

# **TLK1XX Design and Layout Guide**

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*Industrial Interface*

## **ABSTRACT**

Many times when approaching a new design, significant time and effort can be saved by applying correct and recommended design guidelines already in the planning phase. The purpose of this document is to supply these guidelines to the engineer working with the TLK family of products; saving time, effort, and cost, and decreasing time to market for their solution.

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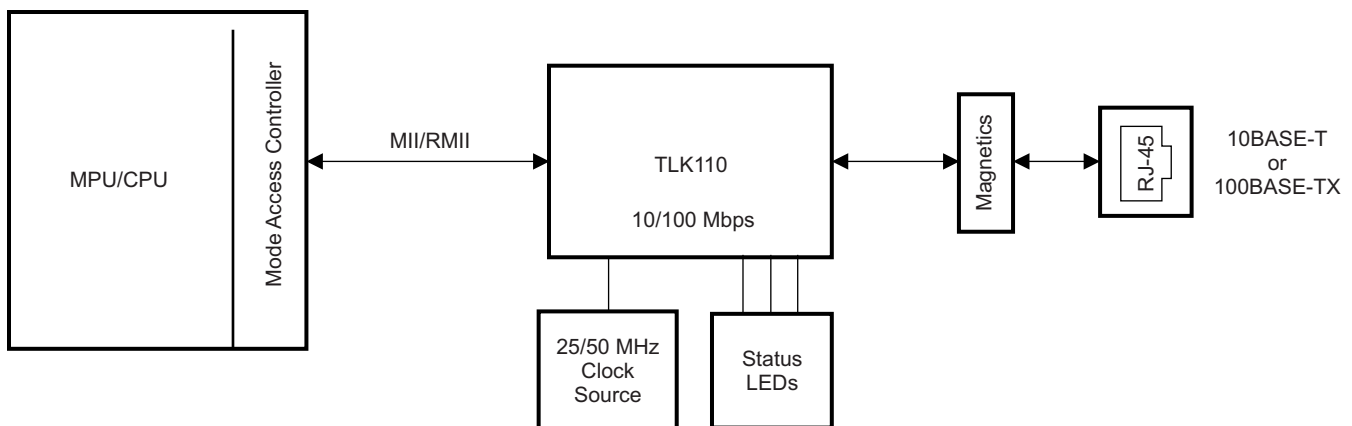
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## 1 Introduction

The TLK1XX family of products are robust, full-featured, low-power, 10/100 physical layer devices. With cable length performance far exceeding IEEE specifications and features that provide lower cost solutions, for both 10BASE-T and 100BASE-TX Ethernet protocols, the devices ensure compatibility and interoperability with other standards-based Ethernet products in these applications:

- High-end peripheral devices
- Industrial controls
- Factory automation
- General embedded applications

Use of this document, in conjunction with product data sheets, application notes, and reference designs, help ensure issue-free system products. In this application note we review: MAC Interface, Physical medium interface, Board design, Power supply, Configuration, and Components selection, among other topics. Product Applicability: TLK110, TLK105, TLK106.



**Figure 1. Typical Application**

## 2 MDI (TP/CAT-V) Connections

The network or medium dependent interface (MDI) connection is via the transmit (TD+ & TD-) and receive (RD+ & RD-) differential pair pins. These connect to a termination network, then to 1:1 magnetics (transformer) and an RJ-45. For space savings, the magnetics and RJ-45 may be a single-integrated component. A standard CAT-V Ethernet cable is then used to connect to the rest of the network. Figure 2 shows the recommended 10/100 Mb/s twisted pair interface circuit.

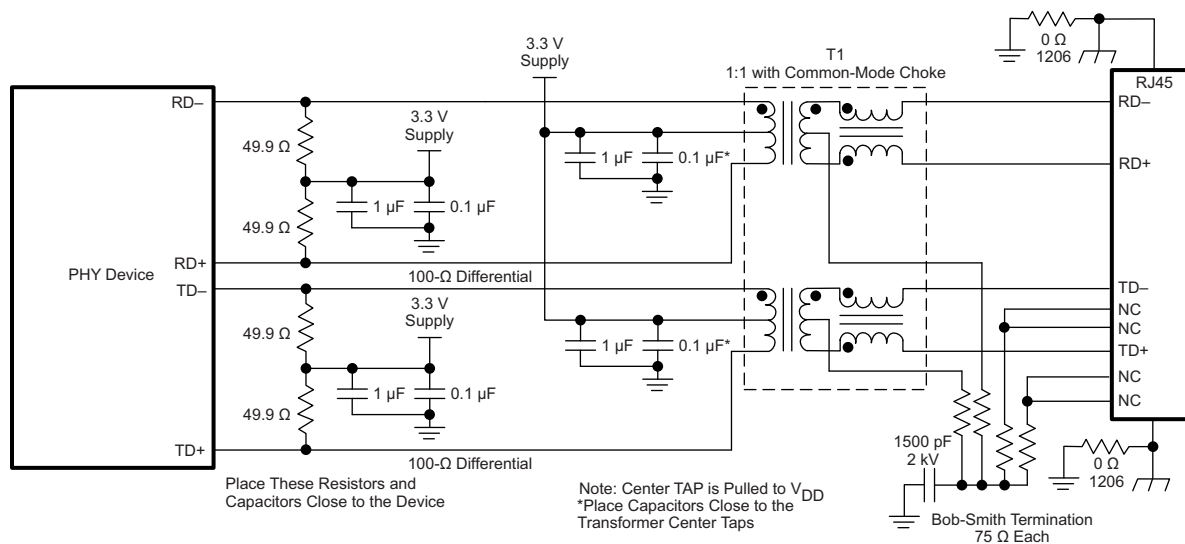


Figure 2. MDI Connection

### 2.1 RJ-45 Connections

The transformer used in the MDI connection provides DC isolation between local circuitry and the network cable. The center tap of the isolated winding has Bob Smith termination through a 75-Ω resistor and a 1000-pF capacitor to chassis ground. The termination capacitor should be rated to a voltage of at least 2 kV.

**NOTE:** Bob-Smith termination does not apply for Power Over Ethernet (PoE) applications.

Bob-Smith termination is used to reduce noise resulting from common mode current flows, as well as reduce susceptibility to any noise from unused wire pairs on the RJ-45. It is described in patent publication US5321372 A.

### 2.2 ESD EMI EMC Recommendations

The following recommendations are provided to improve EMI performance:

- Use a metal shielded RJ-45 connector, and connect the shield to chassis ground.
- Use magnetics with integrated common-mode choking devices with the choke on the side of the PHY (for example PULSE HX1198).
- Do not overlap the circuit and chassis ground planes, keep them isolated. Connect chassis ground and system ground together using one 4700 pF NPO 2000 V 10% across the void between the ground planes on the 1, 2 pair side of the RJ-45.

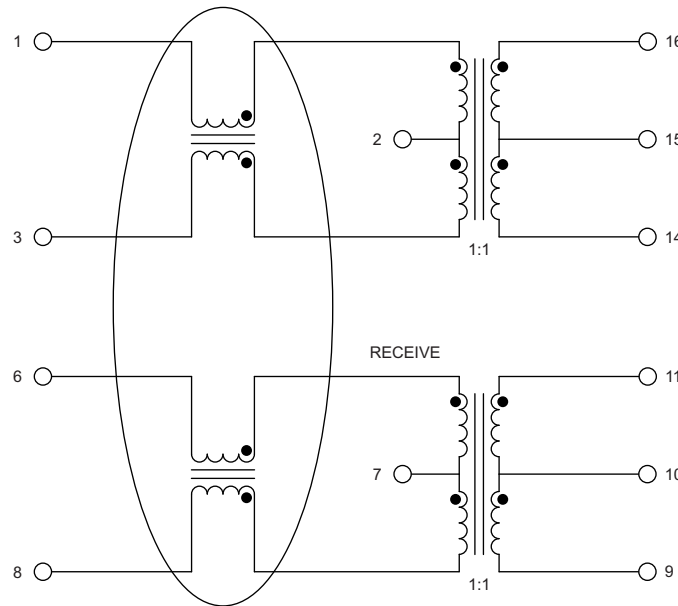


Figure 3. Recommended Magnetics

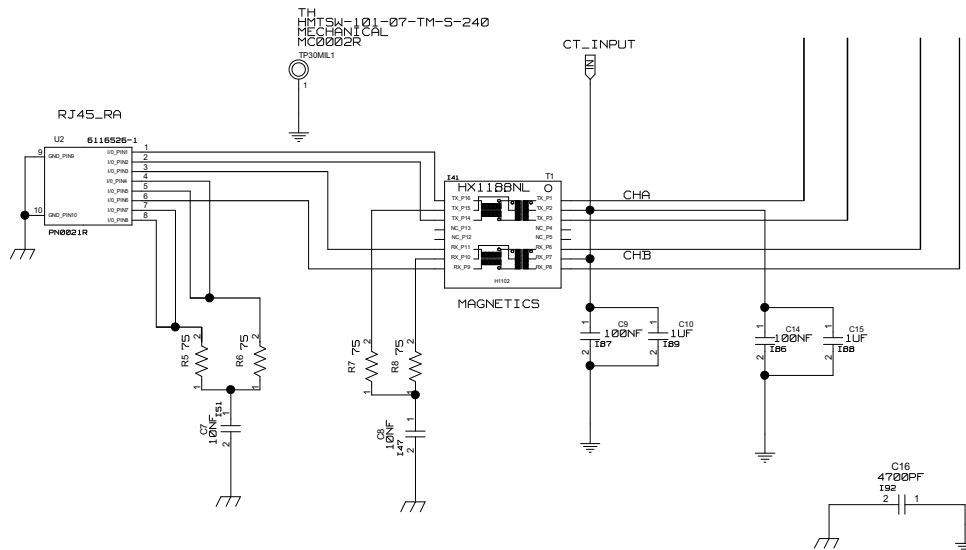


Figure 4. Chassis GND and Board GND Separation

### 2.3 Fiber Optic Implementations

Some TLK1XX family products utilize the MDI interface to connect to fiber optic transceivers. Individual device datasheets describe how to terminate the MDI signals when enabling fiber mode in these devices.

