

ABSTRACT

The purpose of this study is to characterize the single-event effects (SEE) performance due to heavy-ion irradiation of the TPS7H4011-SEP. Heavy-ions with LET_{EFF} of $48 \text{ MeV} \times \text{cm}^2/\text{mg}$ were used to irradiate six production devices. Flux of $\approx 10^5 \text{ ions/cm}^2/\text{s}$ and fluence of 10^7 ions/cm^2 per run were used for the characterization. The results demonstrated that the TPS7H4011-SEP is SEL-free up to $48 \text{ MeV} \times \text{cm}^2/\text{mg}$ at $T = 125^\circ\text{C}$ and SEB/SEGR free up to $48 \text{ MeV} \times \text{cm}^2/\text{mg}$ at $T = 25^\circ\text{C}$. Output signals including V_{OUT} (3% window), SS_TR (edge trigger at 50% below nominal) and PWRGD (edge trigger at 50% below nominal) were monitored to check for transients and SEFIs. The results showed the device is SET and SEFI free up to $48 \text{ MeV} \times \text{cm}^2/\text{mg}$ at $T = 25^\circ\text{C}$.

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1 Introduction

The TPS7H4011-SEP is a 14V, 12A synchronous buck converter optimized for use in a space environment. The peak current mode converter obtains high efficiency with good transient performance and reduced component count.

The wide voltage range of the TPS7H4011-SEP enables the device to be used as a point of load regulator to convert directly from a 12V or 5V rail. The output voltage start-up ramp is controlled by the SS_TR pin. Power sequencing is possible with the EN and PWRGD pins.

The device can be configured with up-to four devices in parallel without an external clock for increased current capabilities. Additionally, various features are included such as differential remote sensing, selectable current limit, a flexible fault input pin, and configurable compensation.

The device is offered in a 44-pin plastic package. General device information and test conditions are listed in [Table 1-1](#). For more detailed technical specifications, user guides, and application notes, see [TPS7H4011-SEP product page](#).

Table 1-1. Overview Information

Description ⁽¹⁾	Device Information
TI Part Number	TPS7H4011-SEP
Orderable Number	TPS7H4011MDDWTSEP
Device Function	Synchronous Buck Converter
Technology	LBC7 (Linear BiCMOS 7)
Exposure Facility	Radiation Effects Facility, Cyclotron Institute, Texas A&M University (15 MeV/nucleon) and Facility for Rare Isotope Beams, K500 Cyclotron (KSEE), Michigan State University (19.5MeV/nucleon)
Heavy Ion Fluence per Run	1.00×10^7 ions / cm ²
Irradiation Temperature	25°C (for SEB/SEGR testing), 25°C (for SET testing), and 125°C (for SEL testing)

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2 Single-Event Effects (SEE)

The primary concern for the TPS7H4011-SEP is the robustness against the destructive single-event effects (DSEE): single-event latch-up (SEL), single-event burnout (SEB), and single-event gate rupture (SEGR). In mixed technologies such as the BiCMOS process used on the TPS7H4011-SEP, the CMOS circuitry introduces a potential for SEL susceptibility.

SEL can occur if excess current injection caused by the passage of an energetic ion is high enough to trigger the formation of a parasitic cross-coupled PNP and NPN bipolar structure (formed between the p-sub and n-well and n+ and p+ contacts) (1,2). The parasitic bipolar structure initiated by a single-event creates a high-conductance path (inducing a steady-state current that is typically orders-of-magnitude higher than the normal operating current) between power and ground that persists (is *latched*) until power is removed, the device is reset, or until the device is destroyed by the high-current state. The TPS7H4011-SEP was tested for SEL at the maximum recommended input voltage (V_{IN}) of 14V. The output load was configured to provide a constant resistance value of 0.2718Ω to create a 12A load on the output. During testing of the six devices, the TPS7H4011-SEP did not exhibit any SEL with heavy-ions with $LET_{EFF} = 48 \text{ MeV}\times\text{cm}^2/\text{mg}$ at flux of $\approx 10^5 \text{ ions/cm}^2/\text{s}$, fluence of $\approx 10^7 \text{ ions/cm}^2$, and a die temperature of $\approx 125^\circ\text{C}$.

The TPS7H4011-SEP was evaluated for SEB/SEGR at a maximum voltage of 14V in enabled and disabled mode. Because it has been shown that the MOSFET susceptibility to burnout decrement with temperature (5), the device was evaluated while operating under room temperatures. The device was tested with no external thermal control device. During the SEB/SEGR testing, not a single current event was observed, demonstrating that the TPS7H4011-SEP is SEB/SEGR-free up to $LET_{EFF} = 48 \text{ MeV}\times\text{cm}^2/\text{mg}$ at a flux of $\approx 10^5 \text{ ions/cm}^2/\text{s}$, fluences of $\approx 10^7 \text{ ions/cm}^2$, and a die temperature of $\approx 25^\circ\text{C}$.

The TPS7H4011-SEP was characterized at V_{IN} of 5V and 12V. During SET testing the V_{OUT} , SS_TR, and PWRGD signals were monitored. During the SET testing, not a single transient was observed, demonstrating that the TPS7H4011-SEP is SET/SEFI-free up to $LET_{EFF} = 48 \text{ MeV}\times\text{cm}^2/\text{mg}$ at a flux of $\approx 10^5 \text{ ions/cm}^2/\text{s}$, fluences of $\approx 10^7 \text{ ions/cm}^2$, and a die temperature of $\approx 25^\circ\text{C}$. For more details on the SET testing of the TPS7H4011-SEP, see [Single-Event Transients \(SET\)](#).

3 Device and Test Board Information

The TPS7H4011-SEP is packaged in a 44-pin plastic package as shown in [Figure 3-1](#). The TPS7H4011-SEP evaluation module (EVM) was used to evaluate the performance and characteristics of the TPS7H4011-SEP under heavy ion radiation. The TPS7H4011EVM is shown in [Figure 3-2](#). The EVM schematic is shown in [Figure 3-3](#).

