High-input impedance, true differential, analog front end (AFE) attenuator circuit for SAR ADCs

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### Input Voltage (OPA197 Buffers) | THS4551 Output, ADC Input | ADS8912B Digital Output
---|---|---
VinP = −12V, VinN = +12V, VinMin (Diff) = −24V | VoutDif = −4.00V, VoutP = 0.25V, VoutN = 4.25V | 238E3, −116509, t0
VinP = +12V, VinN = −12V, VinMax (Diff) = +24V | VoutDif = +4.00V, VoutP = 4.25V, VoutN = 0.25V | 1C71C, +116508

### Supplies and Reference

<table>
<thead>
<tr>
<th>HVDD</th>
<th>HVSS</th>
<th>Vcc</th>
<th>Vee</th>
<th>Vref</th>
<th>Vcm</th>
</tr>
</thead>
<tbody>
<tr>
<td>+15V</td>
<td>−15V</td>
<td>+5.0V</td>
<td>0V</td>
<td>+4.5V</td>
<td>2.5V</td>
</tr>
</tbody>
</table>

### Design Description

This analog front end (AFE) and SAR ADC data acquisition solution can measure true differential voltage signals in the range of ±24V (or absolute input range VinP = ±12V, VinN = ±12V) offering high-input impedance supporting data rates up to 500ksps with 18-bit resolution. A precision, 36-V rail-to-rail amplifier with low-input bias current is used to buffer the inputs of a fully-differential amplifier (FDA). The FDA attenuates and shifts the signal to the differential voltage and common-mode voltage range of the SAR ADC. The values in the component selection section can be adjusted to allow for different input voltage levels.

This circuit implementation is used in accurate measurement of true differential voltage in Application-Specific Test Equipment, Data Acquisition (DAQ) cards, and Analog Input Modules used in Programmable Automation Control (PAC), Discrete Control System (DCS), and Programmable Logic Control (PLC) applications.
Specifications

<table>
<thead>
<tr>
<th>Specification</th>
<th>Goal</th>
<th>Calculated</th>
<th>Simulated</th>
</tr>
</thead>
<tbody>
<tr>
<td>Transient ADC Input Settling (500ksps)</td>
<td>&lt;&lt; 1 LSB; &lt;&lt; 34µV</td>
<td>N/A</td>
<td>0.5µV</td>
</tr>
<tr>
<td>Noise (at ADC Input)</td>
<td>10µV RMS</td>
<td>9.28µV RMS</td>
<td>9.76µV RMS</td>
</tr>
<tr>
<td>Bandwidth</td>
<td>1.25MHz</td>
<td>1.25MHz</td>
<td>1.1MHz</td>
</tr>
</tbody>
</table>

Design Notes
1. Verify the linear range of the op amp (buffer) based on the common mode, output swing specification for linear operation. This is covered in the component selection section. Select an amplifier with low input bias current.
2. Find ADC full-scale range and common-mode range specifications. This is covered in the component selection.
3. Determine the required attenuation for the FDA based on the input signal amplitude, the ADC full-scale range and the output swing specifications of the FDA. This is covered in the component selection section.
4. Select COG capacitors to minimize distortion.
5. Use 0.1% 20ppm/°C film resistors or better for good accuracy, low gain drift, and to minimize distortion.
6. *Understanding and Calibrating the Offset and Gain for ADC Systems* covers methods for error analysis. Review the link for methods to minimize gain, offset, drift, and noise errors.
7. *Introduction to SAR ADC Front-End Component Selection* covers methods for selecting the charge bucket circuit Rfilt and Cfilt. These component values are dependent on the amplifier bandwidth, data converter sampling rate, and data converter design. The values shown here will give good settling and AC performance for the amplifier, gain settings, and data converter in this example. If the design is modified, a different RC filter must be selected. Refer to the *Precision Labs* videos for an explanation of how to select the RC filter for best settling and AC performance.
Component Selection and Settings for Buffer Amplifier and FDA

1. Verify the buffer amplifier input range for linear operation:
   Select Supplies \((V-) = -15V\), \((V+) = +15V\) to allow \(V_{inP} = \pm 12V\) \(V_{inN} = \pm 12V\) range
   \((V-) - 0.1V < V_{cm} < (V+) - 3V\) from OPA197 common-mode voltage specification
   \(-15.1V < V_{cm} < +12V\) allows required \(\pm 12V\) input voltage range

2. Verify the buffer amplifier output range for linear operation:
   \((V-) + 0.6V < V_{out} < (V+) - 0.6V\) from OPA197 Aol specification for linear operation
   \(-14.4V < V_{out} < 14.4V\) allows required \(\pm 12V\) output voltage range

