



# LM2733 SOT-23 パッケージ、40V FET スイッチ内蔵 0.6/1.6MHz 昇圧型コンバータ

## 1 特長

- 40V の DMOS FET スイッチ
- 1.6MHz (「X」)、0.6MHz (「Y」) のスイッチング周波数
- 低  $R_{DS(ON)}$  の DMOS FET
- 最大 1A のスイッチング電流
- 広い入力電圧範囲: 2.7V~14V
- 低いシャットダウン時電流: 1 $\mu$ A 未満
- 5 ピン SOT-23 パッケージ
- 小型コンデンサおよびインダクタを使用
- サイクル単位の電流制限
- 内部補償

## 2 アプリケーション

- 白色 LED 用電流源
- PDA、パームトップ・コンピュータ
- デジタル・カメラ
- 携帯電話、ゲーム機
- ローカル昇圧レギュレータ

## 3 概要

LM2733 スwitchング・レギュレータは、1.6MHz (「X」オプション) と 600kHz (「Y」オプション) の固定周波数で動作する電流モード昇圧型コンバータです。

内蔵の 1A スイッチの電力損失を最小限にすることで可能になった SOT-23 パッケージの使用と、小型インダクタおよびコンデンサの使用により、業界で最高の電力密度を実現しています。これらのソリューションは 40V のスイッチを内蔵しているため、16V 以上の電圧への昇圧に理想的です。

これらの製品は、静止電流の低減とバッテリー駆動時間の延長に使用できるロジック・レベルのシャットダウン・ピンを備えています。

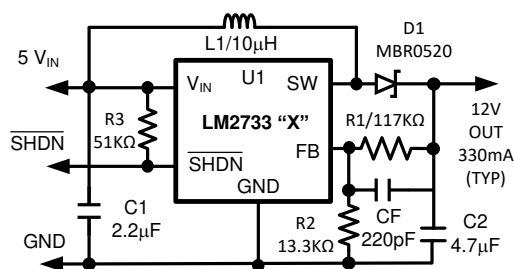
サイクル単位の電流制限とサーマル・シャットダウンによる保護機能を備えています。補償機能を内蔵しているため、設計が簡単であり、部品数を減らせます。

### 製品情報<sup>(1)</sup>

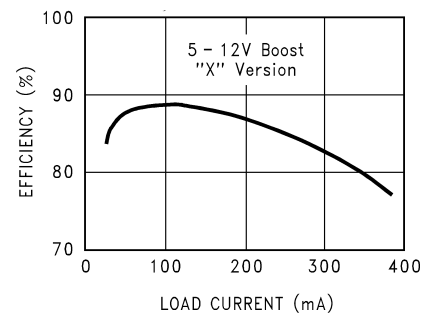
型番	パッケージ	本体サイズ(公称)
LM2733	SOT-23 (5)	2.90mm×1.60mm

(1) 提供されているすべてのパッケージについては、データシートの末尾にある注文情報を参照してください。

### 代表的なアプリケーション回路



### 効率と負荷電流との関係



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## 4 改訂履歴

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

### Revision F (December 2014) から Revision G に変更 Page

- コネクタの配線の誤記を訂正するために「代表的なアプリケーション回路」の図を 変更 ..... 1

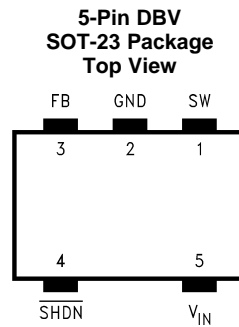
### Revision E (April 2013) から Revision F に変更 Page

- 「ピン構成および機能」セクション、「ESD 定格」表、「機能説明」セクション、「デバイスの機能モード」セクション、「アプリケーションと実装」セクション、「電源に関する推奨事項」セクション、「レイアウト」セクション、「デバイスおよびドキュメントのサポート」セクション、「メカニカル、パッケージ、および注文情報」セクション 追加 ..... 1

### Revision D (April 2013) から Revision E に変更 Page

- Changed layout of National Semiconductor Data Sheet to TI format ..... 11

## 5 Pin Configuration and Functions



### Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
SW	1	O	Drain of the internal FET switch.
GND	2	GND	Analog and power ground.
FB	3	I	Feedback point that connects to external resistive divider.
SHDN	4	I	Shutdown control input. Connect to VIN if this feature is not used.
VIN	5	I	Analog and power input.

## 6 Specifications

### 6.1 Absolute Maximum Ratings<sup>(1)(2)</sup>

	MIN	MAX	UNIT
Input supply voltage (VIN)	−0.4	14.5	V
FB pin voltage	−0.4	6	V
SW pin voltage	−0.4	40	V
SHDN pin voltage	−0.4	VIN + 0.3	V
Power dissipation <sup>(3)</sup>	Internally Limited		
Lead temperature (soldering, 5 sec.)		300	°C
Storage temperature, Tstg	−65	150	°C

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Electrical specifications do not apply when operating the device outside of the limits set forth under the operating ratings which specify the intended range of operating conditions.
- (2) If Military/Aerospace specified devices are required, contact the Texas Instruments Sales Office/ Distributors for availability and specifications.
- (3) The maximum power dissipation which can be safely dissipated for any application is a function of the maximum junction temperature, TJ(MAX) = 125°C, the junction-to-ambient thermal resistance for the SOT-23 package, RθJA = 210°C/W, and the ambient temperature, TA. The maximum allowable power dissipation at any ambient temperature for designs using this device can be calculated using the formula:
- $$P_{(MAX)} = \frac{T_{J(MAX)} - T_A}{\theta_{JA}} = \frac{125 - T_A}{265}$$
- If power dissipation exceeds the maximum specified above, the internal thermal protection circuitry protects the device by reducing the output voltage as required to maintain a safe junction temperature.

### 6.2 ESD Ratings

			VALUE	UNIT
V(ESD)	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins <sup>(1)</sup>	±2000	V
		Machine model	±200	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	MAX	UNIT
Input supply voltage (VIN)	2.7	14	V
SHDN pin voltage	0	VIN	V
Junction temperature	–40	125	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		LM2733	UNIT
		DBV (SOT-23)	
		5 PINS	
RθJA	Junction-to-ambient thermal resistance	210	°C/W
RθJC(top)	Junction-to-case (top) thermal resistance	122	°C/W
RθJB	Junction-to-board thermal resistance	38.4	°C/W
ψJT	Junction-to-top characterization parameter	12.8	°C/W
ψJB	Junction-to-board characterization parameter	37.5	°C/W
RθJC(bot)	Junction-to-case (bottom) thermal resistance	n/a	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) SPRA953 application report.

### 6.5 Electrical Characteristics

Unless otherwise specified: VIN = 5 V, VSHDN = 5 V, IL = 0 A, TJ = 25°C.

