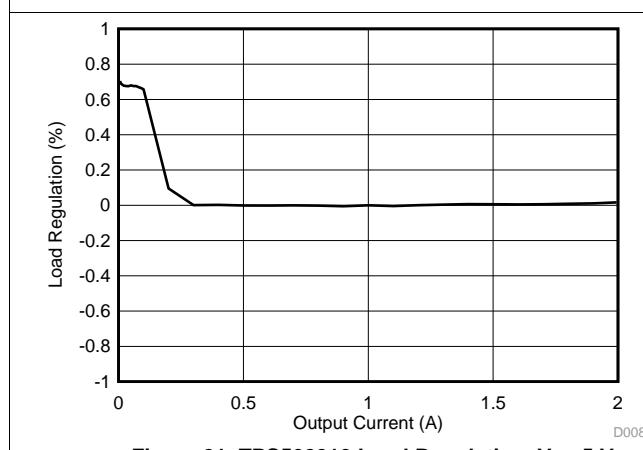
The following application curves were generated using the application circuit of [Figure 18](#).



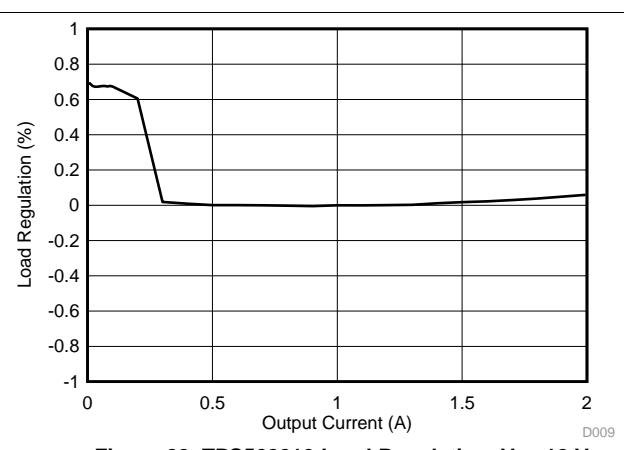
**Figure 19. TPS562210 Efficiency**



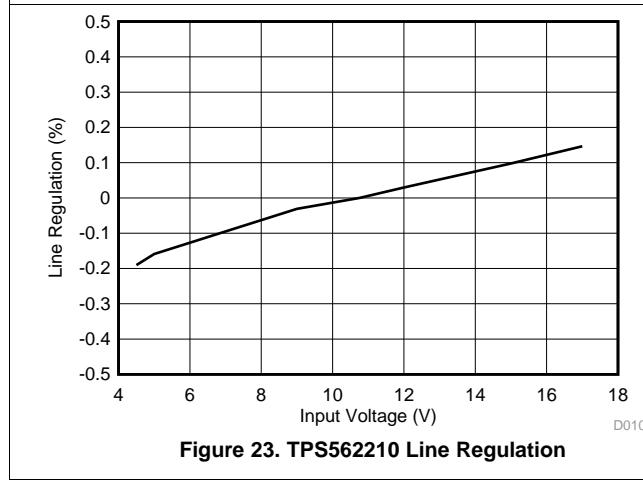
**Figure 20. TPS562210 Light Load Efficiency**



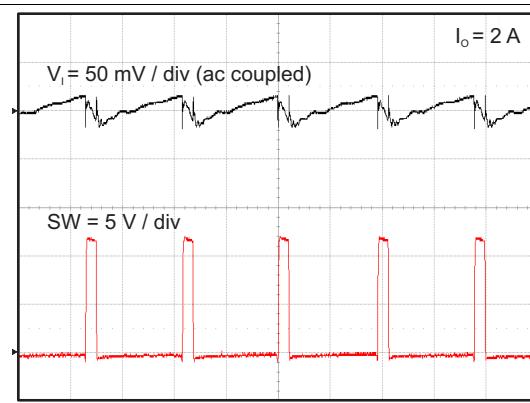
**Figure 21. TPS562210 Load Regulation,  $V_{IN} = 5\text{V}$**



