

# Understanding LDO Performance in the TCAN4550-Q1

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## ABSTRACT

To understand if a low-dropout (LDO) voltage regulator supports the system requirements, several factors have to be considered. Integrated LDOs present opportunities to reduce board space while at the same time presenting challenges for the system design. Package, ambient temperature input and output voltages must be considered when designing the system. In some devices, the LDO also supplies current to internal circuitry that limits the amount available externally. These contribute to the junction temperature of the semiconductor which determines the performance of the LDO. This application note considers the performance of the LDO that is integrated in the TCAN4550-Q1 in relationship to these factors.

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## 1 Introduction

What is a low-dropout (LDO) voltage regulator? In the simplest terms, it is a component that takes a higher input direct current (DC) voltage and reduces this DC voltage to a level that the circuit requires. An example of this would be a 3.3 V regulator that is powered off of a 5 V system. There are many parameters that could be considered when evaluating an LDO. Examples are, but not limited too; input voltage, output voltage and current requirements, both internally and externally. LDOs are offered as a standalone device or integrated into a device that has more functionality. The TCAN4550-Q1 has an integrated 5 V LDO supplying current externally and to the integrated Control Area Network with Flexible Data Rate (CAN FD) transceiver and is the basis for this application note.

## 2 Device Overview

The TCAN4550-Q1 is a CAN FD controller and transceiver system basis chip (SBC) with an integrated 5 V LDO supplying current externally and to the integrated CAN transceiver supporting 12 V battery automotive systems. The LDO provides 5 V  $\pm$  5% output externally and internally. The TCAN4550-Q1 device can source up to 125 mA of current. 70 mA of current is available externally because the CAN transceiver can need up to 50 mA during normal operation provided the design and certain constraints are understood. These factors include package, supply voltage and ambient temperature.

## 3 Device Description

The TCAN4550-Q1 has integrated a CAN FD controller along with a CAN FD transceiver. The device is powered from the battery supply ( $V_{SUP}$ ) and integrates a 5 V LDO to provide 5 V for the CAN FD transceiver. The LDO is capable of supplying 125 mA of current. The LDO also provides 5 V and required current, typically 50 mA, to the integrated CAN transceiver leaving 70 mA is available to the  $V_{CCOUT}$  pin. This type of configuration is typically called a self-power transceiver. The CAN transceiver can consume more current than the typical value provided under heavier loads or bus fault conditions. See the data sheet for the maximum values. This means what is left can be used by an external device.

The supply voltage,  $V_{SUP}$ , and ambient temperature,  $T_A$ , is considered first. As the output voltage,  $V_{CCOUT}$ , is fixed. A change in  $V_{SUP}$  can impact the overall LDO performance and thermal considerations. The equation  $(V_{SUP} - V_{CCOUT}) \times I_{CCOUT}$  is used to arrive at the power consumption of the device. As an example, if  $V_{SUP} = 28$  V,  $V_{CCOUT} = 5$  V and  $I_{CCOUT} = 125$  mA, then the power consumption of the device is 2.88 W. This is realized as heat which impacts the junction temperature,  $T_J$ , of the silicon. This power number is part of the evaluation to determine the impact to overall performance. Temperature is the next consideration as higher the ambient temperature means higher junction temperature. The theoretical junction temperature can be calculated by taking the calculated power and multiplying it with the package thermal resistance and adding the ambient temperature. Selecting the correct thermal resistance is application dependant. Factors to be considered are air flow, board, enclosure and system level thermal designs, see [Semiconductor and IC Package Thermal Metrics](#) for a more detailed description. For typical TCAN4550-Q1 applications,  $R_{\theta JA}$  is the parameter of focus. In the example above, the junction temperature is calculated using  $R_{\theta JA} = 35.25^\circ\text{C/W}$ .  $R_{\theta JA}$  is the thermal resistance between the package and the ambient air surrounding the package, measured in change in degrees celsius per watt of power dissipation. For the TCAN4550-Q1 package the  $R_{\theta JA}$  value is  $35.2^\circ\text{C/W}$  which allows supporting higher currents with higher  $V_{SUP}$  or  $T_A$ .