PARAMETER		TEST CONDITIONS	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>	UNIT
VIN	Input voltage	–40°C ≤ TJ ≤ +125°C	2.7		14	V
ISW	Switch current limit	See <sup>(3)</sup>	1	1.5		A
RDS(ON)	Switch ON resistance	ISW = 100 mA		500	650	mΩ
SHDNTH	Shutdown threshold	Device ON, –40°C ≤ TJ ≤ +125°C	1.5			V
		Device OFF, –40°C ≤ TJ ≤ +125°C			0.50	
ISHDN	Shutdown pin bias current	VSHDN = 0		0		μA
		VSHDN = 5 V		0		
		VSHDN = 5 V, –40°C ≤ TJ ≤ +125°C			2	
VFB	Feedback pin reference voltage	VIN = 3 V		1.230		V
		VIN = 3 V, –40°C ≤ TJ ≤ +125°C	1.205		1.255	
IFB	Feedback pin bias current	VFB = 1.23 V		60		nA
IQ	Quiescent current	VSHDN = 5 V, Switching "X"		2.1		mA
		VSHDN = 5 V, Switching "X", –40°C ≤ TJ ≤ +125°C			3	
		VSHDN = 5 V, Switching "Y"		1.1		
		VSHDN = 5 V, Switching "Y", –40°C ≤ TJ ≤ +125°C			2	
		VSHDN = 5 V, Not Switching		400		μA
		VSHDN = 5 V, Not Switching, –40°C ≤ TJ ≤ +125°C			500	
		VSHDN = 0		0.024	1	
ΔVFB/ΔVIN	FB voltage line regulation	2.7 V ≤ VIN ≤ 14 V		0.02		%/V

(1) Limits are specified by testing, statistical correlation, or design.

(2) Typical values are derived from the mean value of a large quantity of samples tested during characterization and represent the most likely expected value of the parameter at room temperature.

(3) Switch current limit is dependent on duty cycle (see [Typical Characteristics](#)). Limits shown are for duty cycles ≤ 50%.

## Electrical Characteristics (continued)

Unless otherwise specified:  $V_{IN} = 5\text{ V}$ ,  $V_{SHDN} = 5\text{ V}$ ,  $I_L = 0\text{ A}$ ,  $T_J = 25^\circ\text{C}$ .

PARAMETER		TEST CONDITIONS	MIN <sup>(1)</sup>	TYP <sup>(2)</sup>	MAX <sup>(1)</sup>	UNIT
$F_{SW}$	Switching frequency	"X" Option		1.6		MHz
		"X" Option, $-40^\circ\text{C} \leq T_J \leq +125^\circ\text{C}$	1.15		1.85	
		"Y" Option		0.60		
		"Y" Option, $-40^\circ\text{C} \leq T_J \leq +125^\circ\text{C}$	0.40		0.8	
$D_{MAX}$	Maximum duty cycle	"X" Option		93%		
		"X" Option, $-40^\circ\text{C} \leq T_J \leq +125^\circ\text{C}$	87%			
		"Y" Option		96%		
		"Y" Option, $-40^\circ\text{C} \leq T_J \leq +125^\circ\text{C}$	93%			
$I_L$	Switch leakage	Not Switching $V_{SW} = 5\text{ V}$			1	$\mu\text{A}$

## 6.6 Typical Characteristics

Unless otherwise specified:  $V_{IN} = 5\text{ V}$ ,  $\overline{\text{SHDN}}$  pin is tied to  $V_{IN}$ .

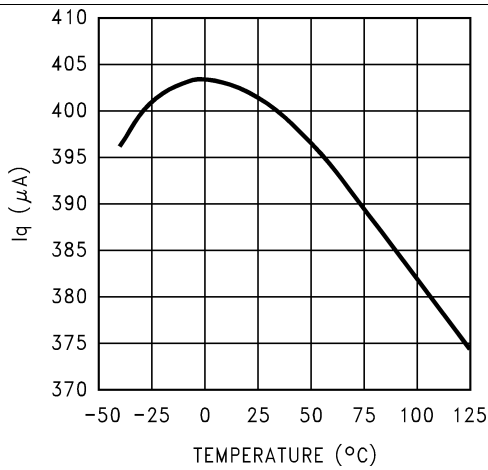


Figure 1.  $I_q$   $V_{IN}$  (Active) vs Temperature - "X"

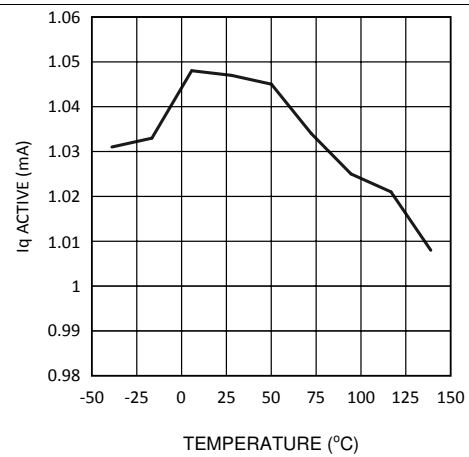


Figure 2.  $I_q$   $V_{IN}$  (Active) vs Temperature - "Y"

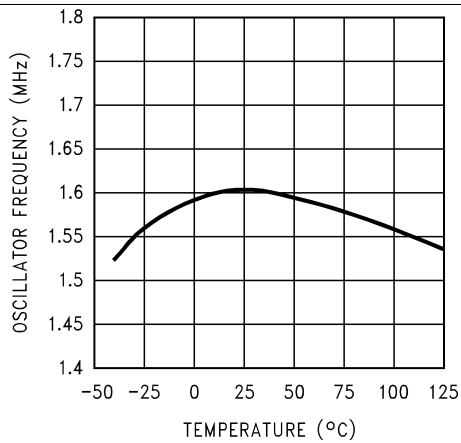


Figure 3. Oscillator Frequency vs Temperature - "X"

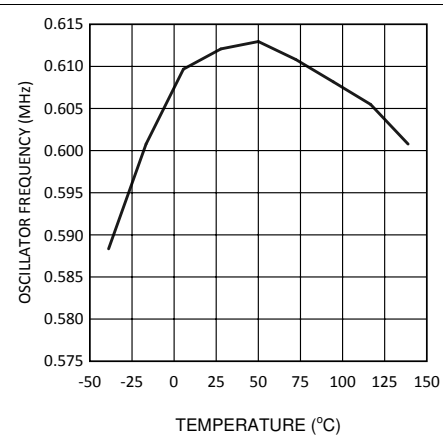


Figure 4. Oscillator Frequency vs Temperature - "Y"

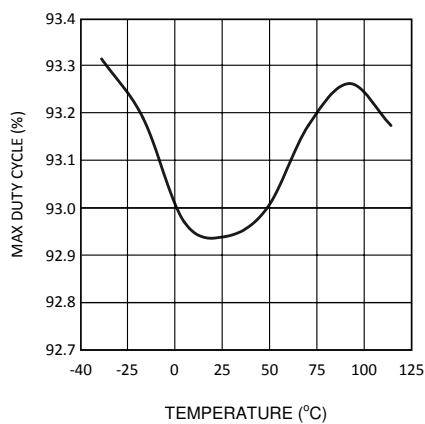


Figure 5. Max. Duty Cycle vs Temperature - "X"

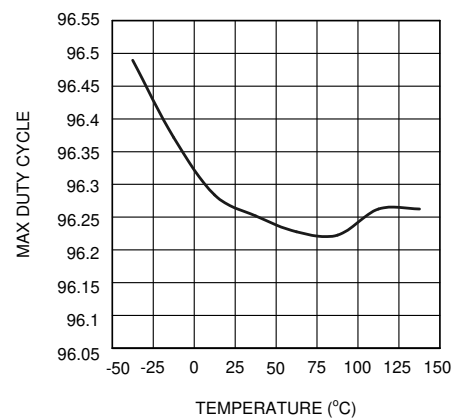
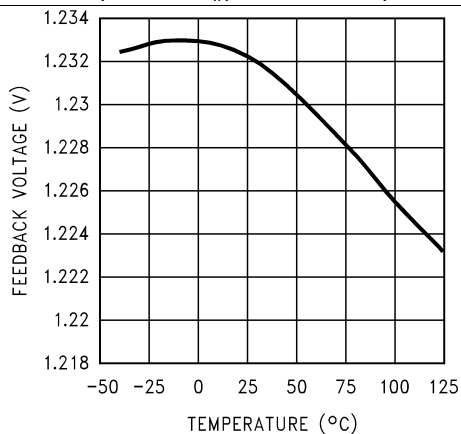