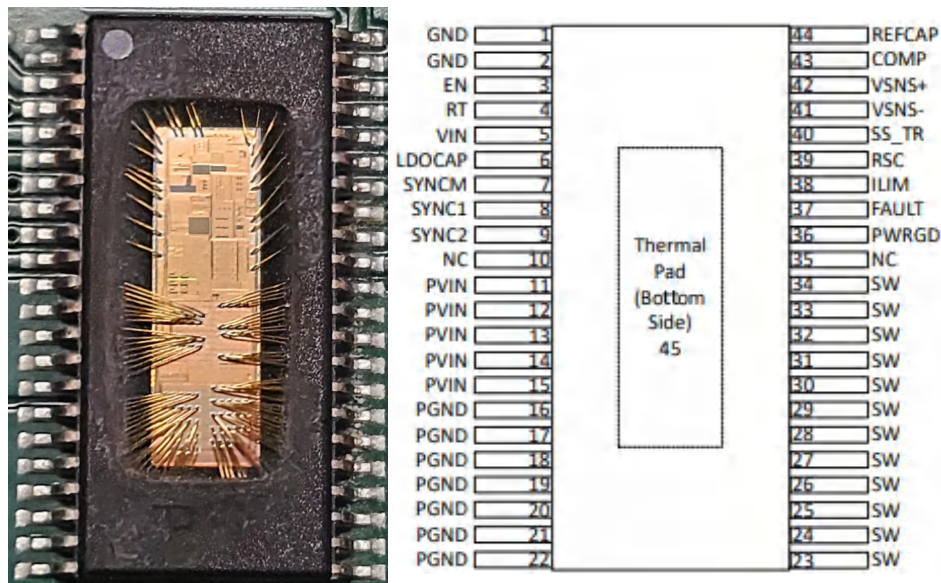


Figure 3-1. Photograph of Delidded TPS7H4011-SEP (Left) and Pinout Diagram (Right)

The package was delidded to reveal the die face for all heavy-ion testing.

Jumper on J5 was populated, J6 was configured in the 2-3 position, J7 was configured in the 1-2 position, and J10 was configured in the 1-2 position for all testing