**Figure 22. TPS562210 Load Regulation,  $V_{IN} = 12\text{V}$**

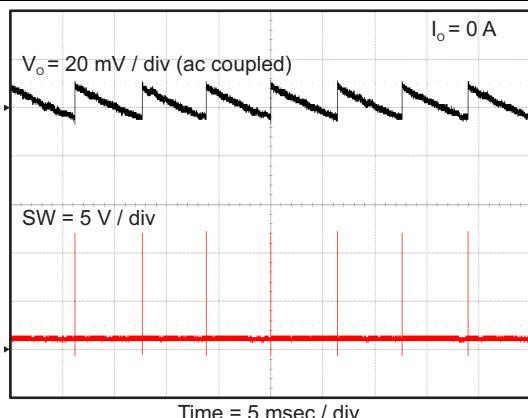


**Figure 23. TPS562210 Line Regulation**

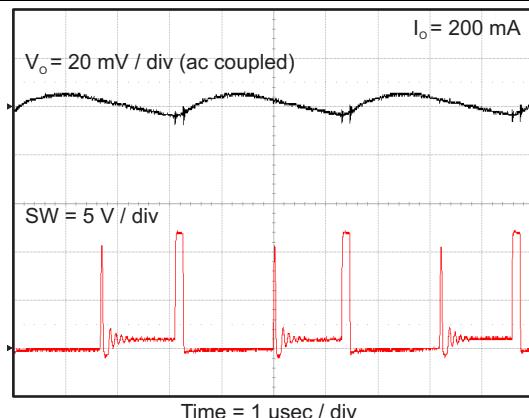


**Figure 24. TPS562210 Input Voltage Ripple**

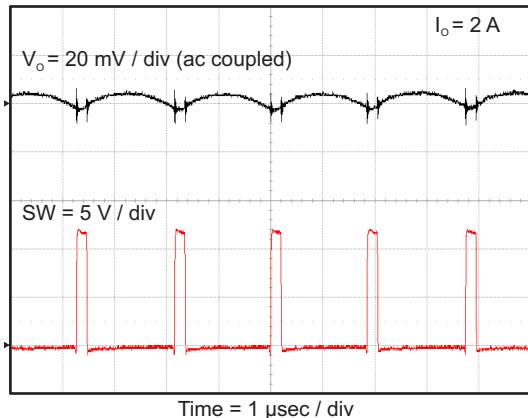
The following application curves were generated using the application circuit of [Figure 18](#).



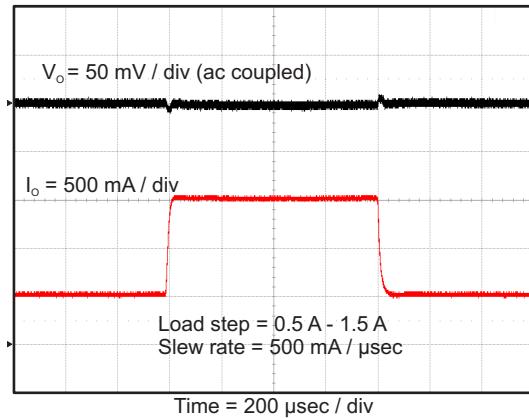
**Figure 25. TPS562210 Output Voltage Ripple**



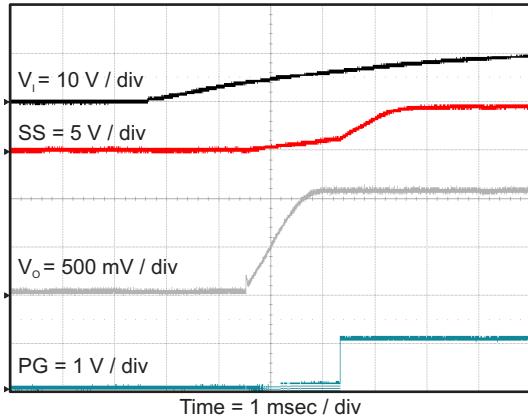
**Figure 26. TPS562210 Output Voltage Ripple**



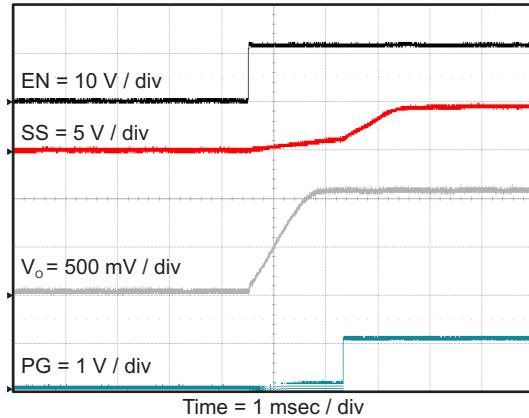
**Figure 27. TPS562210 Output Voltage Ripple**



**Figure 28. TPS562210 Transient Response**

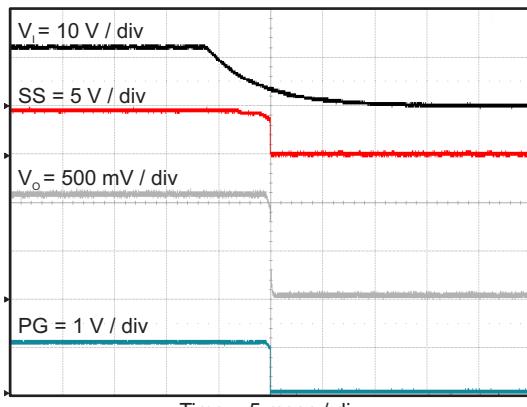


**Figure 29. TPS562210 Start Up Relative To  $V_I$**

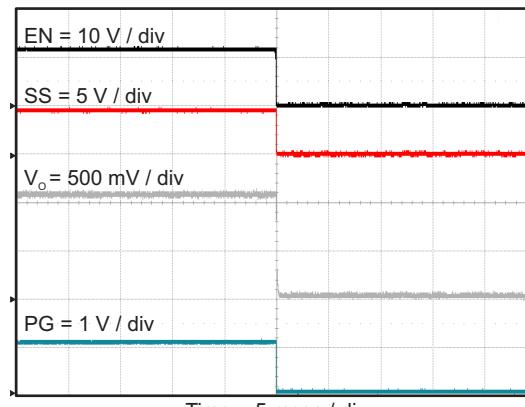


**Figure 30. TPS562210 Start Up Relative To  $En$**

The following application curves were generated using the application circuit of [Figure 18](#).



