









LMH6644-MIL

JAJSDE7 - JUNE 2017

# LMH6644-MIL 低消費電力、130MHz、75mA、レール・ツー・レール出 カアンプ

#### 1 特長

 $(V_S = \pm 5V, T_A = 25^{\circ}C, R_L = 2k\Omega, A_V = +1$ : 特記ない限り標準値)

- -3dB BW (A<sub>V</sub> = +1) 130 MHz
- 電源電圧範囲: 2.7V~12.8V
- スルー・レート (A<sub>V</sub> = -1) 130V/µs<sup>(1)</sup>
- 消費電流(無負荷) 2.7mA/アンプ
- 出力短絡電流: +115mA~145mA
- リニア出力電流: ±75mA
- 入力同相電圧が√よりも0.5V、V+よりも1V拡張
- 出力電圧スイングがレールから40mV
- 入力電圧ノイズ(100kHz): 17nV/√Hz
- 入力電流ノイズ(100kHz): 0.9pA/√Hz
- THD (5MHz,  $R_L = 2k\Omega$ ,  $V_O = 2V_{PP}$ ,  $A_V = +2$ ): -62dBc
- セトリング・タイム: 68ns
- 3V、5V、±5Vで完全に特性を規定
- オーバードライブ回復100ns
- 出力短絡保護<sup>(2)</sup>
- CMVR超過時に出力位相の反転なし

(1) スルー・レートは立ち上がりと立ち下がりのスルー・レートの平均値です。

 $^{(2)}$  出力短絡期間は、 $V_S < 6V$ で、室温またはそれ以下の気温の場合には無制限です。 $V_S > 6V$ の場合、許容される短絡期間は1.5msです。

# 2 アプリケーション

- アクティブ・フィルタ
- CD/DVD ROM
- ADCバッファ・アンプ
- ポータブル・ビデオ
- 電流センス・バッファ

#### 3 概要

LMH6644-MILは真の単一電源電圧帰還アンプで、高速 (130MHz)、低歪み(-62dBc)、非常に高い出力電流(約75mA)を低コストで実現し、同程度の性能を持つ既存の デバイスと比較して消費電力が低減されています。

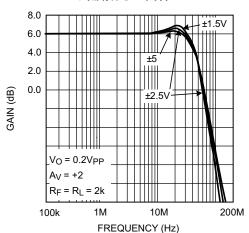
入力同相電圧範囲は、V-よりも0.5V下、V+から1Vまで拡張されています。出力電圧範囲は双方の電源レールの40mV以内まで拡張されているため、低電圧アプリケーションで特に望ましい、広いダイナミック・レンジが得られます。出力段は約75mAの能力を持ち、重負荷を駆動可能です。出力スルー・レートが高い(130V/μs)ため、速度が高い場合も大きなピーク・ツー・ピーク出力スイングを維持でき、3V電源から40MHzという非常に優れたフルパワー帯域幅を実現できます。これらの特性と低コストから、多くの産業用および商業用アプリケーションに理想的です。

### 製品情報(1)

型番	パッケージ	本体サイズ(公称)
LMH6644-MIL	SOIC (14)	8.64mm×3.91mm
LIVINO044-IVIIL	TSSOP (14)	5.00mm×4.40mm

(1) 利用可能なすべてのパッケージについては、このデータシートの末 尾にある注文情報を参照してください。

### 各種の電源における閉ループ・ゲインと 周波数との関係







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# 4 改訂履歴

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

日付	改訂内容	注
2017年6月	*	初版



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### 5 概要(続き)

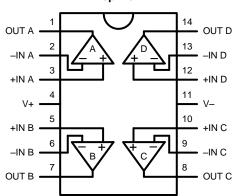
あらゆる動作電圧とモードにおいてデバイスの安定性を保証するため、十分な注意が払われています。その結果、あらゆる ゲイン設定で、重負荷と軽負荷の両方において、周波数応答特性が非常に優れ(150 $\Omega$ 負荷および $A_V = +2$ において、 12MHzまで0.1dBのゲイン平坦性)、ピーキングが最小限(一般に最大値2dB)です。これらの特性と、短いセトリング・タイム (68ns)、低い歪みから、このデバイスはADCバッファでも、高周波数のフィルタ・アプリケーションでも適切に動作します。

このデバイスは、低い差動ゲイン(0.01%)と差動位相(0.01°)の特性から、プロフェッショナル品質のビデオ性能を実現して います。差動ゲインおよび差動位相の特性は、重負荷時(150Ω)でも、出力電圧範囲の全体にわたって適切に維持されま す。



# 6 Pin Configuration and Functions

### Package D14A, PW14A 14-Pin SOIC and 14-Pin TSSOP Top View



#### **Pin Functions**

PIN I/O		1/0	DESCRIPTION
NAME	NO.	1/0	DESCRIPTION
-IN A	2	I	ChA inverting input
+IN A	3	I	ChA non-inverting input
–IN B	6	1	ChB inverting input
+IN B	5	1	ChB non-inverting input
–IN C	9	I	ChC inverting input
+IN C	10	I	ChC non-inverting input
–IN D	13	I	ChD inverting input
+IN D	12	1	ChD non-inverting input
OUT A	1	0	ChA output
OUT B	7	0	ChB output
OUT C	8	0	ChC output
OUT D	14	0	ChD output
V <sup>-</sup>	11	1	Negative supply
V <sup>+</sup>	4	I	Positive supply



### **Specifications**

# 7.1 Absolute Maximum Ratings<sup>(1)(2)</sup>

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT	
V <sub>IN</sub> differential			±2.5	V	
Output short circuit duration		See (3)	and <sup>(4)</sup>		
Supply voltage (V <sup>+</sup> – V <sup>-</sup> )			13.5	V	
Voltage at input/output pins			V <sup>+</sup> +0.8 V <sup>-</sup> -0.8		
Input current			±10	mA	
Junction temperature <sup>(5)</sup>			+150	°C	
Coldering information	Infrared or convection reflow (20 s)		235	°C	
Soldering information	Wave soldering lead temperature (10 s)		260	°C	
Storage temperature range, T <sub>stg</sub>		-65 +150 °			

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications and the test conditions, see the Electrical Characteristics.
- If Military/Aerospace specified devices are required, please contact the TI Sales Office/Distributors for availability and specifications.
- Applies to both single-supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature can result in exceeding the maximum allowed junction temperature of 150°C.
- Output short circuit duration is infinite for  $V_S$  < 6V at room temperature and below. For  $V_S$  > 6V, allowable short circuit duration is 1.5ms.
- The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $R_{\theta JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/R_{\theta JA}$ . All numbers apply for packages soldered directly onto a PC board.