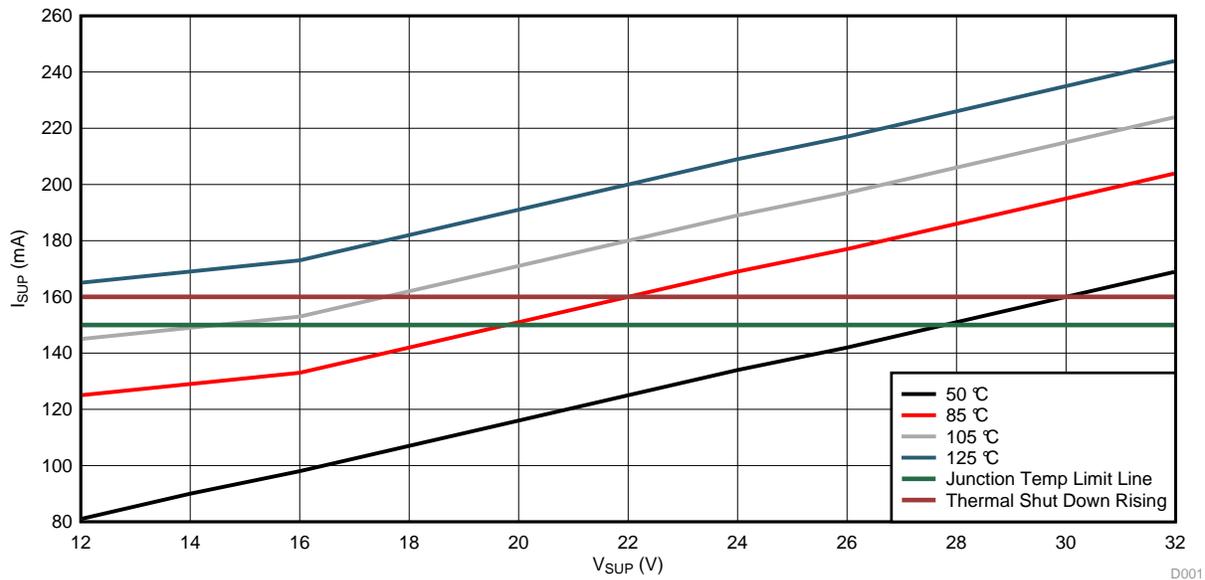
$$(P \times R_{\theta JA}) + T_A = T_J \rightarrow (2.88 \text{ W} \times 35.2^\circ\text{C/W}) + 85^\circ\text{C} = 186.4^\circ\text{C} \quad (1)$$

This is above the maximum junction temperature of  $150^\circ\text{C}$  and results in a thermal shut down event as the  $T_J$  is above  $160^\circ\text{C}$ . Another thermal resistance parameter to consider is  $R_{\theta JB}$  which is the thermal resistance between the silicon junction and the board. Using  $R_{\theta JB} = 12.8^\circ\text{C/W}$  provides a junction temperature of  $121.9^\circ\text{C}$  as an example of how proper thermal considerations can improve the performance of the LDO by using an optimized thermal design for the system.  $R_{\theta JA}$  and  $R_{\theta JB}$  are package and board design dependent and shown here for a high-k board. If best thermal practices are followed with airflow and heat sinks for the board; using  $R_{\theta JB}$  provides higher performance but is beyond the scope of this application note. Packages, such as the RGY used by the TCAN4550-Q1, with thermal pads tend to have better  $R_{\theta JB}$  performance than packages without.

When considering packages, the thermal characteristics are important to consider. Considering the list of thermal information in a data sheet one can see up to four thermal resistance parameters. These are important to understand as they contribute to the equation used to determine the silicon junction temperature which predicts when the device may reach the thermal shut down limit. For the TCAN4550-Q1 devices, the thermal resistance  $R_{\theta JA}$  is considered. In automotive applications, the expectations is that the ambient temperature saturates the system; thus the  $R_{\theta JA}$  is used to understand how the device performs.