Although the termination requirements for fiber mode operation differ from the termination requirements of twisted pair operation, the characteristic impedance of the terminations and the associated signal traces are the same. Therefore, the same MDI signal routing recommendations described in Section 7 apply to Fiber-enabled systems as well.

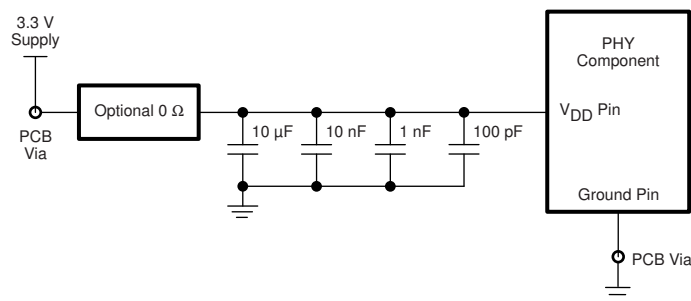
### 3 Power Supply

#### 3.1 Filtering

Bypass the power rails with the following low-impedance surface mount capacitors: 10  $\mu\text{F}$ , 10 nF, 1 nF, and 100 pF. To reduce EMI, place the capacitors as close as possible to the component  $V_{\text{DD}}$  supply pins, preferably between the supply pins and the vias connecting to the power plane. In some systems it may be desirable to add 0- $\Omega$  resistors in series with supply pins, as the resistor pads provide flexibility if adding EMI beads becomes necessary to meet system level certification testing requirements, see [Figure 5](#).

It is recommended the PCB have at least one solid ground plane and one solid  $V_{\text{DD}}$  plane to provide a low impedance power source to the component. This also provides a low impedance return path for non-differential digital MII and clock signals. (See [Figure 5](#).)

Place a 10.0- $\mu\text{F}$  capacitor near the PHY component for local bulk bypassing between the  $V_{\text{DD}}$  and ground planes. The rise time of the  $V_{\text{DD}}$  should be typically 500  $\mu\text{s}$ .



**Figure 5.  $V_{\text{DD}}$  Layout**

### 3.2 Single-Supply Operation

If a single 3.3-V power supply is desired, the TLK10x internal regulator provides the necessary core supply voltages. Place 10- $\mu$ F and 0.1- $\mu$ F ceramic capacitors close to the PFBOOUT pin, the output of the internal regulator. Connect the PFBOOUT pin to the PFBIN1 and PFBIN2 pins. Put a 0.1- $\mu$ F capacitor close to the PFBIN1 and PFBIN2 pins. To operate in this mode, connect the TLK10x supply pins as shown in Figure 6.

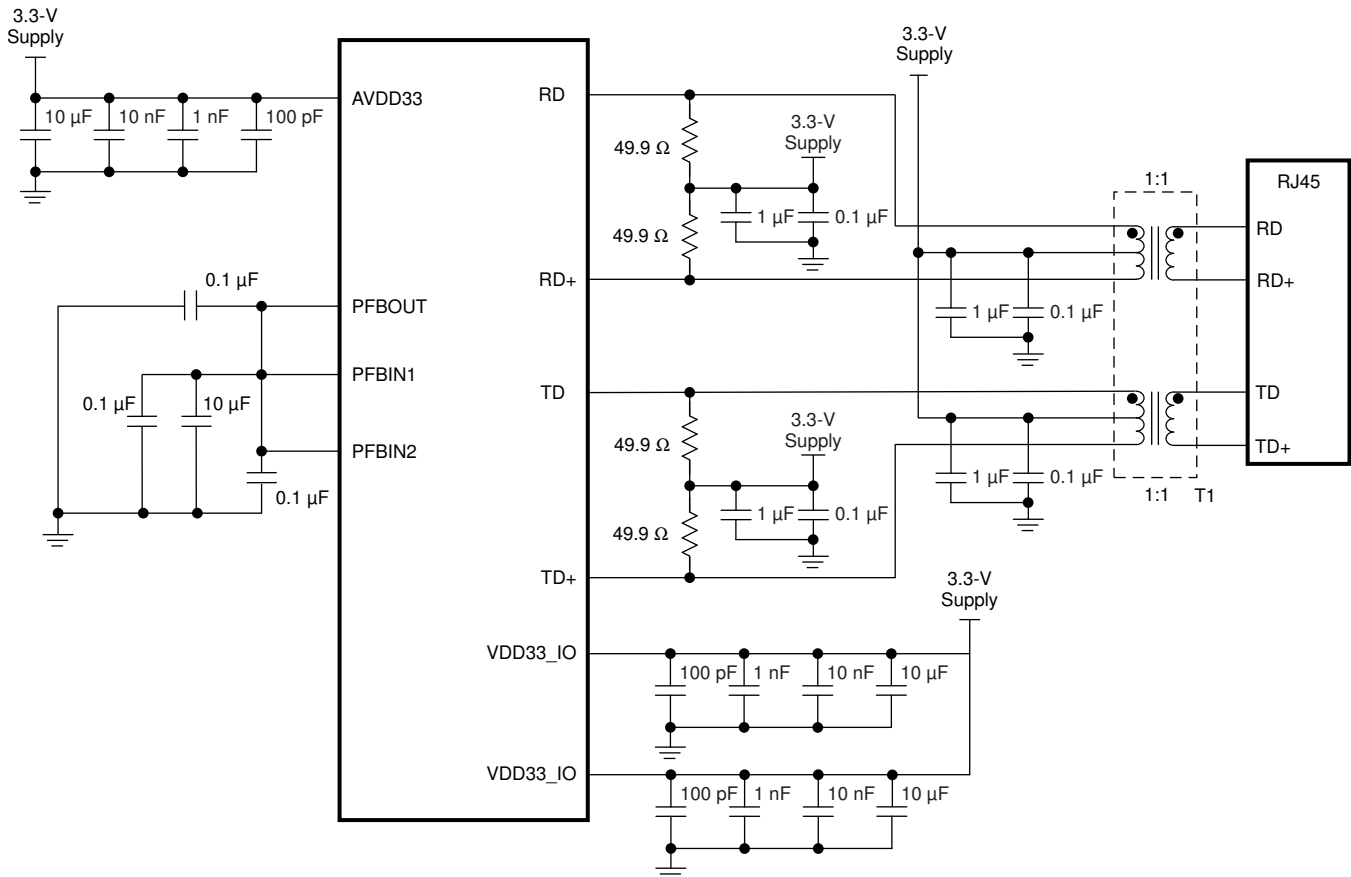


Figure 6. Power Connections for Single-Supply Operation

### 3.3 Dual-Supply Operation

When a 1.55-V external power rail is available on board, the TLK1XX may be configured to work with dual power supply and thus reduce power consumption in the overall system. The TLK1XX dual supply configuration is shown in Figure 7. PFBOU<sub>T</sub> is left floating. The 1.55-V external supply is connected to PFBIN<sub>1</sub> and PFBIN<sub>2</sub>. Furthermore, to lower the power consumption, power down the internal regulator by writing 1 to bit 15 of the VR<sub>CR</sub> register (0x00d0h).

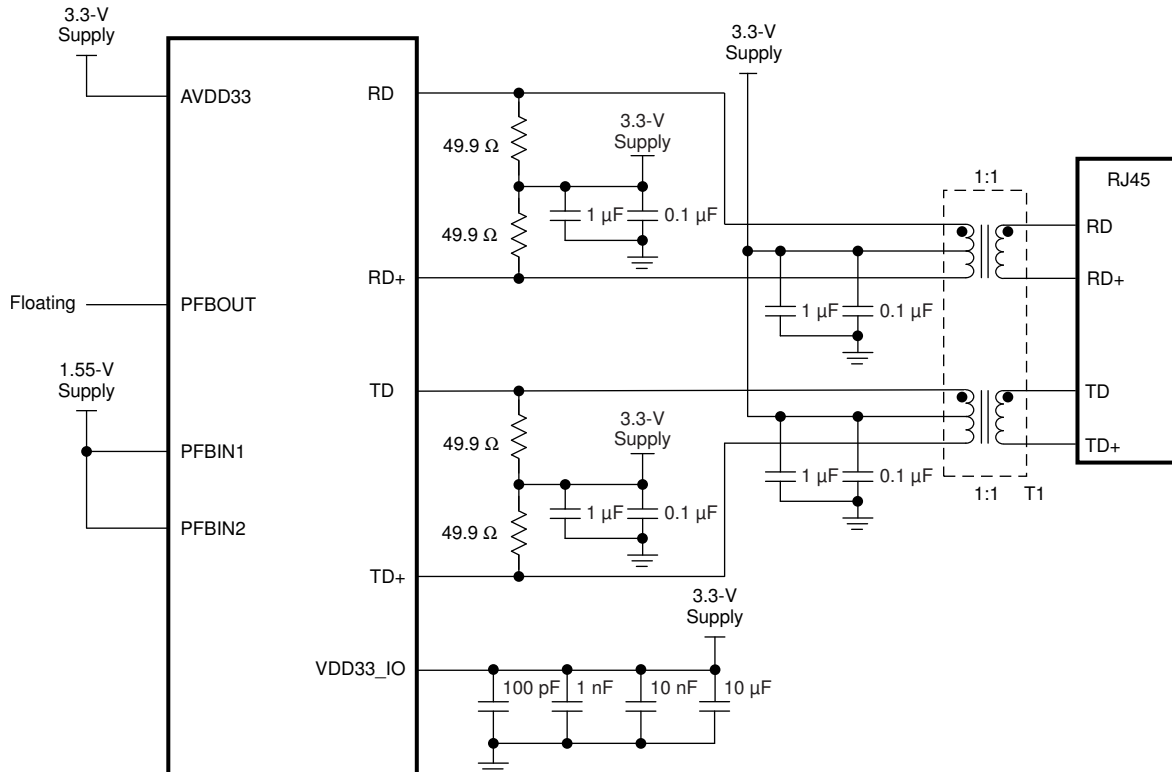


Figure 7. Power Connections for Dual-Supply Operation

### 3.4 I/O Voltage Supply

The TLK1XX I/O's have the flexibility to work with the VDDIO voltage level which is lower than 3.3 V, refer to the VDDIO application note for more thorough information.

