TPS61085A-Q1 650kHz と 1.2MHz、18.5V、昇圧 DC/DC コンバータ

1 特長

- 車載アプリケーション用に AEC-Q100 認定取得済み
  - デバイス温度グレード 2: -40°C～+105°C、T_A
- 入力電圧範囲: 2.3V～6V
- スイッチ電流 2A の 18.5V 昇圧コンバータ
- 650kHz または 1.2MHz のスイッチング周波数を選択可能
- 調整可能なソフト・スタート
- サーマル・シャットダウン
- 低電圧誤動作防止
- 8 ピン VSSOP パッケージ

2 アプリケーション

- 車載用インフォテインメント・クラスタ
  - 計器板、ヘッド・ユニット
  - ラジオ、ナビゲーション
  - オーディオ・アンプ
- 車体用電子機器
  - 車体制御モジュール
  - ゲートウェイ
- テレマティクスおよび緊急通報 (E-Call)
- 先進運転支援システム (ADAS)

3 概要

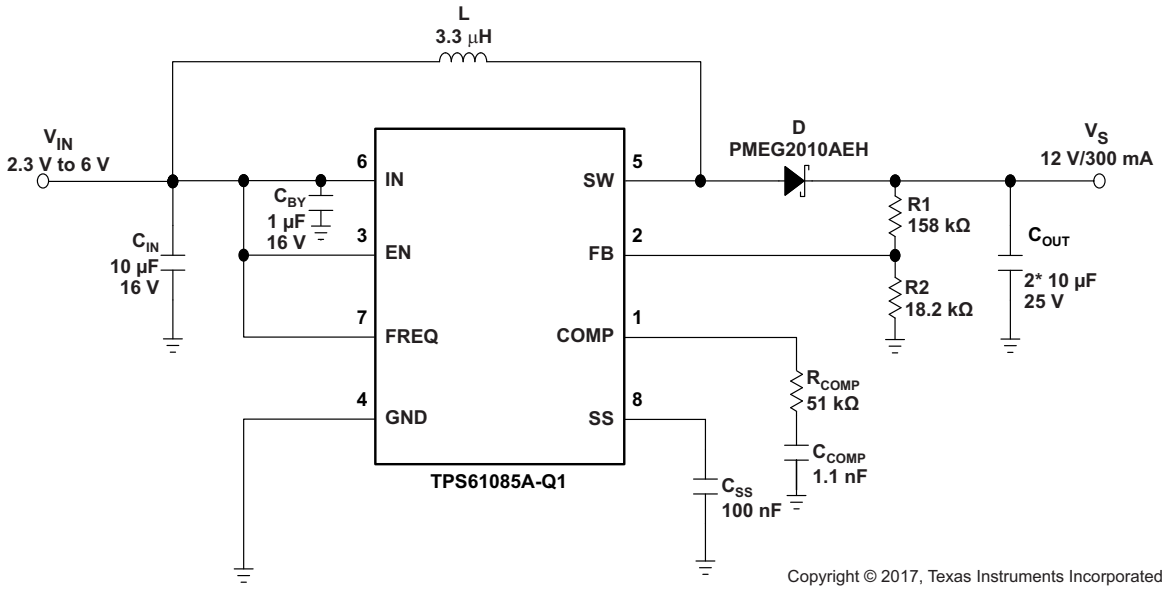
TPS61085A-Q1 デバイスは高周波数、高効率の DC/DC 昇圧コンバータで、2A、0.13Ω の電力スイッチが内蔵され、最大 18.5V の出力電圧を供給可能です。650kHz または 1.2MHz の周波数を選択可能なため、小型の外部インダクタおよびコンデンサを使用でき、高速な過渡応答が得られます。外部補償により、アプリケーションの状況に合わせてレギュレータを最適化できます。特定のソフトスタート・ピンに接続されるコンデンサにより、スタートアップ時の突入電流が最小化されます。

製品情報(1)

型番	パッケージ	本体サイズ(公称)
TPS61085A-Q1	VSSOP (8)	3.00mm×3.00mm

(1) 提供されているすべてのパッケージについては、データシートの末尾にある注文情報を参照してください。

概略回路図



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4 改訂履歴

Revision A (April 2018) から **Revision B** に変更 **Page**

- Web でのデータシートの最初の公開リリース ... 1

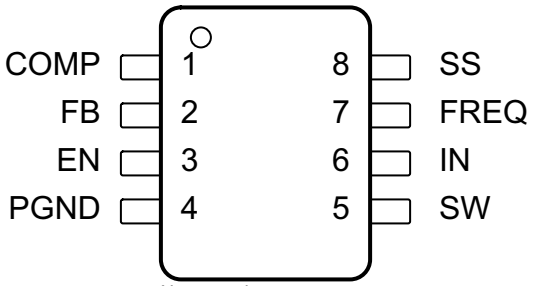
2017年9月発行のものから更新 **Page**

- ステータスを「量産データ」に 変更 ... 1

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5 Pin Configuration and Functions

DGK Package
8-Pin VSSOP
Top View



Not to scale

Pin Functions

PIN		TYPE	DESCRIPTION
NO.	NAME		
1	COMP	I/O	Compensation pin
2	FB	I	Feedback pin
3	EN	I	Shutdown control input. Connect this pin to logic high level to enable the device.
4	PGND	—	Power ground
5	SW	I	Switch pin
6	IN	PWR	Input supply pin
7	FREQ	I	Frequency select pin. The power switch operates at 650 kHz if FREQ is connected to GND and at 1.2 MHz if FREQ is connected to IN.
8	SS	O	Soft-start control pin. Connect a capacitor to this pin if soft-start required. Open = no soft start

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6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)(1)

	MIN	MAX	UNIT
Input voltage, IN(2)	–0.3	7	V
Voltage on pins EN, FB, SS, FREQ, COMP	–0.3	7	V
Voltage on pin SW	–0.3	20	V
Continuous power dissipation	See *Thermal Information*		
Lead temperature (soldering, 10 s)		260	°C
Operating junction temperature	–40	150	°C
Storage temperature, T_{stg}	–65	150	°C

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability
(2) All voltage values are with respect to network ground terminal.

6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), Classification Level 2 per AEC Q100-002(1)	±2000	V
		Charged-device model (CDM), Classification Level C4A per AEC Q100-011	±500	
		Machine model (MM)	±200	

(1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

6.3 Recommended Operating Conditions

		MIN	MAX	UNIT
V_{IN}	Input voltage	2.3	6	V
V_S	Boost output voltage	V_{IN} + 0.5	18.5	V
T_A	Operating free-air temperature	–40	105	°C
T_J	Operating junction temperature	–40	125	°C

6.4 Thermal Information

THERMAL METRIC(1)		TPS61085A-Q1 DGK (VSSOP) 8 PINS	UNIT
$R_{\theta JA}$	Junction-to-ambient thermal resistance	189.7	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	75.4	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	110	°C/W
ψ_{JT}	Junction-to-top characterization parameter	13.7	°C/W
ψ_{JB}	Junction-to-board characterization parameter	108.6	°C/W

(1) For more information about traditional and new thermal metrics, see the application report, *Semiconductor and IC Package Thermal Metrics*.

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6.5 Electrical Characteristics

V_{IN} = 3.3 V, EN = IN, V_S = 12 V, T_A = –40°C to +105°C, typical values are at T_A = 25°C (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
V_{IN}	Input voltage		2.3		6	V
I_Q	Operating quiescent current into IN	Device not switching, V_{FB} = 1.3 V		70	100	µA
I_{SDVIN}	Shutdown current into IN	EN = GND			1	µA
UVLO	Undervoltage lockout threshold	V_{IN} falling			2.2	V
		V_{IN} rising			2.3	
T_{SD}	Thermal shutdown	Temperature rising, T_J		150		°C
$T_{SD(HYS)}$	Thermal shutdown hysteresis			14		°C
LOGIC SIGNALS EN, FREQ						
V_{IH}	High level input voltage	V_{IN} = 2.3 V to 6 V	2			V
V_{IL}	Low level input voltage	V_{IN} = 2.3 V to 6 V			0.5	V
I_{lkg}	Input leakage current	EN = FREQ = GND			0.1	µA
BOOST CONVERTER						
V_S	Boost output voltage		V_{IN} + 0.5		18.5	V
V_{FB}	Feedback regulation voltage		1.230	1.238	1.246	V
gm	Transconductance error amplifier			107		µA/V
I_{FB}	Feedback input bias current	V_{FB} = 1.238 V			0.1	µA
$R_{DS(on)}$	N-channel MOSFET ON-resistance	V_{IN} = V_{GS} = 5 V, I_{SW} = current limit		0.13	0.2	Ω
		V_{IN} = V_{GS} = 3.3 V, I_{SW} = current limit		0.15	0.24	
I_{lkg}	SW leakage current	EN = GND, V_{SW} = 6 V			2	µA
I_{LIM}	N-channel MOSFET current limit		2	2.6	3.2	A
I_{SS}	Soft-start current	V_{SS} = 1.238 V	7	10	13	µA
f_{osc}	Oscillator frequency	FREQ = high	0.9	1.2	1.5	MHz
		FREQ = low	480	650	820	kHz
	Line regulation	V_{IN} = 2.3 V to 6 V, I_{OUT} = 10 mA		0.0002		%/V
	Load regulation	V_{IN} = 3.3 V, I_{OUT} = 1 mA to 400 mA		0.11		%/A

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6.6 Typical Characteristics

The typical characteristics are measured with the 3.3-µH inductor for high-frequency (part number-7447789003) or 6.8-µH inductor for low frequency (part number-B82464G4) and the rectifier diode with part number SL22.