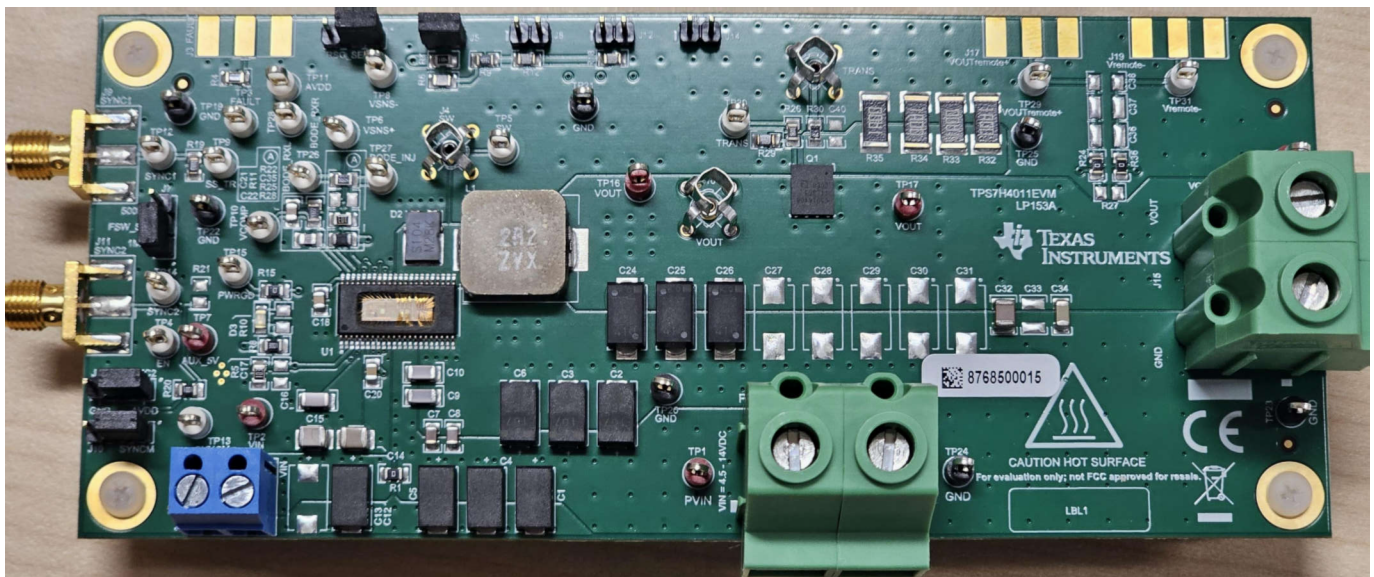


Figure 3-2. TPS7H4011-SEP EVM Top View

Device and Test Board Information

PVIN = VIN = 4.5-14 VDC

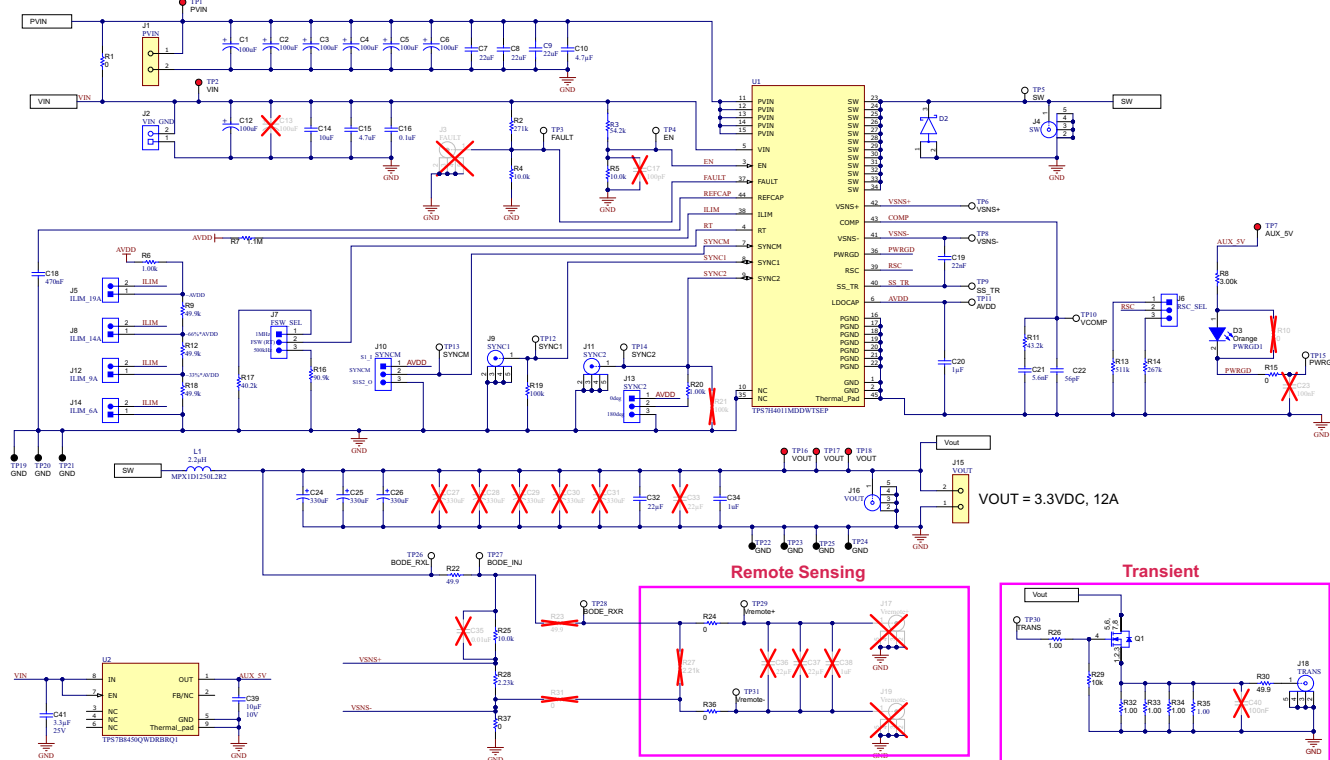


Figure 3-3. TPS7H4011-SEP EVM Schematics

4 Irradiation Facility and Setup

The heavy-ion species used for the SEE studies on this product were provided and delivered by:

- Texas A&M University (TAMU) Cyclotron Radiation Effects Facility using a K500 superconducting cyclotron and an advanced electron cyclotron resonance (ECR) ion source. At the fluxes used, ion beams had good flux stability and high irradiation uniformity over a 1-in diameter circular cross-sectional area for the in-air station. Uniformity is achieved by magnetic defocusing. The flux of the beam is regulated over a broad range spanning several orders of magnitude. For these studies, ion flux of 1.15 to 1.47×10^5 ions/cm²/s was used to provide heavy-ion fluences of 1.00×10^7 ions/cm². The TAMU facility uses a beam port that has a 1-mil Aramica window to allow in-air testing while maintaining the vacuum within the particle accelerator. The in-air gap between the device and the ion beam port window was maintained at 40 mm for all runs.
- Michigan State University (MSU) Facility for Rare Isotope Beams (FRIB) using a K500 superconducting cyclotron (KSEE) and an advanced electron cyclotron resonance (ECR) ion source. At the fluxes used, ion beams had good flux stability and high irradiation uniformity as the beam is collimated to a maximum of 40 mm × 40 mm square cross-sectional area for the in-air and vacuum scintillators. Uniformity is achieved by scattering on a Cu foil and then performing magnetic defocusing. The flux of the beam is regulated over a broad range spanning several orders of magnitude. For these studies, ion flux of 1.03 to 1.13×10^5 ions/cm²/s was used to provide heavy-ion fluences of 1.00×10^7 ions/cm². The KSEE facility uses a beam port that has a 3-mil polyethylene naphthalate (PEN) window to allow in-air testing while maintaining the vacuum within the particle accelerator. The in-air gap between the device and the ion beam port window was maintained at 60 mm for all runs.

For the experiments conducted on this report, 2 ions were used; ¹⁰⁹Ag (TAMU) and ¹⁰⁹Ag (KSEE). Both were used to obtain LET_{EFF} of ≈ 48 MeV·cm²/mg. The total kinetic energies for the ions were:

- ¹⁰⁹Ag (TAMU) = 1.635 GeV (15 MeV/nucleon) – Ion uniformity for these experiments was 94%
- ¹⁰⁹Ag (KSEE) = 2.125 GeV (19.5 MeV/nucleon) – Ion uniformity for these experiments was 91%

Figure 4-1 shows the TPS7H4011EVM used for data collection at the TAMU facility. Although not visible in this photo, the beam port has a 1 mil Aramica window to allow in-air testing while maintaining the vacuum within the accelerator with only minor ion energy loss.