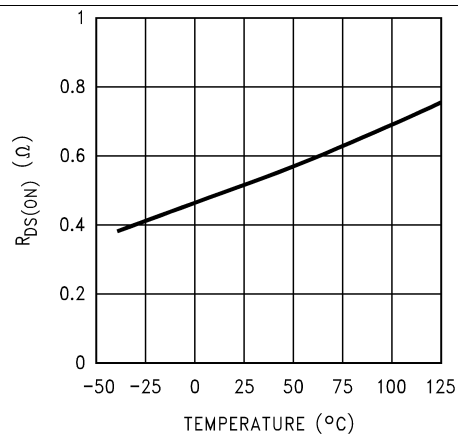
Figure 6. Max. Duty Cycle vs Temperature - "Y"

## Typical Characteristics (continued)

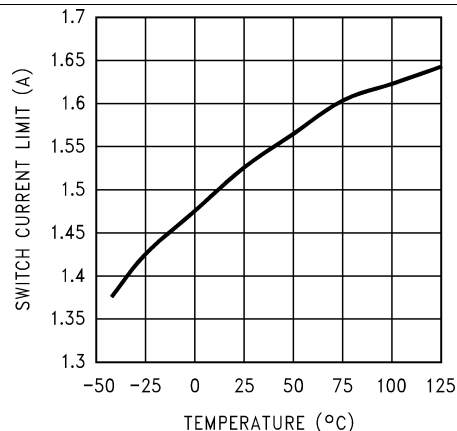
Unless otherwise specified:  $V_{IN} = 5\text{ V}$ ,  $\overline{\text{SHDN}}$  pin is tied to  $V_{IN}$ .



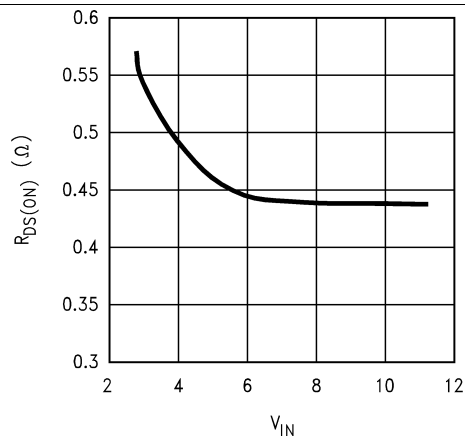
**Figure 7. Feedback Voltage vs Temperature**



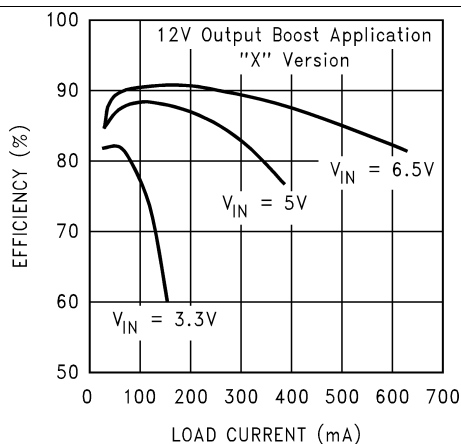
**Figure 8.  $R_{DS(ON)}$  vs Temperature**



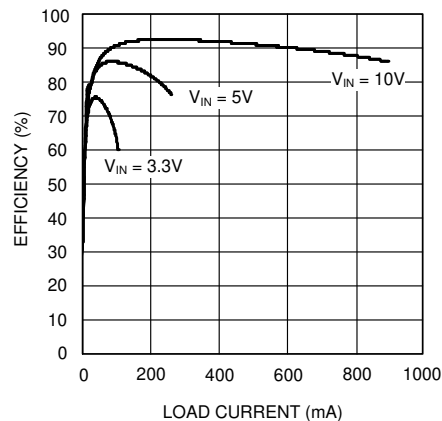
**Figure 9. Current Limit vs Temperature**



**Figure 10.  $R_{DS(ON)}$  vs  $V_{IN}$**



**Figure 11. Efficiency vs Load Current ( $V_{OUT} = 12\text{ V}$ ) - "X"**



**Figure 12. Efficiency vs Load Current ( $V_{OUT} = 15\text{ V}$ ) - "X"**

## Typical Characteristics (continued)

Unless otherwise specified:  $V_{IN} = 5\text{ V}$ ,  $\overline{\text{SHDN}}$  pin is tied to  $V_{IN}$ .

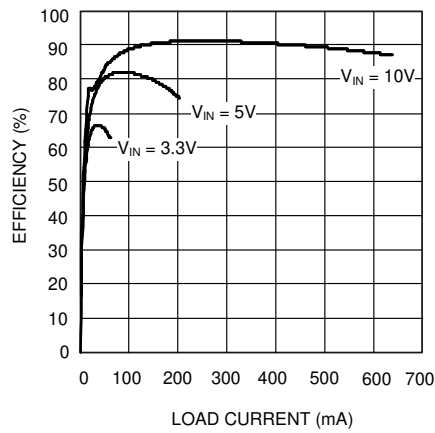


Figure 13. Efficiency vs Load Current ( $V_{OUT} = 20\text{ V}$ ) - "X"

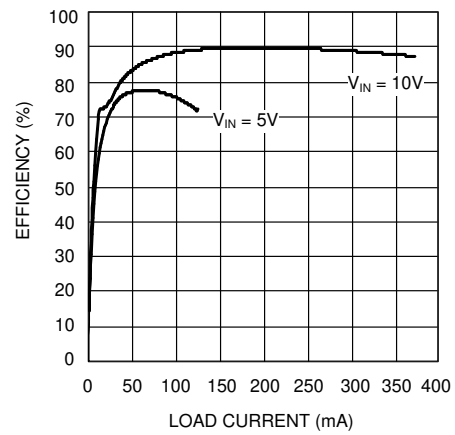


Figure 14. Efficiency vs Load Current ( $V_{OUT} = 25\text{ V}$ ) - "X"

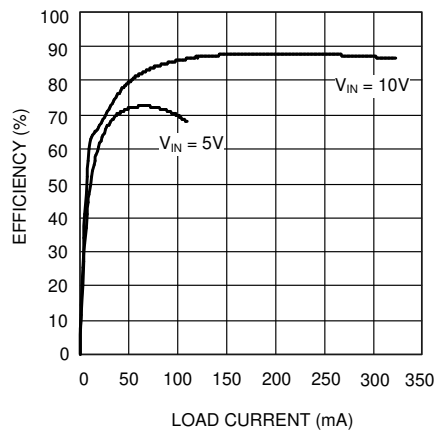


Figure 15. Efficiency vs Load Current ( $V_{OUT} = 30\text{ V}$ ) - "X"

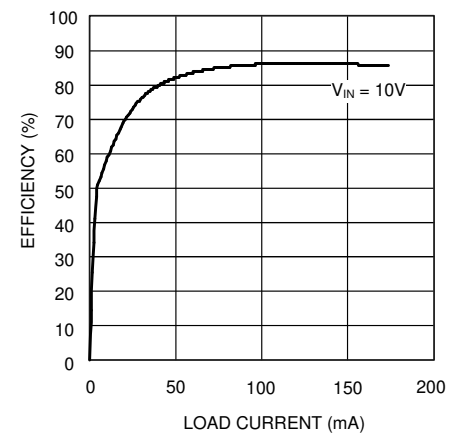


Figure 16. Efficiency vs Load Current ( $V_{OUT} = 35\text{ V}$ ) - "X"