### 3.5 CT Supply

It is recommended to provide a constant power supply to the center tap when connected to a link partner.



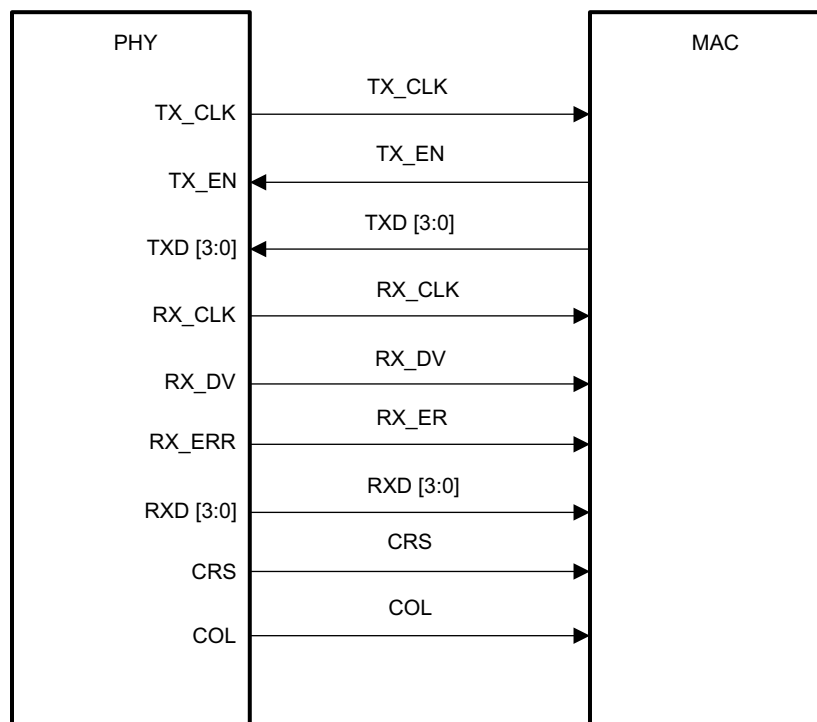
## 4 MAC Interfaces

The TLK1XX family supports both MII and RMIi connectivity to the Media Access Controller (MAC). When using MII, the advantages are in the round trip delay of the data transmission of the PHY. The TLK1XX allows MII mode to maintain state-of-the-art, low deterministic round-trip delay, which is a crucial factor for many automated industrial protocols like EtherCAT, PROFINET, and more. For space-critical designs, RMIi mode is usually used, due to the reduced number of pins required (save both traces on board and number of pins required by host)

### 4.1 Media Independent Interface (MII)

The Media Independent Interface (MII) is a synchronous 4-bit wide nibble data interface that connects the PHY to the MAC in 100B-TX and 10B-T modes. The MII is fully compliant with IEEE802.3-2002 clause 22. The MII signals are summarized below:

Data signals:	MII_TXD [3:0]
	RXD [3:0]
Transmit and receive-valid signals:	MII_TX_EN
	MII_RX_DV
Line-status signals:	CRS (carrier sense)
	COL (collision)



**Figure 8. MII Signaling**

The isolate register 0.10 defined in IEEE802.3-2002 used to electrically isolate the PHY from the MII (if Set, all transactions on the MII interface are ignored by the PHY).

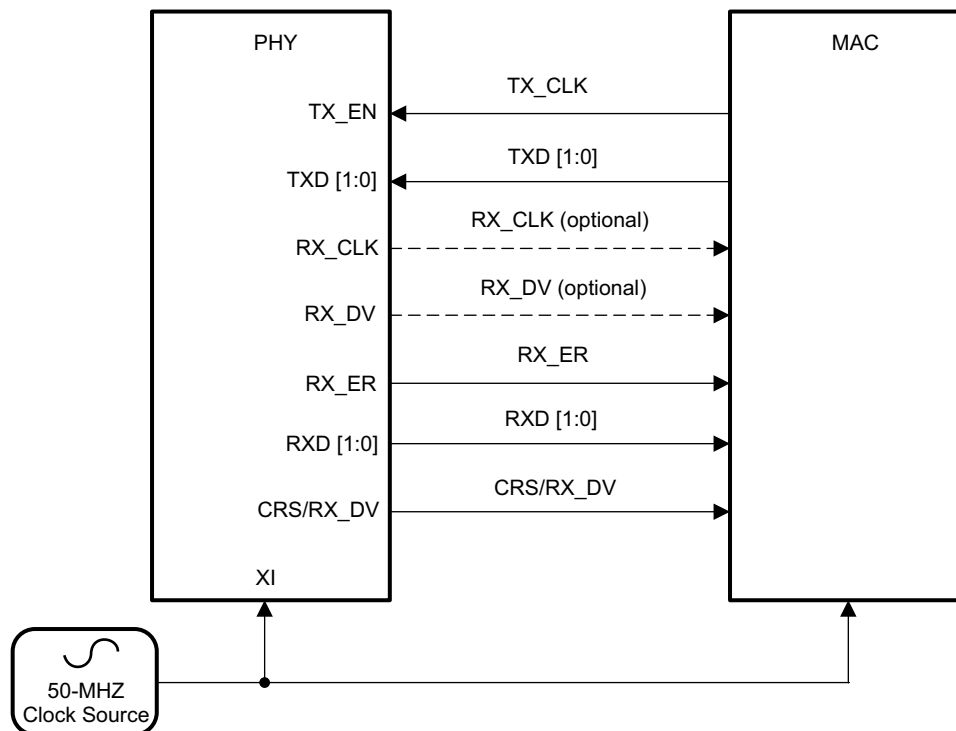
Additionally, the MII interface includes the carrier sense signal CRS, as well as a collision detect signal COL. The CRS signal asserts to indicate the reception of data from the network or as a function of Transmit data in Half Duplex mode. The COL signal asserts as an indication of a collision which can occur During half-duplex operations when both transmit and receive operation occur simultaneously.

## 4.2 Reduced Media Independent Interface (RMII)

TLK110 incorporates the Reduced Media Independent Interface (RMII) as specified in the RMII specification (rev1.2) from the RMII consortium. The purpose of this interface is to provide a low cost alternative to the IEEE 802.3u [2] MII as specified in Clause 22. Architecturally, the RMII specification provides an additional reconciliation layer on either side of the MII, but can be implemented in the absence of an MII.

The RMII specification has the following characteristics:

- It is capable of supporting 10 Mbps and 100 Mbps data rates
- A single clock reference is sourced from the MAC to PHY (or from an external source)
- It provides independent 2 bit wide (di-bit) transmit and receive data paths



**Figure 9. RMII/MAC Connection**

### 4.2.1 MII to RMII Schematic Changes

1. Change the OSC to 50 MHz, connect it to PHY (Xi pin) and MAC
2. External Pull up MII\_MODE (RX\_DV) (Pin 39)
3. No need to connect PHY and MAC with: TXD[3:2],RXD[3:2], TX\_CLK, RX\_CLK

If a given design requires both MII and RMII modes of operation, it is recommended to use a single 50-MHz oscillator on board. While in RMII mode, this is the required configuration, for MII mode, by using register access, the TLK1XX can be configured to work in MII mode also when the source clock is 50 MHz.

## 4.3 Termination Requirement

To reduce digital signal energy, 33-Ω series termination resistors are recommended for all MII output signals (including RXCLK, TXCLK, and RX data signals).

#### 4.4 Recommended Maximum Trace Length

Although RMII and MII are synchronous bus architectures, there are a number of factors limiting signal trace lengths. With a longer trace, the signal becomes more attenuated at the destination and thus more susceptible to noise interference.

Longer traces also act as antennas, and if run on the surface layer, can increase EMI radiation. If a long trace is running near and adjacent to a noisy signal, the unwanted signals could be coupled in as cross talk.

It is recommended to keep the signal trace lengths as short as possible. Ideally, keep the traces under 6 inches.

Trace length matching, to within 2.0 inches on the MII or RMII bus is also recommended. Significant differences in the trace lengths can cause data timing issues.

As with any high-speed data signal, good design practices dictate that impedance should be maintained and stubs should be avoided throughout the entire data path.

### 5 Clock Requirements

TLK1XX family products support either an external CMOS level oscillator source or a crystal resonator device. The X1 pin is the clock input, requiring either 25 or 50 MHz, depending on the MII/RMII mode.

In MII mode, use either a 25-MHz crystal or 50-MHz oscillator. For RMII mode, only a 50-MHz oscillator can be used.

The input clock signal is also buffered and provided as an output signal on some TLK1XX family products.

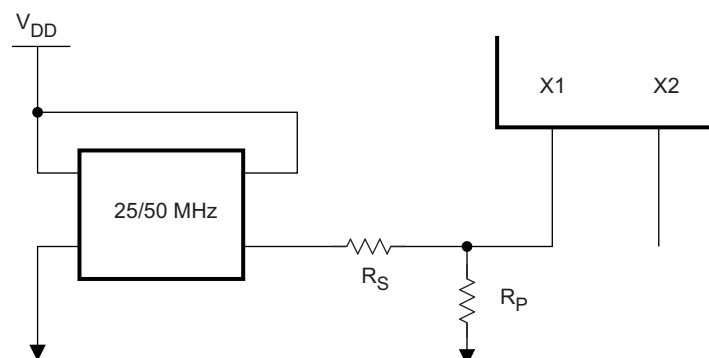
#### 5.1 External Oscillator Clock Source

If an oscillator is used, X1 should be tied to the clock source and X0 should be left floating. No series or load termination is required from the clock source, but may prove beneficial in some circumstances.

