## Analog Engineer's Circuit

Transimpedance amplifier with T-network circuit

## Thexas InsTRUMENTS

## Amplifiers

## Design Goals

| Input |  | Output |  | BW | Supply |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{l}_{\mathrm{iMin}}$ | $\mathrm{l}_{\mathrm{iMax}}$ | $\mathrm{V}_{\text {oMin }}$ | $\mathrm{V}_{\text {oMax }}$ | $\mathrm{f}_{\mathrm{p}}$ | $\mathrm{V}_{\mathrm{cc}}$ | $\mathrm{V}_{\mathrm{ee}}$ |
| 0 A | 100 nA | 0 V | 3.2 V | 10 kHz | 3.3 V | 0 V |

## Design Description

This transimpedance amplifier with a T-network feedback configuration converts an input current into an output voltage. The current-to-voltage gain is based on the T-network equivalent resistance which is larger than any of the resistors used in the circuit. Therefore, the T-network feedback configuration circuit allows for very high gain without the use of large resistors in the feedback or a second gain stage, reducing noise, stability issues, and errors in the system.


## Design Notes

1. $C_{1}$ and $R_{1}$ set the input signal cutoff frequency, $f_{p}$.
2. Capacitor $\mathrm{C}_{1}$ in parallel with $\mathrm{R}_{1}$ helps limit the bandwidth, reduce noise, and also improve the stability of the circuit if high-value resistors are used.
3. The common-mode voltage is the voltage at the non-inverting input and does not vary with input current.
4. A bias voltage can be added to the non-inverting input to bias the output voltage above the minimum output swing for 0 A input current.
5. Using high-value resistors can degrade the phase margin of the circuit and introduce additional noise in the circuit.
6. Avoid placing capacitive loads directly on the output of the amplifier to minimize stability issues.
7. For more information on op amp linear operating region, stability, slew-induced distortion, capacitive load drive, driving ADCs, and bandwidth see the Design References section.

## Design Steps

The transfer function of this circuit follows:

$$
V_{o}=l_{i} \times\left(\frac{R_{2} \times R_{1}}{R_{3}}+R_{1}+R_{2}\right)
$$

1. Calculate the required gain:

$$
\text { Gain }=\frac{V_{\text {oMax }}}{I_{\text {OMax }}}=\frac{3.2 \mathrm{~V}}{100 \mathrm{nA}}=3.2 \times 10^{7} \frac{\mathrm{~V}}{\mathrm{~A}}
$$

2. Choose the resistor values to set the pass-band gain:

$$
\text { Gain }=\left(\frac{R_{2} \times R_{1}}{R_{3}}+R_{1}+R_{2}\right)
$$

Since $R_{1}$ will be the largest resistor value in the system choose this value first then choose $R_{2}$ and calculate $R_{3}$. Select $R_{1}=3.3 \mathrm{M} \Omega$ and $R_{2}=13 \mathrm{k} \Omega$. $R_{1}$ is very large due to the large transimpedance gain of the circuit. $R_{2}$ is in the $\sim 10 \mathrm{k}$ ohm range so the op amp can drive it easily.

$$
R_{3}=\left(\frac{R_{2} \times R_{1}}{G a i n-R_{1}-R_{2}}\right)=\left(\frac{13 \mathrm{k} \Omega \times 3.3 \mathrm{M} \Omega}{3.2 \times 10^{7} \frac{\mathrm{~V}}{\mathrm{~A}}-3.3 \mathrm{M} \Omega-13 \mathrm{k} \Omega}\right)=1.5 \mathrm{k} \Omega
$$

3. Calculate $\mathrm{C}_{1}$ to set the location of $\mathrm{f}_{\mathrm{p}}$.

$$
C_{1}=\frac{1}{2 \pi \times R_{1} \times f_{p}}=\frac{1}{2 \pi \times 3.3 \mathrm{M} \Omega \times 10 \mathrm{kHz}}=4.82 \mathrm{pF} \approx 4.8 \mathrm{pF} \text { (Standard Value) }
$$

4. Run a stability analysis to make sure that the circuit is stable. For more information on how to run a stability analysis see the TI Precision Labs - Op amp: Stability video.

## Design Simulations

DC Simulation Results


## AC Simulation Results



## Design References

1. See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.
2. See SPICE file, SBOMB39.
3. See TIPD176, www.ti.com/tool/tipd176.
4. For more information on many op amp topics including common-mode range, output swing, bandwidth, and how to drive an ADC please visit TI Precision Labs.

## Design Featured Op Amp

| TLV9002 |  |
| :---: | :---: |
| $\mathbf{V}_{\mathbf{c c}}$ | 1.8 V to 5.5 V |
| $\mathbf{V}_{\text {incm }}$ | Rail-to-rail |
| $\mathbf{V}_{\text {out }}$ | Rail-to-rail |
| $\mathbf{V}_{\mathbf{o s}}$ | 0.4 mV |
| $\mathbf{I}_{\mathbf{q}}$ | $60 \mu \mathrm{~A}$ |
| $\mathbf{I}_{\mathbf{b}}$ | 5 pA |
| UGBW | 1 MHz |
| SR | $2 \mathrm{~V} / \mathrm{us}$ |
| \#Channels | $1,2,4$ |
| www.ti.com/product/TLV9002 |  |

## Design Alternate Op Amp

| OPA375 |  |
| :---: | :---: |
| $\mathbf{V}_{\mathbf{c c}}$ | 2.25 V to 5.5 V |
| $\mathbf{V}_{\text {incM }}$ | $\mathrm{V}_{\text {ee }}$ to $\left(\mathrm{V}_{\text {cc }}-1.2 \mathrm{~V}\right)$ |
| $\mathbf{V}_{\text {out }}$ | Rail-to-rail |
| $\mathbf{V}_{\text {os }}$ | 0.15 mV |
| $\mathbf{I}_{\mathbf{q}}$ | $890 \mu \mathrm{~A}$ |
| $\mathbf{I}_{\mathbf{b}}$ | 10 pA |
| UGBW | 10 MHz |
| SR | $4.75 \mathrm{~V} / \mu \mathrm{s}$ |
| \#Channels | 1 |
| www.ti.com/product/OPA375 |  |

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