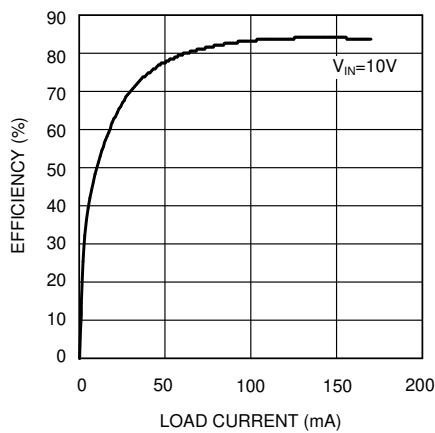


Figure 17. Efficiency vs Load Current ( $V_{OUT} = 40\text{ V}$ ) - "X"

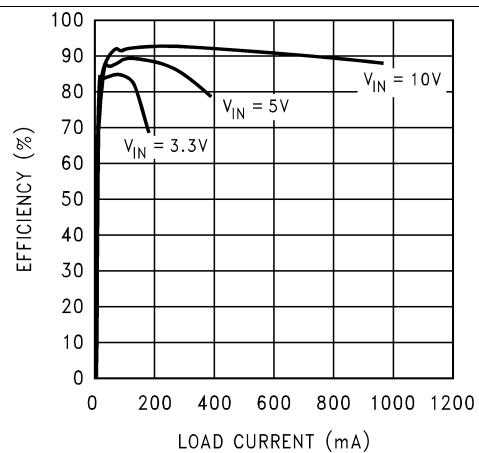


Figure 18. Efficiency vs Load ( $V_{OUT} = 15\text{ V}$ ) - "Y"



## Typical Characteristics (continued)

Unless otherwise specified:  $V_{IN} = 5\text{ V}$ ,  $\overline{\text{SHDN}}$  pin is tied to  $V_{IN}$ .

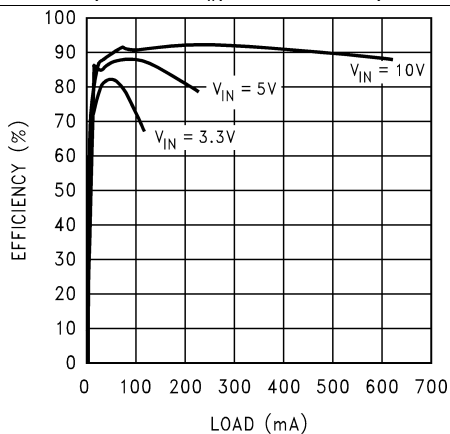


Figure 19. Efficiency vs Load ( $V_{OUT} = 20\text{ V}$ ) - "Y"

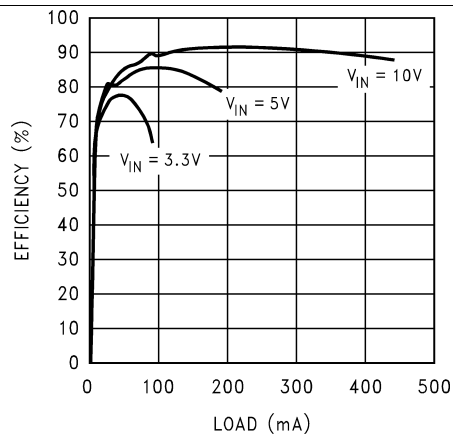


Figure 20. Efficiency vs Load ( $V_{OUT} = 25\text{ V}$ ) - "Y"

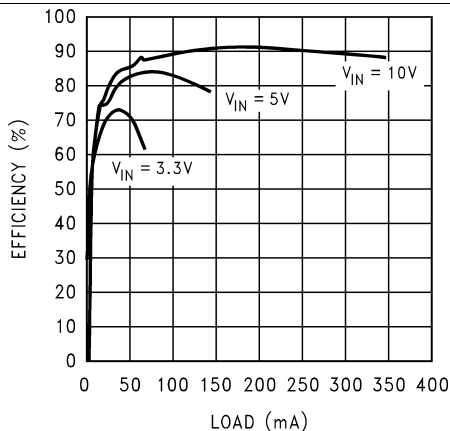


Figure 21. Efficiency vs Load ( $V_{OUT} = 30\text{ V}$ ) - "Y"

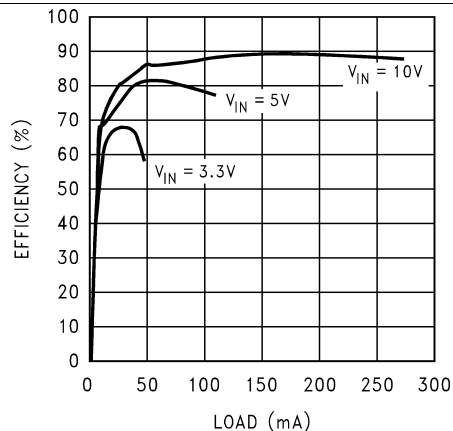


Figure 22. Efficiency vs Load ( $V_{OUT} = 35\text{ V}$ ) - "Y"

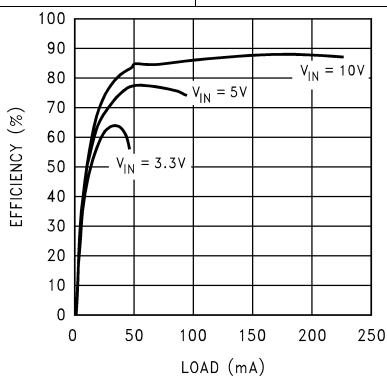


Figure 23. Efficiency vs Load ( $V_{OUT} = 40\text{ V}$ ) - "Y"