For EMI purposes, it may be beneficial to include series termination to limit the energy sourced from the oscillator. If series termination is used, the termination resistor should be placed as close to the oscillator output as possible on the PCB.

For longer traces, series termination coupled with matched parallel termination to ground and matched trace impedance may prove beneficial as well. If a parallel termination resistor is used, it should be placed as closely as possible to the X1 pin.

Connections for using an oscillator are shown in [Figure 10](#). Specifications for CMOS oscillators are listed in [Table 1](#).



**Figure 10. Oscillator Circuit**

## 5.2 Crystal Clock Source

For MII mode, the recommended crystal is a 25-MHz, parallel, 20-pF load crystal resonator. Figure 11 shows a typical circuit for a crystal resonator. The load capacitor values will vary with the crystal vendors; check with the vendor for load recommendations.

Approximate load capacitor values can be calculated by

$$2 \times \text{Crystal load spec} - 7 \text{ pF} = C_L$$

The oscillator circuit is designed to drive a parallel resonance AT cut crystal with a minimum drive level of 100  $\mu\text{W}$  and a maximum of 500  $\mu\text{W}$ . If a crystal is specified for a lower drive level, a current limiting resistor should be placed in series between XO and the crystal.

As a starting point for evaluating an oscillator circuit, if the requirements for the crystal are not known,  $C_{L1}$  and  $C_{L2}$  should be set at 33 pF, and  $R_1$  should be set at 0  $\Omega$ .

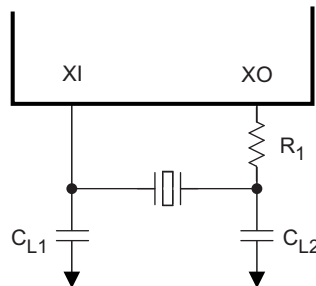


Figure 11. Crystal Oscillator Circuit

## 5.3 Oscillator or Crystal

The parametric specifications for utilizing an external oscillator are shown in Table 1 and Table 2.

The commonly used crystal is *AT cut* and fundamental frequency. This is the recommended type for TLK1XX components since *AT cut* exhibits the most frequency stability over a wide temperature range. The requirements for 25-MHz crystals are listed in Table 3.

In the case where multiple clock sources are needed, a high speed PLL clock distribution driver is recommended. The drivers may be obtained from vendors such as Texas Instruments, Pericom, and Integrated Device Technology. Consult vendor for specifics.

Table 1. 25-MHz Oscillator Requirements

Parameter	Test Conditions	MIN	TYP	MAX	Unit
Frequency			25		MHz
Frequency tolerance	Operational temperature			$\pm 50$	ppm
Frequency stability	1 year aging			$\pm 50$	ppm
Rise/Fall Time	10%–90%			8	ns
Jitter (short term)	Cycle-to-cycle		50		ps
Jitter (long term)	Accumulative over 10 ms			1	ns
Symmetry	Duty cycle	40%		60%	
Load capacitance			15	30	pF

Table 2. 50-MHz Oscillator Requirements

Parameter	Test Conditions	MIN	TYP	MAX	Unit
Frequency			50		MHz
Frequency tolerance	Operational temperature			$\pm 50$	ppm
Frequency stability	1 year aging			$\pm 50$	ppm
Rise/Fall Time	10%–90%			6	ns

**Table 2. 50-MHz Oscillator Requirements (continued)**

Parameter	Test Conditions	MIN	TYP	MAX	Unit
Jitter (short term)	Cycle-to-cycle		50		ps
Jitter (long term)	Accumulative over 10 ms			1	ns
Symmetry	Duty cycle	40%		60%	
Load capacitance			xx	xx	pF

**Table 3. 25-MHz Crystal Requirements**

Parameter	Test Conditions	MIN	TYP	MAX	Unit
Frequency			25		MHz
Frequency tolerance	Operational temperature			±50	ppm
	At 25°C			±50	ppm
Frequency stability	1 year aging			±5	ppm
Load capacitance		10		40	pF

## 6 LED and Non-LED Strap Pins

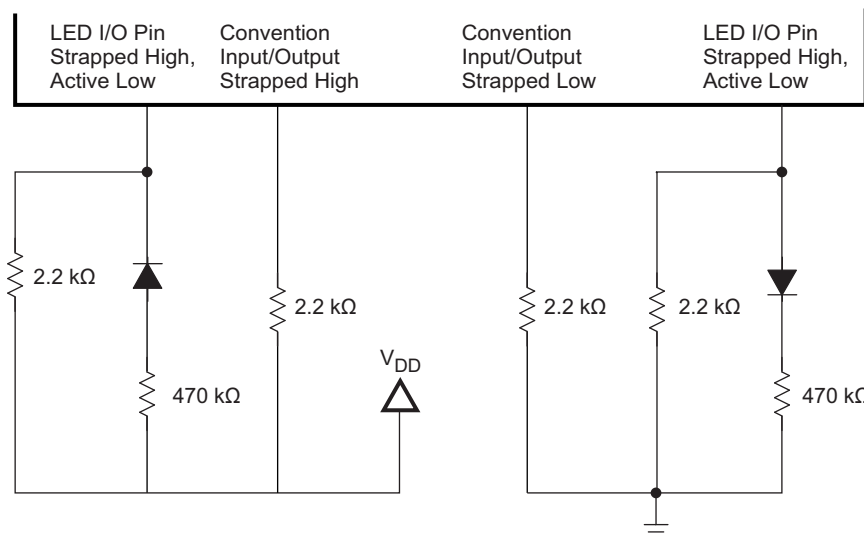
TLK1XX products support both conventional configuration strap input/output pins and multi-purpose Light Emitting Diode (LED) I/O pins. The LED pins can display the status of Link, Speed, Activity, or the presence of Collisions.

Many conventional strap I/O pins have high impedance (10 k to 20 k) default strap resistors present internal to the device. In order to overdrive these internal strap resistors, it is recommended that 2.2 kΩ resistors be used for selecting non-default strap options.

Additionally, even though the internal strap resistors are adequate for configuring the device in most applications, in some applications with noisy environments it is recommended that additional external 2.2 kΩ straps be used to select default options as well.

With regard to multi-purpose LED I/O pins, in order to achieve dual input/output functionality, the active state of each LED output driver is dependent on the input logic level sampled during power-up/reset. For example, if a multifunction LED pin is resistively pulled low, then the corresponding output is configured as active high. Conversely, if an input is resistively pulled high, then the corresponding output is configured as active low.

Figure 12 illustrates example of both conventional and multipurpose LED pin strap configurations.

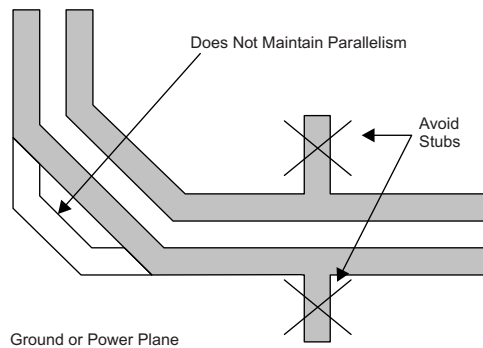


**Figure 12. Strapping and LED Loading Example**

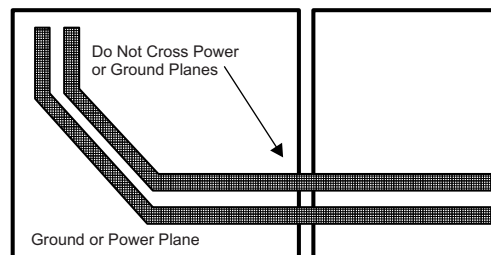
## 7 PCB Layout Considerations

- Place the 49.9-Ω, 1% resistors, and the decoupling capacitors, near the TLK1XX TD± and RD± pins and via directly to the V<sub>DD</sub> plane.
- Avoid stubs on all signal traces, especially the differential signal pairs. See [Figure 13](#).
- Within the pairs (for example, TD+ & TD-) the trace lengths should be run parallel to each other and matched in length. Matched lengths minimize delay differences, avoiding an increase in common mode noise and increased EMI. See [Figure 13](#).
- Ideally, there should be no crossover or via on the signal paths. Vias present impedance discontinuities and should be minimized. Route an entire trace pair on a single layer, if possible.
- Keep PCB trace lengths as short as possible.
- Signal traces should not be run such that they cross a plane split. See [Figure 14](#). A signal crossing a plane split may cause unpredictable return path currents and would likely impact signal quality as well, potentially creating EMI problems.
- MDI signal traces should have 50 Ω to ground or 100-Ω differential controlled impedance. Many tools are available online to calculate this, two are located here:

<http://www.emclab.umr.edu/pcbtlc/index.html>  
[http://www.ultracad/articles/diff\\_z.pdf](http://www.ultracad/articles/diff_z.pdf)



**Figure 13. Differential Signal Pair – Stubs**



**Figure 14. Differential Signal Pair – Plane Crossing**

Optimally, we would want to keep all the traces as short as possible. In those cases where it is not possible, spacings should have the following priority:

1. Distance between the PHY and the 50-Ω termination resistors.
2. Distance between the magnetic and the RJ-45.
3. Distance between the 50-Ω termination resistors and the magnetic.
4. Distance between the MAC and the PHY.

This gives the flexibility to make some adjustments, but hopefully minimizes the impact on performance.

## 7.1 Calculating Impedance

Use the following equations to calculate the differential impedance of the board.