3. Find ADC full-scale input range. In this circuit, \(V_{REF} = 4.5V\):
   \(V_{cm} = \frac{V_{REF} + V_{REF}}{2} = \pm 2.25V\) from ADS8910B datasheet

4. Find the required ADC common-mode voltage:
   \(V_{cm} = \frac{+V_{REF}}{2} = +2.25V\) from ADS8910B datasheet, therefore set FDA VCOM = 2.25V

5. Find FDA absolute output voltage range for linear operation:
   \(0.23V < V_{out} < 4.77V\) from THS4551 output low/high specification for linear operation
   However, the positive range is limited by \(ADC_{Full-Scale Range} = \pm 4.5V\), therefore
   \(0.23V < V_{out} < 4.5V\) where \(V_{outMin} = 0.23V\), \(V_{outMax} = 4.5V\)

6. Find FDA differential output voltage range for linear operation. The general output voltage equations for this circuit follow:
   \(V_{outDMin} = \frac{V_{outDMin}}{2} + V_{cm}\) and \(V_{outDMax} = \frac{V_{outDMax}}{2} + V_{cm}\)
   Re-arrange the equations and solve for \(V_{outDMin}\) and \(V_{outDMax}\):
   Find maximum differential output voltage range based on worst case:
   \(V_{outDMax} = 2 \cdot V_{outMax} - 2 \cdot V_{cm} = 2 \cdot (4.5V) - 2 \cdot (2.25V) = 4.5V\)
   \(V_{outDMin} = 2 \cdot V_{outMin} - 2 \cdot V_{cm} = 2 \cdot (0.23V) - 2 \cdot (2.5V) = -4.04V\)
   Based on combined worst case, choose \(V_{outDMin} = -4.04V\) and \(V_{outDMax} = +4.04V\)

7. Find the FDA differential input voltage range:
   \(V_{inDMin} = V_{inPmax} - V_{inNmin} = +12V - (-12V) = +24V\)
   \(V_{inDMax} = V_{inPmax} - V_{inNmax} = -12V - (+12V) = -24V\)

8. Find FDA required attenuation ratio:
   \(Gain_{FDA} = \frac{V_{outDMax} - V_{outDMin}}{V_{outDMax} - V_{inDMin}} = \frac{(+4.04V) - (-4.04V)}{(+24V) - (-24V)} = 0.166 \frac{V}{V} \approx \frac{1}{6} \frac{V}{V}\)

9. Find standard resistor values to set the attenuation:
   \(Gain_{FDA} = \frac{R_f}{R_f} = \frac{100k\Omega}{6.04k\Omega} = \frac{1}{6.04} \frac{V}{V} \Rightarrow \frac{R_f}{R_f} = \frac{6.04k\Omega}{100k\Omega} \approx \frac{1}{166} \frac{V}{V}\)

10. Find \(C_f\) for cutoff frequency \(f_c\), \(R_{fina} = 1k\Omega\):
    \(C_f = \frac{1}{2 \cdot \pi \cdot f_c \cdot R_{fina}} = \frac{1}{2 \cdot \pi \cdot (1.25MHz) \cdot (1k\Omega)} = 127 pF or 120 pF standard value\)
DC Transfer Characteristics
The following graph shows a linear output response for differential inputs from +24V to –24V.

![DC Transfer Graph]

VoutDiff = -3.973443V
VinDiff = -24V

VoutDiff = +3.973543V
VinDiff = +24V

AC Transfer Characteristics
The simulated bandwidth is approximately 1.1MHz and the gain is –15.62dB which is a linear gain of approximately 0.166V/V (attenuation ratio 6.04V/V).
Noise Simulation

Simplified Noise calculation for rough estimate:

\[ f_c = \frac{1}{2 \cdot \pi \cdot R_f \cdot C_f} = \frac{1}{2 \cdot \pi \cdot (1k\Omega) \cdot (120pF)} = 1.33MHz \]

Noise contribution of OPA197 buffer referred to ADC input

\[ E_{nOPA197} = e_{nOPA197} \cdot \sqrt{K_n \cdot f_c \cdot \text{Gain}_{FDA}} \]
\[ E_{nOPA197} = \left( \frac{5.5nV}{\sqrt{Hz}} \right) \cdot \sqrt{1.57 \cdot 1.33MHz} = 0.166V/V = 1.319\mu V_{RMS} \]