#### 7.2 ESD Ratings

			VALUE	UNIT
		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins (2)	2000	
V <sub>(ESD)</sub>	Electrostatic discharge (1)	Machine model (MM) <sup>(3)</sup>	200	V
* (ESD)	Elocitostatio disortargo	Charged-device model (CDM), per JEDEC specification JESD22-C101, all pins (4)	1000	· ·

- Human body model, 1.5 k $\Omega$  in series with 100 pF. Machine Model, 0  $\Omega$  in series with 200 pF.
- JEDEC document JEP155 states that 2000-V HBM allows safe manufacturing with a standard ESD control process.
- JEDEC document JEP157 states that 200-V MM allows safe manufacturing with a standard ESD control process.
- JEDEC document JEP157 states that 1000-V CDM allows safe manufacturing with a standard ESD control process.

## 7.3 Recommended Operating Conditions<sup>(1)</sup>

over operating free-air temperature range (unless otherwise noted)

	MIN	MAX	UNIT
Supply voltage (V <sup>+</sup> – V <sup>-</sup> )	2.7	12.8	V
Operating temperature range <sup>(2)</sup>	-40	+85	°C

- Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications and the test conditions, see the Electrical Characteristics.
- The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $R_{\theta JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} T_A)/R_{\theta JA}$ . All numbers apply for packages soldered directly onto a PC board.

#### 7.4 Thermal Information

		LMH664	4-MIL	
	THERMAL METRIC <sup>(1)</sup>	D14A	PW14A	UNIT
		14 PINS	14 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance (2)	145	155	°C/W

- For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.
- The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $R_{\theta JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} T_A) / R_{\theta JA}$ . All numbers apply for packages soldered directly onto a PC board.



#### 7.5 3-V Electrical Characteristics

Unless otherwise specified, all limits ensured for  $V^+ = 3 \text{ V}, V^- = 0 \text{ V}, V_{CM} = V_O = V^+/2, V_{ID}$  (input differential voltage) as noted (where applicable) and  $R_L = 2 \text{ k}\Omega$  to  $V^+/2$ 

PA	ARAMETER	TEST CONDITIONS	AT TEMPERATURE EXTREMES			V <sub>CM</sub> =	3 V, V <sup>-</sup> = V <sub>O</sub> = V <sup>+</sup> /2 2 kΩ to \	2, V <sub>ID</sub>	UNIT
			MIN	TYP	MAX	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>	
BW	–3-dB BW	$A_V = +1, V_{OUT} = 200 \text{mV}_{PP}$				80	115		MHz
DVV	-3-ub bvv	$A_V = +2, -1, V_{OUT} = 200 \text{mV}_{PP}$					46		IVII IZ
BW <sub>0.1dB</sub>	0.1-dB gain flatness	$\begin{aligned} &A_V = +2, \ R_L = 150\Omega \ to \ V+/2, \\ &Rf = 402\Omega, \ V_{OUT} = 200 mV_{PP} \end{aligned}$					19		MHz
PBW	Full power bandwidth	$A_V = +1, -1dB, V_{OUT} = 1V_{PP}$					40		MHz
•	Input-referred	f = 100kHz					17		nV/√ <del>Hz</del>
e <sub>n</sub>	voltage noise	f = 1kHz					48		IIV/ VIIZ
	Input-referred	f = 100kHz					0.90		pA/√Hz
i <sub>n</sub>	current noise	f = 1kHz					3.3		pAV VITZ
THD	Total harmonic distortion	$f = 5MHz$ , $V_O = 2V_{PP}$ , $A_V = -1$ , $R_L = 100\Omega$ to $V^+/2$					-48		dBc
DG	Differential gain	$V_{CM} = 1V$ , NTSC, $A_V = +2$ $R_L = 150\Omega$ to $V^+/2$					0.17%		
	3	$R_L = 1k\Omega$ to V <sup>+</sup> /2					0.03%		
DP	Differential	$V_{CM} = 1V$ , NTSC, $A_V = +2$ $R_L = 150\Omega$ to $V^+/2$					0.05		deg
	phase	$R_L = 1k\Omega$ to $V^+/2$					0.03		ŭ
CT Rej.	Cross-talk rejection	f = 5MHz, receiver: $R_f = R_g = 510\Omega$ , $A_V = +2$					47		dB
T <sub>S</sub>	Settling time	$V_{O} = 2V_{PP}$ , ±0.1%, 8pF Load, $V_{S} = 5V$					68		ns
SR	Slew rate (3)	$A_V = -1, V_I = 2V_{PP}$				90	120		V/µs
V <sub>OS</sub>	Input offset voltage				±7		±1	±5	mV
TC V <sub>OS</sub>	Input offset average drift	See (4)					±5		μV/°C
I <sub>B</sub>	Input bias current	See <sup>(5)</sup>			-3.25		-1.50	-2.60	μΑ
Ios	Input offset current				1000		20	800	nA
R <sub>IN</sub>	Common-mode input resistance						3		ΜΩ

<sup>(1)</sup> All limits are ensured by testing or statistical analysis.(2) Typical values represent the most likely parametric norm.

Slew rate is the average of the rising and falling slew rates.

Offset voltage average drift determined by dividing the change in V<sub>OS</sub> at temperature extremes by the total temperature change. Positive current corresponds to current flowing into the device.



3-V Electrical Characteristics (continued)

Unless otherwise specified, all limits ensured for V<sup>+</sup> = 3 V, V<sup>-</sup> = 0 V,  $V_{CM} = V_O = V^+/2$ ,  $V_{ID}$  (input differential voltage) as noted (where applicable) and  $R_L = 2 k\Omega$  to V<sup>+</sup>/2

PARAMETER		TEST CONDITIONS	TEST CONDITIONS  AT TEMPERATURE EXTREMES			V <sub>CM</sub> =	3 V, V <sup>-</sup> = 0 V <sub>O</sub> = V <sup>+</sup> /2 2 kΩ to V	2, V <sub>ID</sub>	UNIT
			MIN	TYP	MAX	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>	
C <sub>IN</sub>	Common-mode input capacitance						2		pF
CMVR	Input common- mode voltage range	CMRR ≥ 50dB	1.6		-0.1	1.8	-0.5 2.0	-0.2	V
CMRR	Common-mode rejection ratio	V <sub>CM</sub> Stepped from 0V to 1.5V				72	95		dB
	Large signal voltage gain	$V_{O} = 0.5V \text{ to } 2.5V$ $R_{L} = 2k\Omega \text{ to } V^{+}/2$	75			80	96		dB
A <sub>VOL</sub>		$V_{O} = 0.5V \text{ to } 2.5V$ $R_{L} = 150\Omega \text{ to } V^{+}/2$	70			74	82		aв
	Output swing	$R_L = 2k\Omega$ to V <sup>+</sup> /2, $V_{ID} = 200$ mV				2.90	2.98		V
.,	high	$R_L = 150\Omega$ to V <sup>+</sup> /2, $V_{ID} = 200$ mV				2.80	2.93		V
Vo	Output swing	$R_L = 2k\Omega$ to V <sup>+</sup> /2, $V_{ID} = -200$ mV					25	75	mV
	low	$R_L = 150\Omega$ to V <sup>+</sup> /2, $V_{ID} = -200$ mV					75	150	IIIV
	Output short	Sourcing to V <sup>+</sup> /2 V <sub>ID</sub> = 200mV <sup>(6)</sup>	35			50	95		A
I <sub>SC</sub>	circuit current	Sinking to V <sup>+</sup> /2 $V_{ID} = -200 \text{mV}^{(6)}$	40			55	110		mA
I <sub>OUT</sub>	Output current	V <sub>OUT</sub> = 0.5V from either supply					±65		mA
+PSRR	Positive power supply rejection ratio	$V^{+} = 3.0V$ to 3.5V, $V_{CM} = 1.5V$			_	75	85	_	dB
I <sub>S</sub>	Supply current (per channel)	No load			4.50		2.70	4.00	mA