## 7 Detailed Description

### 7.1 Overview

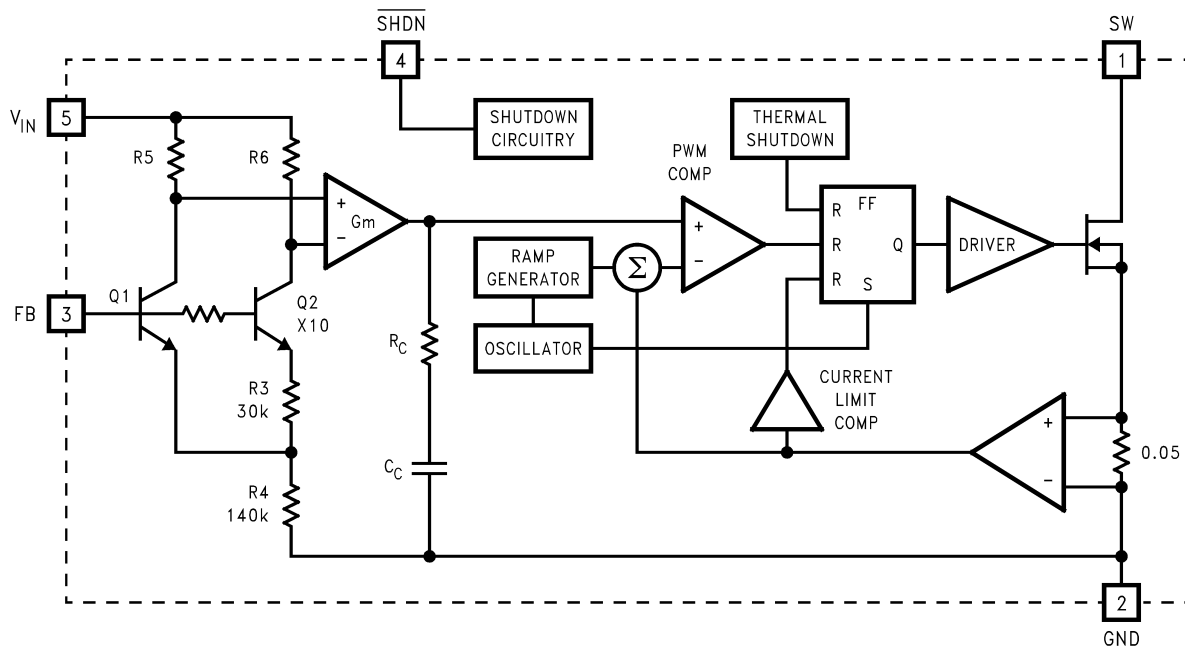
The LM2733 device is a switching converter IC that operates at a fixed frequency (0.6 or 1.6 MHz) using current-mode control for fast transient response over a wide input voltage range and incorporate pulse-by-pulse current limiting protection. Because this is current mode control, a 50 mΩ sense resistor in series with the switch FET is used to provide a voltage (which is proportional to the FET current) to both the input of the pulse width modulation (PWM) comparator and the current limit amplifier.

At the beginning of each cycle, the S-R latch turns on the FET. As the current through the FET increases, a voltage (proportional to this current) is summed with the ramp coming from the ramp generator and then fed into the input of the PWM comparator. When this voltage exceeds the voltage on the other input (coming from the Gm amplifier), the latch resets and turns the FET off. Since the signal coming from the Gm amplifier is derived from the feedback (which samples the voltage at the output), the action of the PWM comparator constantly sets the correct peak current through the FET to keep the output voltage in regulation.

Q1 and Q2 along with R3 - R6 form a bandgap voltage reference used by the IC to hold the output in regulation. The currents flowing through Q1 and Q2 will be equal, and the feedback loop will adjust the regulated output to maintain this. Because of this, the regulated output is always maintained at a voltage level equal to the voltage at the FB node "multiplied up" by the ratio of the output resistive divider.

The current limit comparator feeds directly into the flip-flop, that drives the switch FET. If the FET current reaches the limit threshold, the FET is turned off and the cycle terminated until the next clock pulse. The current limit input terminates the pulse regardless of the status of the output of the PWM comparator.

### 7.2 Functional Block Diagram



### 7.3 Feature Description

#### 7.3.1 Switching Frequency

The LM2733 device is provided with two switching frequencies: the "X" version is typically 1.6 MHz, while the "Y" version is typically 600 kHz. The best frequency for a specific application must be determined based on the tradeoffs involved. See [Switching Frequency](#) in the [Detailed Design Procedure](#) section.

## 7.4 Device Functional Modes

### 7.4.1 Shutdown Pin Operation

The device is turned off by pulling the shutdown pin low. If this function is not going to be used, tie the pin directly to  $V_{IN}$ . If the SHDN function is needed, a pullup resistor must be used to  $V_{IN}$  (approximately 50 k to 100 k $\Omega$  recommended). The SHDN pin must not be left unterminated.

## 8 Application and Implementation

### NOTE

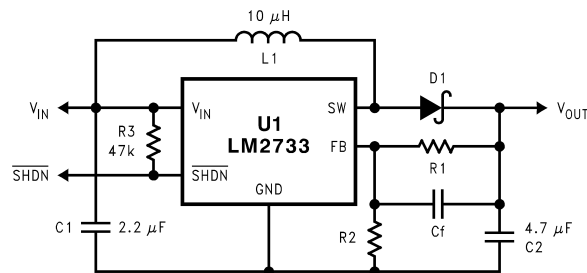
Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

The LM2733 device is a high frequency switching boost regulator that offers small size and high power conversion efficiency. The "X" version of the part operates at 1.6 MHz switching frequency and the "Y" version at 600 kHz.

The LM2733 device targets applications with high output voltages and uses a high voltage FET allowing switch currents up to 1 A. The LM2731 device is similar to the LM2733 device but has a lower voltage FET allowing switch currents up to 1.8 A.

### 8.2 Typical Application



**Figure 24. Basic Application Circuit**

#### 8.2.1 Design Requirements

**Table 1. Circuit Configurations**

COMPONENT	LM2733-X	LM2733-X	LM2733-Y
	LOW VOLTAGE 5-12 V 330 mA typical	HIGH VOLTAGE 20 V 170 mA typical	HIGH VOLTAGE 30 V 110 mA typical
R1	117 K	205 K	309 K
R2	13.3 K	13.3 K	13.3 K
Cf	220 pF	120 pF	82 pF
D1	MBR0520	MBR0530	MBR0540

#### 8.2.2 Detailed Design Procedure

##### 8.2.2.1 Selecting the External Capacitors

The best capacitors for use with the LM2733 device are multi-layer ceramic capacitors. They have the lowest ESR (equivalent series resistance) and highest resonance frequency which makes them optimum for use with high frequency switching converters.

When selecting a ceramic capacitor, use only X5R and X7R dielectric types. Other types such as Z5U and Y5F have such severe loss of capacitance due to effects of temperature variation and applied voltage, they may provide as little as 20% of rated capacitance in many typical applications. Always consult capacitor manufacturer's data curves before selecting a capacitor. High-quality ceramic capacitors can be obtained from Taiyo-Yuden, AVX, and Murata.

### 8.2.2.2 Selecting the Output Capacitor

A single ceramic capacitor of value 4.7  $\mu\text{F}$  to 10  $\mu\text{F}$  provides sufficient output capacitance for most applications. For output voltages below 10 V, a 10- $\mu\text{F}$  capacitance is required. If larger amounts of capacitance are desired for improved line support and transient response, tantalum capacitors can be used in parallel with the ceramics. Aluminum electrolytics with ultra-low ESR such as Sanyo Oscon can be used, but are usually prohibitively expensive. Typical Al electrolytic capacitors are not suitable for switching frequencies above 500 kHz due to significant ringing and temperature rise due to self-heating from ripple current. An output capacitor with excessive ESR can also reduce phase margin and cause instability.

### 8.2.2.3 Selecting the Input Capacitor

An input capacitor is required to serve as an energy reservoir for the current which must flow into the coil each time the switch turns ON. This capacitor must have extremely low ESR, so ceramic is the best choice. TI recommends a nominal value of 2.2  $\mu\text{F}$ , but larger values can be used. Because this capacitor reduces the amount of voltage ripple detected at the input pin, it also reduces the amount of EMI passed back along that line to other circuitry.

### 8.2.2.4 Feedforward Compensation

Although internally compensated, the feedforward capacitor  $C_f$  is required for stability (see [Figure 24](#)). Adding this capacitor puts a zero in the loop response of the converter. Without it, the regulator loop can oscillate. The recommended frequency for the zero  $f_z$  is approximately 8 kHz.  $C_f$  can be calculated using the formula:

$$C_f = 1 / (2 \times \pi \times R_1 \times f_z) \quad (1)$$

### 8.2.2.5 Selecting Diodes

The external diode used in the typical application should be a Schottky diode. If the switch voltage is less than 15 V, a 20-V diode such as the MBR0520 is recommended. If the switch voltage is between 15 V and 25 V, TI recommends a 30-V diode such as the MBR0530. If the switch voltage exceeds 25 V, a 40-V diode such as the MBR0540 should be used.