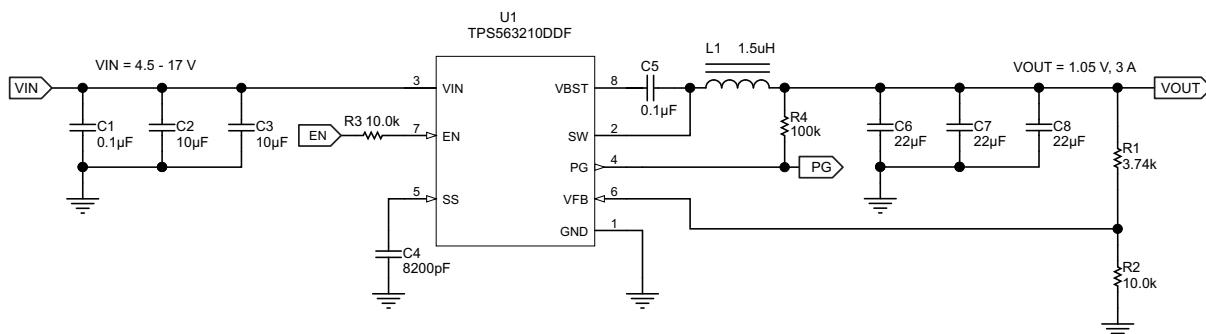
**Figure 31. TPS562210 Shut Down Relative To  $V_i$**



**Figure 32. TPS562210 Shut Down Relative To EN**

The following application curves were generated using the application circuit of [Figure 18](#).

### 9.2.2 TPS563210 4.5-V To 17-V Input, 1.05-V Output Converter



**Figure 33. TPS563210 1.05 V / 3A Reference Design**

#### 9.2.2.1 Design Requirements

For this design example, use the parameters shown in [Table 3](#).

**Table 3. Design Parameters**

PARAMETER	VALUE
Input voltage range	4.5 V to 17 V
Output voltage	1.05 V
Output current	3 A
Output voltage ripple	20 mV/PP

#### 9.2.2.2 Detailed Design Procedures

The detailed design procedure for TPS563210 is the same as for TPS562210 except for inductor selection.

##### 9.2.2.2.1 Output Filter Selection

**Table 4. TPS563210 Recommended Component Values**

Output Voltage (V)	R2 (kΩ)	R3 (kΩ)	L1 (μH)			C6 + C7 + C8 (μF)
			MIN	TYP	MAX	
1	3.09	10.0	1.0	1.5	4.7	20 - 68
1.05	3.74	10.0	1.0	1.5	4.7	20 - 68
1.2	5.76	10.0	1.0	1.5	4.7	20 - 68
1.5	9.53	10.0	1.0	1.5	4.7	20 - 68
1.8	13.7	10.0	1.5	2.2	4.7	20 - 68
2.5	22.6	10.0	1.5	2.2	4.7	20 - 68
3.3	33.2	10.0	1.5	2.2	4.7	20 - 68
5	54.9	10.0	2.2	3.3	4.7	20 - 68
6.5	75	10.0	2.2	3.3	4.7	20 - 68

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 9](#), [Equation 10](#) and [Equation 11](#). The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current. Use 650 kHz for  $f_{SW}$ .

Use 650 kHz for  $f_{SW}$ . Make sure the chosen inductor is rated for the peak current of [Equation 10](#) and the RMS current of [Equation 11](#).

$$I_{I_{P-P}} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}} \quad (9)$$

$$I_{I_{PEAK}} = I_O + \frac{I_{I_{P-P}}}{2} \quad (10)$$

$$I_{I_{O(RMS)}} = \sqrt{I_O^2 + \frac{1}{12} I_{I_{P-P}}^2} \quad (11)$$

For this design example, the calculated peak current is 3.505 A and the calculated RMS current is 3.014 A. The inductor used is a TDK CLF7045T-1R5N with a peak current rating of 7.3-A and an RMS current rating of 4.9-A.

The capacitor value and ESR determines the amount of output voltage ripple. The TPS563209 is intended for use with ceramic or other low ESR capacitors. Recommended values range from 20  $\mu$ F to 68  $\mu$ F. Use [Equation 7](#) to determine the required RMS current rating for the output capacitor. For this design three TDK C3216X5R0J226M 22  $\mu$ F output capacitors are used. The typical ESR is 2 m $\Omega$  each. The calculated RMS current is 0.292A and each output capacitor is rated for 4 A.

### 9.2.2.3 Application Curves

The following application curves were generated using the application circuit of [Figure 33](#).