### 7.1.1 Microstrip Impedance – Single-ended

$$Z_o = \left( \frac{87}{\sqrt{E_r + (1.41)}} \right) \ln \left( 5.98 \frac{H}{0.8W + T} \right) \quad (1)$$

W = Width of the trace  
 H = Height of dielectric above the return plane  
 T = Trace thickness  
 Er = Relative permittivity of the dielectric

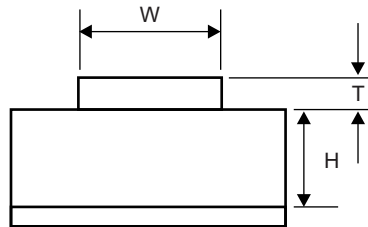


Figure 15. Microstrip Impedance – Single-Ended

### 7.1.2 Microstrip Impedance – Differential

$$Z_{diff} = 2Z_o \left( 1 - 0.48 \left( e^{\left( -0.96 \frac{S}{H} \right)} \right) \right) \quad (2)$$

W = Width of the trace  
 H = Height of dielectric above the return plane  
 T = Trace thickness  
 S = Space between traces  
 Er = Relative permittivity of the dielectric

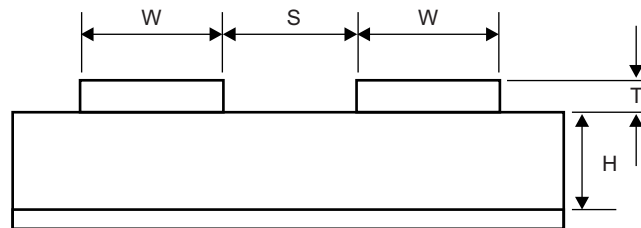


Figure 16. Microstrip Impedance – Differential

For microstrip traces, a solid ground plane is needed under the signal traces. The ground plane helps keep the EMI localized and the trace impedance continuous. Since stripline traces are typically sandwiched between the ground and supply planes, they have the advantage of lower EMI radiation and less noise coupling. The tradeoff of using strip line is a lower propagation speed.

### 7.1.3 Stripline Impedance – Single-ended

$$Z_o = \frac{60}{\sqrt{E_r}} \ln \left( 1.9 \frac{2H + T}{0.8W + T} \right) \quad (3)$$

W = Width of the trace

H = Height of the dielectric above the return plane

T = Trace thickness

Er = Relative permittivity of the dielectric

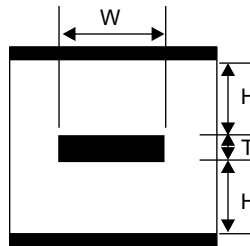


Figure 17. Stripline Impedance – Single-Ended

### 7.1.4 Stripline Impedance – Differential

$$Z_o = 2Z_o \left( 1 - 0.347 \left( e^{\left( -2.9 \frac{S}{H} \right)} \right) \right) \quad (4)$$

W = Width of the trace

H = Height of the dielectric above the return plane

T = Trace thickness

S = Space between traces

Er = Relative permittivity of the dielectric

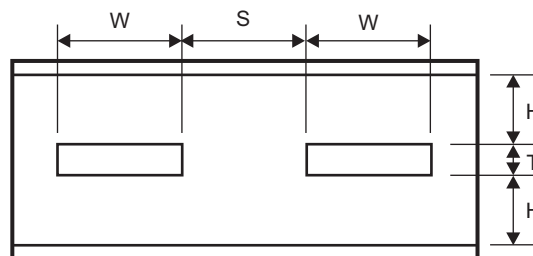
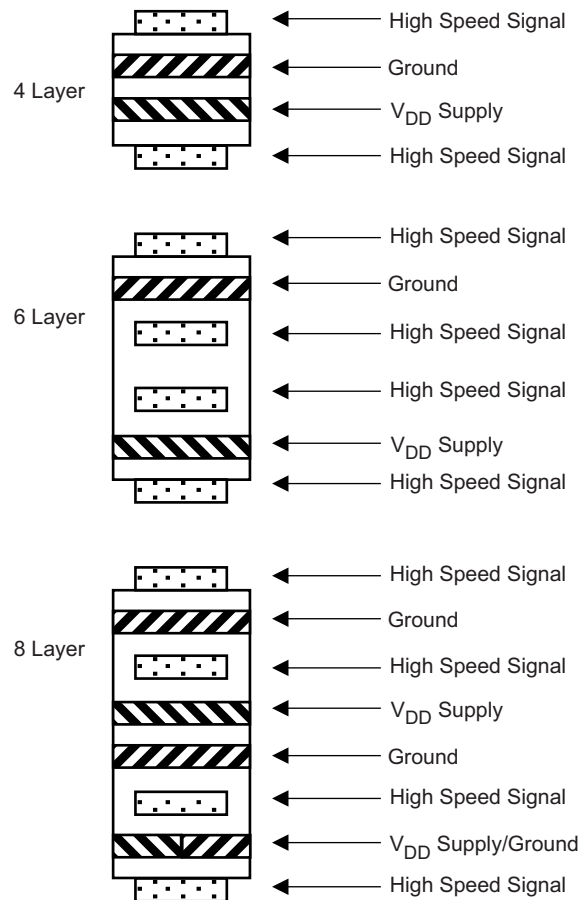


Figure 18. Stripline Impedance – Differential

## 7.2 PCB Layer Stacking

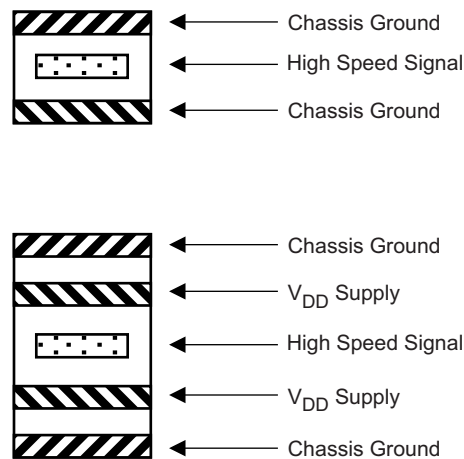
To meet signal integrity and performance requirements, at minimum a four layer PCB is recommended for implementing TLK1XX components in end-user systems. The following layer stack-ups are recommended for 4-, 6-, and 8-layer boards, although other options are possible.





**Figure 19. PCB Stripline Layer Stacking**

Within a PCB it may be desirable to run traces using different methods, microstrip vs. stripline, depending on the location of the signal on the PCB. For example, it may be desirable to change layer stacking where an isolated chassis ground plane is used. [Figure 20](#) illustrates alternative PCB stacking options.



**Figure 20. Alternative PCB Stripline Layer Stacking**

## 8 Magnetics

Within a design, the selection of certain components is very important in respect to the system performance. One of the main components among these is the magnetic. The magnetics have a large impact on the PHY performance. While several components are listed below, the TLK1XX maintains high performance with most existing on the shelf magnetics (RJ45 integrated or not), as long as they compatible with the requirements listed in Table 4. It is recommended that the magnetics include both an isolation transformer and an integrated common mode choke to reduce EMI. When doing the layout, do not run signals under the magnetics. This could cause unwanted noise crosstalk. Likewise, void the planes under discrete magnetics, helping to prevent common-mode noise coupling. To save board space and reduce component count, use an RJ-45 with integrated magnetics.

**Table 4. Magnetics Requirements**

Parameter	TYP	Units	Condition
Turn Ratio	1:1	–	±2%
Insertion Loss	–1	dB	1–100 MHz
Return Loss	–16	dB	1–30 MHz
	–12	dB	30–60 MHz
	–10	dB	60–80 MHz
Differential to common rejection ration	–30	dB	1–50 MHz
	–20	dB	50–150 MHz
Crosstalk	–35	dB	30 MHz
	–30	dB	60 MHz
Isolation	1,500	Vrms	HPOT

Recommended magnetics include:

**Table 5. Recommended Magnetics<sup>(1)</sup>**

Manufacturer	Part Number
Pulse Engineering, Inc.	HX1188
	HX1189

<sup>(1)</sup> Contact magnetics manufacturers for latest part numbers and product specifications. Thoroughly test and validate all magnetics before using them in production.

## 9 ESD Design Guidelines

### 9.1 Board Design Guidelines

The following list refers to guidelines of the external BOM system:

- Capacitors:
  - Solder a HV capacitor between RJ45 and the board GND (refer to [Figure 21](#))
  - Place the capacitor close to lines 1-2 (Channel A).
  - Capacitor value and DC rating has little effect (1.5–3.9 nF, 2 kV and above were used with no noticeable difference).
  - Capacitors on power supplies: 4 caps in parallel, values of 10  $\mu$ F, 1  $\mu$ F, 100 nF and 100 pF (refer to [figure 22](#)).
- Connect the shielding to earth ground as close to the RJ45 connector.
- While TLK supports a large variety of magnetics, it is recommended in some systems to use Pulse's H1198 magnetic (Opposite iso-magnetic architecture in comparison to H1188) with RJ45 without magnetic.

