

## LM148QML Quad 741 Op Amps

Check for Samples: [LM148QML](#)

### FEATURES

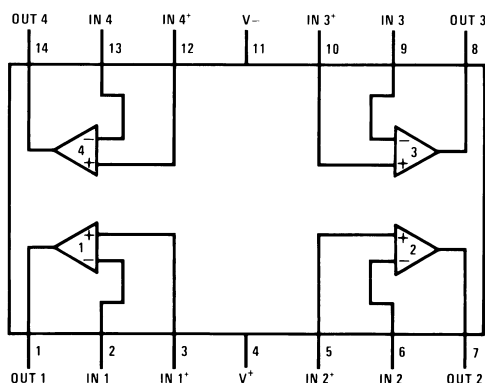
- 741 Op Amp Operating Characteristics
- Class AB Output Stage—No Crossover Distortion
- Pin Compatible with the LM124
- Overload Protection for Inputs and Outputs
- Low Supply Current Drain: 0.6 mA/Amplifier
- Low Input Offset Voltage: 1 mV
- Low Input Offset Current: 4 nA
- Low Input Bias Current 30 nA
- High Degree of Isolation between Amplifiers: 120 dB
- Gain Bandwidth Product (Unity Gain): 1.0 MHz

### DESCRIPTION

The LM148 is a true quad LM741. It consists of four independent, high gain, internally compensated, low power operational amplifiers which have been designed to provide functional characteristics identical to those of the familiar LM741 operational amplifier. In addition the total supply current for all four amplifiers is comparable to the supply current of a single LM741 type op amp. Other features include input offset currents and input bias current which are much less than those of a standard LM741. Also, excellent isolation between amplifiers has been achieved by independently biasing each amplifier and using layout techniques which minimize thermal coupling.

The LM148 can be used anywhere multiple LM741 or LM1558 type amplifiers are being used and in applications where amplifier matching or high packing density is required.

### Connection Diagram

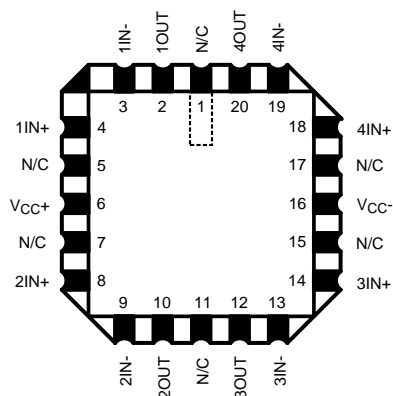


**Figure 1. Top View**  
**See Package Number J0014A**



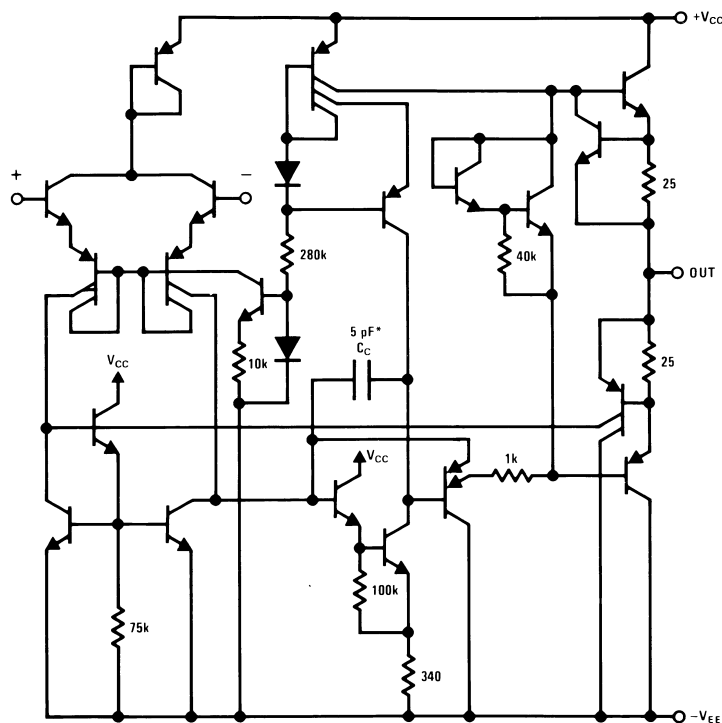
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**Figure 2. Top View**  
See Package Number NAJ0020A

## Schematic Diagram



\* 1 pF in the LM149



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

## Absolute Maximum Ratings<sup>(1)</sup>

Supply Voltage			±22V
Differential Input Voltage			±44V
Output Short Circuit Duration <sup>(2)</sup>			Continuous
Power Dissipation (P <sub>d</sub> at 25°C) <sup>(3)</sup>			1100mW
Thermal Resistance	θ <sub>JA</sub>	CDIP (Still Air)	103°C/W
		CDIP (500LF/ Min Air flow)	52°C/W
		LCCC (Still Air)	90°C/W
		LCCC (500LF/ Min Air flow)	66°C/W
	θ <sub>JC</sub>	CDIP	19°C/W
		LCCC	21°C/W
Maximum Junction Temperature (T <sub>jMAX</sub> )			150°C
Operating Temperature Range			-55°C ≤ T <sub>A</sub> ≤ +125°C
Storage Temperature Range			-65°C ≤ T <sub>A</sub> ≤ +150°C
Lead Temperature (Soldering, 10 sec.) Ceramic			300°C
ESD tolerance <sup>(4)</sup>			500V

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.
- (2) Any of the amplifier outputs can be shorted to ground indefinitely; however, more than one should not be simultaneously shorted as the maximum junction temperature will be exceeded.
- (3) The maximum power dissipation for these devices must be derated at elevated temperatures and is dictated by  $T_{jMAX}$ ,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum available power dissipation at any temperature is  $P_d = (T_{jMAX} - T_A)/\theta_{JA}$  or the number given in the Absolute Maximum Ratings, whichever is less.
- (4) Human body model, 1.5 kΩ in series with 100 pF

## Quality Conformance Inspection

MIL-STD-883, Method 5005 — Group A

Subgroup	Description	Temp ( °C)
1	Static tests at	+25
2	Static tests at	+125
3	Static tests at	-55
4	Dynamic tests at	+25
5	Dynamic tests at	+125
6	Dynamic tests at	-55
7	Functional tests at	+25
8A	Functional tests at	+125
8B	Functional tests at	-55
9	Switching tests at	+25
10	Switching tests at	+125
11	Switching tests at	-55

## Electrical Characteristics

DC PARAMETERS (The following conditions apply to all parameters, unless otherwise specified.)

