Ordering \&
Technical quality documentation

## ADS1285 32-Bit, Delta-Sigma ADC for Seismic Applications

## 1 Features

- Selectable resolution-power modes:
- Dynamic range: 134 dB at $2 \mathrm{~ms}, 11.5 \mathrm{~mW}$
- Dynamic range: 129 dB at $2 \mathrm{~ms}, 4.8 \mathrm{~mW}$
- Flexible digital filter:
- Selectable sinc + FIR + IIR
- Linear or minimum phase
- High-pass filter
- THD: <-120 dB
- CMRR: 125 dB
- Data rates: 125 SPS to 4000 SPS
- Programmable gains: 1 to 64
- PGA bypass option
- SYNC input
- Clock error compensation
- Two-channel multiplexer
- Offset and gain calibration
- General-purpose digital I/Os
- Analog supply operation: $5 \mathrm{~V}, 3.3 \mathrm{~V}$, or $\pm 2.5 \mathrm{~V}$
- Reference voltage options: $5 \mathrm{~V}, 4.096 \mathrm{~V}$, or 2.5 V


## 2 Applications

- Energy exploration
- Passive seismic monitoring
- Earth sciences and geology
- Precision instrumentation


## 3 Description

The ADS1285 is a 32-bit, low-power, analog-to-digital converter (ADC), with a programmable gain amplifier (PGA) and a finite impulse response (FIR) filter. The ADC is designed for the demanding needs of seismology equipment requiring low-noise precision digitization and extended battery run time.

The low-noise PGA allows direct connection of geophones and transformer-coupled hydrophones without the need of an external amplifier.

The ADC incorporates a high-resolution, delta-sigma ( $\Delta \Sigma$ ) modulator and a FIR filter with programmable phase response. The high-pass filter removes dc and low-frequency content from the signal. Clock frequency error is compensated by the sample rate converter with 7-ppb resolution.

Choice of power modes optimize dynamic range verses power consumption. Power consumption is further reduced by PGA bypass operation.

The ADC is available in a compact $5-\mathrm{mm} \times 5-\mathrm{mm}$ VQFN package and is fully specified over the $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ambient temperature range.

Package Information ${ }^{(1)}$

| PART NUMBER | PACKAGE | BODY SIZE (NOM) |
| :--- | :---: | :---: |
| ADS1285 | RHB (VQFN, 32) | $5.00 \mathrm{~mm} \times 5.00 \mathrm{~mm}$ |

(1) For all available packages, see the package option addendum at the end of the data sheet.


## Table of Contents

1 Features............................................................................. 1 .....  1
2 Applications ..... 1
3 Description .....
4 Revision History ..... 2
5 Pin Configuration and Functions .....  3
6 Specifications ..... 4
6.1 Absolute Maximum Ratings ..... 4
6.2 ESD Ratings ..... 4
6.3 Recommended Operating Conditions ..... 4
6.4 Thermal Information ..... 5
6.5 Electrical Characteristics ..... 6
6.6 Timing Requirements: $1.65 \mathrm{~V} \leq \mathrm{IOVDD} \leq 1.95 \mathrm{~V}$ and $2.7 \mathrm{~V} \leq \mathrm{IOVDD} \leq 3.6 \mathrm{~V}$ ..... 10
6.7 Switching Characteristics: $1.65 \mathrm{~V} \leq$ IOVDD $\leq$ 1.95 V and $2.7 \mathrm{~V} \leq \mathrm{IOVDD} \leq 3.6 \mathrm{~V}$. ..... 10
6.8 Timing Diagrams ..... 11
6.9 Typical Characteristics ..... 13
7 Parameter Measurement Information ..... 23
7.1 Noise Performance. ..... 23
8.1 Overview
8.1 Overview ..... 25 ..... 25
8.2 Functional Block Diagram ..... 26
8.3 Feature Description ..... 27
8.4 Device Functional Modes ..... 40
8.5 Programming ..... 44
8.6 Register Map ..... 49
9 Application and Implementation. ..... 54
9.1 Application Information ..... 54
9.2 Typical Application ..... 54
9.3 Power Supply Recommendations ..... 56
9.4 Layout ..... 57
10 Device and Documentation Support ..... 58
10.1 Receiving Notification of Documentation Updates ..... 58
10.2 Support Resources ..... 58
10.3 Trademarks ..... 58
10.4 Electrostatic Discharge Caution ..... 58
10.5 Glossary ..... 58
11 Mechanical, Packaging, and Orderable Information ..... 58
8 Detailed Description ..... 25

## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.
Changes from Revision * (May 2022) to Revision A (December 2022) ..... Page

- First public release, changed document status from Advance Information to Production Data ..... 1


## 5 Pin Configuration and Functions



Figure 5-1. RHB Package, 32 -Pin, $5-\mathrm{mm} \times 5$-mm VQFN (Top View)
Table 5-1. Pin Functions

| PIN |  | FUNCTION | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| NO. | NAME |  |  |
| 1 | AIN1P | Analog input | Channel 1 positive input |
| 2 | AlN1N | Analog input | Channel 1 negative input |
| 3 | AIN2P | Analog input | Channel 2 positive input |
| 4 | AIN2N | Analog input | Channel 2 negative input |
| 5 | CAPP | Analog internal | PGA positive capacitor. Connect a 10-nF C0G capacitor across CAPP and CAPN. |
| 6 | CAPN | Analog internal | PGA negative capacitor. Connect a 10-nF COG capacitor across CAPP and CAPN. |
| 7 | CAPBP | Analog internal | Buffer positive capacitor. Connect a 47-nF COG capacitor to AVSS. |
| 8 | CAPBN | Analog internal | Buffer negative capacitor. Connect a 47-nF C0G capacitor to AVSS. |
| 9 | CAPC | Analog internal | Charge-pump capacitor. Connect a 4.7-nF, minimum 10-V rated capacitor to AGND. |
| 10 | AVSS | Analog supply | PGA negative analog supply. See the Analog Power Supplies section for details. |
| 11 | AVDD1 | Analog supply | PGA positive analog supply. See the Analog Power Supplies section for details. |
| 12 | AVDD2 | Analog supply | Modulator analog supply. See the Analog Power Supplies section for details. |
| 13 | AGND | Analog ground | Analog ground |
| 14 | CAPI | Analog internal | Input bias capacitor. Connect a 100-nF ceramic capacitor to AGND. |
| 15 | GPIO0 | Digital I/O | General-purpose I/O |
| 16 | GPIO1 | Digital I/O | General-purpose I/O |
| 17 | CAPD | Analog output | Digital low-dropout regulator (LDO) output. Connect a 220-nF ceramic capacitor to DGND. |
| 18 | DGND | Ground | Digital ground |
| 19 | IOVDD | Digital supply | Digital I/O power supply. See the IOVDD Power Supply section for details. |
| 20 | CLK | Digital input | ADC clock input |
| 21 | $\overline{\text { CS }}$ | Digital input | Serial interface select, active low |
| 22 | SCLK | Digital input | Serial interface clock |
| 23 | DIN | Digital input | Serial interface data in |
| 24 | DOUT | Digital output | Serial interface data out |
| 25 | DRDY | Digital output | Data ready, active low |
| 26 | SYNC | Digital input | ADC synchronization, active high |
| 27 | RESET | Digital input | ADC reset, active low |
| 28 | PWDN | Digital input | ADC power down, active low |
| 29 | REFN | Analog input | Negative reference input. See the Voltage Reference Input section for details. |
| 30 | REFP | Analog input | Positive reference input. See the Voltage Reference Input section for details. |
| 31 | CAPR | Analog internal | Reference bias capacitor. Connect a $100-\mathrm{nF}$ ceramic capacitor to AVSS. |
| 32 | AVSS | Analog supply | PGA negative supply |
| Thermal pad |  |  | Connect the thermal pad to AVSS. Thermal vias placed in the printed circuit board (PCB) land are optional for placement of bottom side components. |