Table 1. Table of Graphs

			FIGURE
$I_{OUT(max)}$	Maximum load current	vs Input voltage at high frequency (1.2 MHz)	Figure 1
		vs Input voltage at low frequency (650 kHz)	Figure 2
η	Efficiency	vs Load current, V_S = 12 V, V_{IN} = 3.3 V	Figure 3
		vs Load current, V_S = 9 V, V_{IN} = 3.3 V	Figure 4
	Supply current	vs Supply voltage	Figure 5
	Frequency	vs Load current	Figure 6
		vs Supply voltage	Figure 7

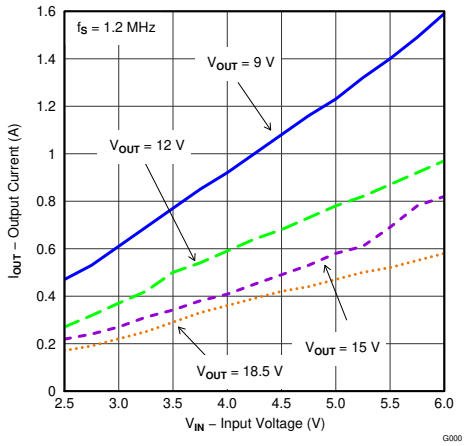


Figure 1. Maximum Load Current vs Input Voltage

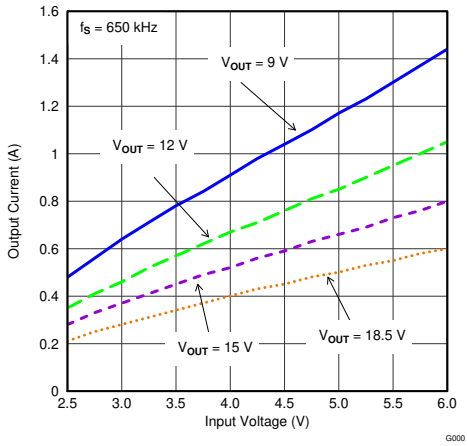


Figure 2. Maximum Load Current vs Input Voltage

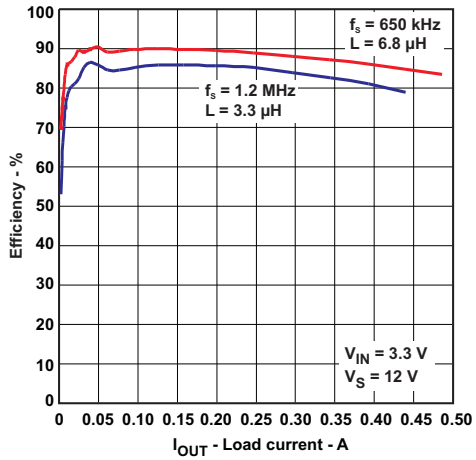


Figure 3. Efficiency vs Load Current, V_S = 12 V, V_{IN} = 3.3 V

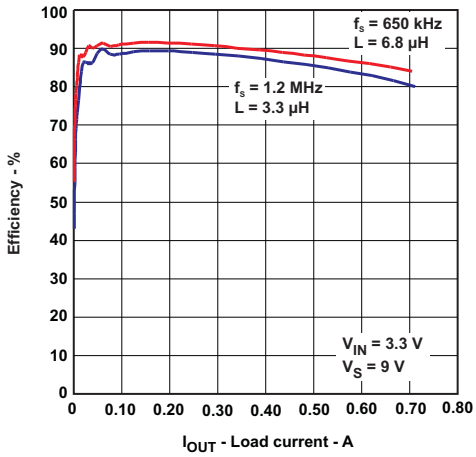


Figure 4. Efficiency vs Load Current, V_S = 9 V, V_{IN} = 3.3 V

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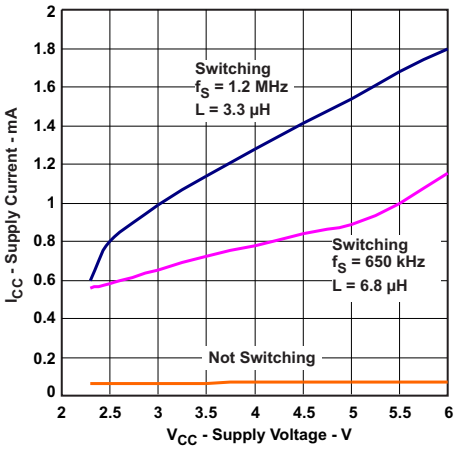


Figure 5. Supply Current vs Supply Voltage

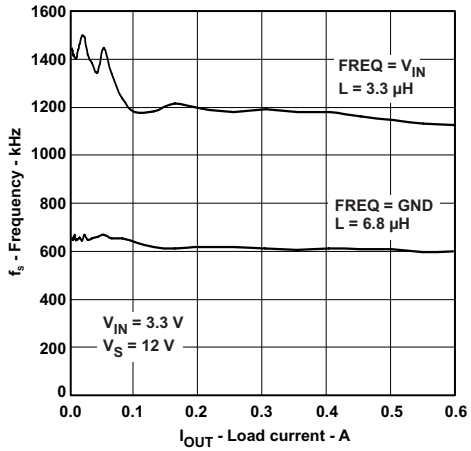


Figure 6. Frequency vs Load Current

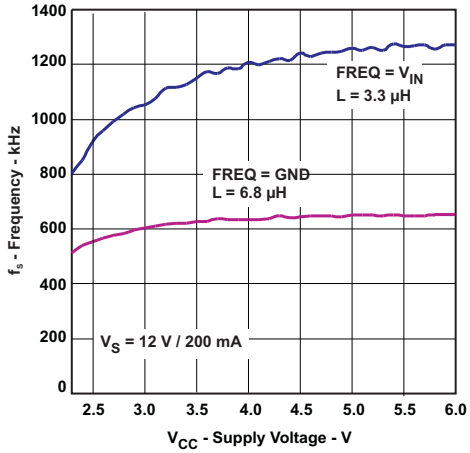


Figure 7. Frequency vs Supply Voltage

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7 Detailed Description

7.1 Overview

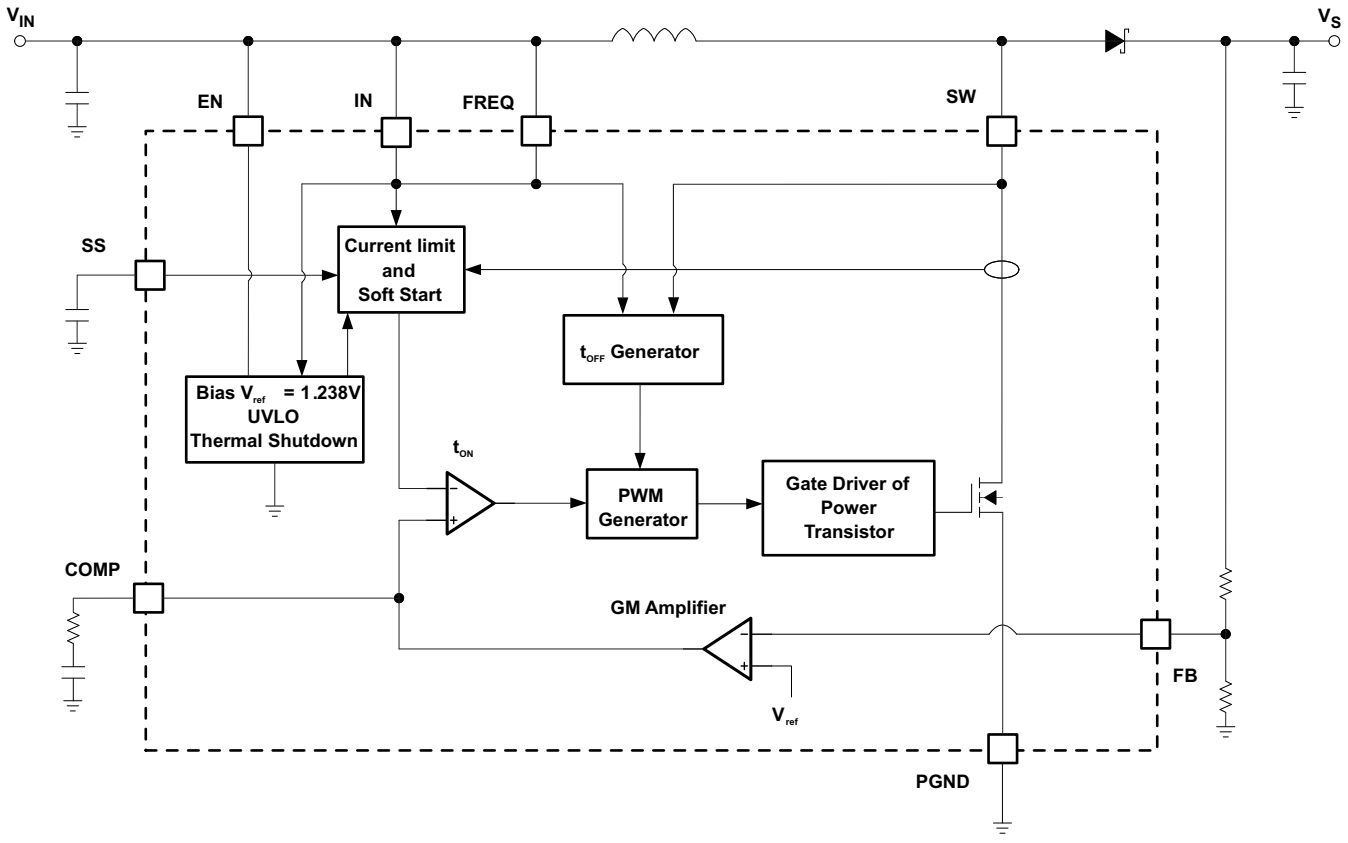
The TPS61085A-Q1 boost converter is designed for output voltages up to 18.5 V with a switch-peak current limit of 2 A minimum. The device, which operates in a current mode scheme with quasi-constant frequency, is externally compensated for maximum flexibility and stability. The switching frequency is selectable between 650 kHz or 1.2 MHz and the minimum input voltage is 2.3 V. To control the inrush current at start-up, a soft-start pin is available.