$V_{CC} = \pm 15V$ ,  $R_S = 0\Omega$

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
$V_{IO}$	Input Offset Voltage	$V_{CM} = 0V$ , $R_S = 50\Omega$		-5	+5	mV	1
				-6	+6	mV	2,3
$I_{IO}$	Input Offset Current	$V_{CM} = 0V$		-25	+25	nA	1
				-75	+75	nA	2,3
$\pm I_{IB}$	Input Bias Current	$V_{CM} = 0V$		1	100	nA	1
				1	325	nA	2,3
$R_{in}$	Input Resistance		See <sup>(1)</sup>	0.8		M $\Omega$	1
PSRR+	Power Supply Rejection Ratio	$+V_{CC} = +15V$ and $+5V$ , $-V_{CC} = -15V$ , $R_S = 50\Omega$		77		dB	1, 2, 3
PSRR-	Power Supply Rejection Ratio	$+V_{CC} = +15V$ , $-V_{CC} = -15V$ and $-5V$ , $R_S = 50\Omega$		77		dB	1, 2, 3
CMRR	Common Mode Rejection Ratio	$+V_{CM} = \pm 12V$ , $R_S = 50\Omega$		70		dB	1, 2, 3
$I_{OS+}$	Short Circuit Current			-55	-14	mA	1
$I_{OS-}$	Short Circuit Current			14	55	mA	1
$I_{CC}$	Power Supply Current			0.4	3.6	mA	1
				0.4	4.5	mA	2, 3
$A_{VS+}$	Large Signal Voltage Gain	$V_{OUT} = 0V$ to $+10V$ , $R_L > 2k\Omega$		50		V/mV	4
				25		V/mV	5, 6
$A_{VS-}$	Large Signal Voltage Gain	$V_{OUT} = 0V$ to $-10V$ , $R_L > 2k\Omega$		50		V/mV	4
				25		V/mV	5, 6
$V_{out+}$	Output Voltage Swing	$R_L = 10k\Omega$		+12		V	4, 5, 6
		$R_L = 2k\Omega$		+10		V	4, 5, 6
$V_{out-}$	Output Voltage Swing	$R_L = 10k\Omega$			-12	V	4, 5, 6
		$R_L = 2k\Omega$			-10	V	4, 5, 6

(1) Parameter specified, Not Tested.

## Electrical Characteristics

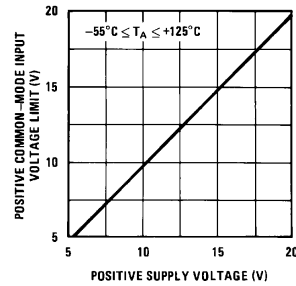
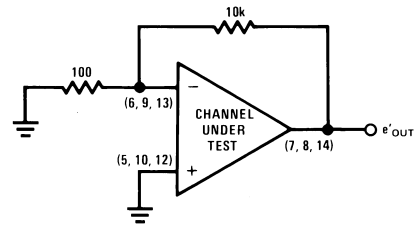
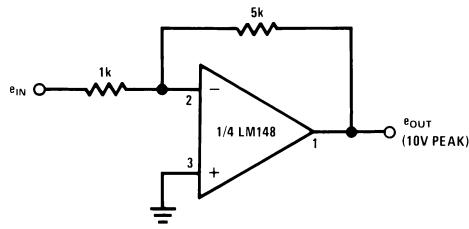
AC PARAMETERS (The following conditions apply to all parameters, unless otherwise specified.)

$V_{CC} = \pm 15V$ ,  $A_V = 1$ ,  $R_S = 0\Omega$

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
$\pm SR$	Slew Rate			0.2		V/ $\mu s$	7, 8A, 8B
$G_{BW}$	Gain Bandwidth Product			0.4	1.4	MHz	7, 8A, 8B

## Cross Talk Test Circuit

$V_S = \pm 15V$



## Typical Performance Characteristics

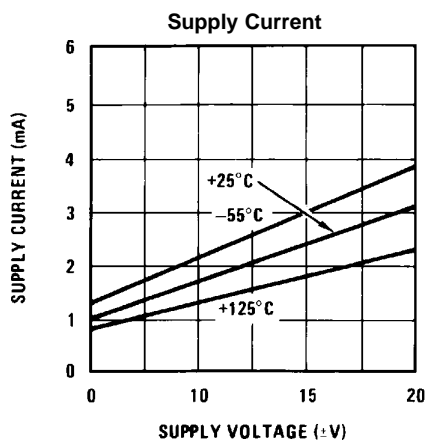


Figure 3.

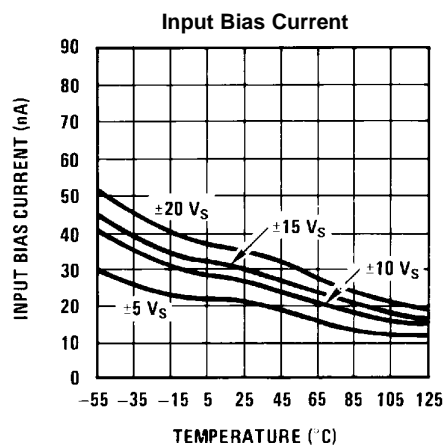


Figure 4.

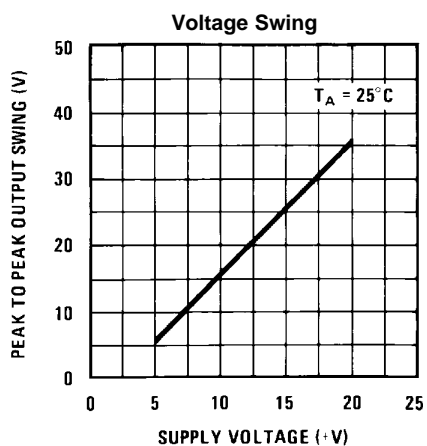


Figure 5.