ADS1285

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) ${ }^{(1)}$

|  |  | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| Power supply voltages | AVDD1 to AVSS | -0.3 | 5.5 | V |
|  | AVSS to AGND | -2.8 | 0.3 |  |
|  | AVDD2 to AGND | -0.3 | 5.5 |  |
|  | AVDD2 to AVSS | -0.3 | 5.5 |  |
|  | IOVDD to DGND | -0.3 | 3.9 |  |
|  | IOVDD to DGND (IOVDD connected to CAPD) | -0.3 | 2.2 |  |
| Grounds | AGND to DGND | -0.3 | 0.3 | V |
| Analog input voltage | AIN1P, AIN1N, AIN2P, AIN2N, REFP, REFN | AVSS - 0.3 | AVDD1 + 0.3 | V |
| Digital input voltage | CLK, DIN, SCLK, $\overline{C S}$, GPIO0, GPIO1, SYNC, RESET, PWDN | DGND - 0.3 | IOVDD + 0.3 | V |
| Input current | Continuous, any digital or analog pin ${ }^{(2)}$ | -10 | 10 | mA |
|  | Junction, $\mathrm{T}_{J}$ |  | 150 | ${ }^{\circ} \mathrm{C}$ |
|  | Storage, $\mathrm{T}_{\text {stg }}$ | -60 | 150 | ${ }^{\circ} \mathrm{C}$ |

(1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If briefly operating outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not sustain damage, but it may not be fully functional - this may affect device reliability, functionality, performance, and shorten the device lifetime.
(2) Analog input pins AIN1P, AIN1N, AIN2P, AIN2N, REFP and REFN are diode-clamped to AVDD1 and AVSS. Limit the input current to 10 mA in the event the analog input voltage exceeds AVDD1 +0.3 V or $\mathrm{AVSS}-0.3 \mathrm{~V}$. Digital input pins are clamped to IOVDD and DGND. Limit the input current if the digital input voltage exceeds IOVDD +0.3 V or DGND -0.3 V .

### 6.2 ESD Ratings

| $\mathrm{V}_{(\text {(ESD })}$ |  | Electrostatic discharge | Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001(1) | VALUE |
| :--- | :--- | :--- | :---: | :---: |
| UNIT |  |  |  |  |
|  |  | Charged-device model (CDM), per JEDEC JESD22-C101 ${ }^{(2)}$ | 2000 | V |

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating ambient temperature range (unless otherwise noted)


### 6.3 Recommended Operating Conditions (continued)

over operating ambient temperature range (unless otherwise noted)

|  |  |  | MIN | NOM | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Calibration range ${ }^{(1)}$ |  |  |  | 6\% | FSR |
| VOLTA | REFERENCE INPUT |  |  |  |  |  |
| $V_{\text {REFN }}$ | Negative reference input |  | AVSS - 0.05 |  |  | V |
| $V_{\text {REFP }}$ | Positive reference input |  |  |  | AVDD1 + 0.1 | V |
|  |  | Reference voltage $=5 \mathrm{~V}$ | 4.9 | 5 | AVDD1 - AVSS + 0.1 | V |
| $V_{\text {REF }}$ | $\mathrm{V}_{\text {REF }}=\mathrm{V}_{\text {REFP }}-\mathrm{V}_{\text {REFN }}$ | Reference voltage $=4.096 \mathrm{~V}$ | 4.0 | 4.096 | 4.2 | V |
|  |  | Reference voltage $=2.5 \mathrm{~V}$ | 2.4 | 2.5 | 2.6 | V |
| DIGITA | PUTS |  |  |  |  |  |
| $\mathrm{V}_{\text {INL }}$ | Low-level input voltage |  |  |  | $0.2 \times$ IOVDD | V |
| $\mathrm{V}_{\text {INH }}$ | High-level input voltage |  | $0.8 \times$ IOVDD |  |  | V |
|  |  | High-power mode | 6 | 8.192 | 8.3 |  |
| $\mathrm{f}_{\text {CLK }}$ | Clock input frequency | Mid-power mode | 6 | 8.192 | 8.3 | MHz |
|  |  | Low-power mode | 3 | 4.096 | 4.15 |  |
| TEMPE | TURE |  |  |  |  |  |
|  |  | Operational | -50 |  | 85 |  |
| A | Ambient temperature | Specification | -40 |  | 85 | C |

(1) Calibration range is the sum of the offset and gain error correction.

