Analog Engineer's Circuit Transimpedance amplifier with T-network circuit



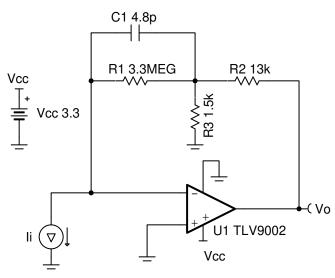
Amplifiers

Design Goals

Input		Output		BW	Supply	
l _{iMin}	I _{iMax}	V _{oMin}	V _{oMax}	fp	V _{cc}	V _{ee}
0A	100nA	0V	3.2V	10kHz	3.3V	0V

Design Description

This transimpedance amplifier with a T-network feedback configuration converts an input current into an output voltage. The current-to-voltage gain is based on the T-network equivalent resistance which is larger than any of the resistors used in the circuit. Therefore, the T-network feedback configuration circuit allows for very high gain without the use of large resistors in the feedback or a second gain stage, reducing noise, stability issues, and errors in the system.



Design Notes

- 1. C_1 and R_1 set the input signal cutoff frequency, f_p .
- 2. Capacitor C₁ in parallel with R₁ helps limit the bandwidth, reduce noise, and also improve the stability of the circuit if high-value resistors are used.
- 3. The common-mode voltage is the voltage at the non-inverting input and does not vary with input current.
- 4. A bias voltage can be added to the non-inverting input to bias the output voltage above the minimum output swing for 0A input current.
- 5. Using high-value resistors can degrade the phase margin of the circuit and introduce additional noise in the circuit.
- 6. Avoid placing capacitive loads directly on the output of the amplifier to minimize stability issues.
- 7. For more information on op amp linear operating region, stability, slew-induced distortion, capacitive load drive, driving ADCs, and bandwidth see the *Design References* section.

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Design Steps

The transfer function of this circuit follows:

$$V_o = I_i \times (\frac{R_2 \times R_1}{R_3} + R_1 + R_2)$$

1. Calculate the required gain:

Gain =
$$\frac{V_{oMax}}{I_{oMax}} = \frac{3.2V}{100nA} = 3.2 \times 10^7 \frac{V}{A}$$

2. Choose the resistor values to set the pass-band gain:

Gain =
$$\left(\frac{R_2 \times R_1}{R_3} + R_1 + R_2\right)$$

Since R_1 will be the largest resistor value in the system choose this value first then choose R_2 and calculate R_3 . Select $R_1 = 3.3M\Omega$ and $R_2 = 13k\Omega$. R_1 is very large due to the large transimpedance gain of the circuit. R_2 is in the ~10k ohm range so the op amp can drive it easily.

$$R_{3} = \left(\frac{R_{2} \times R_{1}}{Gain - R_{1} - R_{2}}\right) = \left(\frac{13k\Omega \times 3.3M\Omega}{3.2 \times 10^{7} \frac{V}{A} - 3.3M\Omega - 13k\Omega}\right) = 1.5k\Omega$$

3. Calculate C_1 to set the location of f_p .

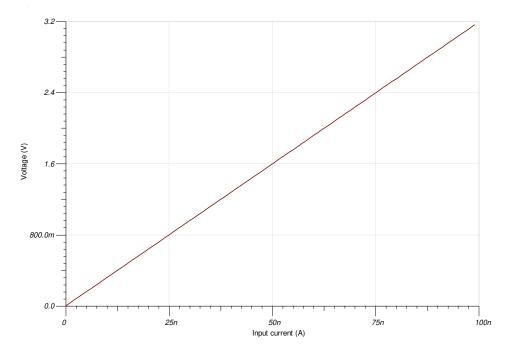
$$C_1 = \frac{1}{2 \pi \times R_1 \times f_p} = \frac{1}{2 \pi \times 3.3 M\Omega \times 10 \text{kHz}} = 4.82 \text{pF} \approx 4.8 \text{pF} \text{ (Standard Value)}$$

4. Run a stability analysis to make sure that the circuit is stable. For more information on how to run a stability analysis see the *TI Precision Labs - Op amp: Stability* video.

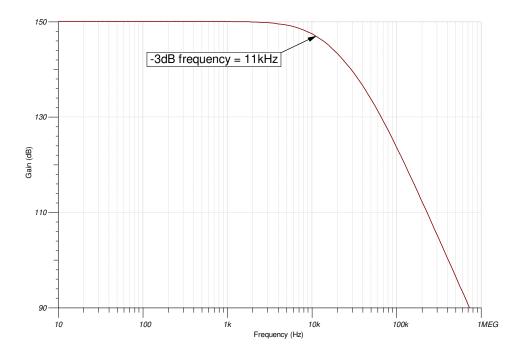


Design Simulations

DC Simulation Results



AC Simulation Results





Design References

- 1. See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.
- 2. See SPICE file, SBOMB39.
- 3. See TIPD176, www.ti.com/tool/tipd176.
- 4. For more information on many op amp topics including common-mode range, output swing, bandwidth, and how to drive an ADC please visit TI Precision Labs.

Design Featured Op Amp

TLV9002				
V _{cc}	1.8V to 5.5V			
V _{inCM}	Rail-to-rail			
V _{out}	Rail–to–rail			
V _{os}	0.4mV			
lq	60µA			
۱ _b	5pA			
UGBW	1MHz			
SR	2V/µs			
#Channels	1, 2, 4			
www.ti.com/product/TLV9002				

Design Alternate Op Amp

OPA375				
V _{cc}	2.25V to 5.5V			
V _{inCM}	V _{ee} to (V _{cc} –1.2V)			
V _{out}	Rail–to–rail			
V _{os}	0.15mV			
lq	890µA			
ال _b	10pA			
UGBW	10MHz			
SR	4.75V/µs			
#Channels	1			
www.ti.com/product/OPA375				

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