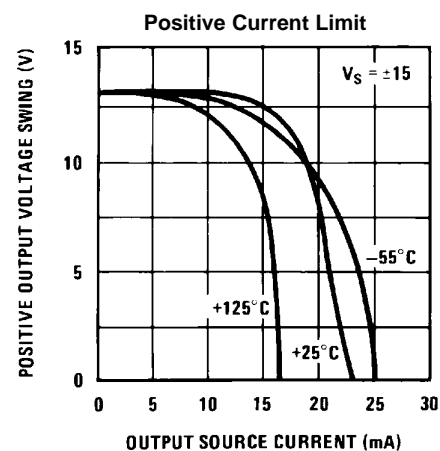


Figure 6.

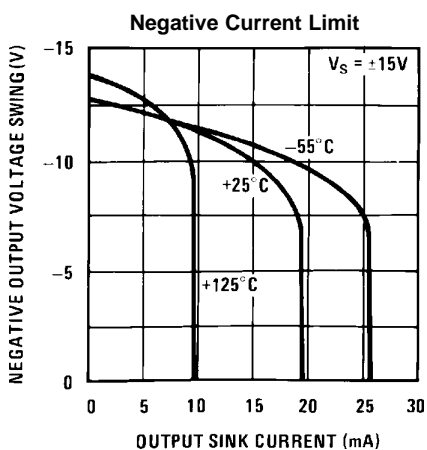


Figure 7.

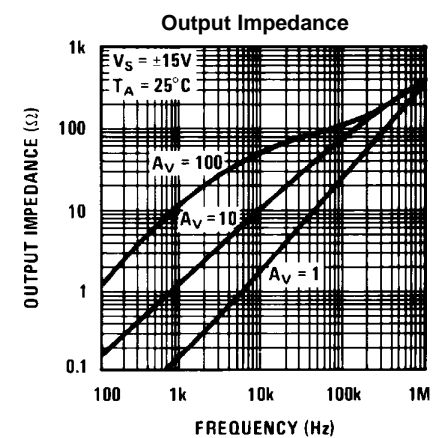


Figure 8.

## Typical Performance Characteristics (continued)

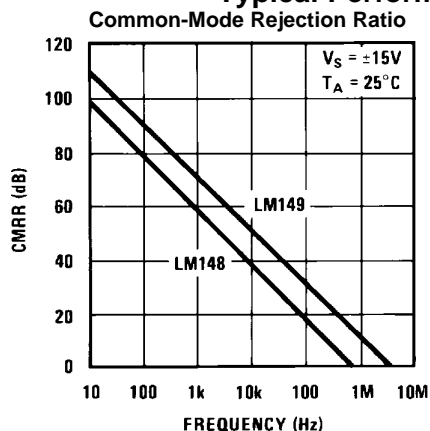


Figure 9.

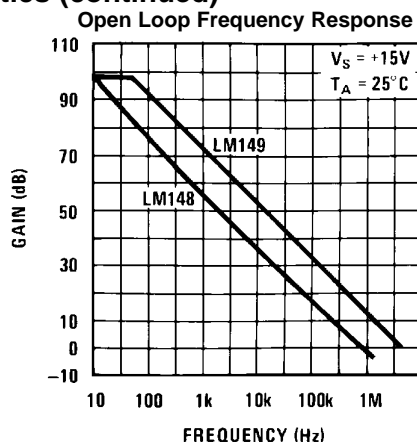


Figure 10.

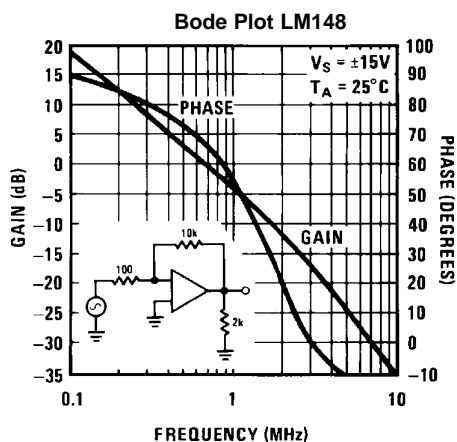


Figure 11.

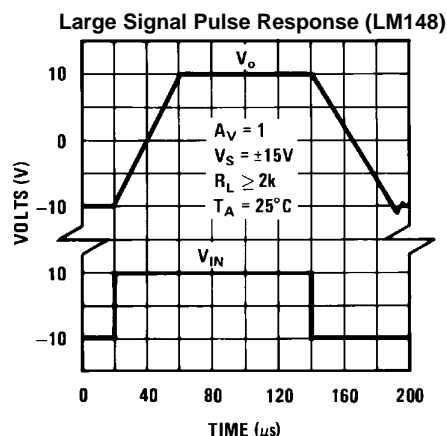


Figure 12.

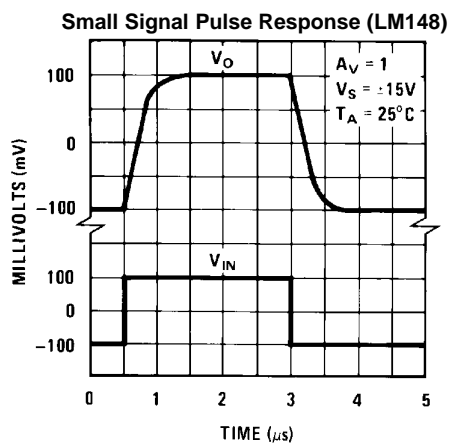


Figure 13.