<sup>(6)</sup> Short circuit test is a momentary test. See Note 7 under 5-V Electrical Characteristics.

# **STRUMENTS**

# 7.6 5-V Electrical Characteristics

Unless otherwise specified, all limits ensured for V<sup>+</sup> = 5 V, V<sup>-</sup> = 0 V, V<sub>CM</sub> = V<sub>O</sub> = V<sup>+</sup>/2, V<sub>ID</sub> (input differential voltage) as noted (where applicable) and R<sub>L</sub> = 2 k $\Omega$  to V<sup>+</sup>/2

`	plicable) and $R_L =$ ARAMETER	TEST CONDITIONS		EMPERAT XTREME	_	$V^{+} = 5 \text{ V}, V^{-} = 0 \text{ V},$ $V_{CM} = V_{O} = V^{+}/2, V_{ID}$ $R_{L} = 2 \text{ k}\Omega \text{ to } V^{+}/2$		UNIT	
			MIN	TYP	MAX	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>	
BW	–3-dB BW	$A_V = +1$ , $V_{OUT} = 200 \text{mV}_{PP}$				90	120		MHz
DW	3 db bw	$A_V = +2, -1, V_{OUT} = 200 \text{mV}_{PP}$					46		IVII IZ
BW <sub>0.1dB</sub>	0.1-dB gain flatness	$A_V = +2$ , $R_L = 150\Omega$ to V+/2, $R_f = 402\Omega$ , $V_{OUT} = 200 \text{mV}_{PP}$					15		MHz
PBW	Full power bandwidth	$A_V = +1, -1dB, V_{OUT} = 2V_{PP}$					22		MHz
	Input-referred	f = 100kHz					17		2)//s/II=
e <sub>n</sub>	voltage noise	f = 1kHz					48		nV/√Hz
:	Input-referred	f = 100kHz					0.90		pA/√Hz
i <sub>n</sub>	current noise	f = 1kHz					3.3		pA/ VHZ
THD	Total harmonic distortion	$f = 5MHz, V_O = 2V_{PP}, A_V = +2$					-60		dBc
DG	Differential gain	NTSC, $A_V = +2$ $R_L = 150\Omega$ to $V^+/2$					0.16%		
-	3 2 2 3	$R_L = 1k\Omega$ to V <sup>+</sup> /2					0.05%		
DP	Differential	NTSC, $A_V = +2$ $R_L = 150\Omega$ to V <sup>+</sup> /2					0.05		deg
	phase	$R_L = 1k\Omega$ to V <sup>+</sup> /2					0.01		
CT Rej.	Cross-talk rejection	f = 5MHz, receiver: $R_f = R_g = 510\Omega$ , $A_V = +2$					47		dB
T <sub>S</sub>	Settling time	V <sub>O</sub> = 2V <sub>PP</sub> , ±0.1%, 8pF Load					68		ns
SR	Slew rate (3)	$A_V = -1$ , $V_I = 2V_{PP}$				95	125		V/µs
V <sub>OS</sub>	Input offset voltage				±7		±1	±5	mV
TC V <sub>OS</sub>	Input offset average drift	See <sup>(4)</sup>					±5		μV/°C
I <sub>B</sub>	Input bias current	See <sup>(5)</sup>			-3.25		-1.70	-2.60	μΑ
I <sub>OS</sub>	Input offset current				1000		20	800	nA
R <sub>IN</sub>	Common-mode input resistance						3		ΜΩ
C <sub>IN</sub>	Common-mode input capacitance						2		pF
CMVR	Input common- mode voltage	CMRR ≥ 50dB	3.6		-0.1	3.8	-0.5 4.0	-0.2	V
CMRR	range Common-mode rejection ratio	V <sub>CM</sub> Stepped from 0V to 3.5V	0.0			72	95		dB
	•	$V_{O} = 0.5V \text{ to } 4.50V$ $R_{L} = 2k\Omega \text{ to } V^{+}/2$	82			86	98		
A <sub>VOL</sub>	Large signal voltage gain	$R_L = 2K\Omega$ to $V/2$ $V_O = 0.5V$ to $4.25V$ $R_L = 150\Omega$ to $V^+/2$	72			76	82		dB

All limits are ensured by testing or statistical analysis.

Typical values represent the most likely parametric norm. Slew rate is the average of the rising and falling slew rates. (3)

Offset voltage average drift determined by dividing the change in VOS at temperature extremes by the total temperature change.

<sup>(5)</sup> Positive current corresponds to current flowing into the device.



5-V Electrical Characteristics (continued)

Unless otherwise specified, all limits ensured for V<sup>+</sup> = 5 V, V<sup>-</sup> = 0 V, V<sub>CM</sub> = V<sub>O</sub> = V<sup>+</sup>/2, V<sub>ID</sub> (input differential voltage) as noted (where applicable) and R<sub>L</sub> = 2 k $\Omega$  to V<sup>+</sup>/2

PARAMETER		TEST CONDITIONS	AT TEMPERATURE EXTREMES		V <sub>CM</sub> =	5 V, V <sup>-</sup> = 0 V <sub>O</sub> = V <sup>+</sup> /2 2 kΩ to V	, V <sub>ID</sub>	UNIT	
			MIN	TYP	MAX	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>	
	Output swing	$R_L = 2k\Omega$ to V <sup>+</sup> /2, $V_{ID} = 200$ mV				4.90	4.98		V
V	high	$R_L = 150\Omega$ to V <sup>+</sup> /2, $V_{ID} = 200$ mV				4.65	4.90		V
Vo	Output swing	$R_L = 2k\Omega$ to V <sup>+</sup> /2, $V_{ID} = -200$ mV					25	100	m\/
low	low	$R_L = 150\Omega$ to V <sup>+</sup> /2, $V_{ID} = -200$ mV					100	150	mV
	Output short	Sourcing to V <sup>+</sup> /2 V <sub>ID</sub> = 200mV <sup>(6)(7)</sup>	40			55	115		A
I <sub>SC</sub>	circuit current	Sinking to V <sup>+</sup> /2 V <sub>ID</sub> = $-200$ mV <sup>(6)(7)</sup>	55			70	140		mA
I <sub>OUT</sub>	Output current	V <sub>O</sub> = 0.5V from either supply					±70		mA
+PSRR	Positive power supply rejection ratio	V <sup>+</sup> = 4.0V to 6V				79	90		dB
Is	Supply current (per channel)	No load			5.00		2.70	4.25	mA

Short circuit test is a momentary test. See Note 7. Output short circuit duration is infinite for  $V_S < 6V$  at room temperature and below. For  $V_S > 6V$ , allowable short circuit duration is 1.5ms.