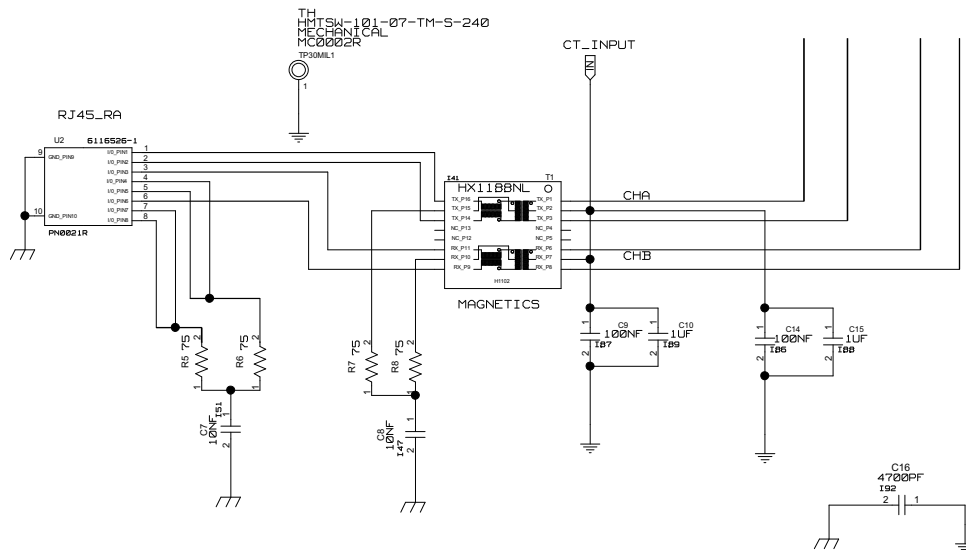
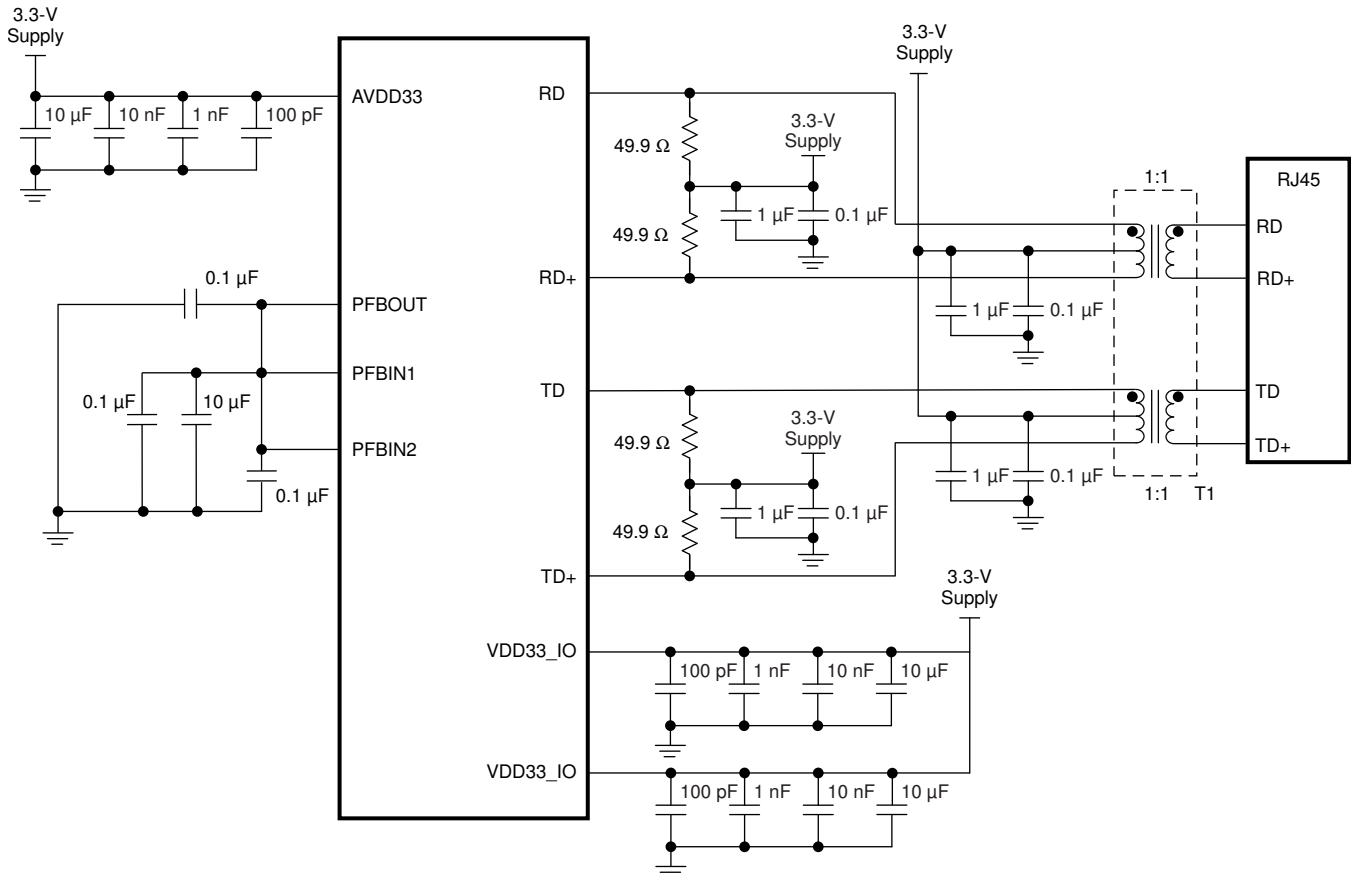


Figure 21. Grounds Separation


**Figure 22. Decoupling Capacitors**

## 9.2 Board Layout Guidelines

Board layout can make extensive enhancements to ESD immunity. To meet signal integrity and performance requirements, at minimum, a four-layer PCB is recommended for implementing TLK1XX components in end-user systems. Refer to [Figure 19](#) for layer stack-ups.

It is strongly recommended to separate the chassis and main ground by layer, as seen in [Figure 23](#).

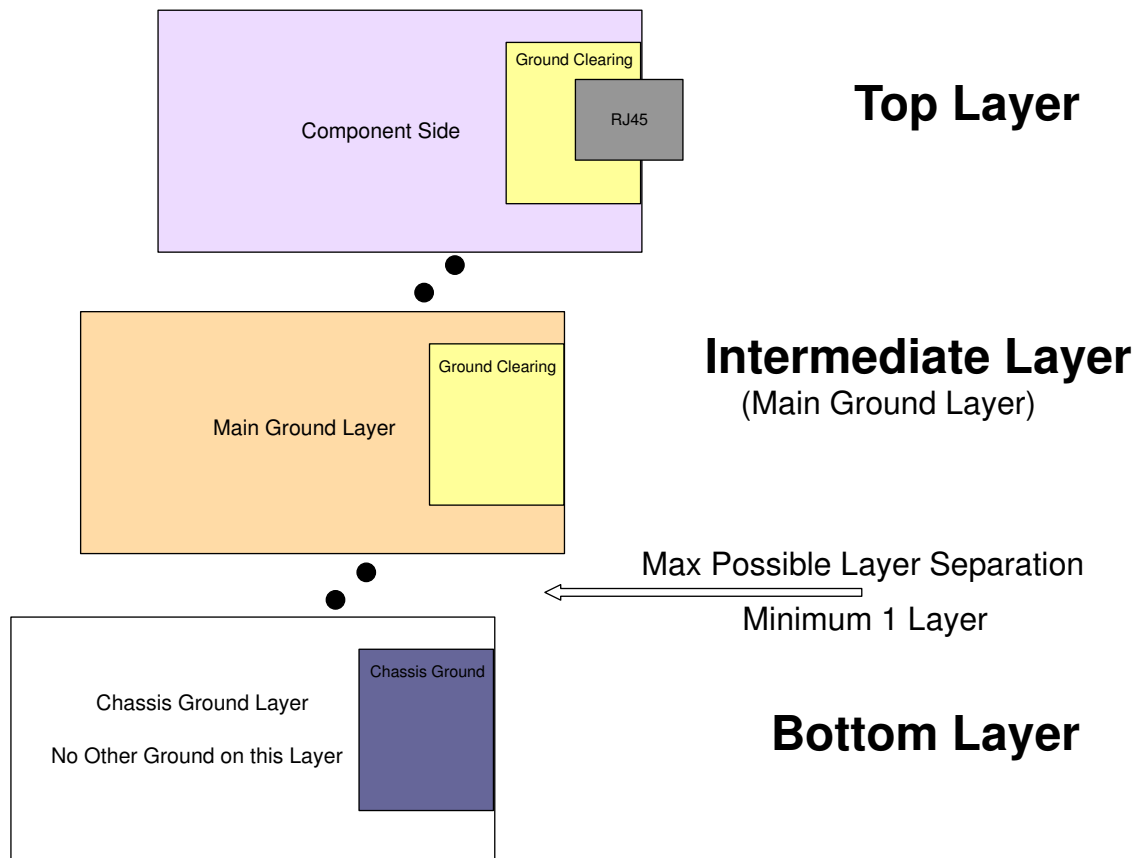


Figure 23. Layer Separation

Grounds and supplies should each have their own dedicated layer.

Please note, if one-layer separation was not possible after all (less recommended), and the RJ45 and main ground are on the same layer, they should be spaced as much as possible – at least 256 mil. Please see [Figure 24](#).

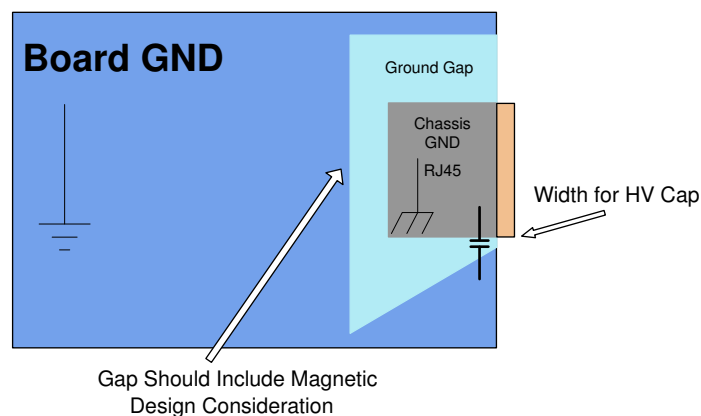


Figure 24. Grounds Layout Separation

The RJ45 ground must be hooked to enable direct connection from the board to the earth ground (this should be the ground connected to the earth ground during ESD test).

## 10 Reset Operation

TLK1XX products include an internal POR function and do not need to be explicitly reset after power up (except for the TLK100), for normal operation. If required during normal operation, the device can be reset by a hardware or a software reset.

### 10.1 Hardware Reset

A hardware reset (HW reset) is accomplished by applying a low pulse (CMOS level), with a duration of at least 1  $\mu$ S, to the RESET\_N. This resets the device such that all registers are re-initialized to default values and the hardware configuration values are re-latched into the device (similar to the power-up and reset operation).

### 10.2 POR\_BYPASS mode (TLK110 only)

This mode is mainly used if faster RESET and wake up (less than the 270 ms) time is required. This RESET is applied after power is ramped up (90% build up at least!). This mode is applicable if POR is at bypass. Connect PIN 20 to pull down (via 2.2-k $\Omega$  resistor). Release the RESET\_N pin 1 ms (minimum requirement) after power activation. The time from RESET\_N release to wake up is 1 ms.