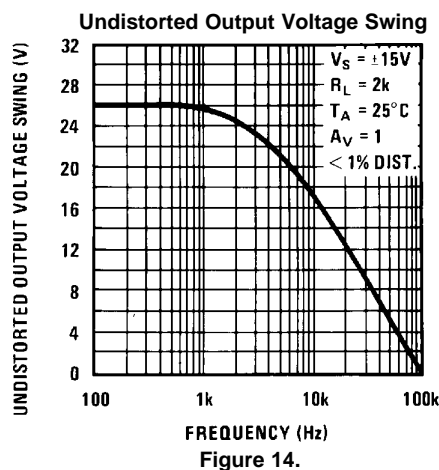
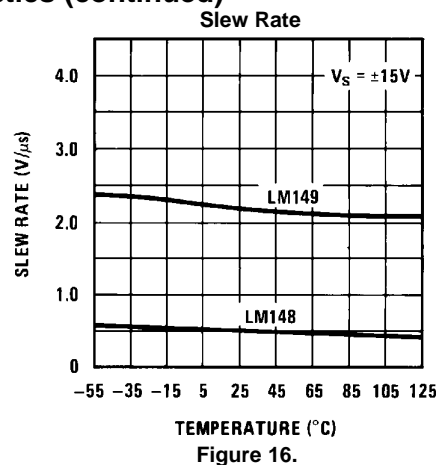
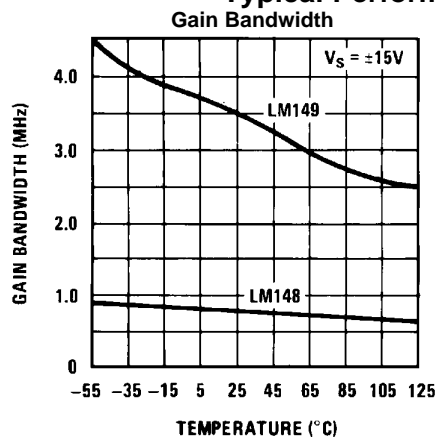
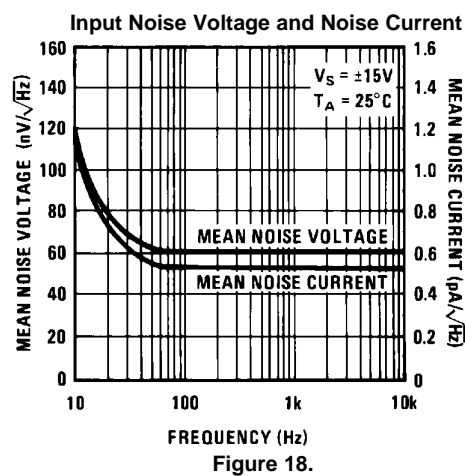
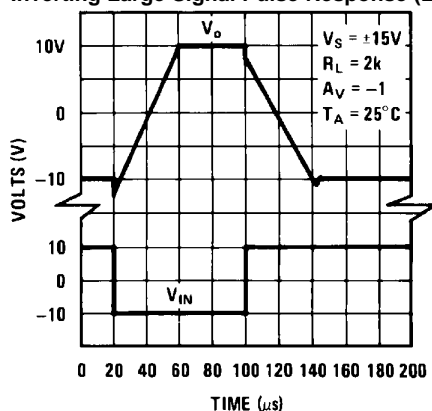


Figure 14.

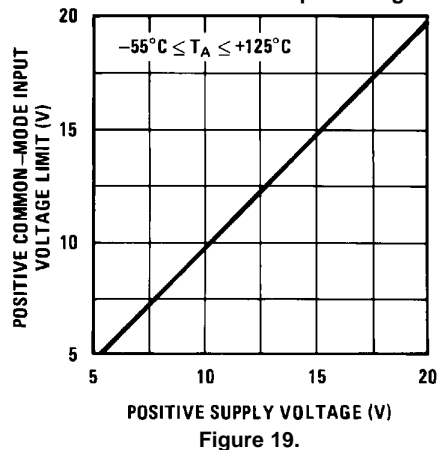
## Typical Performance Characteristics (continued)



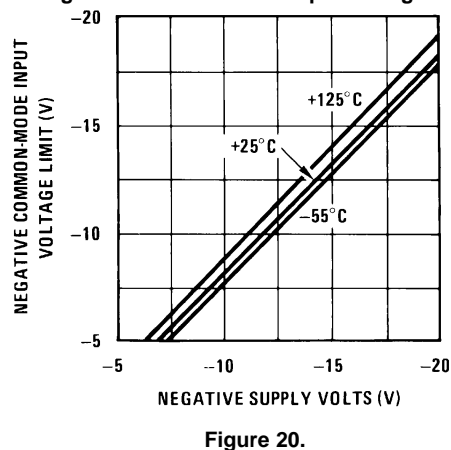
### Inverting Large Signal Pulse Response (LM148)



### Positive Common-Mode Input Voltage Limit



### Negative Common-Mode Input Voltage Limit





## APPLICATION HINTS

The LM148 series are quad low power LM741 op amps. In the proliferation of quad op amps, these are the first to offer the convenience of familiar, easy to use operating characteristics of the LM741 op amp. In those applications where LM741 op amps have been employed, the LM148 series op amps can be employed directly with no change in circuit performance.

The package pin-outs are such that the inverting input of each amplifier is adjacent to its output. In addition, the amplifier outputs are located in the corners of the package which simplifies PC board layout and minimizes package related capacitive coupling between amplifiers.

The input characteristics of these amplifiers allow differential input voltages which can exceed the supply voltages. In addition, if either of the input voltages is within the operating common-mode range, the phase of the output remains correct. If the negative limit of the operating common-mode range is exceeded at both inputs, the output voltage will be positive. For input voltages which greatly exceed the maximum supply voltages, either differentially or common-mode, resistors should be placed in series with the inputs to limit the current.

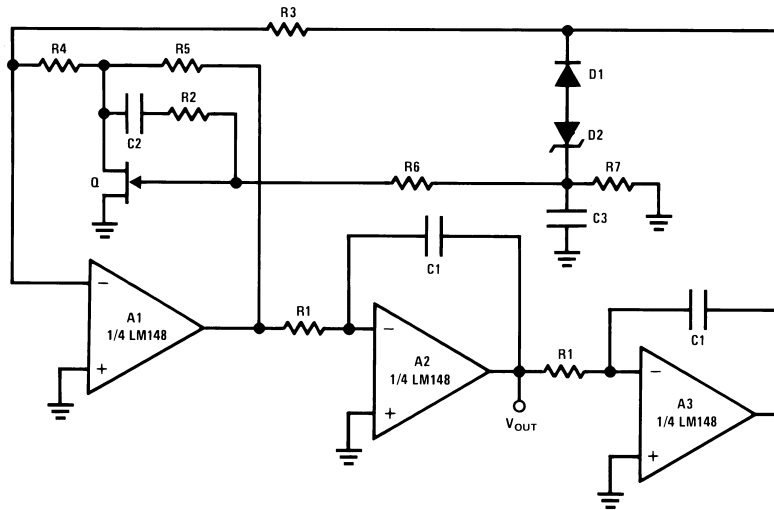
Like the LM741, these amplifiers can easily drive a 100 pF capacitive load throughout the entire dynamic output voltage and current range. However, if very large capacitive loads must be driven by a non-inverting unity gain amplifier, a resistor should be placed between the output (and feedback connection) and the capacitance to reduce the phase shift resulting from the capacitive loading.