The novel topology of the TPS61085A-Q1 boost converteruses adaptive OFF-time to provide superior load and line transient responses. The device also operates over a wider range of applications than conventional converters.

The selectable switching frequency offers the possibility to optimize the design either for the use of small sized components (1.2 MHz) or for higher system efficiency (650 kHz). However, the frequency changes slightly because the voltage drop across the $R_{DS(on)}$ has some influence on the current and voltage measurement and thus on the ON-time (the OFF-time remains constant).

Depending on the load current, the converter operates in continuous conduction mode (CCM), discontinuous conduction mode (DCM), or pulse skip mode to maintain the output voltage.

7.2 Functional Block Diagram



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7.3 Feature Description

7.3.1 Soft Start

The boost converter has an adjustable soft start to prevent high inrush current during start-up. To minimize the inrush current during start-up an external capacitor connected to the soft-start pin SS is used to slowly ramp up the internal current limit of the boost converter when charged with a constant current. When the EN pin is pulled high, the soft-start capacitor (C_{SS}) is immediately charged to 0.3 V. The capacitor is then charged at a constant current of 10 µA typically until the output of the boost converter V_S has reached its power good threshold (90% of V_S nominal value). During this time, the SS voltage directly controls the peak inductor current, starting with 0 A at V_{SS} = 0.3 V up to the full current limit at V_{SS} ≈ 800 mV. The maximum load current is available after the soft start is completed. The larger the capacitor the slower the ramp of the current limit and the longer the soft-start time. A 100-nF capacitor is usually sufficient for most of the applications. When the EN pin is pulled low, the soft-start capacitor is discharged to ground.

7.3.2 Frequency Select Pin (FREQ)

The frequency select pin FREQ allows to set the switching frequency of the device to 650 kHz (FREQ = low) or 1.2 MHz (FREQ = high). Higher switching frequency improves load transient response but reduces slightly the efficiency. The other benefits of higher switching frequency are a lower output ripple voltage and smaller inductor size. Usually, TI recommends using 1.2-MHz switching frequency unless light-load efficiency is a major concern.

7.3.3 Undervoltage Lockout (UVLO)

To avoid misoperation of the device at low input voltages an undervoltage lockout is included that disables the device, if the input voltage falls below 2.2 V.

7.3.4 Thermal Shutdown

A thermal shutdown is implemented to prevent damages due to excessive heat and power dissipation. Typically the thermal shutdown threshold is at T_J = 150°C. When the thermal shutdown is triggered the device stops switching until the temperature falls below typically T_J = 136°C. Then the device starts switching again.

7.3.5 Overvoltage Prevention

If overvoltage is detected on the FB pin (typically 3% above the nominal value of 1.238 V) the part stops switching immediately until the voltage on this pin drops to its nominal value. This prevents overvoltage on the output and secures the circuits connected to the output from excessive overvoltage.

7.4 Device Functional Modes

The converter operates in continuous conduction mode (CCM) as soon as the input current increases above half the ripple current in the inductor. For lower load currents it switches into discontinuous conduction mode (DCM). If the load is further reduced, the part starts to skip pulses to maintain the output voltage.

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8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

With the TPS61085A-Q1 device, a boost regulator with an output voltage of up to 18.5 V can be designed with input voltage ranging from 2.3 V to 6 V. The TPS61085A-Q1 device has a peak switch current limit of 2 A minimum. The device, which operates in a current mode scheme and uses simple external compensation scheme for maximum flexibility and stability. Selectable switching frequency allows the regulator to be optimized either for smaller size (1.2 MHz) or for higher system efficiency (650 KHz). A dedicated soft-start (SS) pin allows the designer to control the inrush current at start-up.

The following section provides a step-by-step design approach for configuring the TPS61085A-Q1 as a voltage regulating boost converter.

8.2 Typical Application

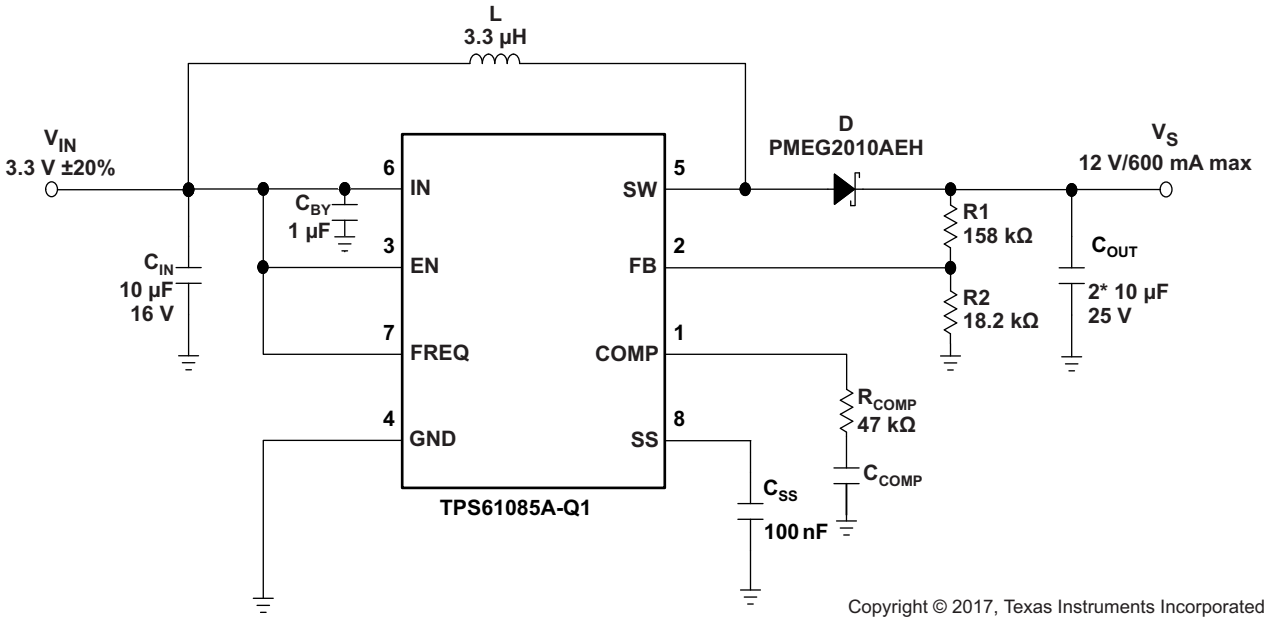


Figure 8. Typical Application, 3.3 V to 12 V (f_{sw} = 1.2 MHz)

8.2.1 Design Requirements

Table 2 lists the design parameters for this application example.

Table 2. TPS61085A-Q1 Output Design Requirements

PARAMETER	VALUE
Input voltage	3.3 V ± 20%
Output voltage	12 V
Output current	600 mA
Switching frequency	1.2 MHz

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8.2.2 Detailed Design Procedure

The first step in the design procedure is to verify that the maximum possible output current of the boost converter supports the specific application requirements. A simple approach is to estimate the converter efficiency, by taking the efficiency numbers from the provided efficiency curves or to use a worst-case assumption for the expected efficiency, for example, 90%.

1. Duty cycle:

$$D = 1 - \frac{V_{IN} \times \eta}{V_S} \quad (1)$$

2. Maximum output current:

$$Iout = \left(I_{swpeak} - \frac{\Delta I_L}{2} \right) \times (1 - D) \quad (2)$$

3. Peak switch current:

$$I_{swpeak} = \frac{\Delta I_L}{2} + \frac{I_{out}}{1 - D}$$

where

$$\Delta I_L = \frac{V_{IN} \times D}{fs \times L} \quad (3)$$

- I_{swpeak} = converter switch current (minimum switch current limit = 2 A)
- fs = Converter switching frequency (typically 1.2 MHz)
- L = Selected inductor value
- η = Estimated converter efficiency (please use the number from the efficiency plots or 90% as an estimation)
- ΔI_L = Inductor peak-to-peak ripple current

The peak switch current is the steady-state peak switch current that the integrated switch, inductor, and external Schottky diode must be able to handle. The calculation must be done for the minimum input voltage where the peak switch current is the highest.

8.2.2.1 Inductor Selection

The TPS61085A-Q1 is designed to work with a wide range of inductors. The main parameter for the inductor selection is the saturation current of the inductor which must be higher than the peak switch current as calculated in *Detailed Design Procedure* with additional margin to cover for heavy load transients. An alternative, more conservative option is to choose an inductor with a saturation current at least as high as the maximum switch current limit of 3.2 A. The other important parameter is the inductor DC resistance. Usually, the lower the DC resistance the higher the efficiency. It is important to note that the inductor DC resistance is not the only parameter determining the efficiency. Especially for a boost converter where the inductor is the energy storage element, the type and core material of the inductor influences the efficiency as well. At high switching frequencies of 1.2-MHz inductor core losses, proximity effects and skin effects become more important. Usually, an inductor with a larger form factor gives higher efficiency. The efficiency difference between different inductors can vary between 2% to 10%. For the TPS61085A-Q1, inductor values between 3 µH and 6 µH are a good choice with a switching frequency of 1.2 MHz, typically 3.3 µH. At 650 kHz, TI recommends inductors between 6 µH and 13 µH, typically 6.8 µH. Table 3 shows a few inductors. Customers must verify and validate these components for suitability with their application before using them.

Typically, TI recommends the inductor current ripple is below 20% of the average inductor current. Calculate the inductor value using Equation 4.