### 10.3 Software Reset

A software reset is accomplished by setting the reset bit (bit 15) of the Basic Mode Control Register (BMCR). The period of time from setting the reset bit, to the time when software reset has concluded is approximately 1 ms.

In a software reset all the registers in the device are reset to default values and the hardware configuration values are maintained. Software driver code must wait 3 ms following a software reset before allowing further serial MII (MDIO/MDC) communications with the device.

## 11 Schematics Example

This section contains the TLK105 and TLK106 schematics.

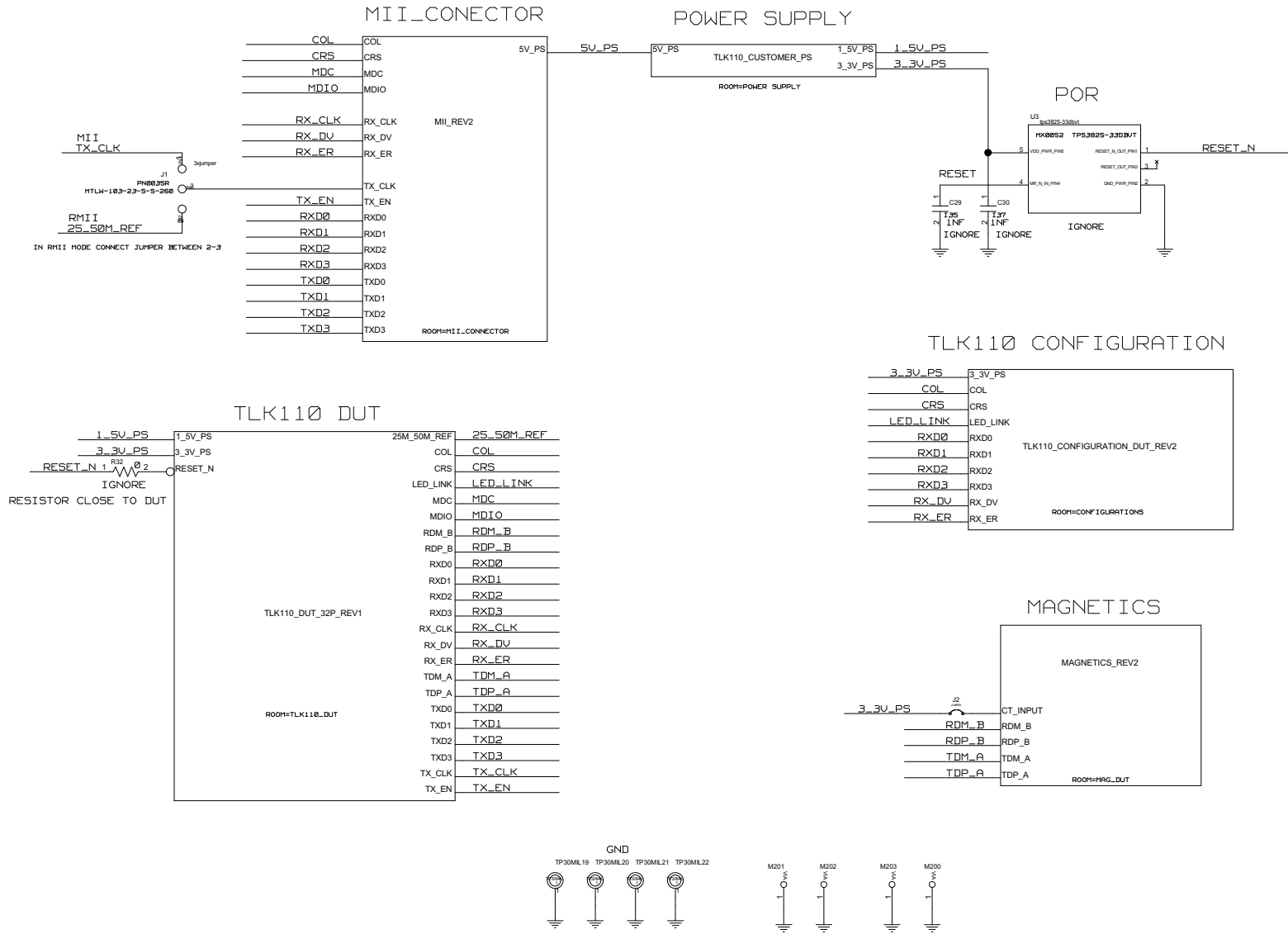


Figure 25. Schematic 1 of 6