# **STRUMENTS**

#### 7.7 ±5-V Electrical Characteristics

Unless otherwise specified, all limits ensured for  $V^+ = 5 \text{ V}$ ,  $V^- = -5 \text{ V}$ ,  $V_{CM} = V_O = 0 \text{ V}$ ,  $V_{ID}$  (input differential voltage) as noted (where applicable) and  $R_1 = 2 k\Omega$  to ground

PARAMETER		TEST CONDITIONS	AT TEMPERATURE EXTREMES			$V^{+} = 5 V, V^{-} = -5 V,$ $V_{CM} = V_{O} = 0 V, V_{ID}$			UNIT	
			MIN	TYP	MAX	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>		
BW –3-dB BW		$A_V = +1$ , $V_{OUT} = 200$ m $V_{PP}$				95	130		MHz	
		$A_V = +2, -1, V_{OUT} = 200 \text{mV}_{PP}$					46		IVITIZ	
BW <sub>0.1dB</sub>	0.1-dB gain flatness	$\begin{aligned} A_V &= +2, \ R_L = 150\Omega \text{ to V+/2}, \\ R_f &= 806\Omega, \ V_{OUT} = 200\text{mV}_{PP} \end{aligned}$					12		MHz	
PBW	Full power bandwidth	$A_V = +1, -1dB, V_{OUT} = 2V_{PP}$					24		MHz	
e <sub>n</sub>	Input-referred	f = 100kHz					17		nV/√ <del>Hz</del>	
	voltage noise	f = 1kHz					48			
i <sub>n</sub>	Input-referred	f = 100kHz					0.90		pA/√ <del>Hz</del>	
current noise		f = 1kHz	Hz		3.3			P/ / 11 12		
THD	Total harmonic distortion	$f = 5MHz, V_O = 2V_{PP}, A_V = +2$					-62		dBc	
DG Differential gain		NTSC, $A_V = +2$ $R_L = 150\Omega$ to $V^+/2$					0.15%			
		$R_L = 1k\Omega$ to $V^+/2$					0.01%			
DP	DP Differential phase	NTSC, $A_V = +2$ $R_L = 150\Omega$ to V <sup>+</sup> /2					0.04		deg	
		$R_L = 1k\Omega$ to $V^+/2$					0.01			
CT Rej.	Cross-talk rejection	f = 5MHz, receiver: $R_f = R_g = 510\Omega$ , $A_V = +2$					47		dB	
T <sub>S</sub>	Settling time	$V_{O} = 2V_{PP}$ , ±0.1%, 8pF Load, $V_{S} = 5V$					68		ns	
SR	Slew rate (3)	$A_V = -1$ , $V_I = 2V_{PP}$				100	135		V/µs	
V <sub>OS</sub>	Input offset voltage				±7		±1	±5	mV	
TC V <sub>OS</sub>	Input offset average drift	See <sup>(4)</sup>					±5		μV/°C	
I <sub>B</sub>	Input bias current	See (5)			-3.25		-1.60	-2.60	μΑ	
I <sub>OS</sub>	Input offset current				1000		20	800	nA	
R <sub>IN</sub>	Common-mode input resistance						3		МΩ	
C <sub>IN</sub>	Common-mode input capacitance						2		pF	
0111/5	Input common-				-5.1		-5.5	-5.2		
CMVR	mode voltage range	CMRR ≥ 50dB	3.6			3.8	4.0		V	
CMRR	Common-mode rejection ratio	V <sub>CM</sub> Stepped from –5V to 3.5V				74	95		dB	

<sup>(2)</sup> 

All limits are ensured by testing or statistical analysis.

Typical values represent the most likely parametric norm.

Slew rate is the average of the rising and falling slew rates.

Offset voltage average drift determined by dividing the change in VOS at temperature extremes by the total temperature change.

Positive current corresponds to current flowing into the device.



±5-V Electrical Characteristics (continued)

Unless otherwise specified, all limits ensured for V<sup>+</sup> = 5 V, V<sup>-</sup> = -5 V, V<sub>CM</sub> = V<sub>O</sub> = 0 V, V<sub>ID</sub> (input differential voltage) as noted (where applicable) and  $R_L = 2 k\Omega$  to ground

PARAMETER		TEST CONDITIONS	AT TEMPERATURE EXTREMES			$V^{+} = 5 V, V^{-} = -5 V,$ $V_{CM} = V_{O} = 0 V, V_{ID}$			UNIT	
			MIN TYP MAX		MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>			
A <sub>VOL</sub>	Large signal	$V_O = -4.5V$ to 4.5V, $R_L = 2k\Omega$	84			88	96		dB	
	voltage gain	$V_O = -4.0V$ to 4.0V, $R_L = 150\Omega$	74			78	82		uБ	
Vo	Output swing	$R_L = 2k\Omega$ , $V_{ID} = 200mV$				4.90	4.96		V	
	high	$R_L = 150\Omega, V_{ID} = 200 \text{mV}$				4.65	4.80		V	
	Output swing	$R_L = 2k\Omega$ , $V_{ID} = -200$ mV		-4		-4.96	-4.90	V		
	low	$R_L = 150\Omega, V_{ID} = -200 \text{mV}$					-4.80	-4.65	V	
Isc	Output short	Sourcing to ground $V_{ID} = 200 \text{mV}^{(6)(7)}$	35			60	115		m ^	
	circuit current	Sinking to ground $V_{ID} = -200 \text{mV}^{(6)(7)}$	65			85	145		mA	
I <sub>OUT</sub>	Output current	$V_O = 0.5V$ from either supply				±75			mA	
PSRR	Power supply rejection ratio	$(V^+, V^-) = (4.5V, -4.5V)$ to $(5.5V, -5.5V)$				78	90		dB	
Is	Supply current (per channel)	No load			5.50		2.70	4.50	mA	

 <sup>(6)</sup> Short circuit test is a momentary test. See <sup>(7)</sup>.
 (7) Output short circuit duration is infinite for V<sub>S</sub> < 6V at room temperature and below. For V<sub>S</sub> > 6V, allowable short circuit duration is 1.5ms.