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$$L = \left(\frac{V_{IN}}{V_S}\right)^2 \times \left(\frac{V_S - V_{IN}}{I_{out_max} \times f}\right) \times \left(\frac{\eta}{0.35}\right)$$

where

- L is the inductor value
- V_{IN} is input voltage
- V_S is boost output voltage
- η is efficiency
- I_{out_max} is the maximum output current
- f is frequency

(4)

Table 3. Inductor Selection

L (µH)	SUPPLIER (1)	COMPONENT CODE	SIZE (L×W×H mm)	DCR TYP (mΩ)	Isat (A)
1.2 MHz					
3.3	Sumida	CDH38D09	4 × 4 × 1	240	1.25
4.7	Sumida	CDPH36D13	5 × 5 × 1.5	155	1.36
3.3	Sumida	CDPH4D19F	5.2 × 5.2 × 2	33	1.5
3.3	Sumida	CDRH6D12	6.7 × 6.7 × 1.5	62	2.2
4.7	Würth Elektronik	7447785004	5.9 × 6.2 × 3.3	60	2.5
5	Coilcraft	MSS7341	7.3 × 7.3 × 4.1	24	2.9
650 kHz					
6.8	Sumida	CDP14D19	5.2 × 5.2 × 2	50	1
10	Coilcraft	LPS4414	4.3 × 4.3 × 1.4	380	1.2
6.8	Sumida	CDRH6D12/LD	6.7 × 6.7 × 1.5	95	1.25
10	Sumida	CDR6D23	5 × 5 × 2.4	133	1.75
10	Würth Elektronik	744778910	7.3 × 7.3 × 3.2	51	2.2
6.8	Sumida	CDRH6D26HP	7 × 7 × 2.8	52	2.9

(1) See *Third-party Products Disclaimer*

8.2.2.2 Rectifier Diode Selection

To achieve high efficiency, a Schottky type must be used for the rectifier diode. The reverse voltage rating must be higher than the maximum output voltage of the converter. The averaged rectified forward current I_{avg}, the Schottky diode requirement is rated for, is equal to the output current I_{out}:

$$I_{avg} = I_{out}$$

(5)

Usually a Schottky diode with 2-A maximum average rectified forward current rating is sufficient for most applications. The Schottky rectifier can be selected with lower forward current capability depending on the output current I_{out} but must be able to dissipate the power. The dissipated power is the average rectified forward current times the diode forward voltage.

$$P_D = I_{avg} \times V_{forward} \quad (6)$$

Typically the diode must be able to dissipate around 500 mW depending on the load current and forward voltage. See Table 4 for few diode options. Customers must verify and validate these components for suitability with their application before using them.

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Table 4. Rectifier Diode Selection

CURRENT RATING (Iavg)	Vr	$V_{forward\ /\ Iavg}$	SUPPLIER(1)	COMPONENT CODE	PACKAGE TYPE
750 mA	20 V	0.425 V / 750 mA	Fairchild Semiconductor	FYV0704S	SOT-23
1 A	20 V	0.39 V / 1 A	NXP	PMEG2010AEH	SOD-123
1 A	20 V	0.52 V / 1 A	Vishay Semiconductor	B120	SMA
1 A	20 V	0.5 V / 1 A	Vishay Semiconductor	SS12	SMA
1 A	20 V	0.44 V / 1 A	Vishay Semiconductor	MSS1P2L	µ-SMP (Low Profile)

(1) See *Third-party Products Disclaimer*

8.2.2.3 Setting the Output Voltage

The output voltage is set by an external resistor divider. Typically, a minimum current of 50 µA flowing through the feedback divider gives good accuracy and noise covering. A standard low-side resistor of 18 kΩ is typically selected. The resistors are then calculated as:

$$R2 = \frac{Vref}{70\mu A} \approx 18k\Omega \qquad R1 = R2 \times \left(\frac{Vs}{Vref} - 1 \right) \tag{7}$$

8.2.2.4 Compensation (COMP)

The regulator loop must be compensated by adjusting the external components connected to the COMP pin. The COMP pin is the output of the internal transconductance error amplifier. Standard values of R_{COMP} = 13 kΩ and C_{COMP} = 3.3 nF works for the majority of the applications.

See Table 5 for dedicated compensation networks giving an improved load transient response. Equation 8 can be used to calculate R_{COMP} and C_{COMP}:

$$R_{COMP} = \frac{110 \cdot V_{IN} \cdot V_s \cdot C_{OUT}}{L \cdot I_{OUT}} \qquad C_{COMP} = \frac{V_s \cdot C_{OUT}}{7.5 \cdot I_{OUT} \cdot R_{COMP}} \tag{8}$$

Table 5. Recommended Compensation Network Values at High/Low Frequency

FREQUENCY	L	V_S	V_{IN} ±20%	R_{COMP}	C_{COMP}
High (1.2 MHz)	3.3 µH	15 V	5 V	82 kΩ	1.1 nF
			3.3 V	75 kΩ	1.6 nF
		12 V	5 V	51 kΩ	1.1 nF
			3.3 V	47 kΩ	1.6 nF
		9 V	5 V	30 kΩ	1.1 nF
			3.3 V	27 kΩ	1.6 nF
Low (650 kHz)	6.8 µH	15 V	5 V	43 kΩ	2.2 nF
			3.3 V	39 kΩ	3.3 nF
		12 V	5 V	27 kΩ	2.2 nF
			3.3 V	24 kΩ	3.3 nF
		9 V	5 V	15 kΩ	2.2 nF
			3.3 V	13 kΩ	3.3 nF

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Table 5 gives conservatives R_{COMP} and C_{COMP} values for certain inductors, input and output voltages providing a very stable system. For a faster response time, a higher R_{COMP} value can be used to enlarge the bandwidth, as well as a slightly lower value of C_{COMP} to keep enough phase margin. These adjustments must be performed in parallel with the load transient response monitoring of TPS61085A-Q1.

8.2.2.5 Input Capacitor Selection

For good input voltage filtering, TI recommends low-ESR ceramic capacitors. TPS61085A-Q1 has an analog input (IN). Therefore, TI highly recommends placing a 1-uF bypass capacitor as close as possible to the IC from IN to GND.

One 10-µF ceramic input capacitor is sufficient for most of the applications. For better input voltage, filtering this value can be increased. Refer to Table 6 and typical applications for input capacitor recommendations. Customers must verify and validate these components for suitability with their application before using them.

8.2.2.6 Output Capacitor Selection

For best output voltage filtering, TI recommends a low ESR output capacitor like ceramic capacitor. Two 10-µF ceramic output capacitors (or one 22-µF) work for most of the applications. Higher capacitor values can be used to improve the load transient response.

Pay attention to the derating of capacitor value with the DC voltage.

Table 6. Rectifier Input and Output Capacitor Selection

	CAPACITOR	VOLTAGE RATING	SUPPLIER(1)	COMPONENT CODE
C_{IN}	10 µF/1206	16 V	Taiyo Yuden	EMK212 BJ 106KG
IN bypass	1 µF/0603	16 V	Taiyo Yuden	EMK107 BJ 105KA
C_{OUT}	10 µF/1206	25 V	Taiyo Yuden	TMK316 BJ 106KL

(1) See *Third-party Products Disclaimer*

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8.2.3 Application Curves

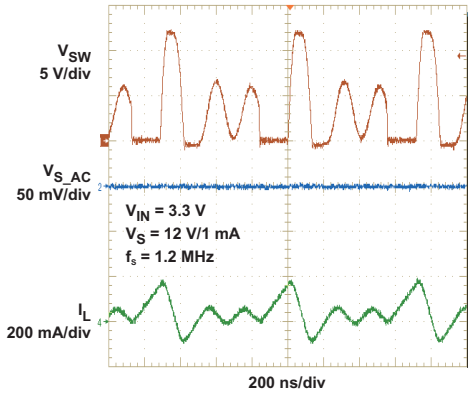


Figure 9. PWM Switching Discontinuous Conduction Mode

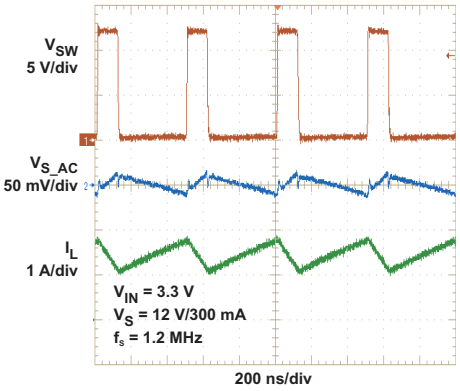


Figure 10. PWM Switching Continuous Conduction Mode

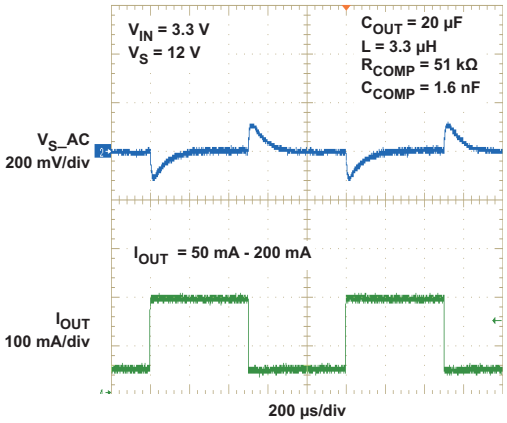


Figure 11. Load Transient Response High Frequency (1.2 MHz)

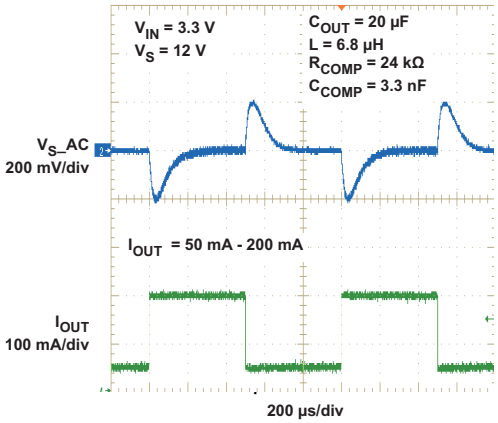


Figure 12. Load Transient Response Low Frequency (650 kHz)

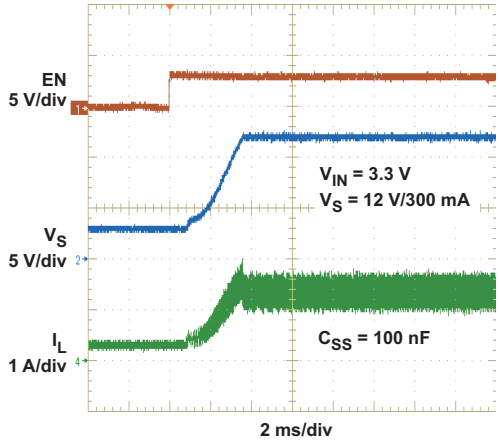


Figure 13. Soft Start

8.3 System Examples

Figure 14 to Figure 21 show application circuit examples using the TPS61085A-Q1 device. These circuits must be fully validated and tested by customers before using these circuits in their designs. TI does not warrant the accuracy or completeness of these circuits, nor does TI accept any responsibility for them.