# MAGNETICS

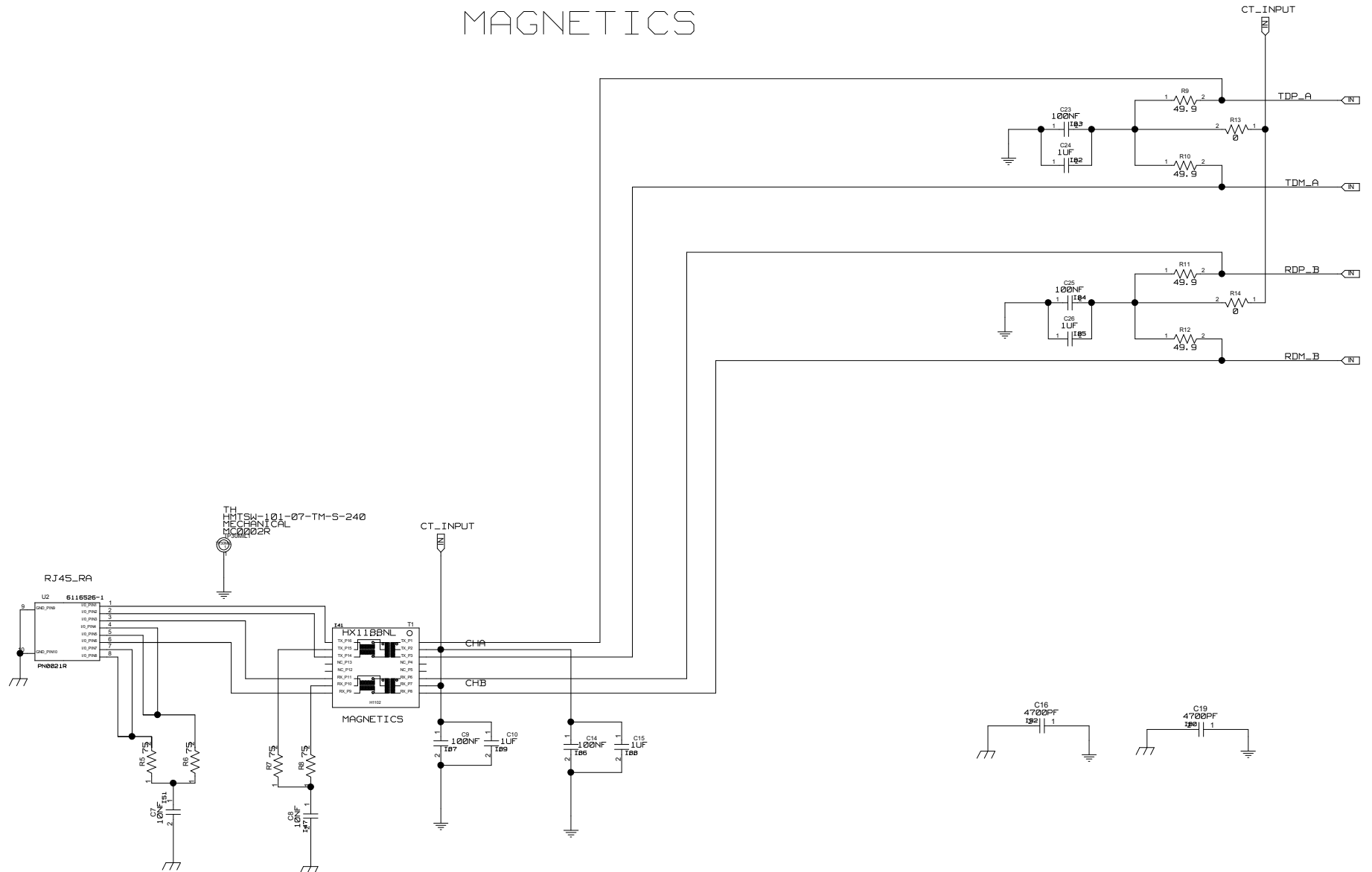


Figure 26. Schematic 2 of 6



+

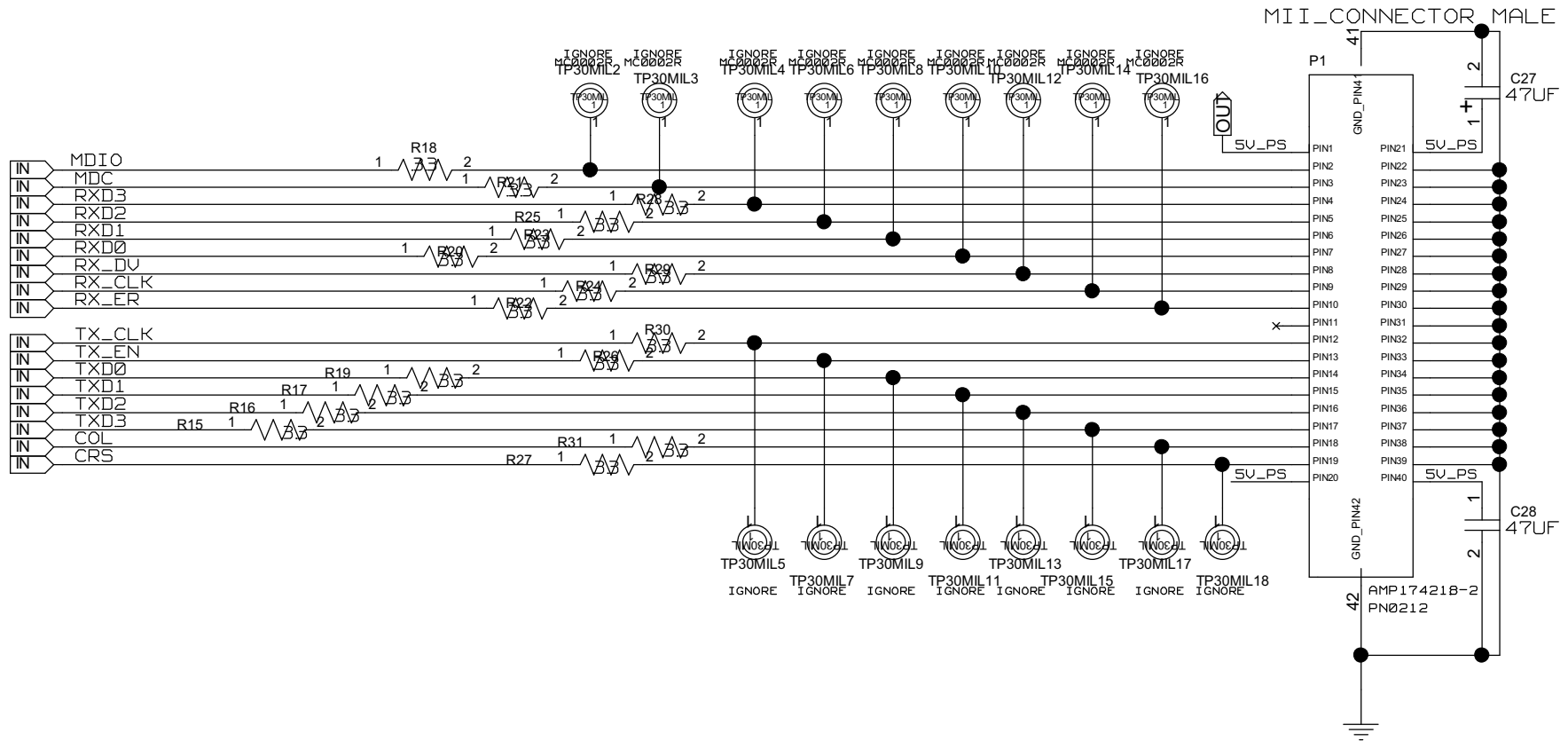


Figure 27. Schematic 3 of 6

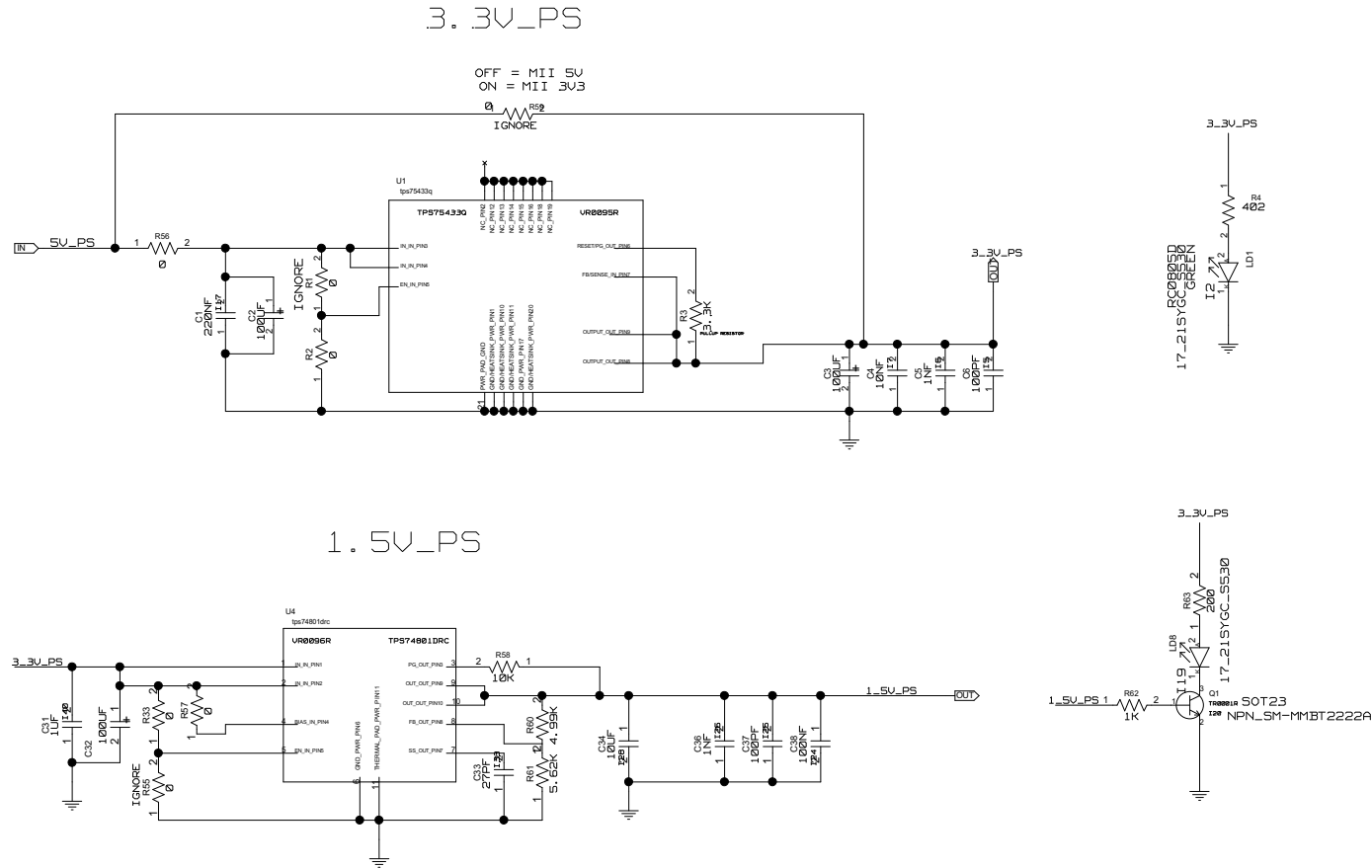


Figure 28. Schematic 4 of 6



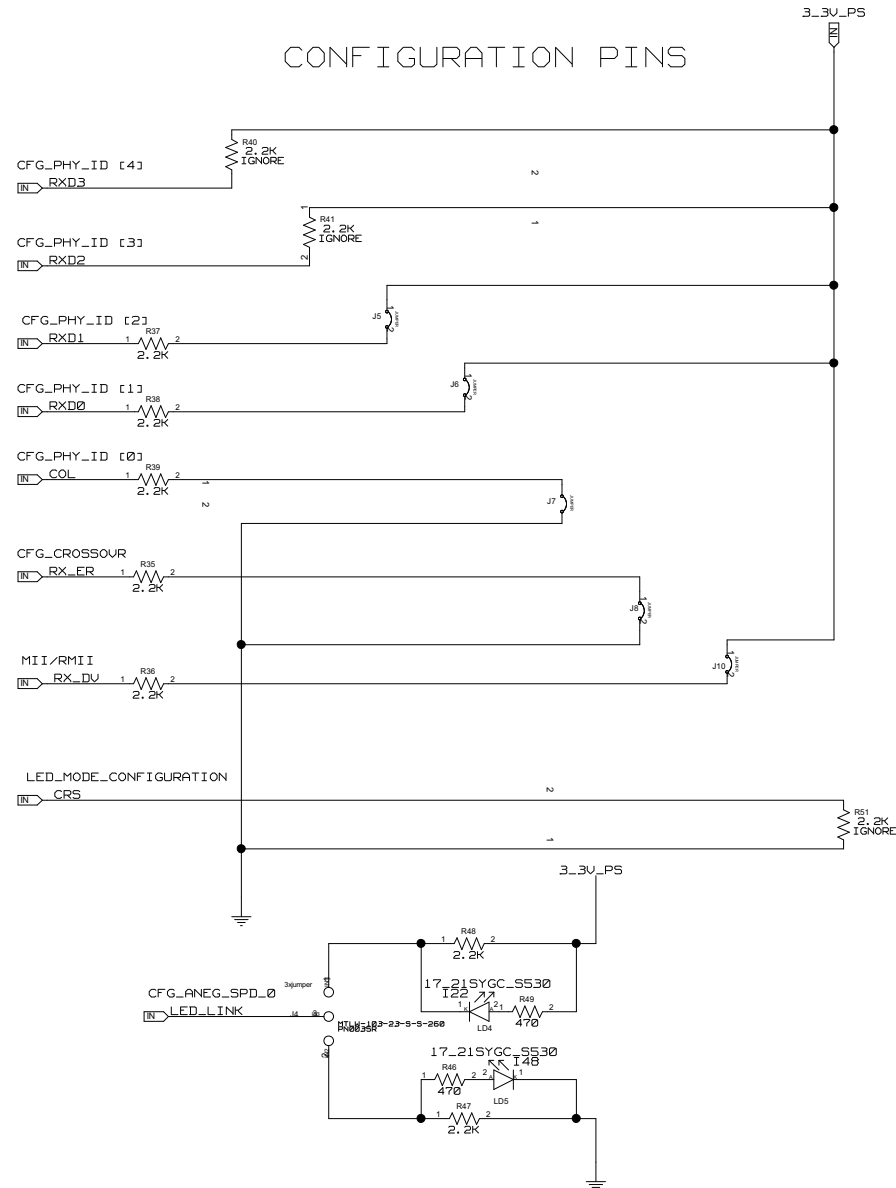


Figure 30. Schematic 6 of 6

## 12 Other Applicable Documents

Use the following documents in conjunction with this document, to assist in designing with the TLK1XX products:

- [TLK110 datasheet](#)
- TLK105 and TLK106 Data Sheet ([SLLSEB8](#))
- Transformerless application note ([SLLA327](#))
- PBO application note ([SLLA328](#))

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