Most switching power supplies are designed with closed-loop feedback circuitry to provide stable power under various transient and load conditions. The feedback methodology options fall into two general categories, voltage mode control (VMC) and current mode control (CMC). Both methodologies have their strengths and weaknesses that determine the appropriate selection for the end-equipment application.

Control Methodologies
Voltage mode control utilizes a scaled value of the output voltage as the feedback signal. This methodology provides simple, straightforward feedback architecture for the control path. However, this method has several disadvantages that should be noted. The most significant disadvantage is output voltage regulation requires sensing a change in output voltage and propagation through the entire feedback signal and filter before the output is appropriately compensated. This can generate an unacceptably slow response for systems that desire high levels of regulation. The feedback compensation of the supply requires a higher level of analysis to address the two poles introduced by the output low-pass filter. Additionally, the feedback component values must be adjusted since different input voltages affect the overall loop gain.

Current mode control addresses the above shortfalls of voltage mode control by using the inductor current waveform for control. This signal is included with the output voltage feedback loop as a second, fast response control loop. The additional feedback loop does potentially increase the circuit/feedback complexity, so the advantages need to be evaluated as part of the design requirements.

By using the inductor current as part of the feedback control:
1. The added current feedback loop responds faster compared with only using the output voltage for feedback control. Additionally, with the inductor current information, the circuit can be designed to provide pulse by pulse current limiting allowing rapid detection and control for current limiting needs.
2. The power supply looks like a voltage controlled current source. This permits a modular supply design to allow load sharing between multiple supplies in a parallel configuration.
3. The effects of the inductor in the control loop can be minimized since the current feedback loop effectively reduces the compensation to a single pole requirement.

While current mode control addresses some of the drawbacks of VMC, it introduces challenges that can affect the circuit performance. The addition of the current feedback loop increases the complexity of the control/feedback circuit and circuit analysis. Stability across the entire range of duty cycles and sensitivity to noise signals are other items that need to be considered in the selection of current mode control. CMC can further be broken down into several different types of control schemes: peak, valley, emulated, hysteretic, and average CMC. The below text discusses the two most common methodologies used in circuit design — peak and average current mode control.

Peak Current Mode Control
Peak current mode control (PCMC) utilizes the current waveform directly as the ramp waveform into the PWM-generation comparator instead of an externally generated sawtooth—or triangle—signal like VMC. The upslope portion of the inductor current or high-side transistor current waveform is used to provide a fast response control loop in addition to the existing voltage control loop. As shown in Figure 1, the current signal is compared with the output of the voltage error amplifier to generate the PWM control signal for the power supply.

![Figure 1. Block Diagram of PCMC circuit](image-url)
current is as small as possible to reduce power loss due to the measurement. This small–valued resistor results in a small amplitude feedback signal. Since the inductor current waveform is used directly as the comparator input signal, PCMC is known to be susceptible to noise and voltage transients. Using a current sense amplifier like the INA240 with high common-mode rejection ratio (CMRR) provides suppression of transients associated with pulse-width modulation (PWM) signals and systems. The gain flexibility of the INA240 allows the inductor current waveform to be amplified to provide a larger signal for comparison without the need for additional gain or sacrificing performance. Additionally, the low offset and gain errors provide a reduction in design variations and changes across temperature. To utilize PCMC, the inductor current necessitates a high common–mode voltage measurement. The INA240 common–mode range allows for a wide range in supply input and output voltages.

It should be noted that PCMC most often adds slope compensation to address stability issues with duty cycles greater than 50%. The slope compensation is added to the inductor current before being used as the comparator input signal.

The INA240 provides performance and features for measurement accuracy which is needed to maintain good control signal integrity. The INA240 features a 25μV maximum input offset voltage and a 0.20% maximum gain error specification at room temperature. Temperature stability is important to maintain system performance and the INA240 provides input offset voltage drift of 250nV/°C with a 2.5ppm/°C amplifier gain drift. The INA240 features enhanced PWM rejection to improve performance with large common-mode transients and a wide common-mode input range for maximum design variance for supply output voltages.

**Alternative Device Recommendations**

Based on system requirements, alternative devices are available that can provide the needed performance and functionality. The LMP8601 family provides lower performance levels than the INA240 for in-line sensing applications. The INA282 allows current measurement for high common-mode voltages, making it ideal for high voltage DC application that do not have PWM signals. The INA290 is a high-voltage current sense amplifier with high bandwidth packaged in a small SC-70 package.

**Table 1. Alternative Device Recommendations**

<table>
<thead>
<tr>
<th>Device</th>
<th>Optimized Parameters</th>
<th>Performance Trade-Off</th>
</tr>
</thead>
<tbody>
<tr>
<td>INA253</td>
<td>Integrated Low inductive precision shunt: 2mΩ, 0.1%, Enhanced PWM rejection</td>
<td>+/-15A maximum continuous current at TA = 85°C</td>
</tr>
<tr>
<td>INA282</td>
<td>Low power, High Gain Options, High Supply Voltage</td>
<td>No Enhanced PWM Rejection, Higher drift specifications</td>
</tr>
<tr>
<td>INA290</td>
<td>Wide Common–Mode Input Range, High bandwidth, Small SC-70 package</td>
<td>No Enhanced PWM Rejection, Unidirectional, Common–mode range does not include ground</td>
</tr>
</tbody>
</table>

**Table 2. Adjacent Tech Notes**

<table>
<thead>
<tr>
<th>Note</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>SBOA189</td>
<td>Precision Brightness and Color Mixing in LED Lighting Using Discrete Current Sense Amplifiers</td>
</tr>
<tr>
<td>SBOA174</td>
<td>Current Sensing in an H-Bridge</td>
</tr>
<tr>
<td>SBOA176</td>
<td>Switching Power Supply Current Measurements</td>
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