

How to Sample the Small APD Current Precisely With the TPS61390 Boost Converter

Helen Chen

ABSTRACT

In the optical receivers and modules application, even a 5-µA APD current needs to be detected precisely. The TPS61390 and TPS61391 devices are high voltage boost converters for biasing the APD. They can accurately mirror the APD current. This application report presents guidance on how to select the resistors from the MON1, MON2 to GND so that the APD current can be precisely detected.

| | Contents | |
|---|------------------------------|---|
| 1 | Introduction | 1 |
| 2 | Device Calculation | |
| 3 | Typical Application | 3 |
| 4 | Summary | 4 |
| 5 | References | |
| | List of Figures | |
| 1 | TPS61390 Typical Application | 2 |
| | List of Tables | |
| 1 | Design Requirement | 3 |

Trademarks

All trademarks are the property of their respective owners.

1 Introduction

The TPS61390 device is a fully-integrated boost converter with an 85-V FET to convert a low-input voltage to a higher voltage for biasing the APD. The device can accurately mirror the APD current ranging from 0.5 μ A to 2 mA. There are two ratio options for the current proportional to APD current: the MON1 (4:5) and MON2 (1:5). By connecting a resistor from the mirror output (MON1 or MON2) to GND, the current flowing through the APD is converted into the voltage crossing the resistor from MON1, MON2 to GND.

This application note provides the MON1 and MON2 voltage calculation formula, then shows how to select the resistors from the MON1, MON2 to GND based on a continuous optical current application.

1



www.ti.com

Device Calculation

2 **Device Calculation**

Figure 1 shows the TPS61390 typical application circuit. There are two current mirror options for TPS61390: the gain of 4:5 (MON1) and 1:5 (MON2). The maximum voltage of MON1 and MON2 is 2.5 V.

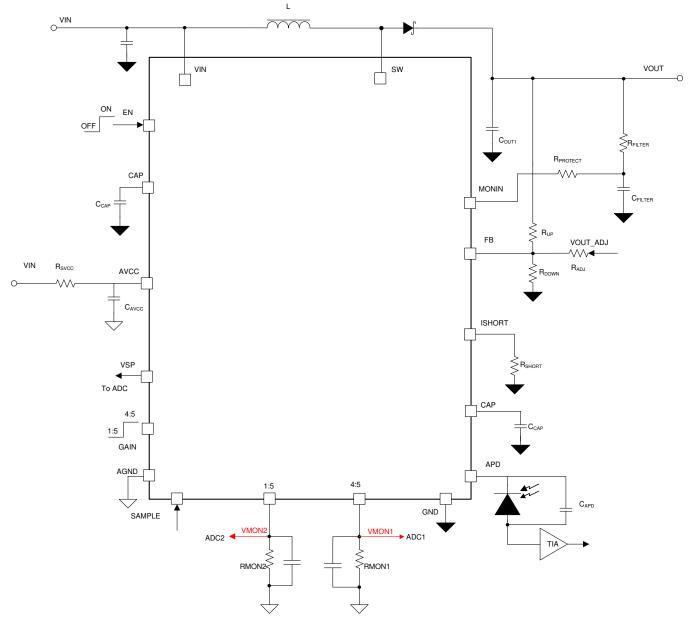


Figure 1. TPS61390 Typical Application

The voltage measured on the MON1 pin can be calculated with Equation 1. VMON1 = 0. 8 × I _{APD} × RMON1 + I _{BIAS} × RMON1

The voltage measured on the MON2 pin can be calculated by Equation 2. $VMON2 = 0.2 \times I_{APD} \times RMON2 + I_{BIAS} \times RMON2$

where:

- VMON1 is the voltage sampled on the MON1 pin
- VMON2 is the voltage sampled on the MON2 pin
- I_{APD} is the current flowing through the APD pin
- RMON1 is the resistor connecting with MON1 pin
- How to Sample the Small APD Current Precisely With the TPS61390 Boost Converter

(1)

2



www.ti.com

- RMON2 is the resistor connecting with MON2 pin
- I_{BIAS} is the bias current of current mirror

(2)

The bias current is around 20 μ A (typical) when there is no APD current flowing through. The bias voltage of MON1 or MON2 is 60 mV given a 3-k Ω MON resistor connected with MON1 or MON2, or 100 mV given a 4.99-k Ω MON resistor connected with MON1 or MON2.