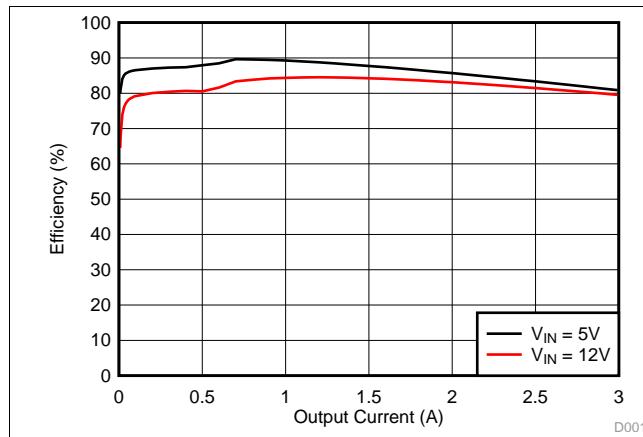


Figure 34. TPS563210 Efficiency

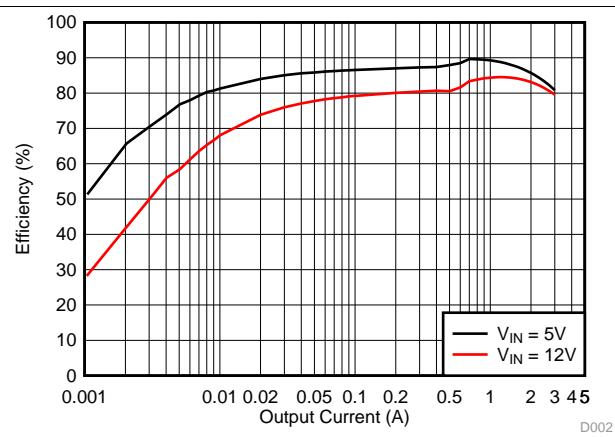


Figure 35. TPS563210 Light Load Efficiency

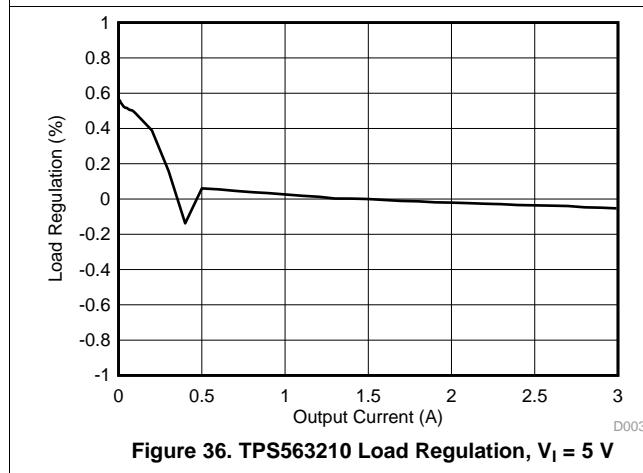


Figure 36. TPS563210 Load Regulation,  $V_I = 5$  V

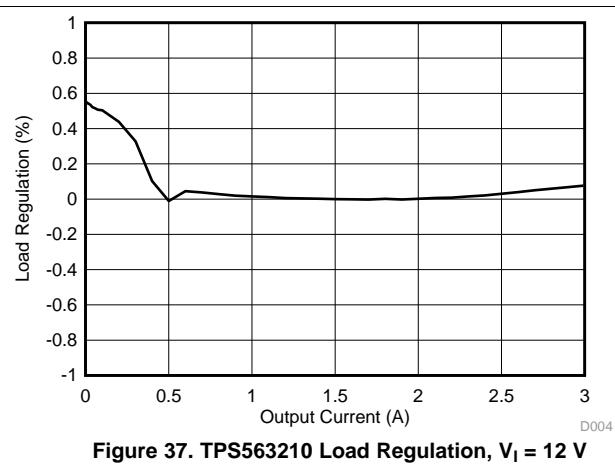
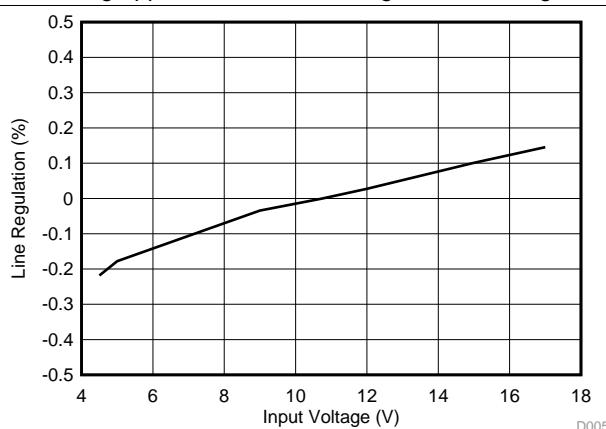
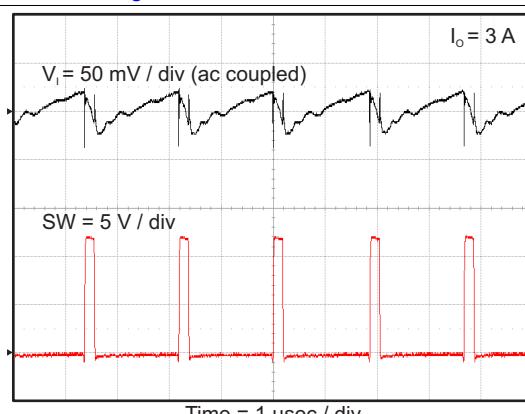