# TEXAS INSTRUMENTS

## 7.8 Typical Performance Characteristics

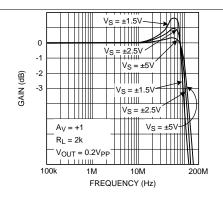
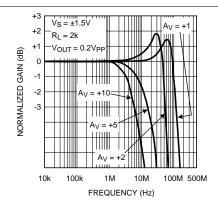


Figure 1. Closed Loop Frequency Response for Various Supplies

Figure 2. Closed Loop Gain vs Frequency for Various Gain



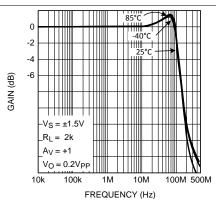
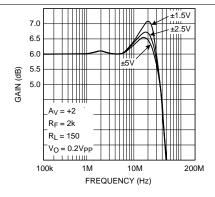


Figure 3. Closed Loop Gain vs Frequency for Various Gain

Figure 4. Closed Loop Frequency Response for Various Temperature



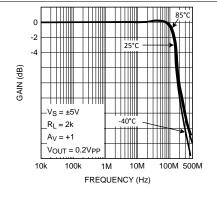


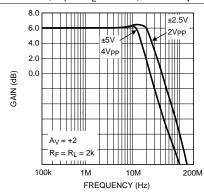
Figure 5. Closed Loop Gain vs Frequency for Various Supplies

Figure 6. Closed Loop Frequency Response for Various Temperature



# **Typical Performance Characteristics (continued)**

 $V^+$  = +5 V,  $V^-$  = -5 V,  $R_F$  =  $R_L$  = 2 k $\Omega$ , unless specified otherwise.



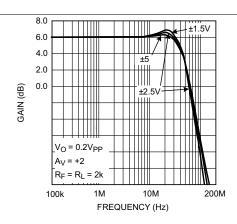
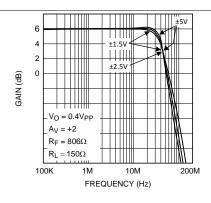


Figure 7. Large Signal Frequency Response

Figure 8. Closed Loop Small Signal Frequency Response for Various Supplies



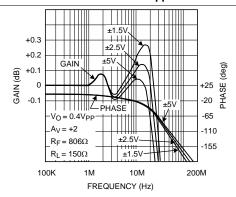
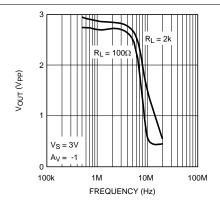


Figure 9. Closed Loop Frequency Response for Various Supplies

Figure 10. ±0.1dB Gain Flatness for Various Supplies



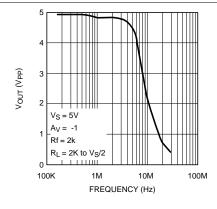
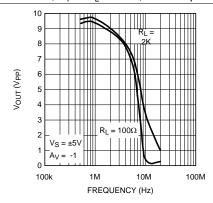


Figure 11.  $V_{OUT}$  ( $V_{PP}$ ) for THD < 0.5%

Figure 12.  $\rm V_{OUT}$  (V\_{PP}) for THD < 0.5%

# TEXAS INSTRUMENTS

## **Typical Performance Characteristics (continued)**



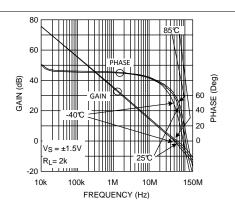
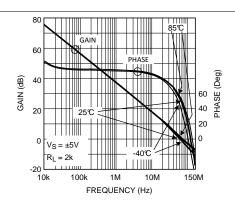


Figure 13.  $V_{OUT}$  ( $V_{PP}$ ) for THD < 0.5%

Figure 14. Open Loop Gain/Phase for Various Temperature



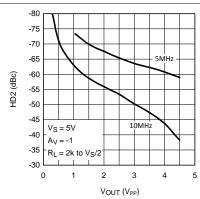
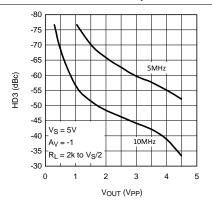


Figure 15. Open Loop Gain/Phase for Various Temperature

Figure 16. HD2 (dBc) vs Output Swing



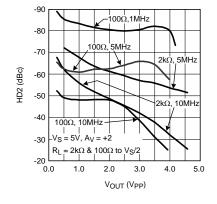
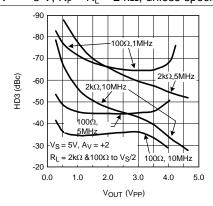


Figure 17. HD3 (dBc) vs Output Swing

Figure 18. HD2 vs Output Swing



**Typical Performance Characteristics (continued)** 



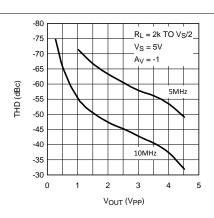


Figure 19. HD3 vs Output Swing

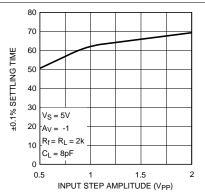


Figure 20. THD (dBc) vs Output Swing

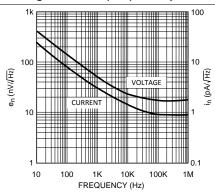


Figure 21. Settling Time vs Input Step Amplitude (Output Slew and Settle Time)

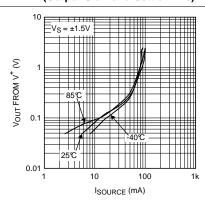


Figure 22. Input Noise vs Frequency

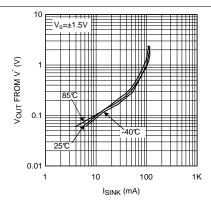
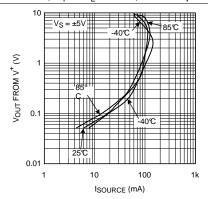


Figure 23.  $V_{OUT}$  from V<sup>+</sup> vs  $I_{SOURCE}$ 

Figure 24.  $V_{OUT}$  from  $V^-$  vs  $I_{SINK}$ 

#### TEXAS INSTRUMENTS

## **Typical Performance Characteristics (continued)**



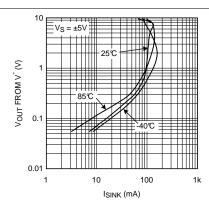
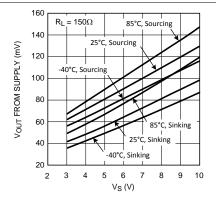