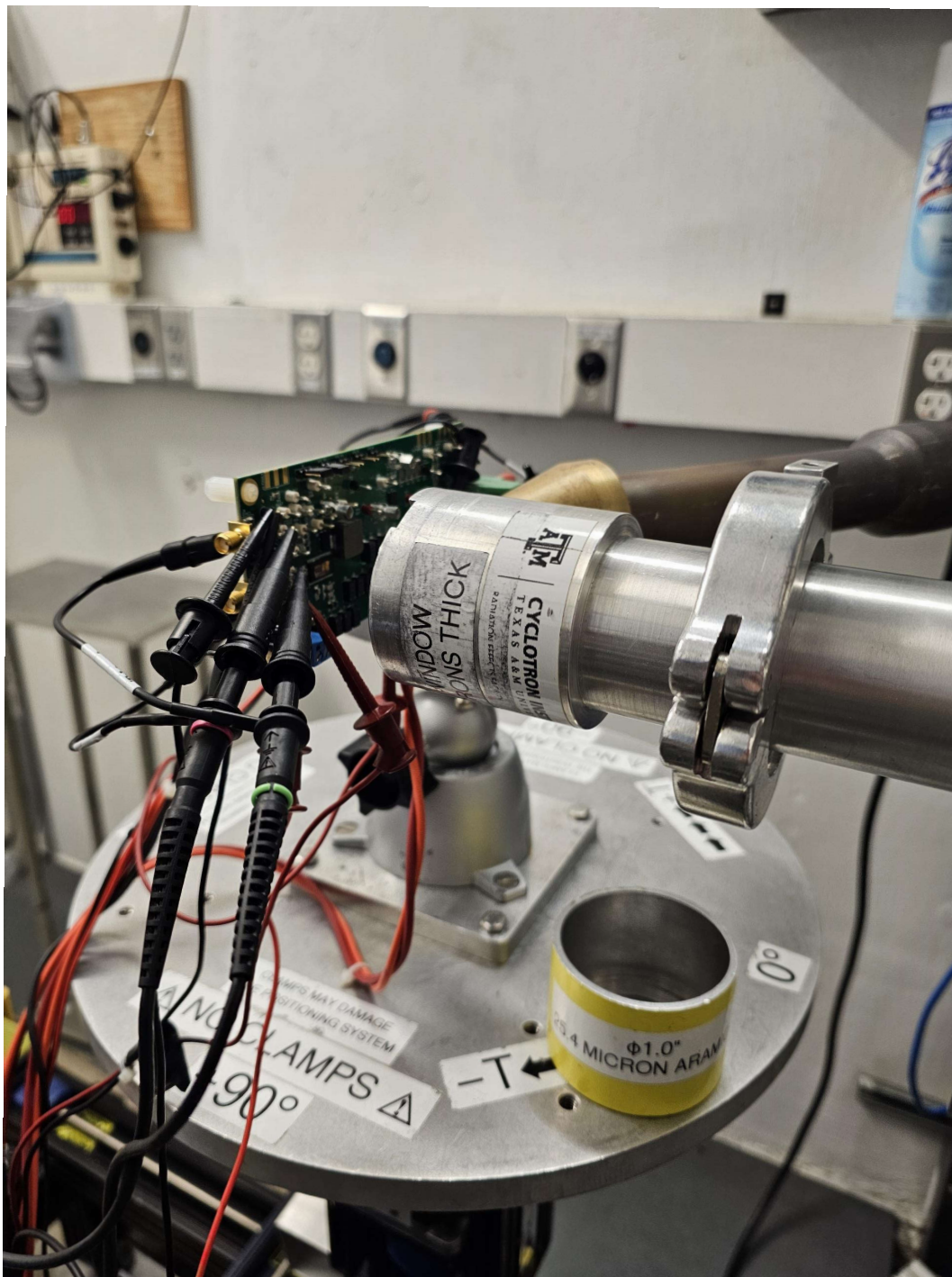


Figure 4-1. TPS7H4011-SEP EVM in Front of the Heavy-Ion Beam Exit Port at the Texas A&M Cyclotron

5 LET_{EFF} and Range Calculation

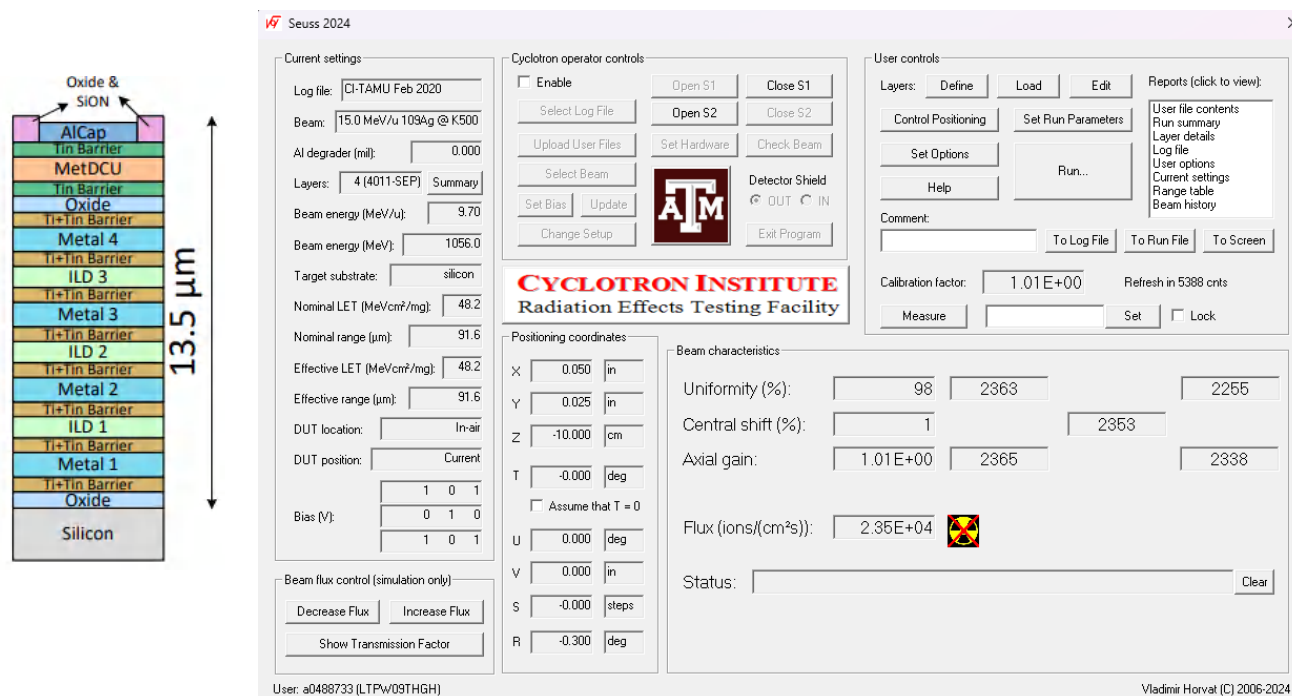


Figure 5-1. Generalized Cross-Section of the LBC7 Technology BEOL Stack on the TPS7H4011-SEP (Left) and SEUSS 2020 Application Used to Determine Key Ion Parameters (Right)

The TPS7H4011-SEP is fabricated in the TI Linear BiCMOS 250-nm process with a back-end-of-line (BEOL) stack consisting of four levels of standard thickness aluminum and Damascene copper. The total stack height from the surface of the passivation to the silicon surface is 13.5 μm based on nominal layer thickness as shown in [Figure 5-1](#). Accounting for energy loss through the degrader, copper foil, beam port window, air gap, and the BEOL stack of the TPS7H4011-SEP, the effective LET (LET_{EFF}) at the surface of the silicon substrate and the depth was determined with:

- SEUSS 2024 Software (provided by the Texas A&M Cyclotron Institute and based on the latest SRIM-2013 [7] models).
- MSU Stack-Up Calculator (provided by MSU FRIB based on the latest SRIM-2013 [7] models).

The results are shown in [Ion LET_{EFF} and Range in Silicon](#).

Table 5-1. Ion LET_{EFF} and Range in Silicon

Facility	Ion Type	Beam Energy (MeV/nucleon)	Degrader Steps (#)	Degrader Angle	Copper Foil Width (μm)	Beam Port Window	Air Gap (mm)	Angle of Incidence	LET _{EFF} (MeV·cm²/mg)	Range in Silicon (μm)
TAMU	¹⁰⁹ Ag	15	0	0	-	1-mil Aramica	40	0	48.2	91.6
KSEE	¹⁰⁹ Ag	19.5	-	-	5	3-mil PEN	60	0	48	89.3

6 Test Setup and Procedures

There were two input supplies used to power the TPS7H4011-SEP which provided V_{IN} and EN. The V_{IN} for the device was provided through Channel 3 of an N6705C power module and ranged from 5 and 12V for SET to 14V for SEL and SEB/SEGR. EN was powered by Channel 1 of an E36311A power supply and ranged from 0V for SEB Off to 5V for all other testing.

The instrument used to load the TPS7H4011-SEP was a Chroma 63600 E-Load that was used in Constant Resistance (CR) mode. The value of CR was 0.2718Ω and provided a 12A load on the device.