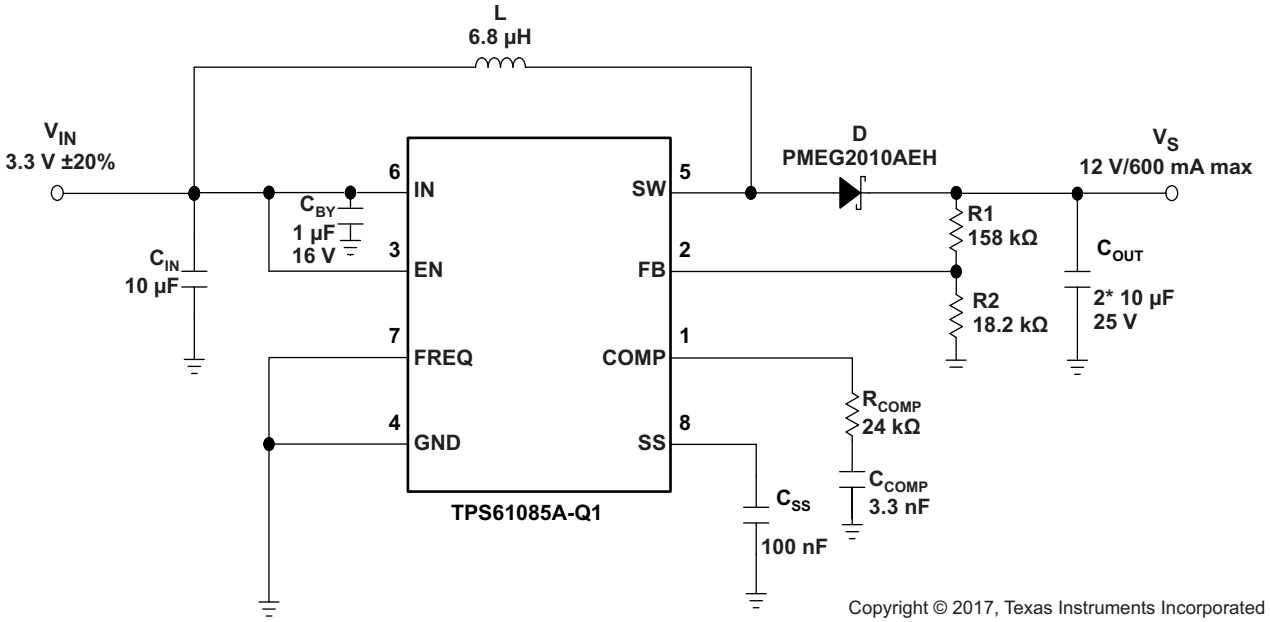


Figure 14. Typical Application, 3.3 V to 12 V (f_{sw} = 650 kHz)

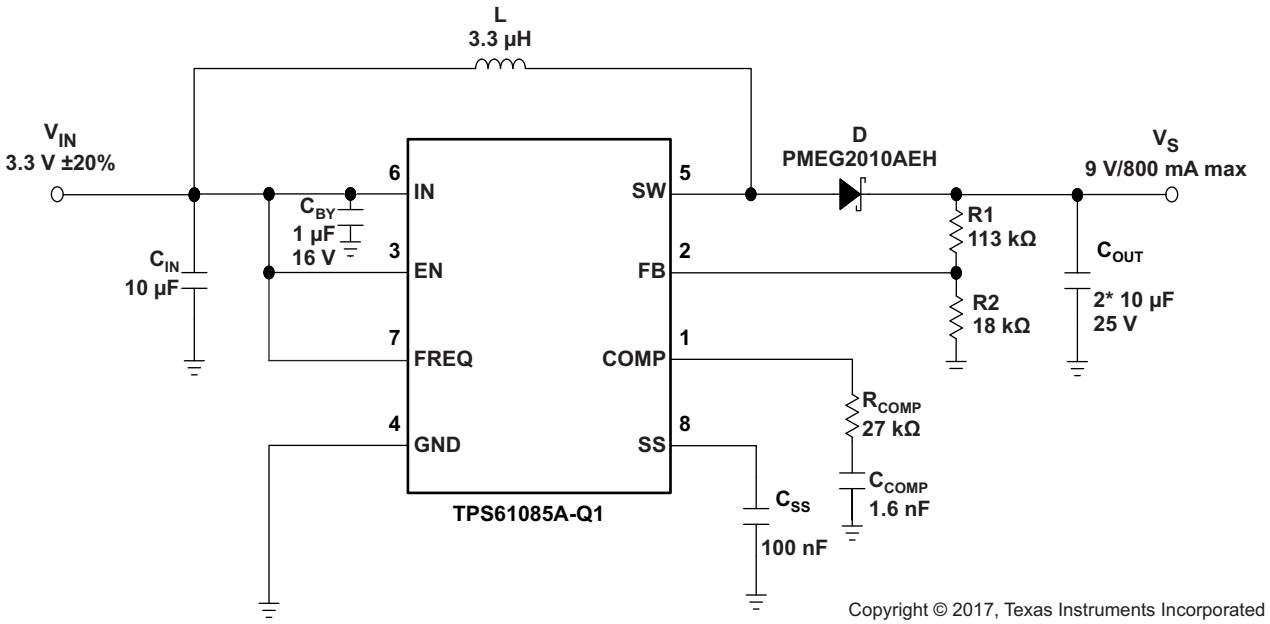


Figure 15. Typical Application, 3.3 V to 9 V (f_{sw} = 1.2 MHz)

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System Examples (continued)

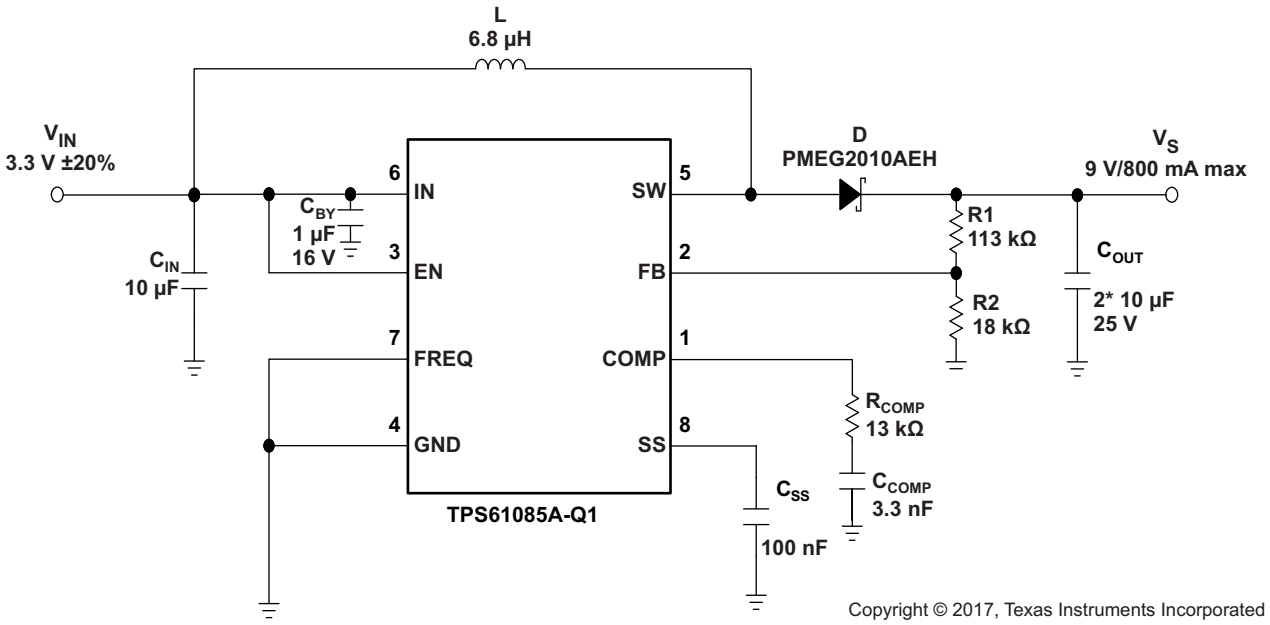


Figure 16. Typical Application, 3.3 V to 9 V (f_{sw} = 650 kHz)