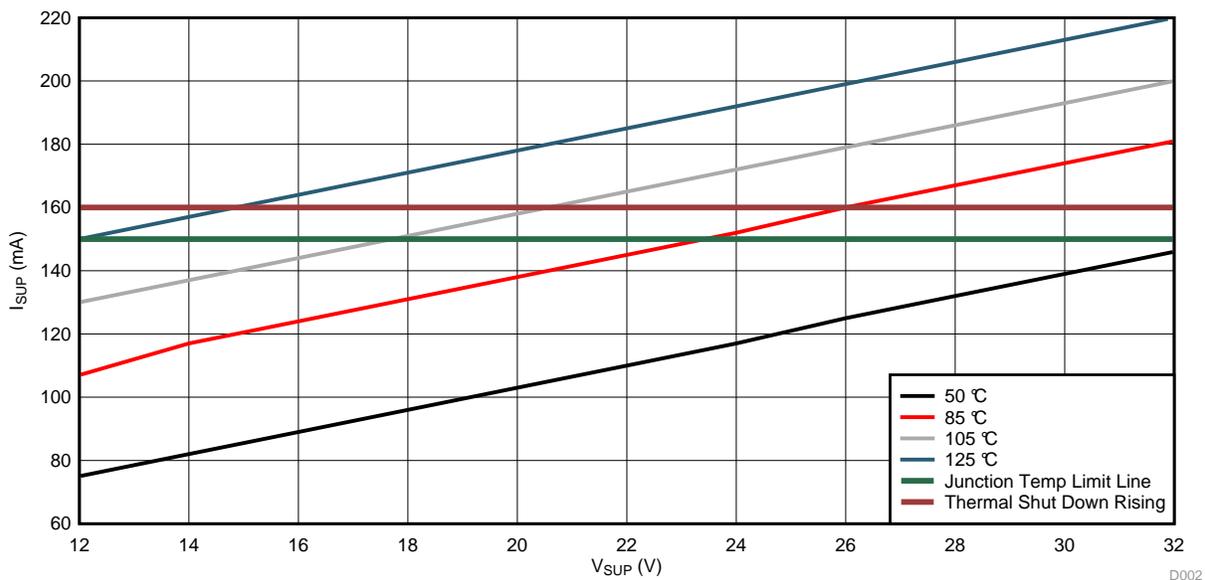
The TCAN4550-Q1 is designed with a maximum junction temperature of  $150^\circ\text{C}$  and has a built in thermal shut down feature at  $160^\circ\text{C}$ . The junction temperature is the temperature the CMOS transistor junction should not exceed to meet long term reliability. The thermal shut down feature exists to protect the device in case an external fault causes the junction temperature to rise enough to damage the device. The three following charts show the theoretical junction temperature based upon  $V_{SUP}$ , ambient temperature and amount of current being sourced externally and internally. The graphs have two lines that represent the

maximum junction temperature, dark green, and the rising temperature thermal shut down point, dark red. When the device is consistently operating in the temperature region between the maximum  $T_J$  and thermal shut down the life of the device may shorten. The application design should keep the junction temperature below the green line, maximum  $T_J$ . Figure 1 to Figure 2 show the theoretical performance with the 5 V output based upon a 125 mA and 100 mA external and internal load.