The primary signal monitored on the EVM was V_{OUT} and this was done using a PXIe-5172 scope card with a 3% window trigger based on the nominal measured value of V_{OUT} . All SEL, SEB On, and SET testing used these conditions with only the SEB Off testing having different conditions. The conditions for SEB Off were a positive edge trigger at 0.5V which would check to see if the device ever incorrectly turned on while it was disabled. The secondary signals monitored were the PWRGD and SS_TR pins. These signals were monitored on their own PXIe-5172 cards and were configured to have negative edge triggers. Both had a negative edge trigger at 50% below nominal.

All equipment was controlled and monitored using a custom-developed LabVIEW™ program (PXI-RadTest) running on a HP-Z4™ desktop computer. The computer communicates with the PXI chassis via an MXI controller and NI PXIe-8381 remote control module.

[Equipment Settings and Parameters Used During the SEE Testing of the TPS7H4011-SEP](#) shows the connections, limits, and compliance values used during the testing. [Figure 6-1](#) shows a block diagram of the setup used for SEE testing of the TPS7H4011-SEP.

Table 6-1. Equipment Settings and Parameters Used During the SEE Testing of the TPS7H4011-SEP

Pin Name	Equipment Used	Capability	Compliance	Range of Values Used
V_{IN}	N6705C (CH #3)	60V, 17A	5A	5 to 14V
EN	E36311A (CH #1)	6V, 5A	0.1A	0V, 5V
V_{OUT}	PXIe-5172 (1)	100MS/s	—	100MS/s
SS_TR	PXIe-5172 (2)	100MS/s	—	100MS/s
PWRGD	PXIe-5172 (3)	100MS/s	—	100MS/s
V_{OUT}	Chroma 63600 E-Load	80A	High	—

All boards used for SEE testing were fully checked for functionality. Dry runs were also performed to ensure that the test system was stable under all bias and load conditions prior to being taken to the test facilities. During the heavy-ion testing, the LabVIEW control program powered up the TPS7H4011-SEP device and set the external sourcing and monitoring functions of the external equipment. After functionality and stability was confirmed, the beam shutter was opened to expose the device to the heavy-ion beam. The shutter remained open until the target fluence was achieved (determined by external detectors and counters). During irradiation, the NI scope cards continuously monitored the signals. When the output exceeded the pre-defined 3% window trigger, a data capture was initiated. No sudden increases in current were observed (outside of normal fluctuations) on any of the test runs and indicated that no SEL or SEB/SEGR events occurred during any of the tests.

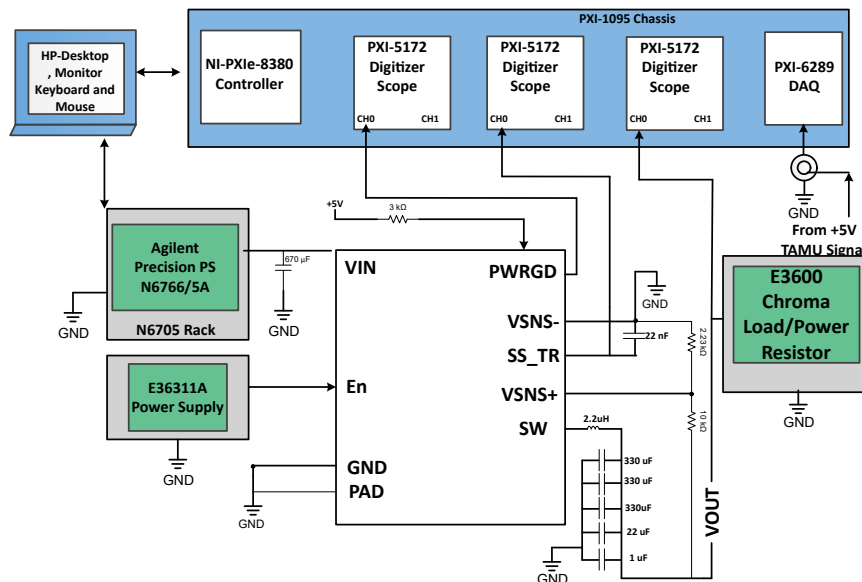


Figure 6-1. Block Diagram of the SEE Test Setup for the TPS7H4011-SEP

7 Destructive Single-Event Effects (DSEE)

7.1 Single-Event Latch-up (SEL) Results

During the SEL testing the device was heated to 125°C by using PID controlled heat gun (MISTRAL 6 System (120V, 2400W)). The temperature of the die was constantly monitored during testing at TAMU through an IR camera integrated into the control loop to create closed-loop temperature control. The die temperature was verified using a standalone FLIR thermal camera prior to exposure to heavy ions at KSEE.

The species used for the SEL testing was ^{109}Ag (TAMU) at 15 MeV/nucleon and ^{109}Ag (KSEE) at 19.5 MeV/nucleon. For both ions an angle of incidence of 0° was used to achieve a LET_{EFF} of $\approx 48 \text{ MeV}\times\text{cm}^2/\text{mg}$ (for more details refer to [Table 5-1](#)). The kinetic energy in the vacuum for ^{109}Ag (TAMU) is 1.635 GeV and ^{109}Ag (KSEE) is 2.125 GeV. Flux of approximately $10^5 \text{ ions}/\text{cm}^2/\text{s}$ and a fluence of approximately $10^7 \text{ ions}/\text{cm}^2$ per run was used. Run duration to achieve this fluence was ≈ 2 minutes. The six devices were powered up and exposed to the heavy-ions using the maximum recommended input voltage of 14V with the maximum recommended load of 12A. No SEL events were observed during all six runs, indicating that the TPS7H4011-SEP is SEL-free up to $48 \text{ MeV}\times\text{cm}^2/\text{mg}$. [Table 7-1](#) shows the SEL test conditions and results. [Figure 7-1](#) shows a plot of the current versus time for run 1.

Table 7-1. Summary of TPS7H4011-SEP SEL Test Condition and Results

Run Number	Unit Number	Facility	Ion	LET_{EFF} (MeV \times cm ² /mg)	Flux (ions/cm ² /s)	Fluence (ions/cm ²)	V _{IN} (V)	I _{OUT} (A)	SEL (# Events)
1	1	TAMU	^{109}Ag	48	1.36×10^5	1×10^7	14	12	0
2	2	TAMU	^{109}Ag	48	1.29×10^5	1×10^7	14	12	0
3	3	TAMU	^{109}Ag	48	1.32×10^5	1×10^7	14	12	0
4	4	TAMU	^{109}Ag	48	1.24×10^5	1×10^7	14	12	0
5	5	KSEE	^{109}Ag	48	1.08×10^5	1×10^7	14	12	0
6	6	KSEE	^{109}Ag	48	1.13×10^5	1×10^7	14	12	0

Using the MFTF method shown in [Single-Event Effects \(SEE\) Confidence Interval Calculations](#) and combining (or summing) the fluences of the six runs at 125°C (6×10^7), the upper-bound cross-section (using a 95% confidence level) is calculated as: $\sigma_{\text{SEL}} \leq 6.15 \times 10^{-8} \text{ cm}^2/\text{device}$ for $\text{LET}_{\text{EFF}} = 48 \text{ MeV}\times\text{cm}^2/\text{mg}$ and $T = 125^\circ\text{C}$.