Figure 37. TPS563210 Load Regulation,  $V_I = 12$  V

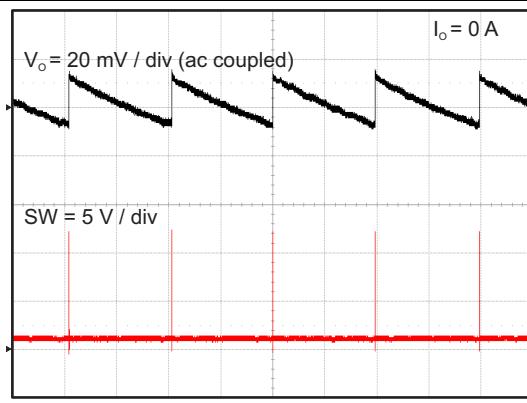
The following application curves were generated using the application circuit of [Figure 33](#).



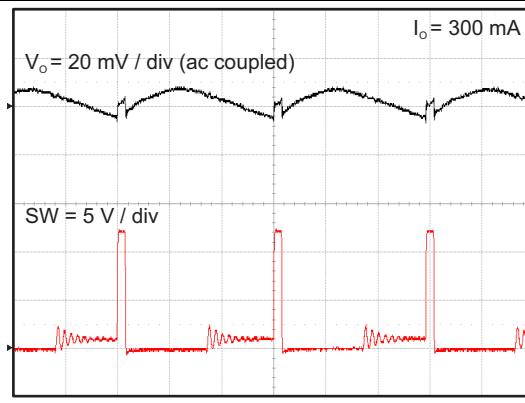
**Figure 38. TPS563210 Line Regulation**



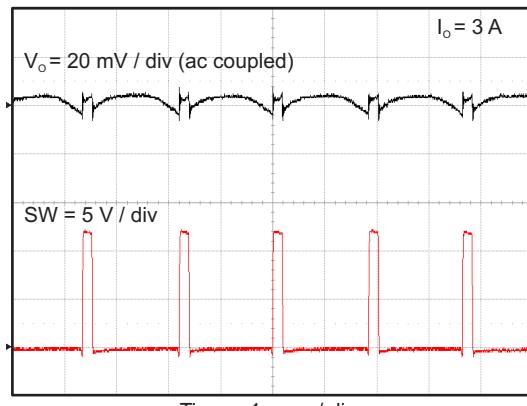
**Figure 39. TPS563210 Input Voltage Ripple**



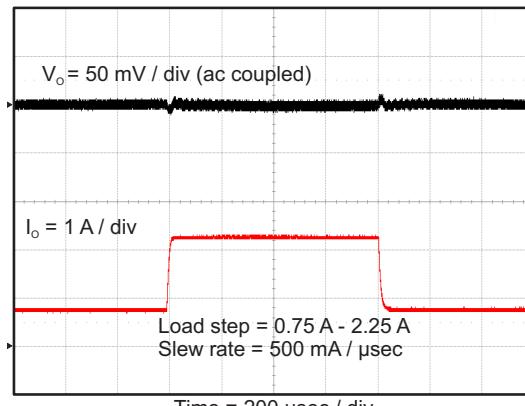
**Figure 40. TPS563210 Output Voltage Ripple**



**Figure 41. TPS563210 Output Voltage Ripple**

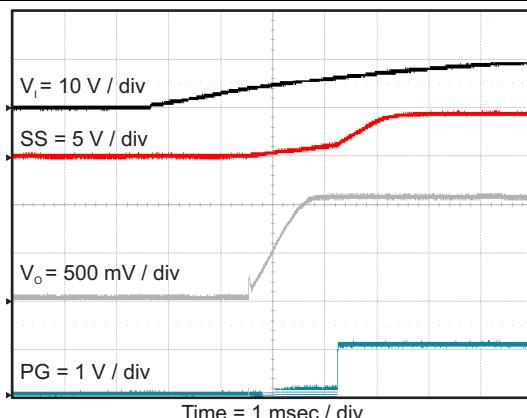


**Figure 42. TPS563210 Output Voltage Ripple**

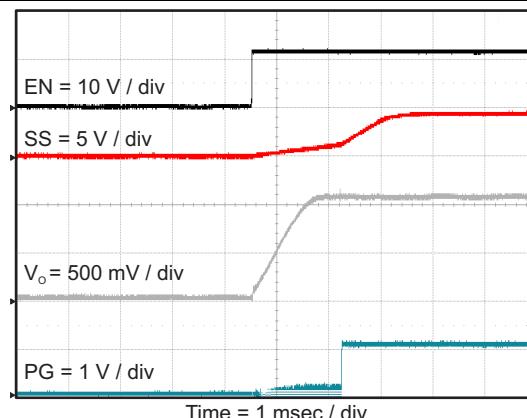


**Figure 43. TPS563210 Transient Response**

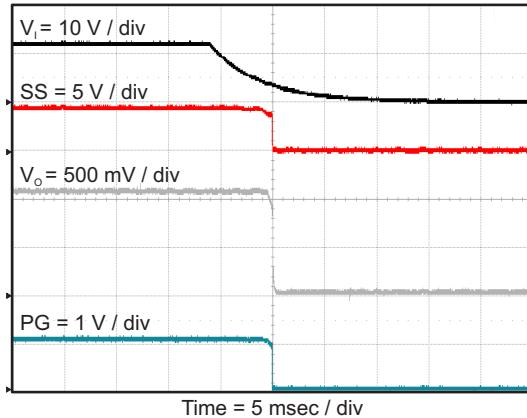
The following application curves were generated using the application circuit of [Figure 33](#).