$V_{CC} = 5\text{ V}$  at 125 mA Load

**Figure 1. Junction Temperature vs Ambient Temperature**



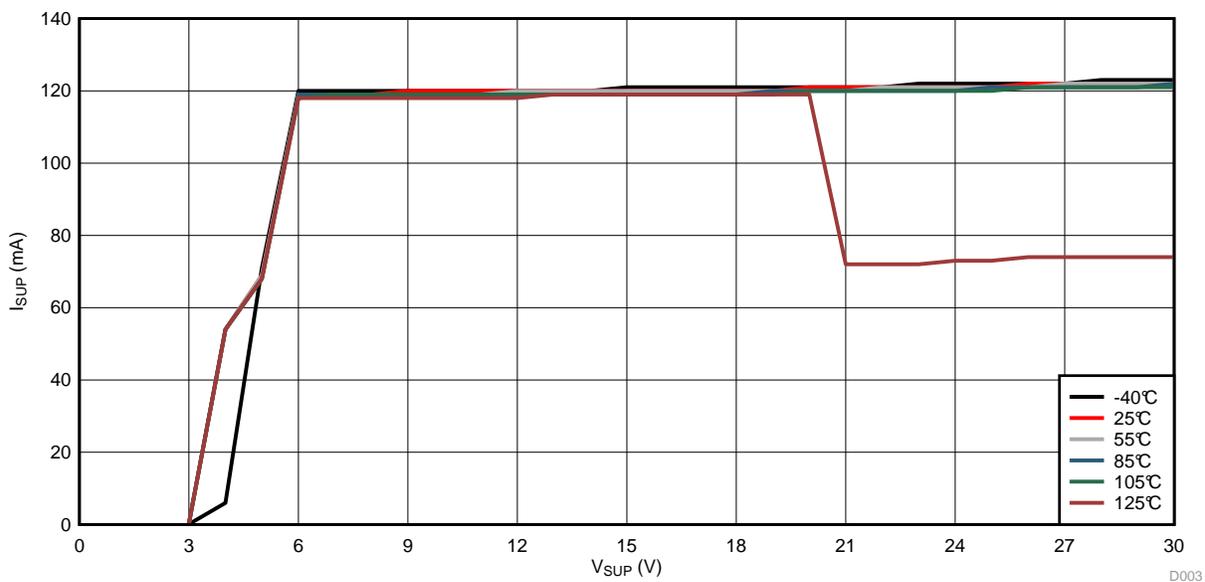
$V_{CC} = 5\text{ V}$  at 100 mA Load

**Figure 2. Junction Temperature vs  $V_{SUP}$  vs Ambient Temperature**

The actual performance of the LDO aligns with the expected theoretical values when using the lab evaluation module and thermal stream that heats or cools the air around the device. [Figure 3](#) and [Figure 4](#) provide the data based upon 70 mA load at 5 V with CAN bus held dominant with a 60 Ω and 50 Ω load. [Figure 5](#) and [Figure 6](#) shows the  $V_{CCOUT}$  value under these same conditions.

[Figure 3](#) shows the behavior of the 5 V LDO in relationship to  $I_{SUP}$ ,  $V_{SUP}$ , LDO load of 70 mA, CAN bus dominant, CAN bus load of 60 Ω and ambient temperature. The  $I_{SUP}$  current is based upon a 70 mA load on  $V_{CCOUT}$  and the CAN bus held dominant which together comes out to about 120 mA. As can be seen, an ambient temperature of 125°C can cause a thermal shut down event when  $V_{SUP}$  reaches 20 V and  $V_{CCOUT}$  is providing 70 mA to a load. The load on the CAN bus is 60 Ω. When the CAN bus load is 50 Ω a  $V_{SUP}$  of 19 V can trigger the same decrease.

The reason the curve shows  $I_{SUP}$  dropping off is due to the internal junction temperature  $T_j$  exceeding the thermal shut down temperature. At this point, the LDO and CAN transceiver are turned off. Even though the figure shows the current leveling off to approximately 74.5 mA; in reality it drops to the μA area. This is happening in milliseconds and cools down prior the  $t_{UV/TSD}$  timer expiring, which would put the device into sleep mode. As the junction temperature drops below thermal shut down point of 150°C the device enters standby mode. As the 70 mA load was still connected,  $I_{SUP}$  shows this current plus the normal standby current which is approximately 4.5 mA. As this is happening quickly, the figures do not show the drop to microamps but shows  $I_{SUP}$  leveling out to 74.5 mA. If the TSD event is prolonged, the current drops to microamps and  $V_{CCOUT}$  drops to 0 V once the decoupling capacitor discharges. When there is 50 Ω bus load this can also happen at 105°C when  $V_{SUP}$  is at 29 V as seen in [Figure 4](#)