The output current of each amplifier in the package is limited. Short circuits from an output to either ground or the power supplies will not destroy the unit. However, if multiple output shorts occur simultaneously, the time duration should be short to prevent the unit from being destroyed as a result of excessive power dissipation in the IC chip.

As with most amplifiers, care should be taken lead dress, component placement and supply decoupling in order to ensure stability. For example, resistors from the output to an input should be placed with the body close to the input to minimize "pickup" and maximize the frequency of the feedback pole which capacitance from the input to ground creates.

A feedback pole is created when the feedback around any amplifier is resistive. The parallel resistance and capacitance from the input of the device (usually the inverting input) to AC ground set the frequency of the pole. In many instances the frequency of this pole is much greater than the expected 3 dB frequency of the closed loop gain and consequently there is negligible effect on stability margin. However, if the feedback pole is less than approximately six times the expected 3 dB frequency a lead capacitor should be placed from the output to the input of the op amp. The value of the added capacitor should be such that the RC time constant of this capacitor and the resistance it parallels is greater than or equal to the original feedback pole time constant.

## Typical Applications—LM148



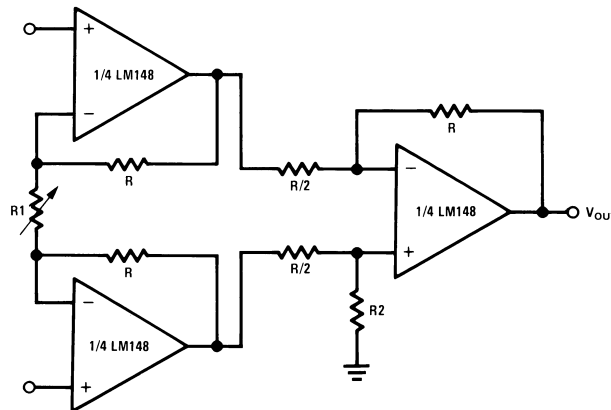
$$f = \frac{1}{2\pi R_1 C_1} \times \sqrt{K}, K = \frac{R_4 R_5}{R_3} \left( \frac{1}{r_{DS}} + \frac{1}{R_4} + \frac{1}{R_5} \right), r_{DS} \approx \frac{R_{ON}}{\left( 1 - \frac{V_{GS}}{V_P} \right)^{1/2}}$$

$f_{MAX} = 5 \text{ kHz}$ ,  $THD \leq 0.03\%$

$R_1 = 100\text{k pot.}$ ,  $C_1 = 0.0047 \mu\text{F}$ ,  $C_2 = 0.01 \mu\text{F}$ ,  $C_3 = 0.1 \mu\text{F}$ ,  $R_2 = R_6 = R_7 = 1\text{M}$ ,  
 $R_3 = 5.1\text{k}$ ,  $R_4 = 12\Omega$ ,  $R_5 = 240\Omega$ ,  $Q = \text{NS5102}$ ,  $D_1 = 1\text{N914}$ ,  $D_2 = 3.6\text{V avalanche diode (ex. LM103)}$ ,  $V_S = \pm 15\text{V}$

A simpler version with some distortion degradation at high frequencies can be made by using A1 as a simple inverting amplifier, and by putting back to back zeners in the feedback loop of A3.

**Figure 21. One Decade Low Distortion Sinewave Generator**

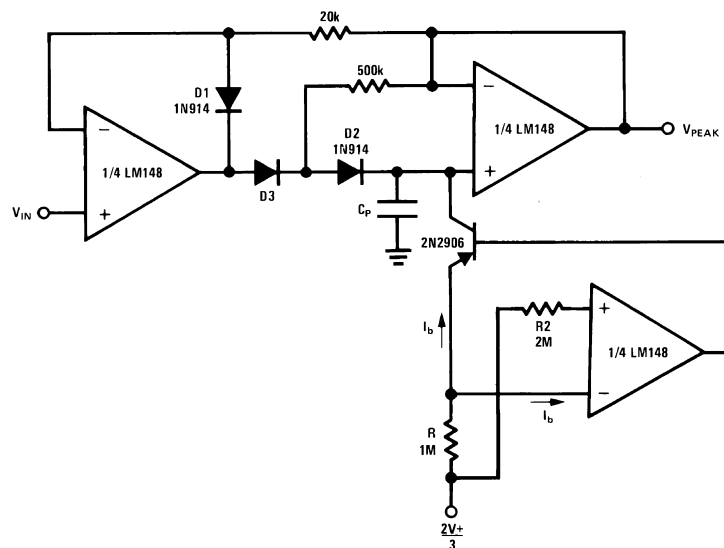


$$V_{OUT} = 2 \left( \frac{2R}{R_1} + 1 \right), V_S - 3\text{V} \leq V_{IN CM} \leq V_S + - 3\text{V},$$