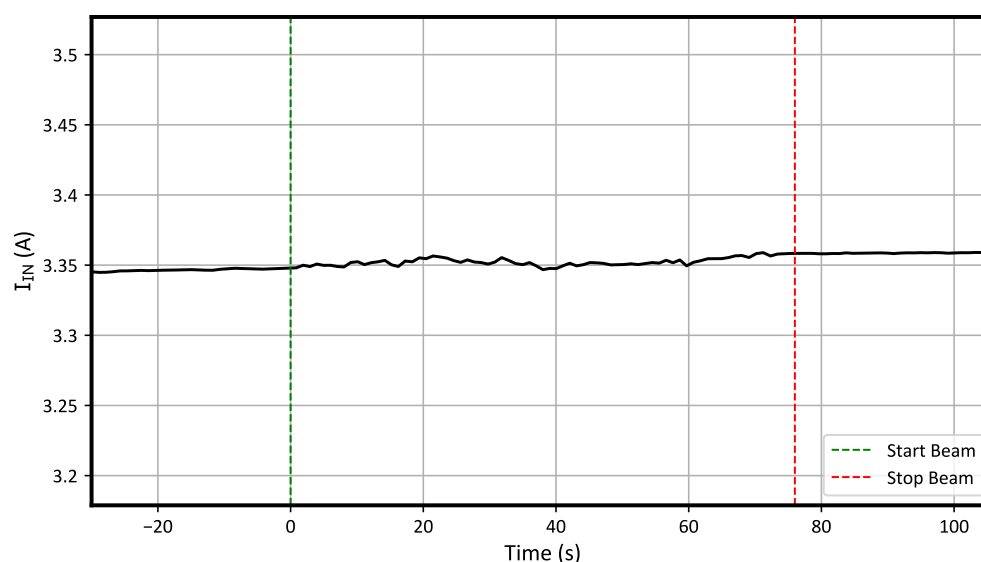


Figure 7-1. SEL Current versus Time for Run 1 of the TPS7H4011-SEP at $T = 125^\circ\text{C}$ ($V_{\text{OUT}} = 3.3\text{V}$)

7.2 Single-Event Burnout (SEB) and Single-Event Gate Rupture (SEGR) Results

During the SEB/SEGR characterization, the device was tested at room temperature of $\approx 25^{\circ}\text{C}$. The device was tested under both the enabled and disabled mode. For the SEB-Off mode the device was disabled using the EN-pin by forcing 0V (using Channel 1 of a E36311A Keysight PS). During the SEB/SEGR testing with the device enabled/disabled, not a single input current event was observed.

The species used for the SEB testing was ^{109}Ag (TAMU) at 15 MeV/nucleon and ^{109}Ag (KSEE) at 19.5 MeV/nucleon. For both ions an angle of incidence of 0° was used to achieve a LET_{EFF} of $\approx 48 \text{ MeV}\cdot\text{cm}^2/\text{mg}$ (for more details refer to [Table 5-1](#)). The kinetic energy in the vacuum for ^{109}Ag (TAMU) is 1.635 GeV and ^{109}Ag (KSEE) is 2.125 GeV. Flux of approximately $10^5 \text{ ions/cm}^2/\text{s}$ and a fluence of approximately 10^7 ions/cm^2 per run was used. Run duration to achieve this fluence was ≈ 2 minutes. The six devices (same as used in SEL testing) were powered up and exposed to the heavy-ions using the maximum recommended input voltage of 14V with the max recommended load of 12A. No SEB/SEGR current events were observed during the 12 runs, indicating that the TPS7H4011-SEP is SEB/SEGR-free up to $\text{LET}_{\text{EFF}} = 48 \text{ MeV}\cdot\text{cm}^2/\text{mg}$ and across the full electrical specifications. [Summary of TPS7H4011-SEP SEB/SEGR Test Condition and Results](#) shows the SEB/SEGR test conditions and results.

Table 7-2. Summary of TPS7H4011-SEP SEB/SEGR Test Condition and Results

Run Number	Unit Number	Facility	ION	LET_{EFF} ($\text{MeV} \times \text{cm}^2/\text{mg}$)	FLUX ($\text{ions/cm}^2/\text{s}$)	FLUENCE (ions/cm^2)	Enabled Status	V_{IN} (V)	I_{OUT} (A)	SEB EVENT?
7	1	TAMU	^{109}Ag	48	1.36×10^5	1.00×10^7	EN	14	12	No
8		TAMU	^{109}Ag	48	1.15×10^5	1.00×10^7	DIS	14	12	No
9	2	TAMU	^{109}Ag	48	1.33×10^5	1.00×10^7	EN	14	12	No
10		TAMU	^{109}Ag	48	1.45×10^5	1.00×10^7	DIS	14	12	No
11	3	TAMU	^{109}Ag	48	1.41×10^5	1.00×10^7	EN	14	12	No
12		TAMU	^{109}Ag	48	1.30×10^5	1.00×10^7	DIS	14	12	No
13	4	TAMU	^{109}Ag	48	1.24×10^5	1.00×10^7	EN	14	12	No
14		TAMU	^{109}Ag	48	1.21×10^5	1.00×10^7	DIS	14	12	No
15	5	KSEE	^{109}Ag	48	1.11×10^5	1.00×10^7	EN	14	12	No
16		KSEE	^{109}Ag	48	1.09×10^5	1.00×10^7	DIS	14	12	No
17	6	KSEE	^{109}Ag	48	1.05×10^5	1.00×10^7	EN	14	12	No
18		KSEE	^{109}Ag	48	1.05×10^5	1.00×10^7	DIS	14	12	No

Using the MFTF method described in [Single-Event Effects \(SEE\) Confidence Interval Calculations application report](#), the upper-bound cross-section (using a 95% confidence level) is calculated as:

$$\sigma_{\text{SEB}} \leq 3.07 \times 10^{-8} \text{ cm}^2/\text{device for } \text{LET}_{\text{EFF}} = 48 \text{ MeV}\cdot\text{cm}^2/\text{mg and } T = 25^{\circ}\text{C}.$$