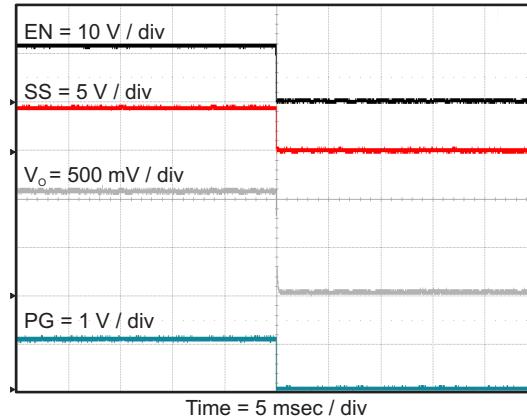
**Figure 44. TPS563210 Start Up Relative To  $V_i$**



**Figure 45. TPS563210 Start Up Relative To EN**



**Figure 46. TPS563210 Shut Down Relative To  $V_i$**



**Figure 47. TPS563210 Shut Down Relative To EN**

## 10 Power Supply Recommendations

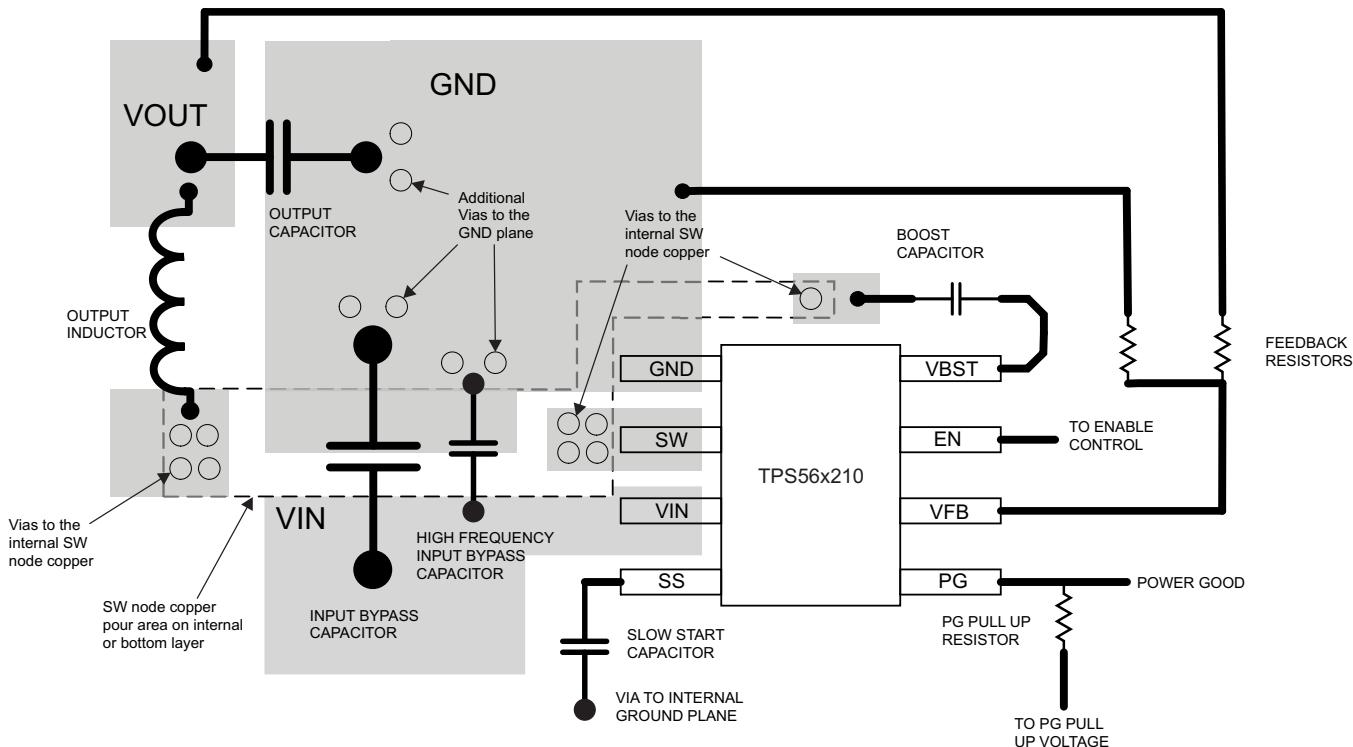
The TPS562210 and TPS563210 are designed to operate from input supply voltage in the range of 4.5 V to 17 V. Buck converters require the input voltage to be higher than the output voltage for proper operation. The maximum recommended operating duty cycle is 65%. Using that criteria, the minimum recommended input voltage is  $V_O / 0.65$ .