$V_S = \pm 15\text{V}$

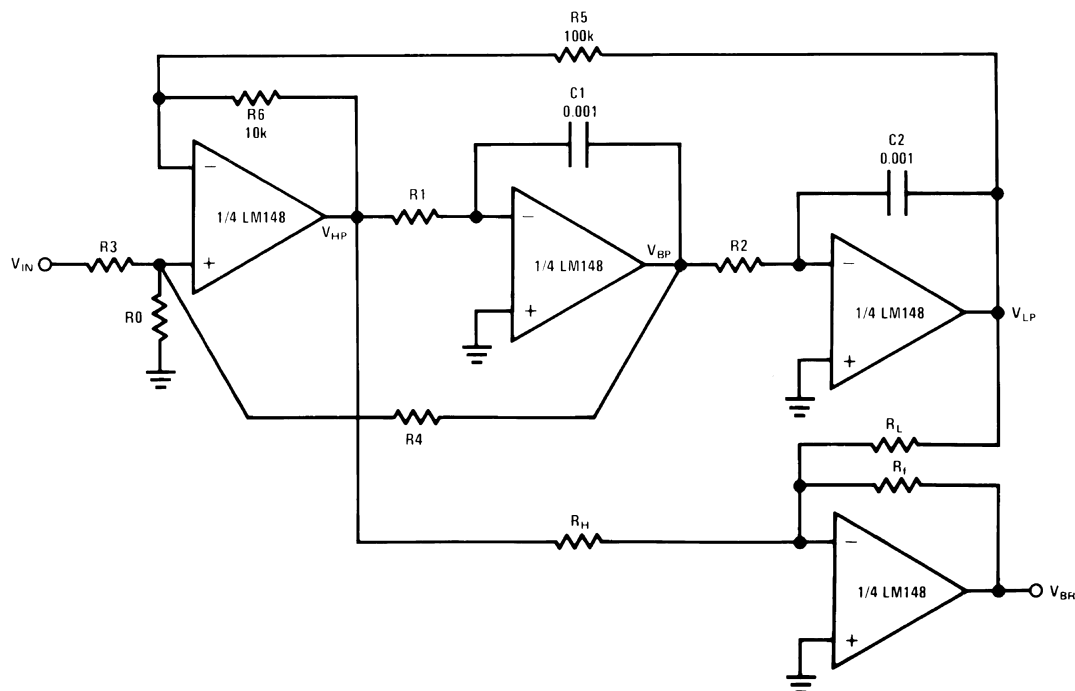
$R = R_2$ , trim  $R_2$  to boost CMRR

**Figure 22. Low Cost Instrumentation Amplifier**



Adjust R for minimum drift  
D3 low leakage diode  
D1 added to improve speed  
 $V_S = \pm 15V$

**Figure 23. Low Drift Peak Detector with Bias Current Compensation**



Tune Q through R0,  
For predictable results:  $f_o Q \leq 4 \times 10^4$   
Use Band Pass output to tune for Q

$$\frac{V(s)}{V_{IN}(s)} = \frac{N(s)}{D(s)}, D(s) = s^2 + \frac{s\omega_o}{Q} + \omega_o^2$$

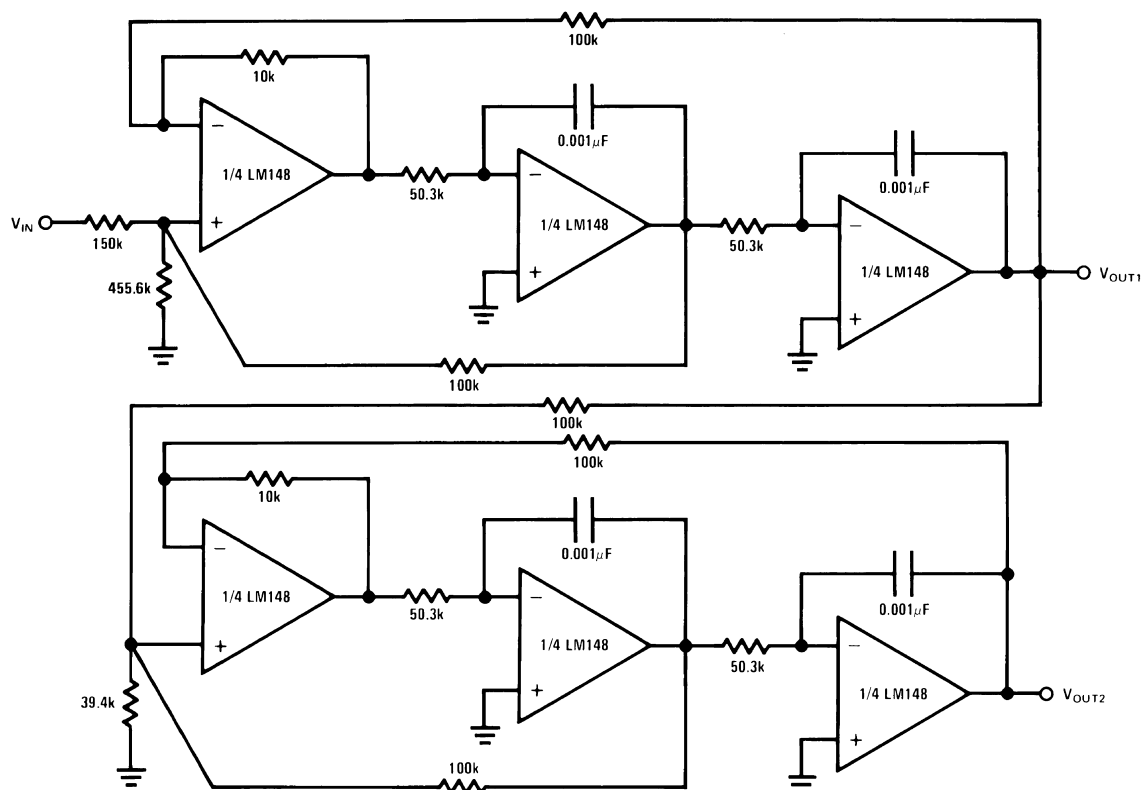
$$N_{HP}(s) = s^2 H_{OHP}, N_{BP}(s) = \frac{-s\omega_o H_{OBP}}{Q}, N_{LP} = \omega_o^2 H_{OLP}$$

$$f_o = \frac{1}{2\pi} \sqrt{\frac{R_6}{R_5}} \sqrt{\frac{1}{t_1 t_2}}, t_i = R_i C_i, Q = \left( \frac{1 + R_4/R_3 + R_4/R_0}{1 + R_6/R_5} \right) \left( \frac{R_6 t_1}{R_5 t_2} \right)^{1/2}$$

$$f_{NOTCH} = \frac{1}{2\pi} \left( \frac{R_H}{R_L t_1 t_2} \right)^{1/2}, H_{OHP} = \frac{1 + R_6/R_5}{1 + R_3/R_0 + R_3/R_4}, H_{OBP} = \frac{1 + R_4/R_3 + R_4/R_0}{1 + R_3/R_0 + R_3/R_4}$$