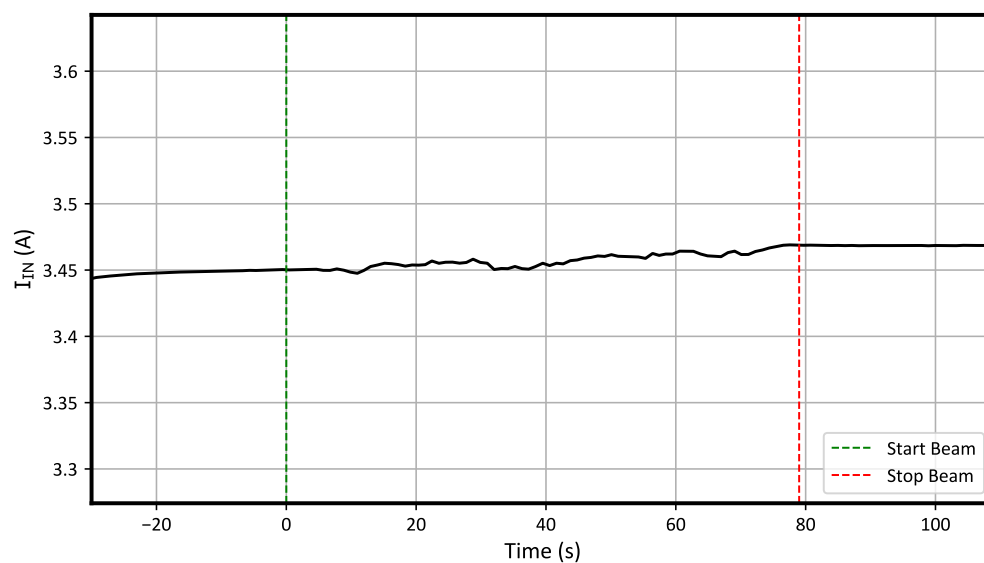


Figure 7-2. SEB On Current vs Time for Run 7 of the TPS7H4011-SEP at T = 25°C ($V_{OUT} = 3.3V$)

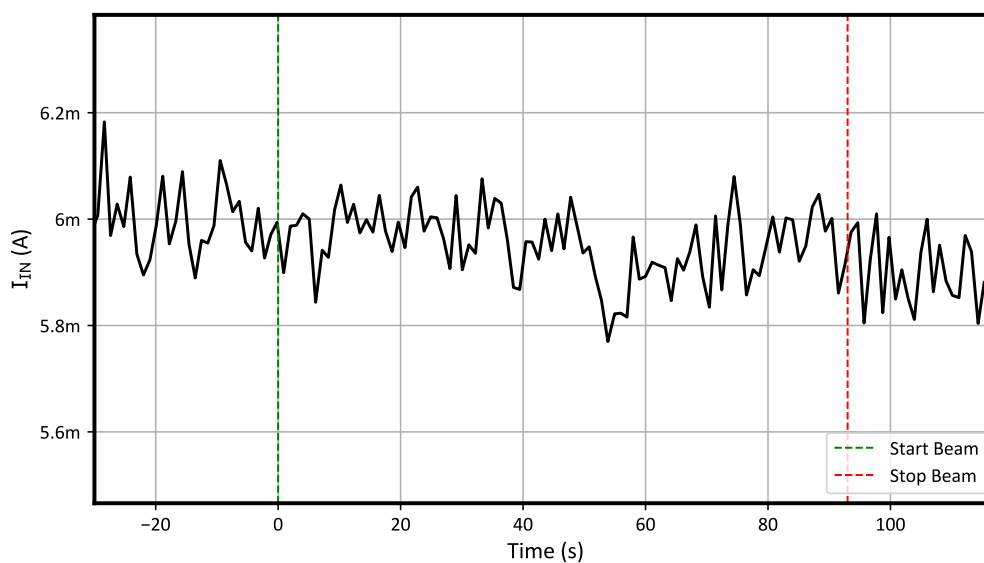


Figure 7-3. SEB Off Current vs Time for Run 8 of the TPS7H4011-SEP at T = 25°C ($V_{OUT} = 0-V$)

8 Single-Event Transients (SET)

SETs are defined as heavy-ion-induced transients upsets on the VOUT, SS_TR, or PWRGD of the TPS7H4011-SEP.

The species used for the SET testing was ^{109}Ag (TAMU) at 15 MeV/nucleon and ^{109}Ag (KSEE) at 19.5 MeV/nucleon. For both ions an angle of incidence of 0° was used to achieve a LET_{EFF} of $\approx 48 \text{ MeV} \times \text{cm}^2/\text{mg}$ (for more details refer to [Table 5-1](#)). Flux of approximately $10^5 \text{ ions/cm}^2/\text{s}$ and a fluence of 10^7 ions/cm^2 , per run were used for the SET characterization discussed on this chapter. Over the course of testing six devices, not a single transient or SEFI was recorded on any of the monitored signals indicating that the TPS7H4011-SEP is SET/SEFI free up to $\text{LET}_{\text{EFF}} = 48 \text{ MeV} \times \text{cm}^2/\text{mg}$.

Waveform size, sample rate, trigger type, value, and signal for all scopes used is presented on [Table 8-1](#).

Table 8-1. Scope Settings

Scope Model	Trigger Signal	Trigger Type	Trigger Value	Record Length	Sample Rate
PXIe-5172 (1)	VOUT	Window	$\pm 3\%$	50k	100MS/s
PXIe-5172 (2)	SS_TR	Edge/Negative	50%	50k	100MS/s
PXIe-5172 (3)	PWRGD	Edge/Negative	50%	50k	100MS/s

Table 8-2. Summary of TPS7H4011-SEP SET Test Condition and Results

Run Number	Unit Number	Facility	ION	LET_{EFF} (MeV \times cm^2/mg)	V_{IN} (V)	FLUX (ions/ cm^2/s)	Fluence (ions/ cm^2)	$V_{\text{OUT SET}} \geq 3\% $ (#)	SS_TR SET (#)	PWRGD SET (#)
19	1	TAMU	^{109}Ag	48	12	3.18×10^4	1.00×10^7	0	0	0
20		TAMU	^{109}Ag	48	5	3.11×10^4	1.00×10^7	0	0	0
21	2	TAMU	^{109}Ag	48	12	5.65×10^4	1.00×10^7	0	0	0
22		TAMU	^{109}Ag	48	5	5.47×10^4	1.00×10^7	0	0	0
23	3	TAMU	^{109}Ag	48	12	6.01×10^4	1.00×10^7	0	0	0
24		TAMU	^{109}Ag	48	5	6.25×10^4	1.00×10^7	0	0	0
25	4	TAMU	^{109}Ag	48	12	6.84×10^4	1.00×10^7	0	0	0
26		TAMU	^{109}Ag	48	5	6.94×10^4	1.00×10^7	0	0	0
27	5	KSEE	^{109}Ag	48	12	1.03×10^5	1.00×10^7	0	0	0
28	6	KSEE	^{109}Ag	48	12	1.12×10^5	1.00×10^7	0	0	0