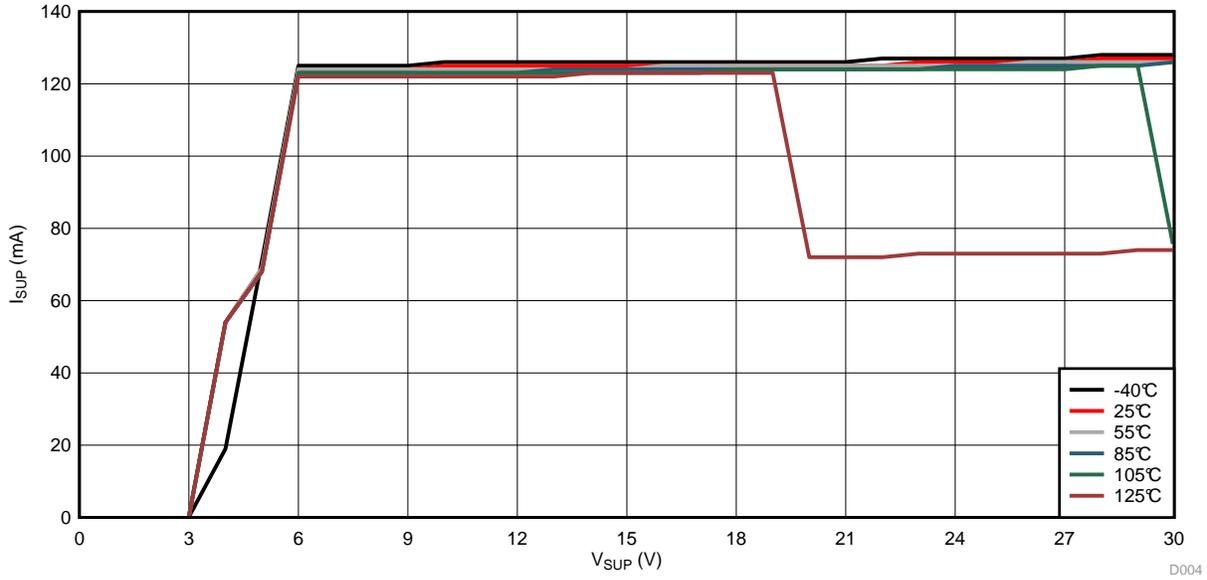


$V_{CCOUT} = 5\text{ V}$   
 $V_{IO} = 5\text{ V}$

$I_{CCOUT} = 70\text{ mA}$

CANH and CANL Load = 60 Ω

**Figure 3.  $I_{SUP}$  Current vs  $V_{SUP}$  vs Ambient Temperature with 60 Ω Load**

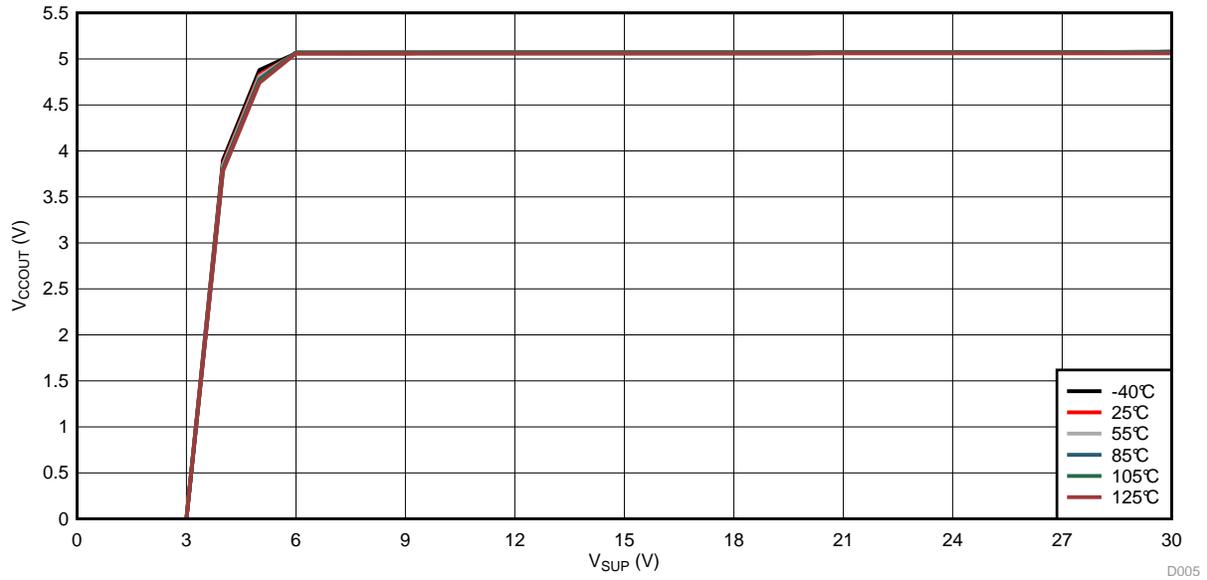


V<sub>CC</sub> = 5 V  
V<sub>IO</sub> = 5 V

I<sub>CCOUT</sub> = 70 mA

CANH and CANL Load = 50 Ω

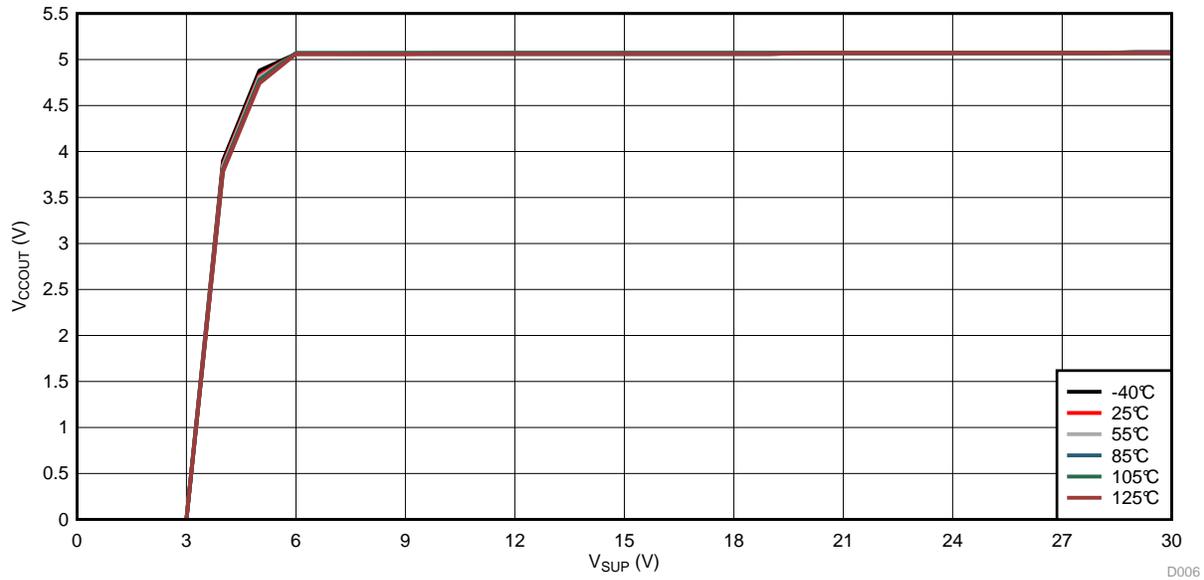
Figure 4. I<sub>SUP</sub> Current vs V<sub>SUP</sub> vs Ambient Temperature with 50 Ω Load



I<sub>VCCOUT</sub> Load = 70 mA

CANH and CANL Load = 60 Ω

Figure 5. LDO Output Voltage vs V<sub>SUP</sub> vs Ambient Temperature


 $I_{SUP}$  Load = 70 mA

 CANH and CANL Load = 50  $\Omega$ 
**Figure 6. LDO Output Voltage vs  $V_{SUP}$  vs Ambient Temperature**

#### 4 Summary

The LDO in the TCAN4550-Q1 can supply 5 V at 125 mA. As the LDO supplies the CAN transceiver, not all of the 125 mA can be utilized by an external load. When considering LDO sourcing requirements, expected system behavior needs to be considered when a CAN bus fault takes place, requiring more current to the CAN transceiver. If the expected behavior is no interruption to the load, then supporting a reduced  $I_{CCOUT}$  load is warranted. A reasonable trade off would be a 50 mA load on  $V_{CCOUT}$  with normal CAN bus operating conditions. For the best performance, special care must be taken to design a board and system that meets the thermal needs. For devices that have thermal pads, the thermal pad must be soldered to a good solid ground plan. Based upon the data, [Table 1](#) provides typical performance for specific data points.

**Table 1. TCAN4550-Q1 Performance**

Device	$V_{CCOUT}$ (V)	$I_{CCOUT}$ (mA)	$V_{SUP}$ (V)	$T_A$ ( $^{\circ}$ C)
TCAN4550-Q1	5	70	14	105

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