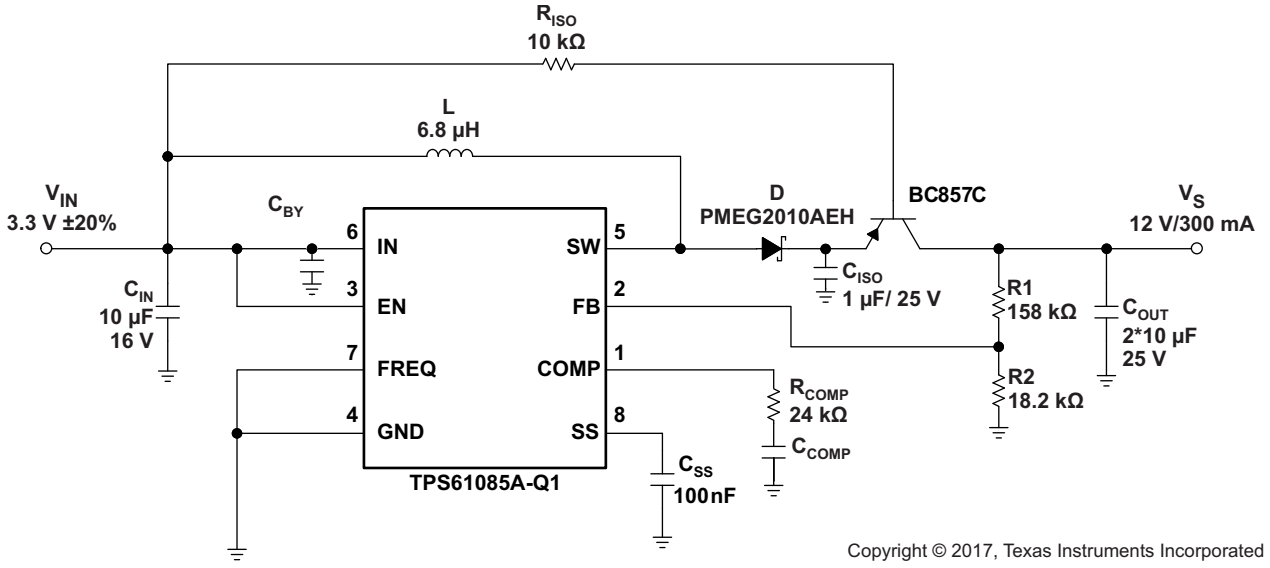


Figure 17. Typical Application With External Load Disconnect Switch

System Examples (continued)

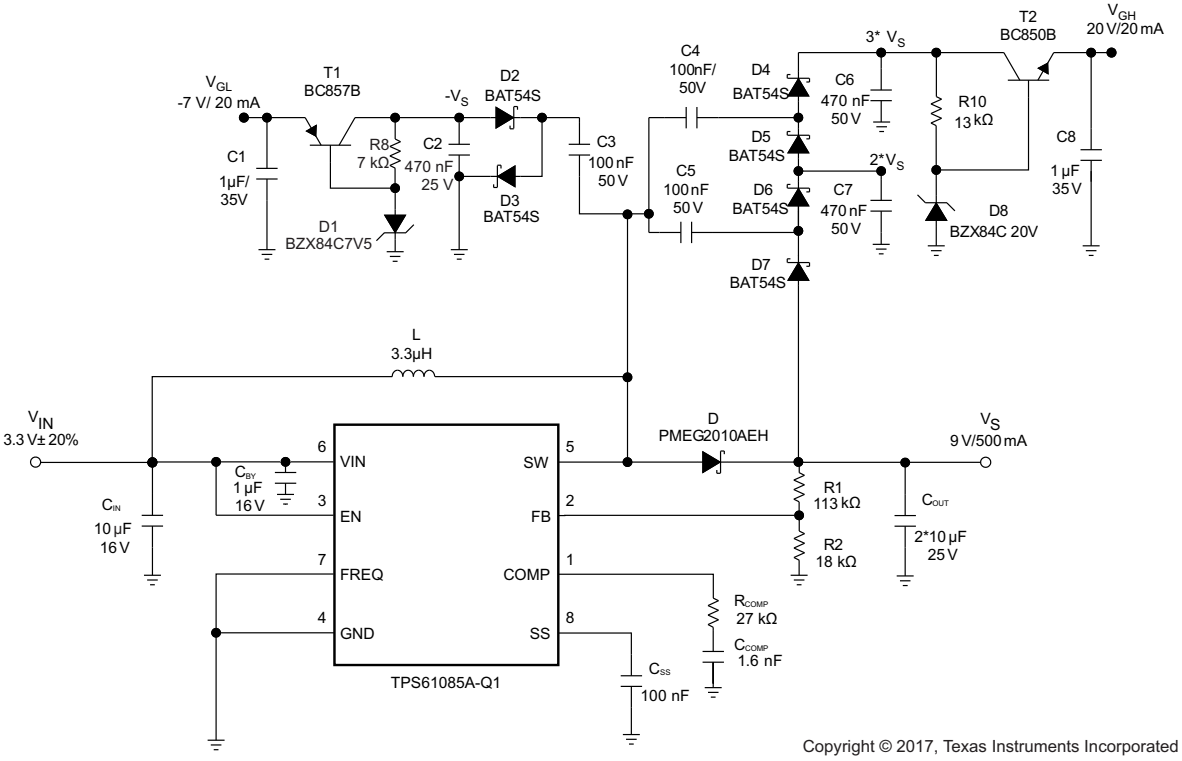


Figure 18. Typical Application 3.3 V to 9 V (f_{SW} = 1.2 MHz) For TFT LCD With External Charge Pumps (VGH, VGL)

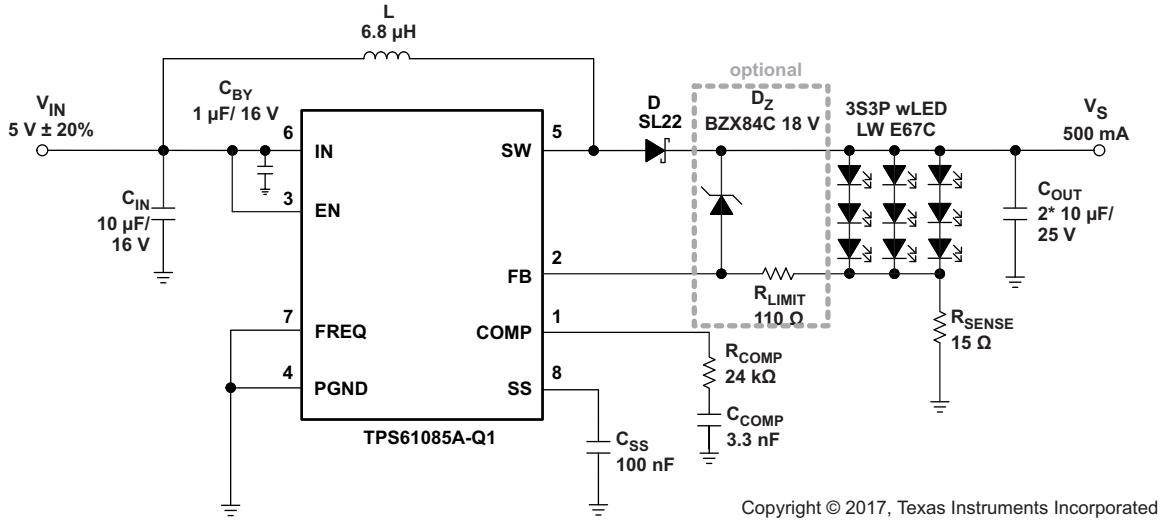


Figure 19. Simple Application (5-V Input, f_{SW} = 650 kHz) For wLED Supply (3S3P) (With Optional Clamping Zener Diode)

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System Examples (continued)

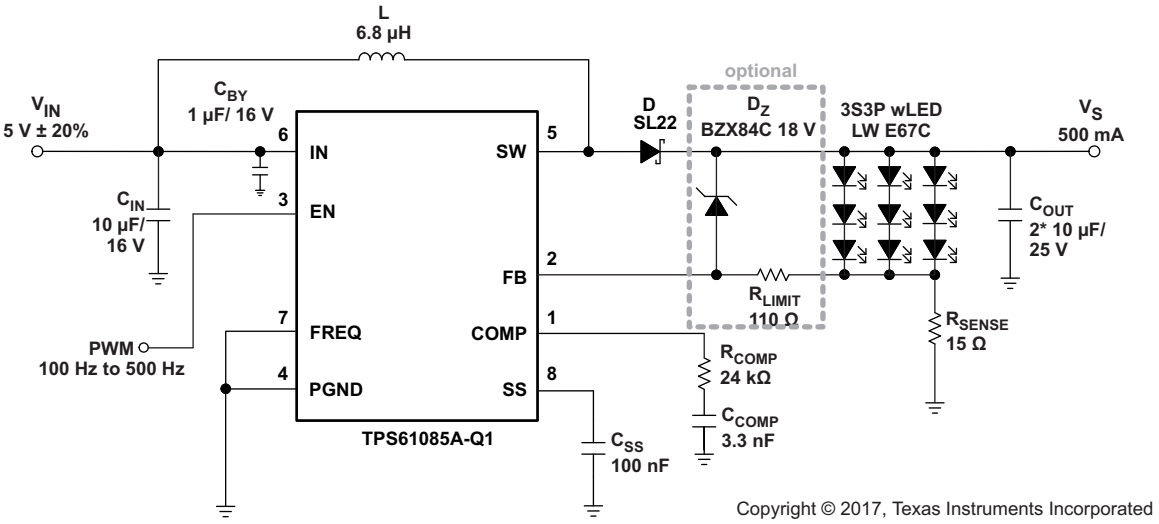


Figure 20. Simple Application (3.3-V Input, f_{SW} = 650 kHz) For wLED Supply (3S3P) With Adjustable Brightness Control Using a PWM Signal on the Enable Pin (With Optional Clamping Zener Diode)