3 Typical Application

3.1 Design Requirement

Table 1 shows the design requirement of this application report.

Table 1. Design Requirement

| Parameter | Value |
|---------------------|-------------|
| Input voltage range | 2.7 V–5.5 V |
| Output voltage | 48 V |
| Operating frequency | 700 kHz |
| APD current | 0 to 2 mA |

3.2 Design Procedure

The MCU will sample the MON1 pin voltage (VMON1) and the MON2 pin voltage (VMON2). When the APD current is low, VMON1 will be sampled, when the APD current gets higher and VMON1 reaches the full detection scale, VMON2 will be sampled.

The maximum voltage of MON1 and MON2 is clamped at 2.5 V. The lowest level of this clamping voltage is 2.3 V, considering lot-to-lot difference. So to leave some margin, the full scale voltage is set at 2.1 V in this application report.

The value of RMON1 and RMON2 can be deduced from Equation 1 and Equation 2.

$$RMON1 = \frac{VMON1}{0.8 \times I_{APD} + I_{BIAS}} = \frac{V_{FULL}}{0.8 \times I_{APD} + I_{BIAS}}$$
(3)
$$RMON2 = \frac{VMON2}{0.2 \times I_{APD} + I_{BIAS}} = \frac{V_{FULL}}{0.2 \times I_{APD} + I_{BIAS}}$$
(4)

If setting the target full scale maximum sampling current through the MON1 pin at 500 μ A, set the target full scale maximum sampling current through the MON2 pin at 2 mA, then the resistance of RMON1 and RMON2 can be calculated out with Equation 5:

$$\mathsf{RMON1} = \frac{2.1 \text{ V}}{0.8 \times 500 \text{ }\mu\text{A} + 20 \text{ }\mu\text{A}} = 5 \quad \mathbf{k}\Omega \tag{5}$$

So RMON1 = RMON2 = $4.99 \text{ k}\Omega$ can be chosen in this application report.

$$\mathsf{RMON2} = \frac{2.1 \text{ V}}{0.2 \times 2 \text{ mA} + 20 \ \mu \text{A}} = 5 \quad \mathbf{k}\Omega \tag{6}$$

From the previous equations, it is known that when the resistance of RMON1 and RMON2 is the same, then the full scale detection voltage is the same. Then as a result, the maximum sampling current through the MON2 pin is 4 times that of through the MON1 pin.

The resistance of RMON1 and RMON2 can also be set at different values based on the real application. For example, if the resistance of RMON2 is one fourth of RMON1, then under the same energy, the voltage across RMON1 is 16 times of the voltage across RMON2, which is a 12 dB difference.

If the target maximum detection current is very small, much less than 1 mA, then RMON1 and RMON2 can choose a $10-k\Omega$ resistance to achieve higher detection precision.

3



Summary

4 Summary

This application report describes how to sample the APD current precisely by choosing a right resistor at the MON1 pin and the MON2 pin. When the resistance of RMON1 and RMON2 is equal, the maximum sampling current through the MON2 pin is 4 times that of through the MON1 pin. The resistance of RMON1 and RMON2 can also be set at different values based on the real application.

5 References

- 1. Texas Instruments, *TPS61390 85-V*_{OUT} Boost Converter With Current Mirror and Sample / Hold Data Sheet
- 2. Texas Instruments, TPS61391 85-V_{out} Boost Converter with Current Mirror Integrated Data Sheet

IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to TI's Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2022, Texas Instruments Incorporated