## 11 Layout

### 11.1 Layout Guidelines

1. VIN and GND traces should be as wide as possible to reduce trace impedance. The wide areas are also of advantage from the view point of heat dissipation.
2. The input capacitor and output capacitor should be placed as close to the device as possible to minimize trace impedance.
3. Provide sufficient vias for the input capacitor and output capacitor.
4. Keep the SW trace as physically short and wide as practical to minimize radiated emissions.
5. Do not allow switching current to flow under the device.
6. A separate VOUT path should be connected to the upper feedback resistor.
7. Make a Kelvin connection to the GND pin for the feedback path.
8. Voltage feedback loop should be placed away from the high-voltage switching trace, and preferably has ground shield.
9. The trace of the VFB node should be as small as possible to avoid noise coupling.
10. The GND trace between the output capacitor and the GND pin should be as wide as possible to minimize its trace impedance.

### 11.2 Layout Example



## 12 Device and Documentation Support

### 12.1 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

**Table 5. Related Links**

PARTS	PRODUCT FOLDER	SAMPLE & BUY	TECHNICAL DOCUMENTS	TOOLS & SOFTWARE	SUPPORT & COMMUNITY
TPS562210	<a href="#">Click here</a>				
TPS563210	<a href="#">Click here</a>				

### 12.2 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

**TI E2E™ Online Community** *TI's Engineer-to-Engineer (E2E) Community.* Created to foster collaboration among engineers. At [e2e.ti.com](http://e2e.ti.com), you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 12.3 Trademarks

D-CAP2, Eco-mode, E2E are trademarks of Texas Instruments.

Blu-ray Disc is a trademark of Blu-ray Disc Association.

### 12.4 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 12.5 Glossary

[SLYZ022](#) — *TI Glossary.*

This glossary lists and explains terms, acronyms, and definitions.

## 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS562210DDFR.A	NRND	Production	SOT-23-THIN (DDF)   8	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	2210
TPS562210DDFR.B	NRND	Production	SOT-23-THIN (DDF)   8	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	2210
TPS562210DDFT.A	NRND	Production	SOT-23-THIN (DDF)   8	250   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	2210
TPS562210DDFT.B	NRND	Production	SOT-23-THIN (DDF)   8	250   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	2210
TPS563210DDFR.A	NRND	Production	SOT-23-THIN (DDF)   8	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	3210
TPS563210DDFR.B	NRND	Production	SOT-23-THIN (DDF)   8	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	3210
TPS563210DDFT.A	NRND	Production	SOT-23-THIN (DDF)   8	250   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	3210
TPS563210DDFT.B	NRND	Production	SOT-23-THIN (DDF)   8	250   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	3210

<sup>(1)</sup> **Status:** For more details on status, see our [product life cycle](#).