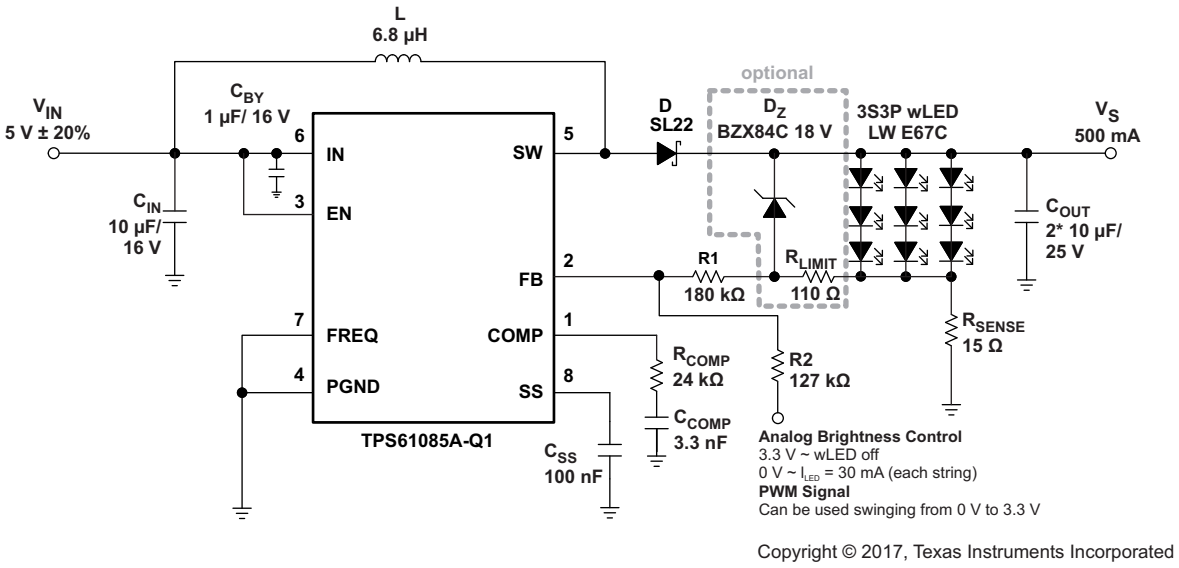


Figure 21. Simple Application (3.3-V Input, f_{SW} = 650 kHz) For wLED Supply (3S3P) With Adjustable Brightness Control Using an Analog Signal on the Feedback Pin (With Optional Clamping Zener Diode)

9 Power Supply Recommendations

The TPS61085A-Q1 is designed to operate from an input voltage supply range from 2.3 V to 6 V. The required power supply for the TPS61085A-Q1 must have a current rating according to the output voltage and output current of the TPS61085A-Q1.

10 Layout

10.1 Layout Guidelines

For all switching power supplies, the layout is an important step in the design, especially at high peak currents and high switching frequencies. If the layout is not carefully done, the regulator could show stability problems as well as EMI problems.

Layout Example provides an example of layout design with the TPS61085A-Q1 device.

- Use wide and short traces for the main current path and for the power ground tracks.
- The input capacitor, output capacitor, and the inductor must be placed as close as possible to the IC.
- Use a common ground node for power ground and a different one for control ground to minimize the effects of ground noise. Connect these ground nodes at the GND terminal of the IC.
- The most critical current path for all boost converters is from the switching FET, through the rectifier diode, then the output capacitors, and back to ground of the switching FET. Therefore, the output capacitors and their traces must be placed on the same board layer as the IC and as close as possible between the SW pin and the GND terminal of the IC.

10.2 Layout Example

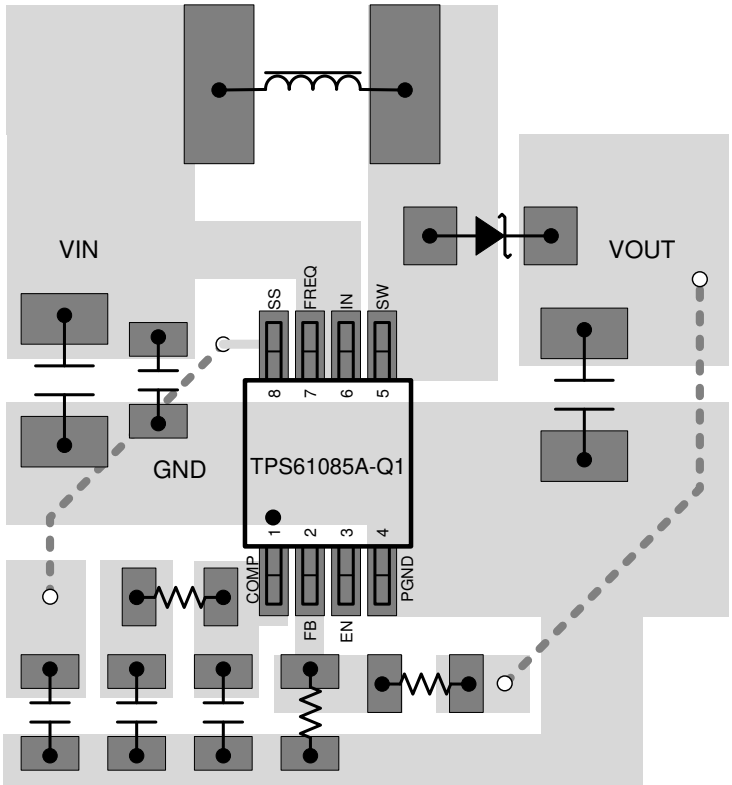


Figure 22. TPS61085A-Q1 Layout Example

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11 デバイスおよびドキュメントのサポート

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11.6 Glossary

SLYZ022 — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

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PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package | Pins	Package qty | Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS61085ATDGKRQ1	Active	Production	VSSOP (DGK) | 8	2000 | LARGE T&R	Yes	Call TI | Nipdauag	Level-3-260C-168 HR	-40 to 125	1EGV
TPS61085ATDGKRQ1.B	Active	Production	VSSOP (DGK) | 8	2000 | LARGE T&R	Yes	Call TI	Level-3-260C-168 HR	-40 to 125	1EGV
TPS61085ATDGKTQ1	Active	Production	VSSOP (DGK) | 8	250 | SMALL T&R	Yes	Call TI | Nipdauag	Level-3-260C-168 HR	-40 to 125	1EGV
TPS61085ATDGKTQ1.B	Active	Production	VSSOP (DGK) | 8	250 | SMALL T&R	Yes	Call TI	Level-3-260C-168 HR	-40 to 125	1EGV

(1) **Status:** For more details on status, see our product life cycle.

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

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(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

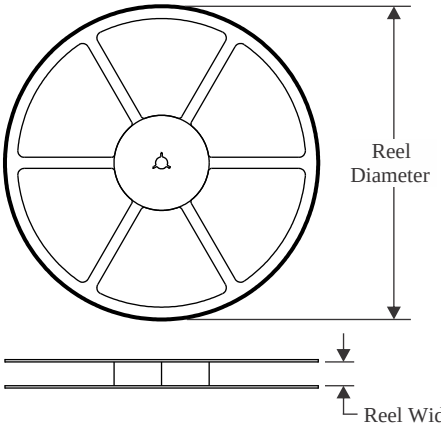
Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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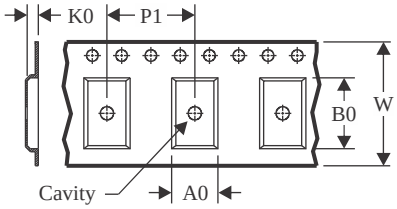
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TAPE AND REEL INFORMATION

REEL DIMENSIONS

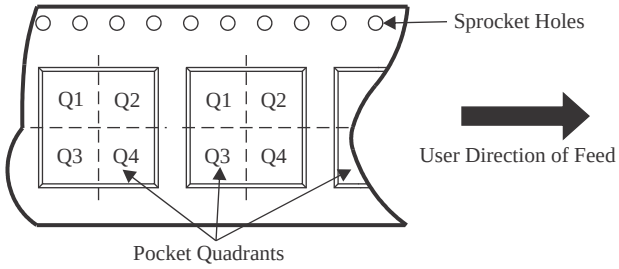


TAPE DIMENSIONS



A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

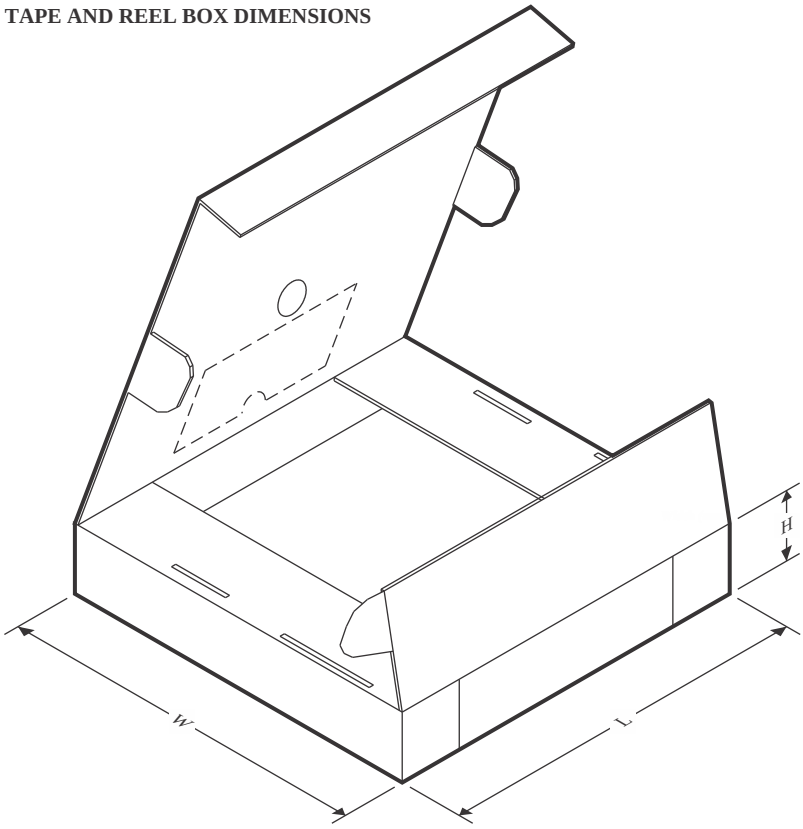
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS61085ATDGKRQ1	VSSOP	DGK	8	2000	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
TPS61085ATDGKRQ1	VSSOP	DGK	8	2000	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
TPS61085ATDGKTQ1	VSSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
TPS61085ATDGKTQ1	VSSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