The MBR05XX series of diodes are designed to handle a maximum average current of 0.5 A. For applications exceeding 0.5 A average but less than 1 A, a Microsemi UPS5817 can be used.

### 8.2.2.6 Setting the Output Voltage

The output voltage is set using the external resistors  $R_1$  and  $R_2$  (see [Figure 24](#)). A value of approximately 13.3 k $\Omega$  is recommended for  $R_2$  to establish a divider current of approximately 92  $\mu\text{A}$ .  $R_1$  is calculated using the formula:

$$R_1 = R_2 \times (V_{\text{OUT}}/1.23 - 1) \quad (2)$$

### 8.2.2.7 Switching Frequency

The device options provide for two fixed frequency operating conditions 1.6 MHz, and 600 kHz. Chose the operating frequency required noting the following trade-offs:

Higher switching frequency means the inductors and capacitors can be made smaller and cheaper for a given output voltage and current. The down side is that efficiency is slightly lower because the fixed switching losses occur more frequently and become a larger percentage of total power loss. EMI is typically worse at higher switching frequencies because more EMI energy will be seen in the higher frequency spectrum where most circuits are more sensitive to such interference.

### 8.2.2.8 Duty Cycle

The maximum duty cycle of the switching regulator determines the maximum boost ratio of output-to-input voltage that the converter can attain in continuous mode of operation. The duty cycle for a given boost application is defined as:

$$\text{Duty Cycle} = \frac{V_{\text{OUT}} + V_{\text{DIODE}} - V_{\text{IN}}}{V_{\text{OUT}} + V_{\text{DIODE}} - V_{\text{SW}}} \quad (3)$$

This applies for continuous mode operation.

The equation shown for calculating duty cycle incorporates terms for the FET switch voltage and diode forward voltage. The actual duty cycle measured in operation will also be affected slightly by other power losses in the circuit such as wire losses in the inductor, switching losses, and capacitor ripple current losses from self-heating. Therefore, the actual (effective) duty cycle measured may be slightly higher than calculated to compensate for these power losses. A good approximation for effective duty cycle is :

$$DC \text{ (eff)} = (1 - \text{Efficiency} \times (V_{IN}/V_{OUT})) \quad (4)$$

Where the efficiency can be approximated from the curves provided.

### 8.2.2.9 Inductance Value

The first question we are usually asked is: “How small can I make the inductor?” (because they are the largest sized component and usually the most costly). The answer is not simple and involves tradeoffs in performance. Larger inductors mean less inductor ripple current, which typically means less output voltage ripple (for a given size of output capacitor). Larger inductors also mean more load power can be delivered because the energy stored during each switching cycle is:

$$E = L/2 \times (I_p)^2 \quad (5)$$

Where “ $I_p$ ” is the peak inductor current. An important point to observe is that the LM2733 device will limit its switch current based on peak current. This means that since  $I_p$  (maximum) is fixed, increasing  $L$  will increase the maximum amount of power available to the load. Conversely, using too little inductance may limit the amount of load current which can be drawn from the output.

Best performance is usually obtained when the converter is operated in “continuous” mode at the load current range of interest, typically giving better load regulation and less output ripple. Continuous operation is defined as not allowing the inductor current to drop to zero during the cycle. It should be noted that all boost converters shift over to discontinuous operation as the output load is reduced far enough, but a larger inductor stays “continuous” over a wider load current range.

To better understand these tradeoffs, a typical application circuit (5V to 12V boost with a 10  $\mu\text{H}$  inductor) will be analyzed. We will assume:

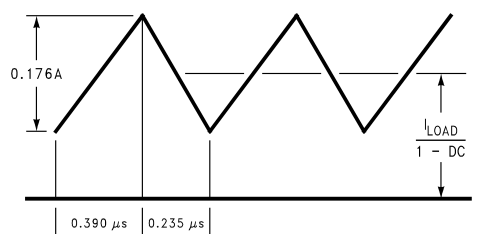
$$V_{IN} = 5 \text{ V}, V_{OUT} = 12 \text{ V}, V_{DIODE} = 0.5 \text{ V}, V_{SW} = 0.5 \text{ V}$$

Since the frequency is 1.6 MHz (nominal), the period is approximately 0.625  $\mu\text{s}$ . The duty cycle will be 62.5%, which means the ON time of the switch is 0.390  $\mu\text{s}$ . It should be noted that when the switch is ON, the voltage across the inductor is approximately 4.5 V.

Using the equation:

$$V = L (di/dt) \quad (6)$$

We can then calculate the  $di/dt$  rate of the inductor which is found to be 0.45 A/ $\mu\text{s}$  during the ON time. Using these facts, we can then show what the inductor current will look like during operation:

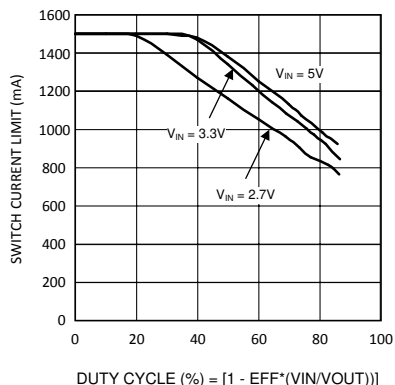


**Figure 25. 10- $\mu\text{H}$  Inductor Current,  
5-V – 12-V Boost (LM2733X)**

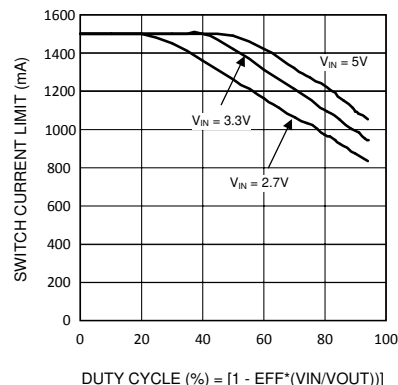
During the 0.390  $\mu\text{s}$  ON time, the inductor current ramps up 0.176 A and ramps down an equal amount during the OFF time. This is defined as the inductor “ripple current”. It can also be seen that if the load current drops to about 33 mA, the inductor current will begin touching the zero axis which means it will be in discontinuous mode. A similar analysis can be performed on any boost converter, to make sure the ripple current is reasonable and continuous operation will be maintained at the typical load current values.