$$H_{OLP} = \frac{1 + R_5/R_6}{1 + R_3/R_0 + R_3/R_4}$$

**Figure 24. Universal State-Variable Filter**



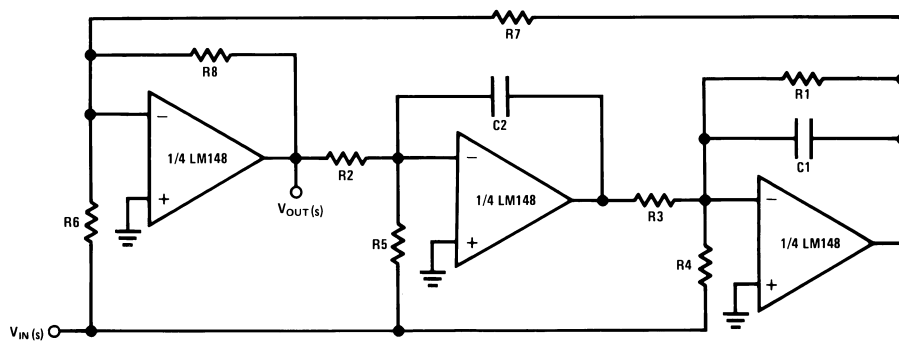
Use general equations, and tune each section separately

$Q_{1stSECTION} = 0.541$ ,  $Q_{2ndSECTION} = 1.306$

The response should have 0 dB peaking

Figure 25. A 1 kHz 4 Pole Butterworth

Figure 26.



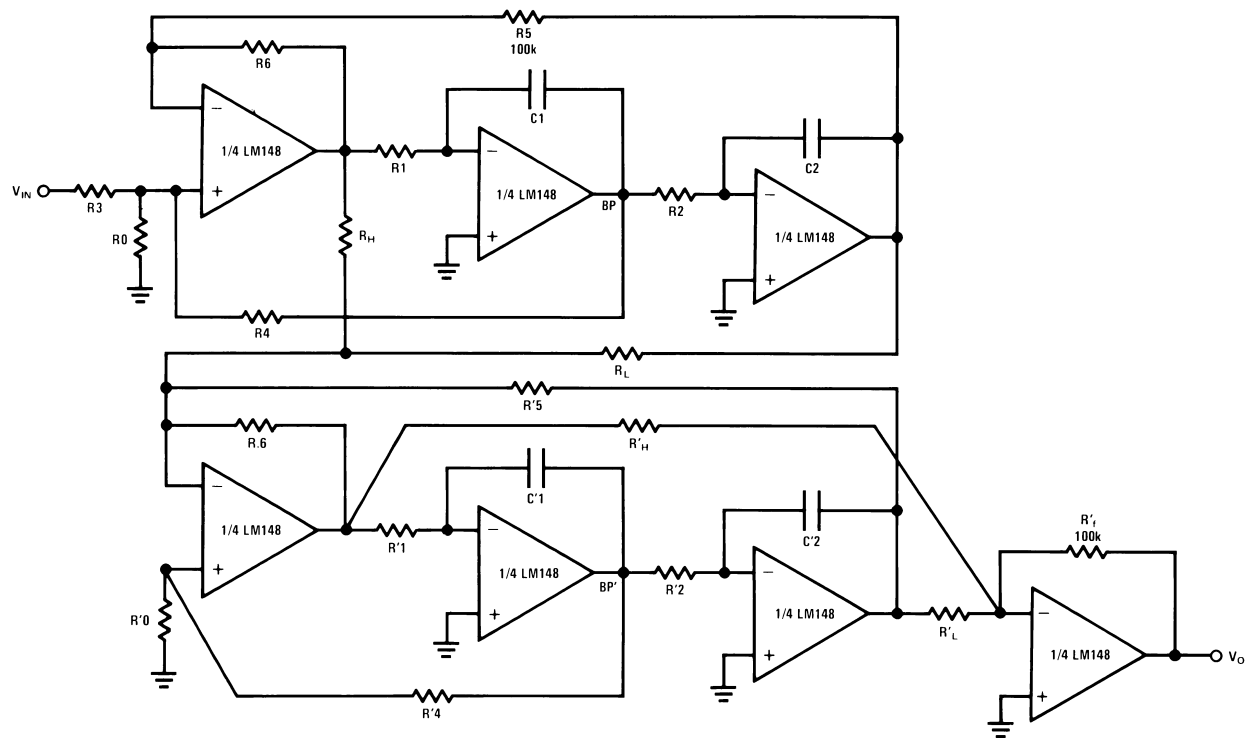
$$Q = \sqrt{\frac{R8}{R7}} \times \frac{R1C1}{\sqrt{R3C2R2C1}}, f_o = \frac{1}{2\pi} \sqrt{\frac{R8}{R7}} \times \frac{1}{\sqrt{R2R3C1C2}}, f_{NOTCH} = \frac{1}{2\pi} \sqrt{\frac{R6}{R3R5R7C1C2}}$$

$$\text{Necessary condition for notch: } \frac{1}{R6} = \frac{R1}{R4R7}$$

EX:  $f_{NOTCH} = 3$  kHz,  $Q = 5$ ,  $R1 = 270k$ ,  $R2 = R3 = 20k$ ,  $R4 = 27k$ ,  $R5 = 20k$ ,  $R6 = R8 = 10k$ ,  $R7 = 100k$ ,  $C1 = C2 = 0.001 \mu F$

Better noise performance than the state-space approach.