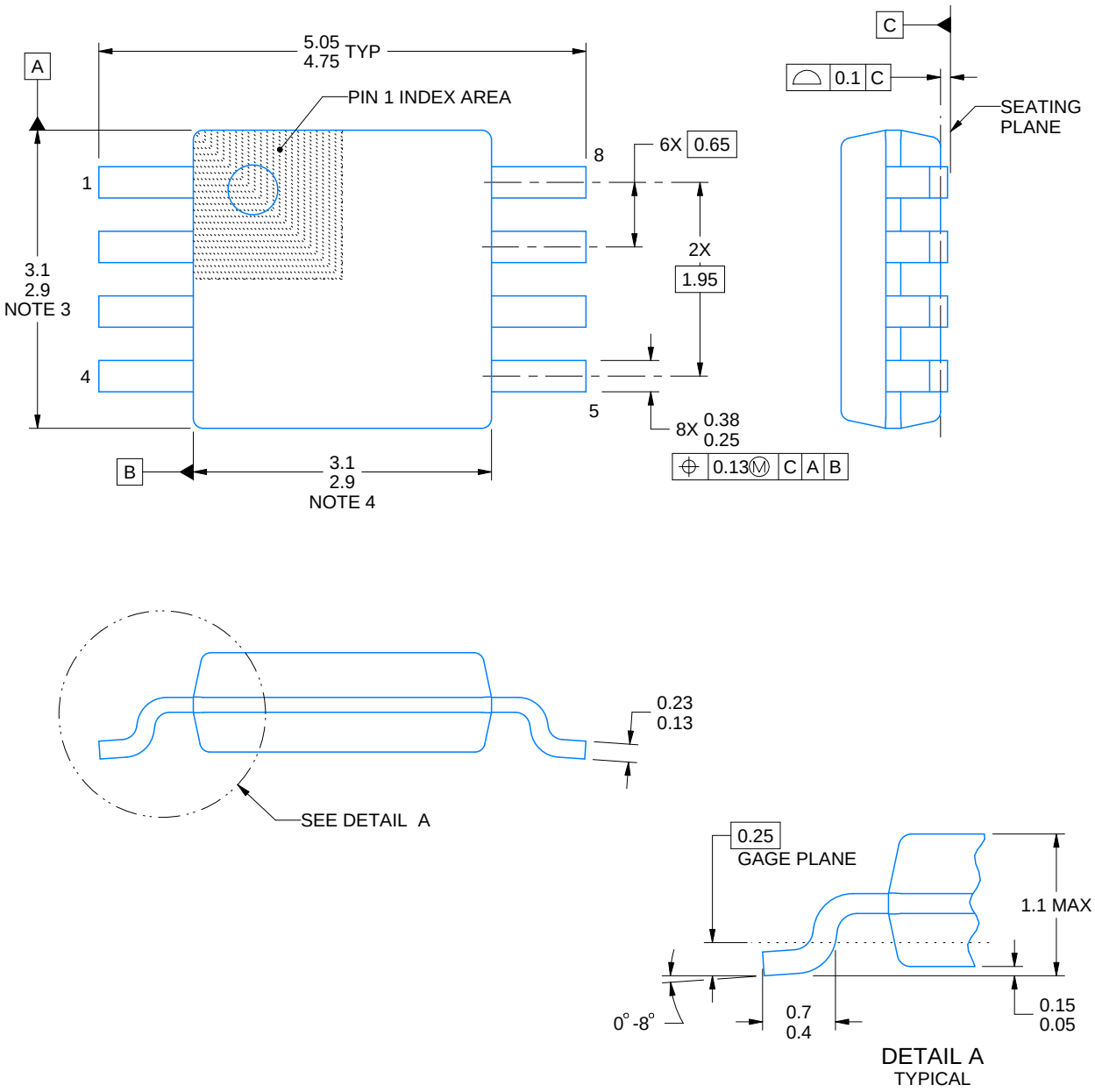
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS61085ATDGKRQ1	VSSOP	DGK	8	2000	353.0	353.0	32.0
TPS61085ATDGKRQ1	VSSOP	DGK	8	2000	353.0	353.0	32.0
TPS61085ATDGKTQ1	VSSOP	DGK	8	250	213.0	191.0	35.0
TPS61085ATDGKTQ1	VSSOP	DGK	8	250	210.0	185.0	35.0

PACKAGE OUTLINE

DGK0008A

VSSOP - 1.1 mm max height

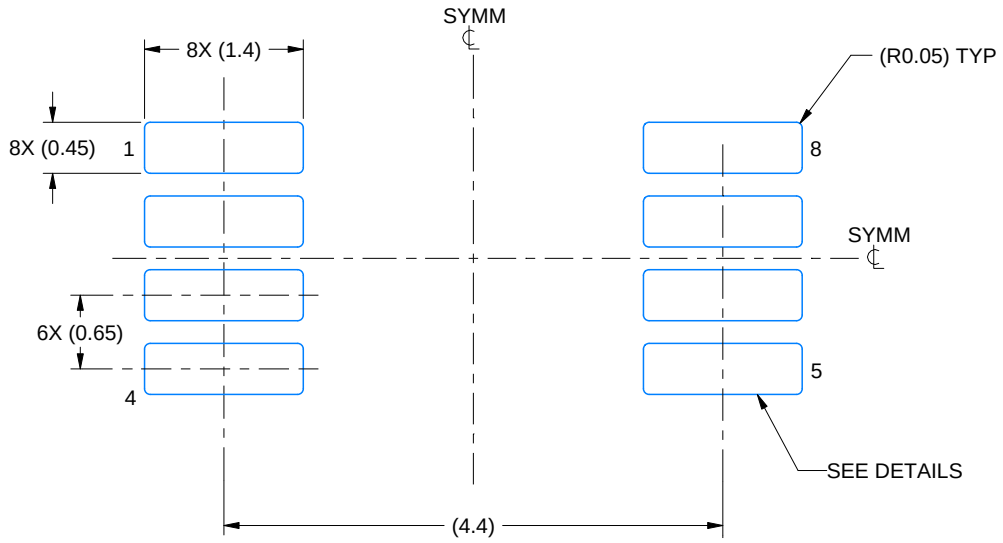
SMALL OUTLINE PACKAGE



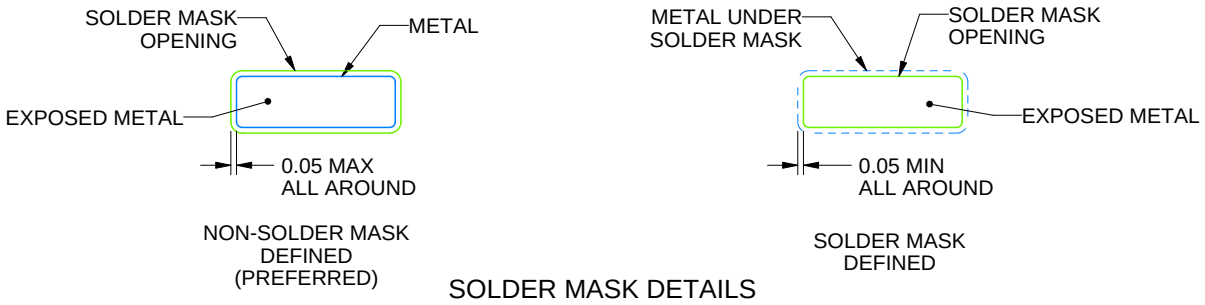
PowerPAD is a trademark of Texas Instruments.

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 15X

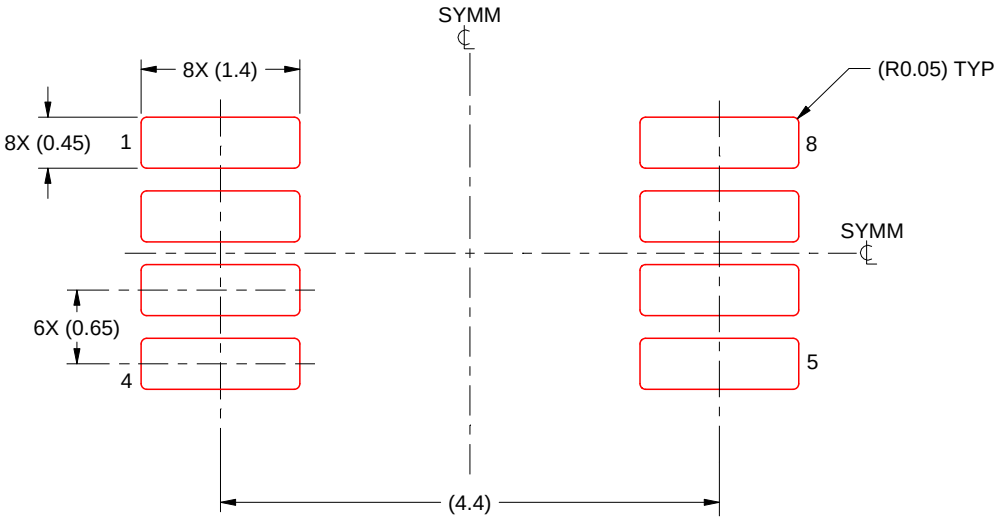


SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.



SOLDER PASTE EXAMPLE
SCALE: 15X

4214862/A 04/2023

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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