### 8.2.2.10 Maximum Switch Current

The maximum FET switch current available before the current limiter cuts in is dependent on duty cycle of the application. This is illustrated in the graphs below which show both the typical and specified values of switch current for both the "X" and "Y" versions as a function of effective (actual) duty cycle:



**Figure 26. Switch Current Limit vs Duty Cycle - "X"**



**Figure 27. Switch Current Limit vs Duty Cycle - "Y"**

### 8.2.2.11 Calculating Load Current

As shown in the figure which depicts inductor current, the load current is related to the average inductor current by the relation:

$$I_{\text{LOAD}} = I_{\text{IND}}(\text{AVG}) \times (1 - \text{DC}) \quad (7)$$

Where "DC" is the duty cycle of the application. The switch current can be found by:

$$I_{\text{SW}} = I_{\text{IND}}(\text{AVG}) + \frac{1}{2} (I_{\text{RIPPLE}}) \quad (8)$$

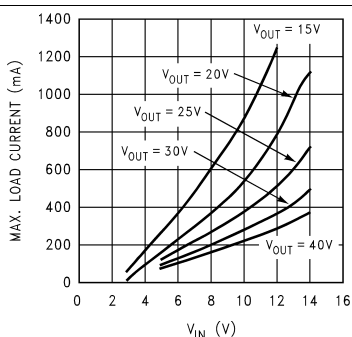
Inductor ripple current is dependent on inductance, duty cycle, input voltage and frequency:

$$I_{\text{RIPPLE}} = \text{DC} \times (V_{\text{IN}} - V_{\text{SW}}) / (f \times L) \quad (9)$$

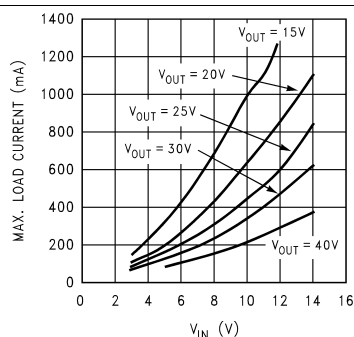
combining all terms, we can develop an expression which allows the maximum available load current to be calculated:

$$I_{\text{LOAD}}(\text{max}) = (1 - \text{DC}) \times (I_{\text{SW}}(\text{max}) - \text{DC} \times (V_{\text{IN}} - V_{\text{SW}}) / 2fL) \quad (10)$$

The equation shown to calculate maximum load current takes into account the losses in the inductor or turn-OFF switching losses of the FET and diode. For actual load current in typical applications, we took bench data for various input and output voltages for both the "X" and "Y" versions of the LM2733 device and displayed the maximum load current available for a typical device in graph form:



**Figure 28. Max. Load Current vs  $V_{\text{IN}}$  - "X"**



**Figure 29. Max. Load Current vs  $V_{\text{IN}}$  - "Y"**

### 8.2.2.12 Design Parameters $V_{SW}$ and $I_{SW}$

The value of the FET "ON" voltage (referred to as  $V_{SW}$  in the equations) is dependent on load current. A good approximation can be obtained by multiplying the "ON Resistance" of the FET times the average inductor current.

FET on resistance increases at  $V_{IN}$  values below 5 V, since the internal N-FET has less gate voltage in this input voltage range (see [Typical Characteristics](#)). Above  $V_{IN} = 5$  V, the FET gate voltage is internally clamped to 5 V.

The maximum peak switch current the device can deliver is dependent on duty cycle. The minimum value is specified to be  $> 1$  A at duty cycle below 50%. For higher duty cycles, see [Typical Characteristics](#).

### 8.2.2.13 Thermal Considerations

At higher duty cycles, the increased ON time of the FET means the maximum output current will be determined by power dissipation within the LM2733 FET switch. The switch power dissipation from ON-state conduction is calculated by:

$$P_{(SW)} = DC \times I_{IND(AVE)}^2 \times R_{DS(ON)} \quad (11)$$

There will be some switching losses as well, so some derating needs to be applied when calculating IC power dissipation.

### 8.2.2.14 Minimum Inductance

In some applications where the maximum load current is relatively small, it may be advantageous to use the smallest possible inductance value for cost and size savings. The converter will operate in discontinuous mode in such a case.

The minimum inductance should be selected such that the inductor (switch) current peak on each cycle does not reach the 1-A current limit maximum. To understand how to do this, an example will be presented.

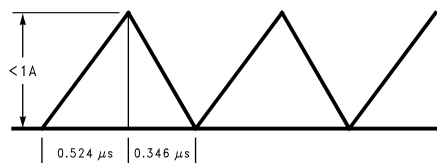
In the example, the LM2733X will be used (nominal switching frequency 1.6 MHz, minimum switching frequency 1.15 MHz). This means the maximum cycle period is the reciprocal of the minimum frequency:

$$T_{ON(max)} = 1/1.15M = 0.870 \mu s \quad (12)$$

We will assume the input voltage is 5 V,  $V_{OUT} = 12$  V,  $V_{SW} = 0.2$  V,  $V_{DIODE} = 0.3$  V. The duty cycle is:

Duty Cycle = 60.3%

Therefore, the maximum switch ON time is  $0.524 \mu s$ . An inductor should be selected with enough inductance to prevent the switch current from reaching 1A in the  $0.524 \mu s$  ON time interval (see below):



**Figure 30. Discontinuous Design, 5V–12V Boost (LM2733X)**

The voltage across the inductor during ON time is 4.8V. Minimum inductance value is found by:

$$V = L \times di/dt, L = V \times (dt/di) = 4.8 (0.524\mu/1) = 2.5 \mu H \quad (13)$$

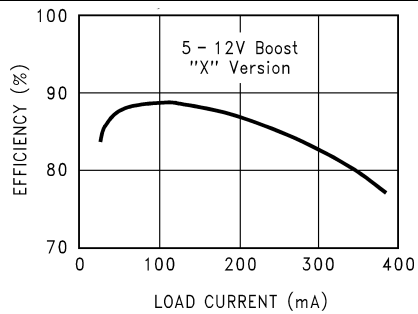
In this case, a  $2.7 \mu H$  inductor could be used assuming it provided at least that much inductance up to the 1A current value. This same analysis can be used to find the minimum inductance for any boost application. Using the slower switching "Y" version requires a higher amount of minimum inductance because of the longer switching period.

### 8.2.2.15 Inductor Suppliers

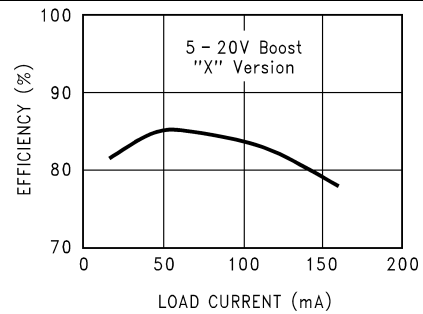
Some of the recommended suppliers of inductors for this product include, but not limited to are Sumida, Coilcraft, Panasonic, TDK and Murata. When selecting an inductor, make certain that the continuous current rating is high enough to avoid saturation at peak currents. A suitable core type must be used to minimize core (switching) losses, and wire power losses must be considered when selecting the current rating.



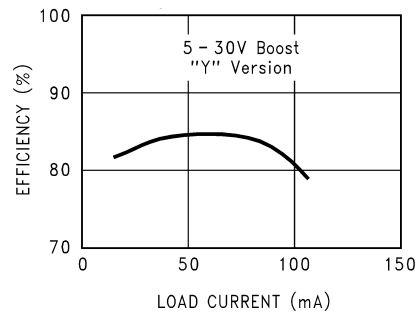
### 8.2.3 Application Curves



**Figure 31. Efficiency vs. Load Current (5-12V, X-version)**



**Figure 32. Efficiency vs. Load Current (5-20V X-version)**



**Figure 33. Efficiency vs. Load Current (5 - 30V Y-version)**

## 9 Power Supply Recommendations

The device input voltage range is 2.7 V to 14 V.

The voltage on the shutdown pin should not exceed the voltage on the VIN pin. For applications that do not require a shutdown function the shutdown pin may be connected to the VIN pin. In this case a 47-K $\Omega$  resistor is recommended to be connected between these pins.