### 6.4 Thermal Information

| THERMAL METRIC ${ }^{(1)}$ |  | ADS1285 | UNIT |
| :---: | :---: | :---: | :---: |
|  |  | RHB (VQFN) |  |
|  |  | 32 PINS |  |
| $\mathrm{R}_{\text {өJA }}$ | Junction-to-ambient thermal resistance | 30 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {өJC(top) }}$ | Junction-to-case (top) thermal resistance | 19.4 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {өJB }}$ | Junction-to-board thermal resistance | 10.9 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\psi_{\text {JT }}$ | Junction-to-top characterization parameter | 0.2 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\psi_{\mathrm{JB}}$ | Junction-to-board characterization parameter | 10.8 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {өJC(bot) }}$ | Junction-to-case (bottom) thermal resistance | 1.8 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

### 6.5 Electrical Characteristics

minimum and maximum specifications over $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; typical specifications are at $25^{\circ} \mathrm{C}$; all specifications are at
AVDD1 $=5 \mathrm{~V}$, $\operatorname{AVDD2}=2.5 \mathrm{~V}$ to 5 V , $\mathrm{AVSS}=0 \mathrm{~V}$, $\operatorname{IOVDD}=1.8 \mathrm{~V}, \mathrm{~V}_{\mathrm{REFP}}=4.096 \mathrm{~V}, \mathrm{~V}_{\mathrm{REFN}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{PGA}$ gain $=1$, $\mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}$ (4.096 MHz low-power mode) and $\mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


## DC PERFORMANCE

| $e_{n}$ | Noise |  |  | See Noise Performance section for details |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OS }}$ | Offset error | PGA operation |  | $\begin{array}{r} -350 / \text { gain }-10 \\ -600 \end{array}$ | $\begin{array}{r}  \pm 30 / \text { gain }+5 \\ \pm 50 \end{array}$ | 350/gain + 10 | $\mu \mathrm{V}$ |
|  |  | Buffer operation |  |  |  | 600 |  |
|  |  | After calibration |  | $\pm 1$ |  |  |  |
|  | Offset error drift | PGA operation |  | 0.5/gain |  |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  |  | Buffer operation |  | 1 |  |  |  |
|  | Gain error | PGA operation, gain = 1 |  | -0.05\% | $\pm 0.02 \%$ | 0.05\% |  |
|  |  | After calibration |  | 2 |  |  | ppm |
|  |  | Buffer operation |  | -0.07\% | $\pm 0.05 \%$ | 0.07\% |  |
|  | Gain match | Relative to PGA gain = 1 |  | -0.2\% | $\pm 0.06 \%$ | 0.2\% |  |
|  | Gain drift | All PGA gains |  | 2 |  |  | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| CMRR | Common-mode rejection ratio | $\mathrm{f}=60 \mathrm{~Hz}$ |  | 104 | 120 |  | dB |
| PSRR | Power-supply rejection ratio | $\begin{array}{\|l\|} \hline \text { AVDD2 } \\ \hline \text { AVSS, AVDD1 } \end{array}$ | At dc | 80 | 95 |  | dB |
|  |  |  |  | 85 | 110 |  | dB |
|  |  | IOVDD |  | 100 | 120 |  | dB |

ADS1285
www.ti.com

### 6.5 Electrical Characteristics (continued)

minimum and maximum specifications over $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; typical specifications are at $25^{\circ} \mathrm{C}$; all specifications are at AVDD1 $=5 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}$ to 5 V , AVSS $=0 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{~V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\mathrm{REFN}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}$, PGA gain $=1$,
$\mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}$ (4.096 MHz low-power mode) and $\mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)