Figure 27. A 3 Amplifier Bi-Quad Notch Filter



$$R1C1 = R2C2 = t$$

$$R'1C'1 = R'2C'2 = t'$$

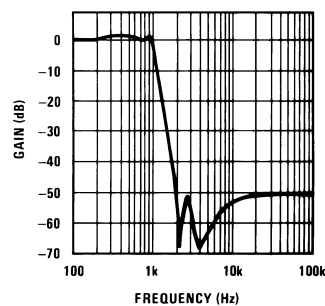
$f_C = 1 \text{ kHz}$ ,  $f_S = 2 \text{ kHz}$ ,  $f_p = 0.543$ ,  $f_z = 2.14$ ,  $Q = 0.841$ ,  $f'_p = 0.987$ ,  $f'_z = 4.92$ ,  $Q' = 4.403$ , normalized to ripple BW

$$f = \frac{1}{2\pi R1C1} \times \sqrt{K}, K = \frac{R4R5}{R3} \left( \frac{1}{r_{DS}} + \frac{1}{R4} + \frac{1}{R5} \right), r_{DS} \approx \frac{R_{ON}}{\left( 1 - \frac{V_{GS}}{V_P} \right)^{1/2}}$$

Use the BP outputs to tune  $Q$ ,  $Q'$ , tune the 2 sections separately

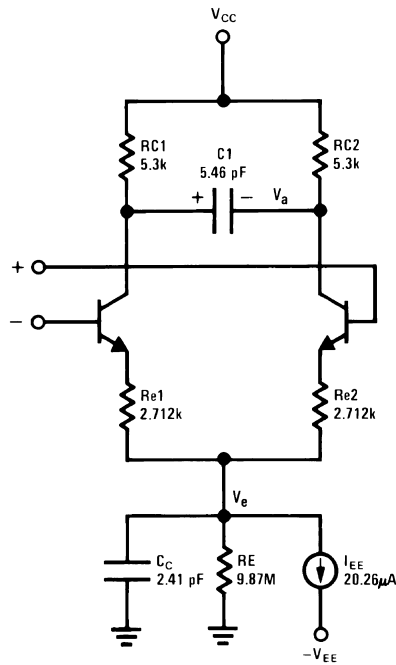
$R1 = R2 = 92.6k$ ,  $R3 = R4 = R5 = 100k$ ,  $R6 = 10k$ ,  $R0 = 107.8k$ ,  $R_L = 100k$ ,  $R_H = 155.1k$ ,  $R'1 = R'2 = 50.9k$ ,  $R'4 = R'5 = 100k$ ,  $R'6 = 10k$ ,  $R'0 = 5.78k$ ,  $R'_L = 100k$ ,  $R'_H = 248.12k$ ,  $R'f = 100k$ . All capacitors are  $0.001 \mu F$ .

**Figure 28. A 4th Order 1 kHz Elliptic Filter (4 Poles, 4 Zeros)**



**Figure 29. Lowpass Response**

## Typical Simulation



For more details, see IEEE Journal of Solid-State Circuits, Vol. SC-9, No. 6, December 1974

$$\omega_1 = 112I_S = 8 \times 10^{-16}$$

$$\omega_2 = 144 \cdot C2 = 6 \text{ pF for LM149}$$

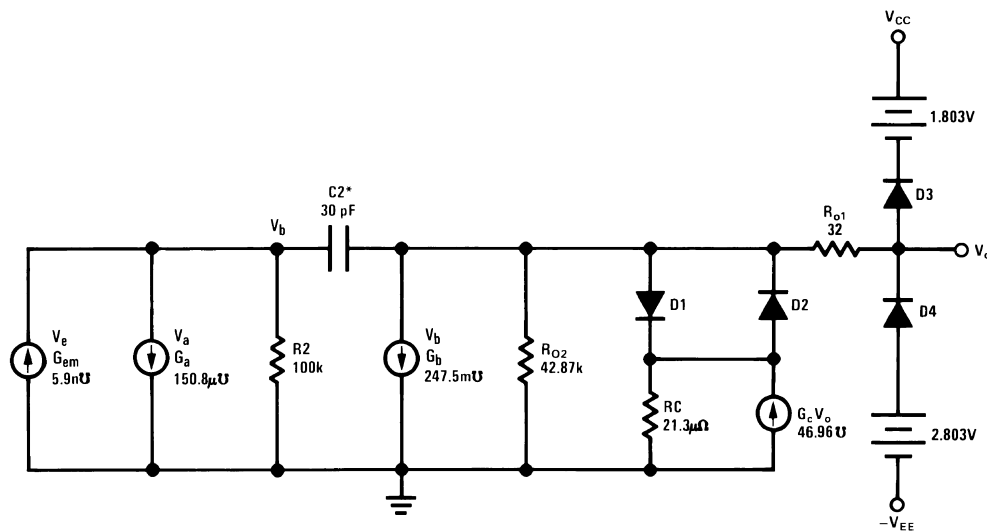


Figure 30. LM148, LM741 Macromodel for Computer Simulation

## REVISION HISTORY SECTION

Date Released	Revision	Section	Originator	Changes
02/08/05	A	New Release, Corporate format	L. Lytle	1 MDS data sheet converted into one Corp. data sheet format. MNLM148-X, Rev. 2A2. MDS data sheet will be archived.
03/20/13	A	All		Changed layout of National Data Sheet to TI format



PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
LM148 MD8	Active	Production	DIESALE (Y)   0	100   JEDEC TRAY (5+1)	Yes	Call TI	Level-1-NA-UNLIM	-55 to 125	
<a href="#">LM148J/883</a>	Active	Production	CDIP (J)   14	25   TUBE	No	SNPB	Level-1-NA-UNLIM	-55 to 125	LM148J/883 Q

- (1) **Status:** For more details on status, see our [product life cycle](#).
- (2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.
- (3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.
- (4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.
- (5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.
- (6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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## TUBE



\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (μm)	B (mm)
LM148J/883	J	CDIP	14	25	506.98	15.24	13440	NA

**J 14**

## GENERIC PACKAGE VIEW

**CDIP - 5.08 mm max height**

CERAMIC DUAL IN LINE PACKAGE



Images above are just a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.

4040083-5/G

**J0014A****PACKAGE OUTLINE****CDIP - 5.08 mm max height**

CERAMIC DUAL IN LINE PACKAGE



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**NOTES:**

1. All controlling linear dimensions are in inches. Dimensions in brackets are in millimeters. Any dimension in brackets or parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This package is hermetically sealed with a ceramic lid using glass frit.
4. Index point is provided on cap for terminal identification only and on press ceramic glass frit seal only.
5. Falls within MIL-STD-1835 and GDIP1-T14.



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# EXAMPLE BOARD LAYOUT

J0014A

CDIP - 5.08 mm max height

CERAMIC DUAL IN LINE PACKAGE



LAND PATTERN EXAMPLE  
NON-SOLDER MASK DEFINED  
SCALE: 5X



4214771/A 05/2017

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