9 Event Rate Calculations

Event rates were calculated for LEO (ISS) and GEO environments by combining CREME96 orbital integral flux estimations and simplified SEE cross-sections according to methods described in [Heavy Ion Orbital Environment Single-Event Effects Estimations](#). Assume a minimum shielding configuration of 100mils (2.54mm) of aluminum, and *worst-week* solar activity (this is similar to a 99% upper bound for the environment). Using the 95% upper-bounds for SEL, SEB/SEGR, and SET the event rate calculations for SEL, SEB/SEGR, and SET are shown on [Table 9-1](#), [Table 9-2](#), and [Table 9-3](#), respectively. Note that this number is for reference since no SEL, SEB/SEGR, or SET events were observed.

Table 9-1. SEL Event Rate Calculations for Worst-Week LEO and GEO Orbits

Orbit Type	Onset LET _{EFF} (MeV-cm ² /mg)	CREME96 Integral FLUX (/day/cm ²)	σSAT (cm ²)	Event Rate (/day)	Event Rate (FIT)	MTBE (Years)
LEO (ISS)	48	4.50 × 10 ⁻⁴	6.15 × 10 ⁻⁸	2.77 × 10 ⁻¹¹	2.77 × 10 ⁻³	9.90 × 10 ⁷
GEO		1.48 × 10 ⁻³		9.08 × 10 ⁻¹¹	3.78 × 10 ⁻³	3.02 × 10 ⁷

Table 9-2. SEB/SEGR Event Rate Calculations for Worst-Week LEO and GEO Orbits

Orbit Type	Onset LET _{EFF} (MeV-cm ² /mg)	CREME96 Integral FLUX (/day/cm ²)	σSAT (cm ²)	Event Rate (/day)	Event Rate (FIT)	MTBE (Years)
LEO (ISS)	48	4.50 × 10 ⁻⁴	3.07 × 10 ⁻⁸	1.38 × 10 ⁻¹¹	5.77 × 10 ⁻⁴	1.98 × 10 ⁸
GEO		1.48 × 10 ⁻³		4.54 × 10 ⁻¹¹	1.89 × 10 ⁻³	6.04 × 10 ⁷

Table 9-3. SET Event Rate Calculations for Worst-Week LEO and GEO Orbits

Orbit Type	Onset LET _{EFF} (MeV-cm ² /mg)	CREME96 Integral FLUX (/day/cm ²)	σSAT (cm ²)	Event Rate (/day)	Event Rate (FIT)	MTBE (Years)
LEO (ISS)	48	4.50 × 10 ⁻⁴	3.69 × 10 ⁻⁸	1.66 × 10 ⁻¹¹	6.92 × 10 ⁻⁴	1.65 × 10 ⁸
GEO		1.48 × 10 ⁻³		5.45 × 10 ⁻¹¹	2.27 × 10 ⁻³	5.03 × 10 ⁷

10 Summary

The purpose of this study was to characterize the effect of heavy-ion irradiation on the single-event effect (SEE) performance of the TPS7H4011-SEP synchronous buck converter. Heavy-ions with $LET_{EFF} = 48 \text{ MeV} \times \text{cm}^2/\text{mg}$ were used for the SEE characterization campaign. Flux of $\approx 10^5 \text{ ions/cm}^2/\text{s}$ and fluences of $\approx 10^7 \text{ ions/cm}^2$ per run were used for the characterization. The SEE results demonstrated that the TPS7H4011-SEP is free of destructive SEL and SEB and SET/SEFI up to $LET_{EFF} = 48 \text{ MeV} \times \text{cm}^2/\text{mg}$ across the full electrical specifications. CREME96-based worst-week event-rate calculations for LEO(ISS) and GEO orbits for the DSEE and SET are presented for reference.

A References

1. M. Shoga and D. Binder, "Theory of Single Event Latchup in Complementary Metal-Oxide Semiconductor Integrated Circuits", *IEEE Trans. Nucl. Sci.*, Vol. 33(6), Dec. 1986, pp. 1714-1717.
2. G. Bruguier and J. M. Palau, "Single particle-induced latchup", *IEEE Trans. Nucl. Sci.*, Vol. 43(2), Mar. 1996, pp. 522-532.
3. G. H. Johnson, J. H. Hohl, R. D. Schrimpf and K. F. Galloway, "Simulating single-event burnout of n-channel power MOSFET's," in *IEEE Transactions on Electron Devices*, vol. 40, no. 5, pp. 1001-1008, May 1993.
4. J. R. Brews, M. Allenspach, R. D. Schrimpf, K. F. Galloway, J. L. Titus and C. F. Wheatley, "A conceptual model of a single-event gate-rupture in power MOSFETs," in *IEEE Transactions on Nuclear Science*, vol. 40, no. 6, pp. 1959-1966, Dec. 1993.
5. G. H. Johnson, R. D. Schrimpf, K. F. Galloway, and R. Koga, "Temperature dependence of single event burnout in n-channel power MOSFETs [for space application]," *IEEE Trans. Nucl. Sci.*, 39(6), Dec. 1992, pp. 1605-1612.
6. Texas A&M University, [Cyclotron Radiation Effects Facility](#), webpage.
7. Ziegler, James F. [The Stopping and Range of Ions in Matter \(SRIM\) software tools](#), webpage.
8. D. Kececioglu, "Reliability and Life Testing Handbook", Vol. 1, PTR Prentice Hall, New Jersey, 1993, pp. 186-193.
9. Vanderbilt University, [ISDE CRÈME-MC](#), webpage.
10. A. J. Tylka, J. H. Adams, P. R. Boberg, et al., "CREME96: A Revision of the Cosmic Ray Effects on Micro-Electronics Code", *IEEE Trans. on Nucl. Sci.*, Vol. 44(6), Dec. 1997, pp. 2150-2160.
11. A. J. Tylka, W. F. Dietrich, and P. R. Boberg, "Probability distributions of high-energy solar-heavy-ion fluxes from IMP-8: 1973-1996", *IEEE Trans. on Nucl. Sci.*, Vol. 44(6), Dec. 1997, pp. 2140-2149.

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