Figure 25. V<sub>OUT</sub> from V<sup>+</sup> vs I<sub>SOURCE</sub>

Figure 26. V<sub>OUT</sub> from V<sup>-</sup> vs I<sub>SINK</sub>



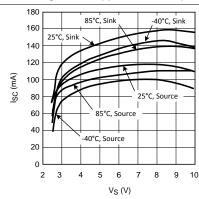
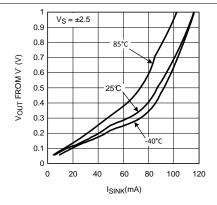


Figure 27. Swing vs V<sub>S</sub>

Figure 28. Short Circuit Current (to V<sub>S</sub>/2) vs V<sub>S</sub>



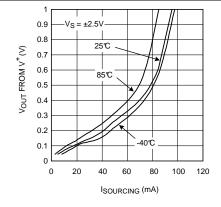


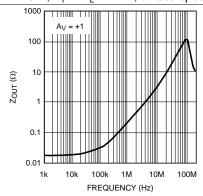
Figure 29. Output Sinking Saturation Voltage vs I<sub>OUT</sub>

Figure 30. Output Sourcing Saturation Voltage vs  $I_{\text{OUT}}$ 





## **Typical Performance Characteristics (continued)**



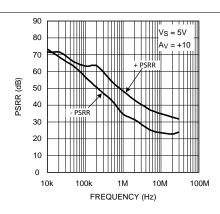
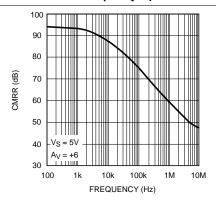


Figure 31. Closed Loop Output Impedance vs Frequency A<sub>V</sub> = +1

Figure 32. PSRR vs Frequency



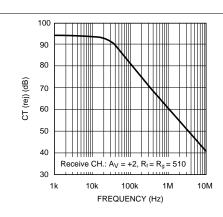
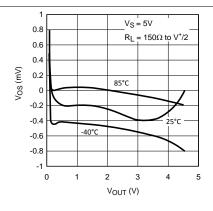


Figure 33. CMRR vs Frequency

Figure 34. Crosstalk Rejection vs Frequency (Output to Output)



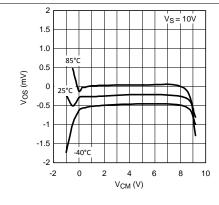


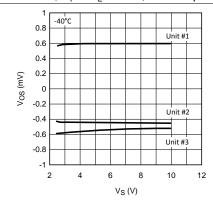
Figure 35. V<sub>OS</sub> vs V<sub>OUT</sub> (Typical Unit)

Figure 36.  $V_{OS}$  vs  $V_{CM}$  (Typical Unit)

# TEXAS INSTRUMENTS

# **Typical Performance Characteristics (continued)**

 $V^+ = +5 \text{ V}, V^- = -5 \text{ V}, R_F = R_L = 2 \text{ k}\Omega$ , unless specified otherwise.



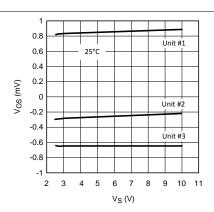
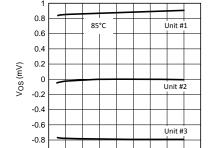


Figure 37. V<sub>OS</sub> vs V<sub>S</sub> (for 3 Representative Units)



3 4 5

2

Figure 38.  $V_{OS}$  vs  $V_{S}$  (for 3 Representative Units)

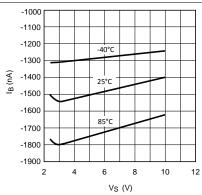


Figure 39. V<sub>OS</sub> vs V<sub>S</sub> (for 3 Representative Units)

6 7

V<sub>S</sub>(V)

8 9 10 12

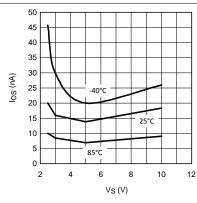


Figure 40.  $\rm I_B \ vs \ V_S$ 

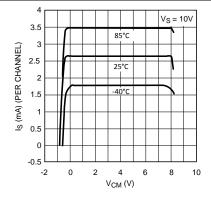


Figure 41.  $I_{OS}$  vs  $V_{S}$ 

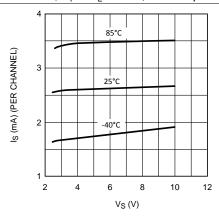
Figure 42. Is vs  $V_{\text{CM}}$ 





# **Typical Performance Characteristics (continued)**

 $V^+ = +5 \text{ V}, V^- = -5 \text{ V}, R_F = R_L = 2 \text{ k}\Omega$ , unless specified otherwise.



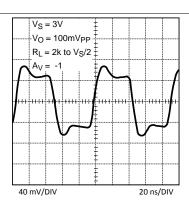


Figure 43. I<sub>S</sub> vs V<sub>S</sub>



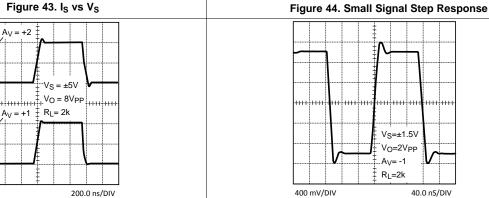


Figure 45. Large Signal Step Response

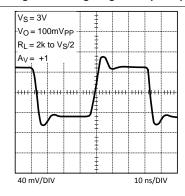


Figure 46. Large Signal Step Response

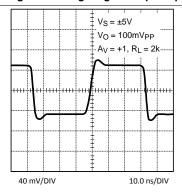


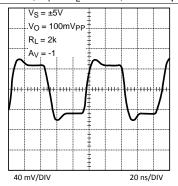
Figure 47. Small Signal Step Response

Figure 48. Small Signal Step Response

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# TEXAS INSTRUMENTS

# **Typical Performance Characteristics (continued)**



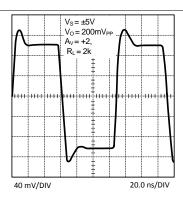


Figure 49. Small Signal Step Response

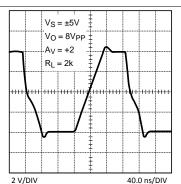


Figure 50. Small Signal Step Response

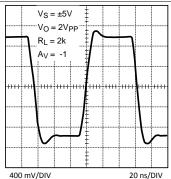


Figure 51. Large Signal Step Response

Figure 52. Large Signal Step Response

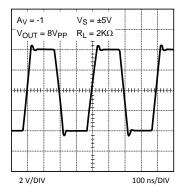


Figure 53. Large Signal Step Response



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#### 8 Detailed Description

#### 8.1 Overview

The LMH6644-MIL is based on proprietary VIP10 dielectrically isolated bipolar process. This device architecture features the following:

- Complimentary bipolar devices with exceptionally high f<sub>t</sub> (~8 GHz) even under low-supply voltage (2.7 V) and low-bias current.
- A class A-B turn-around stage with improved noise, offset, and reduced power dissipation compared to similar speed devices (patent pending).
- Common Emitter push-push output stage capable of 75-mA output current (at 0.5 V from the supply rails) while consuming only 2.7 mA of total supply current per channel. This architecture allows output to reach within mV of either supply rail.
- Consistent performance over the entire operating supply voltage range with little variation for the most important specifications (for example, BW, SR, I<sub>OUT</sub>, and so forth)
- Significant power saving (~40%) compared to competitive devices on the market with similar performance.