## 10 Layout

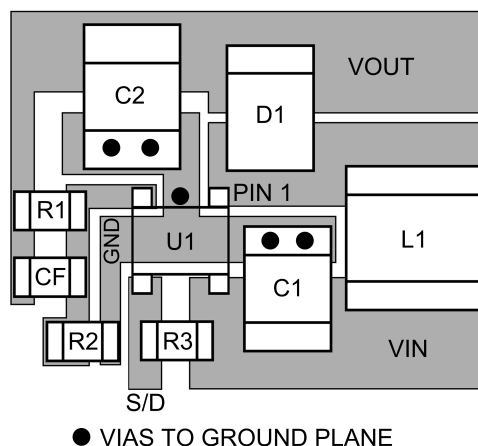
### 10.1 Layout Guidelines

High frequency switching regulators require very careful layout of components in order to get stable operation and low noise. All components must be as close as possible to the LM2733 device. It is recommended that a 4-layer PCB be used so that internal ground planes are available.

Some additional guidelines to be observed:

1. Keep the path between L1, D1, and C2 extremely short. Parasitic trace inductance in series with D1 and C2 will increase noise and ringing.
2. The feedback components R1, R2 and CF must be kept close to the FB pin of U1 to prevent noise injection on the FB pin trace.
3. If internal ground planes are available (recommended) use vias to connect directly to ground at pin 2 of U1, as well as the negative sides of capacitors C1 and C2.

### 10.2 Layout Example



**Figure 34. Recommended PCB Component Layout**

## 11 デバイスおよびドキュメントのサポート

### 11.1 商標

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### 11.3 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 メカニカル、パッケージ、および注文情報

以降のページには、メカニカル、パッケージ、および注文に関する情報が記載されています。この情報は、そのデバイスについて利用可能な最新のデータです。このデータは予告なく変更されることがあり、ドキュメントが改訂される場合もあります。本データシートのブラウザ版を使用されている場合は、画面左側の説明をご覧ください。

## PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">LM2733XMF/NOPB</a>	Active	Production	SOT-23 (DBV)   5	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52A
LM2733XMF/NOPB.A	Active	Production	SOT-23 (DBV)   5	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52A
LM2733XMF/NOPB.B	Active	Production	SOT-23 (DBV)   5	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52A
<a href="#">LM2733XMF/NOPB</a>	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52A
LM2733XMF/NOPB.A	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52A
LM2733XMF/NOPB.B	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52A
<a href="#">LM2733YMF/NOPB</a>	Active	Production	SOT-23 (DBV)   5	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52B
LM2733YMF/NOPB.A	Active	Production	SOT-23 (DBV)   5	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52B
LM2733YMF/NOPB.B	Active	Production	SOT-23 (DBV)   5	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52B
<a href="#">LM2733YMF/NOPB</a>	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52B
LM2733YMF/NOPB.A	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52B
LM2733YMF/NOPB.B	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	S52B

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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## TAPE AND REEL INFORMATION



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM2733XMF/NOPB	SOT-23	DBV	5	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM2733XMF/NOPB	SOT-23	DBV	5	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM2733YMF/NOPB	SOT-23	DBV	5	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM2733YMF/NOPB	SOT-23	DBV	5	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3

## TAPE AND REEL BOX DIMENSIONS

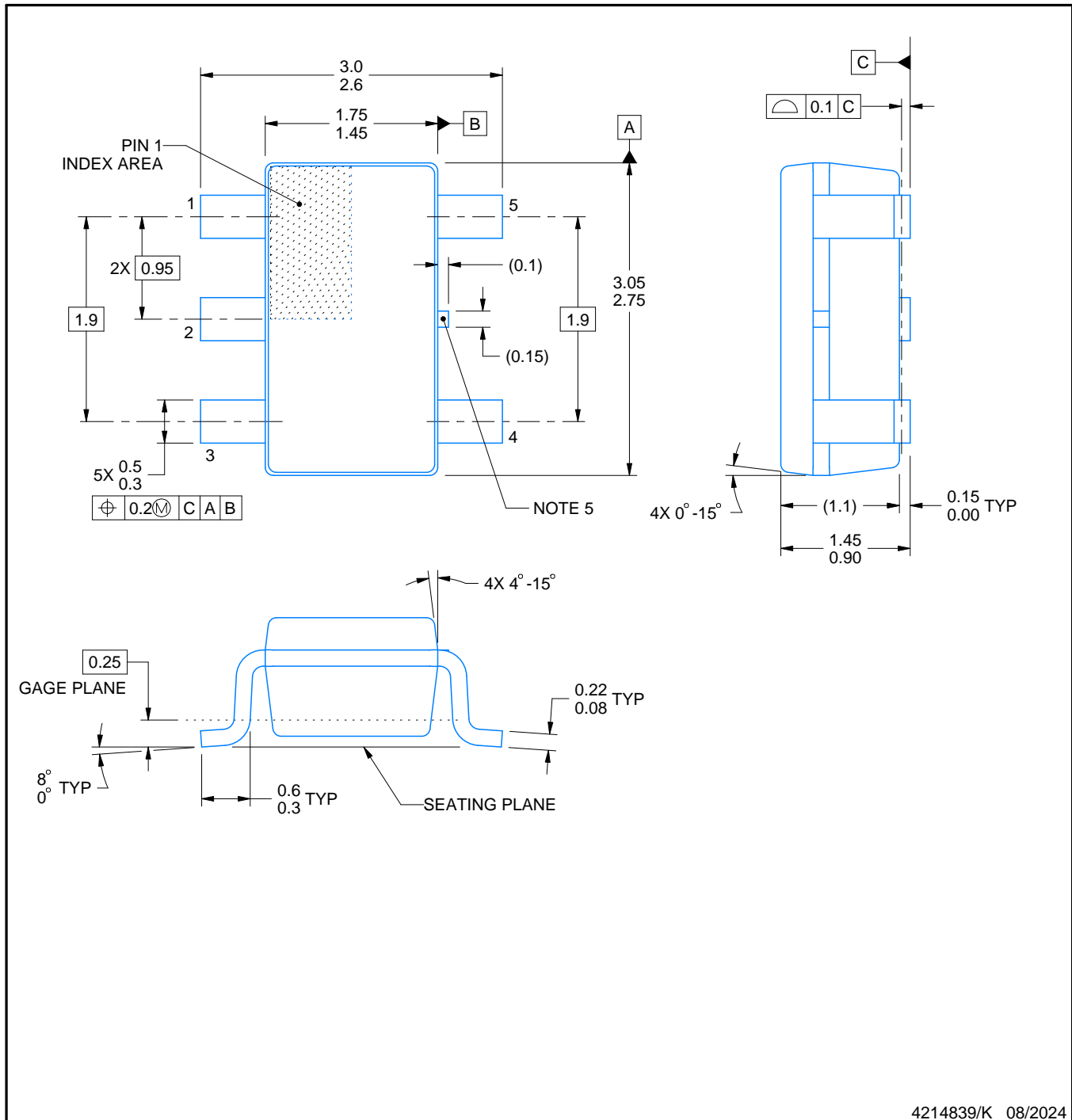


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM2733XMF/NOPB	SOT-23	DBV	5	1000	210.0	185.0	35.0
LM2733XMF/NOPB	SOT-23	DBV	5	3000	210.0	185.0	35.0
LM2733YMF/NOPB	SOT-23	DBV	5	1000	210.0	185.0	35.0
LM2733YMF/NOPB	SOT-23	DBV	5	3000	210.0	185.0	35.0

**DBV0005A****PACKAGE OUTLINE****SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



4214839/K 08/2024

**NOTES:**

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-178.
4. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25 mm per side.
5. Support pin may differ or may not be present.



# EXAMPLE BOARD LAYOUT

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

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NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

## EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

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NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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