Noise of THS4551 FDA referred to ADC input

Noise gain: \( NG = 1 + R_f / R_b = 1 + \frac{1.00k\Omega}{6.04k\Omega} = 1.166 \)

\[ e_{noFDA} = \sqrt{\left( e_{nFDA} \cdot NG \right)^2 + 2 \left( i_{nFDA} \cdot R_f \right)^2 + 2 \left( 4kT R_f \cdot NG \right)} \]
\[ e_{noFDA} = \sqrt{\left( 3.4nV/\sqrt{Hz} \cdot 1.166V/V \right)^2 + 2 \left( 0.5pA/\sqrt{Hz} \cdot 1k\Omega \right)^2 + 2 \left( 16.56 \cdot 10^{-18} \cdot 1.166V/V \right)} \]
\[ e_{noFDA} = 7.40nV/\sqrt{Hz} \]
\[ E_{nFDA} = e_{noFDA} \cdot \sqrt{K_n \cdot f_c} = \left( 7.40nV/\sqrt{Hz} \right) \cdot \sqrt{1.57 \cdot 1.33MHz} = 9.28\mu V_{RMS} \]

Total Noise = \[ \sqrt{E_{nFDA}^2 + E_{nOPA197}^2} = \sqrt{(9.28\mu V_{RMS})^2 + (1.32\mu V_{RMS})^2} = 9.37\mu V_{RMS} \]

Note that calculated and simulated match well. Refer to Calculating the Total Noise for ADC Systems for detailed theory on this subject.
Stability Simulation

The following circuit is used in TINA to measure loop gain and verify phase margin using AC transfer analysis in TINA. Resistors $R_{\text{ISO}} = 10\Omega$ are used inside the feedback loop to increase phase margin. The circuit has 45 degrees of phase margin. Refer to TI Precision Labs - Op Amps: Stability 4 for detailed theory on this subject.
Transient ADC Input Settling Simulation

The following simulation shows settling to a 24-V DC differential input signal with the OPA197 buffers inputs set at +12V and −12V. This type of simulation shows that the sample and hold kickback circuit is properly selected. Refer to *Refine the Rfilt and Cfilt Values* for detailed theory on this subject.

![Diagram showing Vacq and Verror over time with Verror = 168nV]

**Vacq**

**Verror**

**Time (s)**

3.90u 4.95u 6.00u
Design Featured Devices

<table>
<thead>
<tr>
<th>Device</th>
<th>Key Features</th>
<th>Link</th>
<th>Similar Devices</th>
</tr>
</thead>
<tbody>
<tr>
<td>ADS8912B</td>
<td>18-bit resolution, 500-kps sample rate, integrated reference buffer, fully-differential input, Vref input range 2.5V to 5V.</td>
<td><a href="http://www.ti.com/product/ADS8912B">www.ti.com/product/ADS8912B</a></td>
<td><a href="http://www.ti.com/adcs">www.ti.com/adcs</a></td>
</tr>
<tr>
<td>THS4551</td>
<td>FDA, 150-MHz bandwidth, Rail-to-Rail Output, VosDriftMax = 1.8µV/°C, e_n = 3.3nV/rtHz</td>
<td><a href="http://www.ti.com/product/THS4551">www.ti.com/product/THS4551</a></td>
<td><a href="http://www.ti.com/opamp">www.ti.com/opamp</a></td>
</tr>
<tr>
<td>OPA197</td>
<td>36V, 10-MHz bandwidth, Rail-to-Rail Input/Output, VosMax = ±250µV, VosDriftMax = ±2.5µV/°C, bias current = ±5pA</td>
<td><a href="http://www.ti.com/product/OPA197">www.ti.com/product/OPA197</a></td>
<td><a href="http://www.ti.com/opamp">www.ti.com/opamp</a></td>
</tr>
<tr>
<td>REF5045</td>
<td>VREF = 4.5V, 3 ppm/°C drift, 0.05% initial accuracy, 4µVpp/V noise</td>
<td><a href="http://www.ti.com/product/REF5045">www.ti.com/product/REF5045</a></td>
<td><a href="http://www.ti.com/voltageref">www.ti.com/voltageref</a></td>
</tr>
</tbody>
</table>

(1) The REF5045 can be directly connected to the ADS8912B without any buffer because the ADS8912B has a built in internal reference buffer. Also, the REF5045 has the required low noise and drift for precision SAR applications. The THS4551 provides the attenuation and common-mode level shifting to the voltage range of the SAR ADC. In addition, this FDA is commonly used in high-speed precision fully-differential SAR applications as it has sufficient bandwidth to settle to charge kickback transients from the ADC input sampling. The OPA197 is a 36-V operational amplifier that provides a very high input impedance front end, buffering the FDA inputs.

Design References
See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.

Link to Key Files

Revision History

<table>
<thead>
<tr>
<th>Revision</th>
<th>Date</th>
<th>Change</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>March 2019</td>
<td>Downstyle the title and changed title role to 'Data Converters'. Added link to circuit cookbook landing page.</td>
<td></td>
</tr>
</tbody>
</table>
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