#### 8.2 Functional Block Diagram

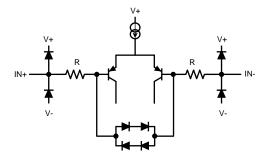


Figure 54. Input Equivalent Circuit

#### 8.3 Feature Description

The LMH6644-MIL is a drop-in replacement for the AD805X family of high-speed op amps in most applications. In addition, the LMH6644-MIL will typically save about 40% on power dissipation, due to lower supply current, when compared to competition. All AD805X family's specified parameters are included in the list of LMH6644-MIL ensured specifications in order to ensure equal or better level of performance. However, as in most high-performance parts and due to subtleties of applications, it is strongly recommended that the performance of the part to be evaluated is tested under actual operating conditions to ensure full compliance to all specifications.

#### 8.4 Device Functional Modes

With 3-V supplies and a common-mode input voltage range that extends 0.5 V below V $^-$ , the LMH6644-MIL find applications in low voltage/low power applications. Even with 3-V supplies, the -3dB BW (@ A $_V$  = +1) is typically 115 MHz with a tested limit of 80 MHz. Production testing guarantees that process variations will not compromise speed. High-frequency response is exceptionally stable, confining the typical -3dB BW over the industrial temperature range to  $\pm 2.5\%$ .

As seen in *Typical Performance Characteristics*, the LMH6644-MIL output current capability (~75 mA) is enhanced compared to AD805X. This enhancement increases the output load range, adding to the LMH6644-MIL's versatility. Since LMH6644-MIL is capable of high-output current, device junction temperature should not to exceed the Absolute Maximum Ratings.

# TEXAS INSTRUMENTS

### 9 Application and Implementation

#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

This device was designed to avoid output phase reversal. With input overdrive, the output is kept near supply rail (or as closed to it as mandated by the closed loop gain setting and the input voltage). See Figure 56.

However, if the input voltage range of -0.5 V to 1 V from V<sup>+</sup> is exceeded by more than a diode drop, the internal ESD protection diodes will start to conduct. The current in the diodes should be kept at or below 10 mA.

Output overdrive recovery time is less than 100 ns as can be seen in Figure 57.

#### 9.2 Typical Application

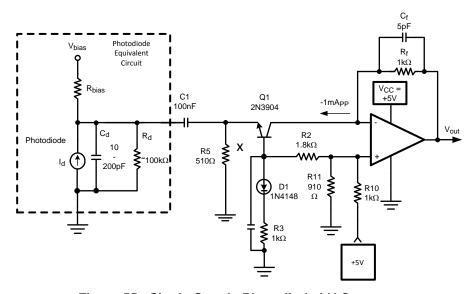


Figure 55. Single-Supply Photodiode I-V Converter

#### 9.2.1 Design Requirements

The circuit shown in Figure 55 is used to amplify the current from a photodiode into a voltage output. In this circuit, the emphasis is on achieving high bandwidth and the transimpedance gain setting is kept relatively low. Because of its high-slew-rate limit and high speed, the LMH6644-MIL lends itself well to such an application. This circuit achieves approximately 1 V/mA of transimpedance gain and capable of handling up to 1 mApp from the photodiode. Q1, in a common base configuration, isolates the high capacitance of the photodiode (Cd) from the op amp input in order to maximize speed. Input is AC coupled through C1 to ease biasing and allow single supply operation. With 5-V single supply, the device input/output is shifted to near half supply using a voltage divider from VCC. Note that Q1 collector does not have any voltage swing and the Miller effect is minimized. D1, tied to Q1 base, is for temperature compensation of Q1's bias point. Q1 collector current was set to be large enough to handle the peak-to-peak photodiode excitation and not too large to shift the U1 output too far from mid-supply.



**Typical Application (continued)** 

#### 9.2.1.1 Input and Output Topology

All input / output pins are protected against excessive voltages by ESD diodes connected to V<sup>+</sup> and V<sup>-</sup> rails (see Figure 54). These diodes start conducting when the input / output pin voltage approaches 1  $V_{be}$  beyond V<sup>+</sup> or V<sup>-</sup> to protect against over voltage. These diodes are normally reverse biased. Further protection of the inputs is provided by the two resistors (R in Figure 54), in conjunction with the string of anti-parallel diodes connected between both bases of the input stage. The combination of these resistors and diodes reduces excessive differential input voltages approaching 2  $V_{be}$ . This occurs most commonly when the device is used as a comparator (or with little or no feedback) and the device inputs no longer follow each other. In such a case, the diodes may conduct. As a consequence, input current increases and the differential input voltage is clamped. It is important to make sure that the subsequent current flow through the device input pins does not violate the Absolute Maximum Ratings of the device. To limit the current through this protection circuit, extra series resistors can be placed. Together with the built-in series resistors of several hundred ohms, these external resistors can limit the input current to a safe number (that is, less than 10 mA). Be aware that these input series resistors may impact the switching speed of the device and could slow down the device.

#### 9.2.1.2 Single-Supply, Low-Power Photodiode Amplifier

The circuit shown in Figure 55 is used to amplify the current from a photodiode into a voltage output. In this circuit, the emphasis is on achieving high bandwidth and the transimpedance gain setting is kept relatively low. Because of its high slew rate limit and high speed, the LMH6644-MIL lends itself well to such an application.

This circuit achieves approximately 1V/mA of transimpedance gain and capable of handling up to  $1mA_{pp}$  from the photodiode. Q1, in a common base configuration, isolates the high capacitance of the photodiode ( $C_d$ ) from the Op Amp input in order to maximize speed. Input is AC coupled through C1 to ease biasing and allow single-supply operation. With 5-V single supply, the device input/output is shifted to near half supply using a voltage divider from  $V_{CC}$ . Note that Q1 collector does not have any voltage swing and the Miller effect is minimized. D1, tied to Q1 base, is for temperature compensation of Q1's bias point. Q1 collector current was set to be large enough to handle the peak-to-peak photodiode excitation and not too large to shift the U1 output too far from mid-supply.