<sup>(2)</sup> **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

<sup>(4)</sup> **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

**Important Information and Disclaimer:** The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

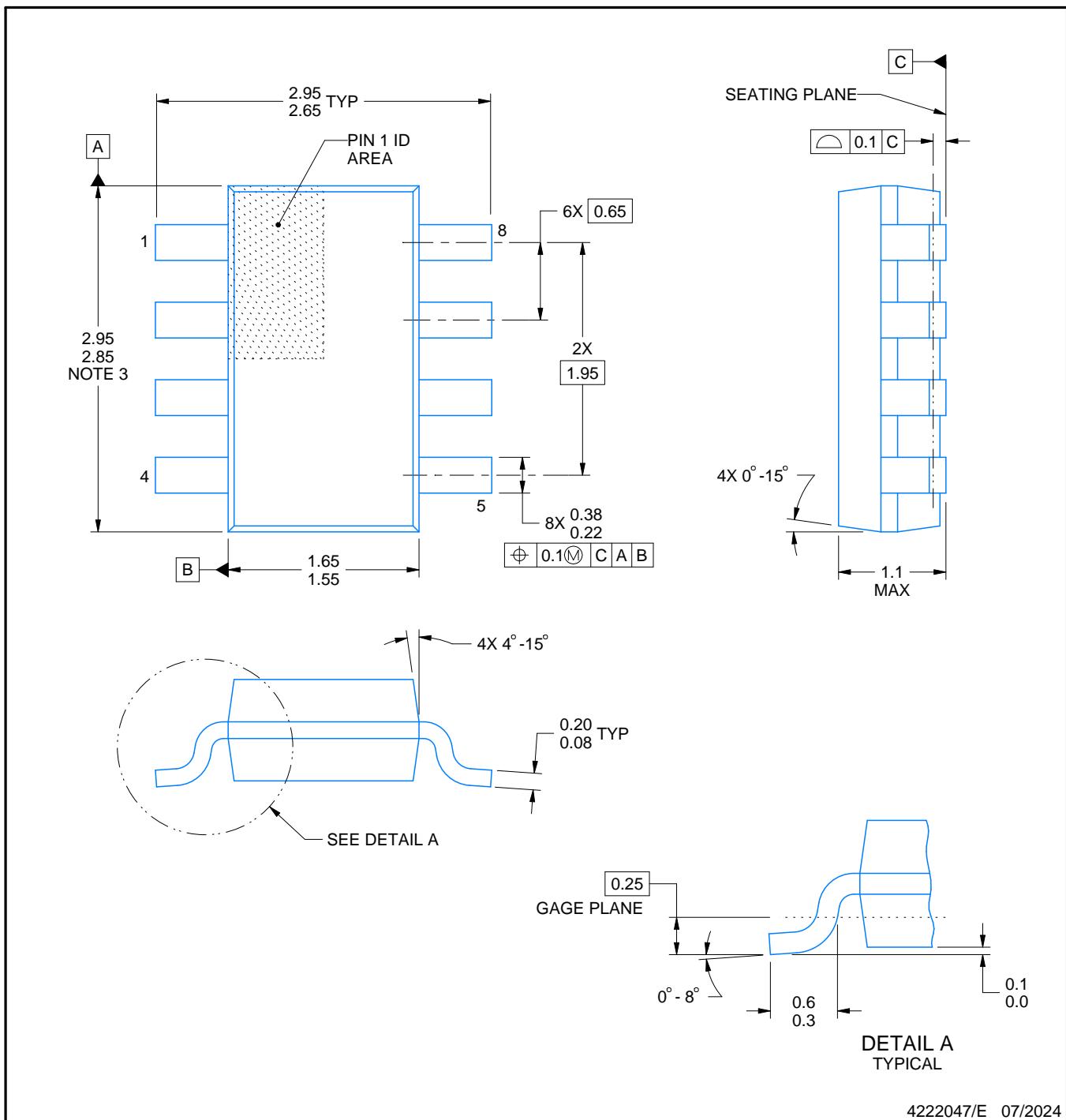
# PACKAGE OUTLINE

DDF0008A



SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



4222047/E 07/2024

## NOTES:

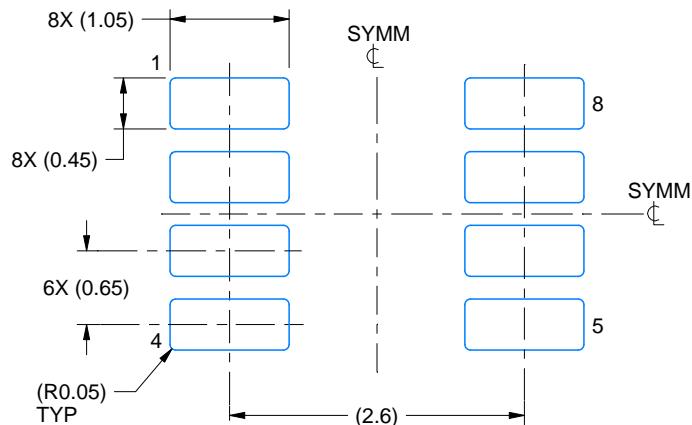
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.

# EXAMPLE BOARD LAYOUT

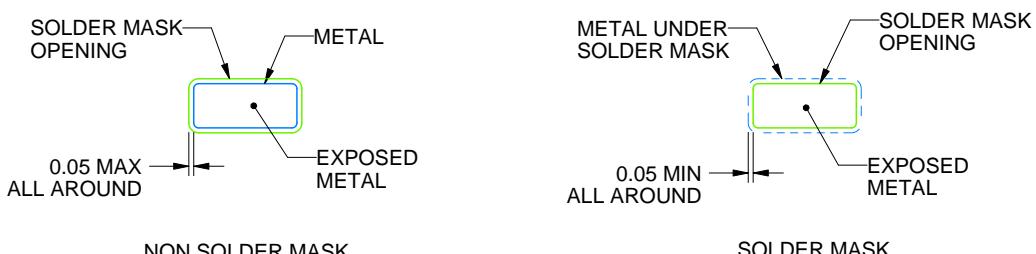
DDF0008A

SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

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NOTES: (continued)

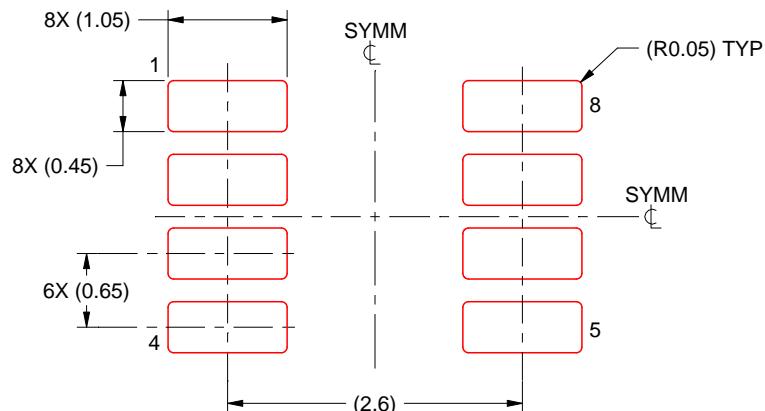
4. Publication IPC-7351 may have alternate designs.
5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DDF0008A

SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

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NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
7. Board assembly site may have different recommendations for stencil design.

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