No matter how low an  $R_f$  is selected, there is a need for  $C_f$  in order to stabilize the circuit. The reason for this is that the Op Amp input capacitance and Q1 equivalent collector capacitance together  $(C_{IN})$  will cause additional phase shift to the signal fed back to the inverting node.  $C_f$  will function as a zero in the feedback path counteracting the effect of the  $C_{IN}$  and acting to stabilized the circuit. By proper selection of  $C_f$  such that the Op Amp open loop gain is equal to the inverse of the feedback factor at that frequency, the response is optimized with a theoretical  $45^{\circ}$  phase margin.

$$C_F = \text{ } \sim \text{ } SQRT \left[ (C_{IN})/(2\pi \cdot GBWP \cdot R_F) \right]$$

where

GBWP is the Gain Bandwidth Product of the Op Amp
 (1)

Optimized as such, the I-V converter will have a theoretical pole, f<sub>p</sub>, at:

$$f_P = SQRT \left[ GBWP/(2\pi R_F \cdot C_{IN}) \right]$$
 (2)

With op amp input capacitance of 3 pF and an estimate for Q1 output capacitance of about 3 pF as well,  $C_{IN} = 6$  pF. From the typical performance plots, GBWP is approximately 57 MHz. Therefore, with  $R_f = 1$ k, from Equation 1 and Equation 2:

$$C_f = \sim 4.1 \text{ pF and } f_0 = 39 \text{ MHz}$$
 (3)

For this example, optimum  $C_f$  was empirically determined to be around 5 pF. This time domain response is shown in Figure 58 below showing about 9-ns rise/fall times, corresponding to about 39 MHz for  $f_p$ . The overall supply current from the +5 V supply is around 5 mA with no load.

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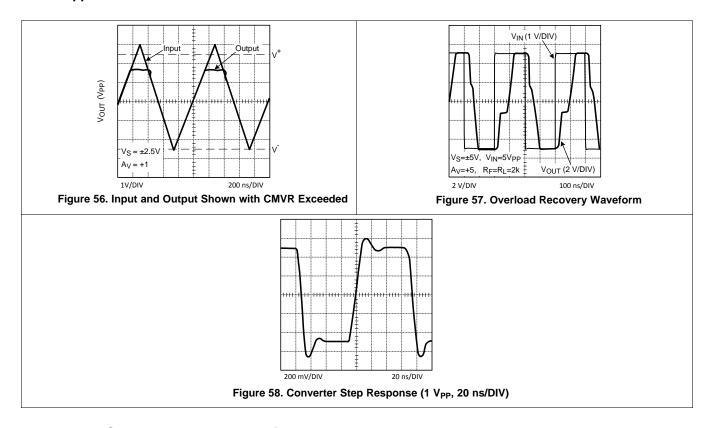
#### **Typical Application (continued)**

#### 9.2.2 Detailed Design Procedure

No matter how low an Rf is selected, there is a need for  $C_f$  in order to stabilize the circuit. The reason for this is that the op amp input capacitance and Q1 equivalent collector capacitance together ( $C_{IN}$ ) will cause additional phase shift to the signal fed back to the inverting node.  $C_f$  will function as a zero in the feedback path counteracting the effect of the  $C_{IN}$  and acting to stabilized the circuit. By proper selection of  $C_f$  such that the Op Amp open loop gain is equal to the inverse of the feedback factor at that frequency, the response is optimized with a theoretical 45° phase margin where GBWP is the Gain Bandwidth Product of the Op Amp, optimized as such, the I-V converter will have a theoretical pole, fp, at: (2) With Op Amp input capacitance of 3pF and an estimate for Q1 output capacitance of about 3 pF as well,  $C_{IN}$  = 6 pF. From the typical performance plots, GBWP is approximately 57 MHz. Therefore, with Rf = 1k, from Equation 2 and Equation 3 :  $C_f$  = ~4.1 pF and fp = 39 MHz.

For this example, optimum  $C_f$  was empirically determined to be around 5 pF. This time domain response is shown in Figure 58 showing about 9 ns rise/fall times, corresponding to about 39 MHz for fp. The overall supply current from the +5-V supply is around 5 mA with no load.

#### 9.2.3 Application Curves



# 10 Power Supply Recommendations

The LMH6644-MIL device can operate off a single supply or with dual supplies. The input CM capability of the parts (CMVR) extends all the way down to the V- rail to simplify single supply applications. Supplies should be decoupled with low inductance, often ceramic, capacitors to ground less than 0.5 inches from the device pins. The use of ground plane is recommended, and as in most high speed devices, it is advisable to remove ground plane close to device sensitive pins such as the inputs.

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### 11 Layout

#### 11.1 Layout Guidelines

Generally, a good high-frequency layout will keep power supply and ground traces away from the inverting input and output pins. Parasitic capacitances on these nodes to ground will cause frequency response peaking and possible circuit oscillations (see Application Note OA-15, "Frequent Faux Pas in Applying Wideband Current Feedback Amplifiers", SNOA367, for more information). Texas Instruments suggests the following evaluation boards as a guide for high-frequency layout and as an aid in device testing and characterization:

**Table 1. Printed Circuit Board Layout And Component Values** 

DEVICE	PACKAGE	EVALUATION BOARD PN			
LMH6644MA	14-Pin SOIC	LMH730231			
LMH6644MT	14-Pin TSSOP	LMH730131			

Another important parameter in working with high-speed and high-performance amplifiers is the component values selection. Choosing external resistors that are large in value will effect the closed loop behavior of the stage because of the interaction of these resistors with parasitic capacitances. These capacitors could be inherent to the device or a by-product of the board layout and component placement. Either way, keeping the resistor values lower, will diminish this interaction to a large extent. On the other hand, choosing very low value resistors could load down nodes and will contribute to higher overall power dissipation.

#### 11.2 Layout Example

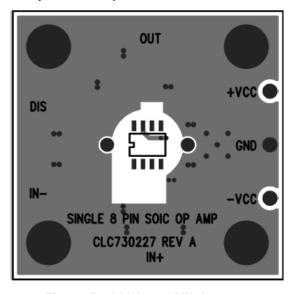


Figure 59. LMH6644-MIL Layer 1

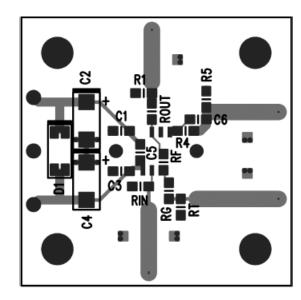


Figure 60. LMH6644-MIL Layer 2

# 12 デバイスおよびドキュメントのサポート

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#### 12.5 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

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#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
						(4)	(5)		
LMH6644 MDC	Active	Production	DIESALE (Y)   0	100   NOT REQUIRED	Yes	Call TI	Level-1-NA-UNLIM	-40 to 85	
LMH6644-MDC.A	Active	Production	DIESALE (Y)   0	100   NOT REQUIRED	Yes	Call TI	Level-1-NA-UNLIM	-40 to 85	

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

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