|  | PARAMETER | TEST CONDITIONS |  | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC PERFORMANCE |  |  |  |  |  |  |
| en-MOD | Modulator voltage noise density | $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$ |  | 25 |  | $\mathrm{n} V / \sqrt{\mathrm{Hz}}$ |
| THD | Total harmonic distortion | $\begin{aligned} & \text { High-power mode, } \\ & \mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}, \\ & \text { AVDD1 }=3.3 \mathrm{~V}, \\ & \text { AVSS }=0 \mathrm{~V}, \\ & \mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \\ & \mathrm{~V}_{\text {IN }}=-0.5 \mathrm{dBFS} \end{aligned}$ | Buffer operation | -123 | -114 | dB |
|  |  |  | PGA gain = 2 | -119 |  |  |
|  |  |  | PGA gain $=4$ | -125 | -116 |  |
|  |  |  | PGA gain $=8$ | -124 |  |  |
|  |  |  | PGA gain $=16$ | -123 | -116 |  |
|  |  |  | PGA gain = 32 and 64 | -125 |  |  |
|  |  | Mid-power mode, $V_{\text {REF }}=2.5 \mathrm{~V}$, AVDD1 $=3.3 \mathrm{~V}$, AVSS $=0 \mathrm{~V}$, $\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}$, $\mathrm{V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$ | Buffer operation | -122 | -113 | dB |
|  |  |  | PGA gain = 2 | -120 |  |  |
|  |  |  | PGA gain $=4$ | -125 | -118 |  |
|  |  |  | PGA gain $=8$ | -124 |  |  |
|  |  |  | PGA gain $=16$ | -123 | -115 |  |
|  |  |  | PGA gain = 32 and 64 | -125 |  |  |
|  |  | $\begin{aligned} & \text { Low-power mode, } \\ & \mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}, \\ & \text { AVDD1 }=3.3 \mathrm{~V}, \\ & \text { AVSS }=0 \mathrm{~V}, \\ & \mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \\ & \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS} \end{aligned}$ | Buffer operation | -124 | -117 | dB |
|  |  |  | PGA gain = 2 | -122 |  |  |
|  |  |  | PGA gain $=4$ | -124 | -116 |  |
|  |  |  | PGA gain $=8$ | -125 |  |  |
|  |  |  | PGA gain $=16$ | -123 | -115 |  |
|  |  |  | PGA gain = 32 and 64 | -124 |  |  |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}, \\ & \text { AVDD1 }=5 \mathrm{~V}, \\ & \text { AVSS }=0 \mathrm{~V}, \\ & \mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \\ & \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS} \end{aligned}$ | Buffer operation | -119 | -114 | dB |
|  |  |  | PGA gain = 1 | -119 | -111 |  |
|  |  |  | PGA gain $=2$ | -125 |  |  |
|  |  |  | PGA gain $=4$ | -122 | -114 |  |
|  |  |  | PGA gain $=8$ | -118 |  |  |
|  |  |  | PGA gain $=16$ | -117 | -111 |  |
|  |  |  | PGA gain = 32 and 64 | -125 |  |  |
|  |  | Mid-power mode, $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$, AVDD1 $=5 \mathrm{~V}$, AVSS $=0 \mathrm{~V}$, <br> $\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}$, <br> $\mathrm{V}_{\text {IN }}=-0.5 \mathrm{dBFS}$ | Buffer operation | -119 | -112 | dB |
|  |  |  | PGA gain = 1 | -119 | -111 |  |
|  |  |  | PGA gain $=2$ | -125 |  |  |
|  |  |  | PGA gain $=4$ | -124 | -115 |  |
|  |  |  | PGA gain $=8$ | -119 |  |  |
|  |  |  | PGA gain $=16$ | -117 | -111 |  |
|  |  |  | PGA gain = 32 and 64 | -124 |  |  |
|  |  | Low-power mode, <br> $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$, <br> AVDD1 $=5 \mathrm{~V}$, <br> AVSS $=0 \mathrm{~V}$, <br> $\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}$, <br> $\mathrm{V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$ | Buffer operation | -123 | -117 | dB |
|  |  |  | PGA gain = 1 | -121 | -115 |  |
|  |  |  | PGA gain = 2 | -124 |  |  |
|  |  |  | PGA gain $=4$ | -125 | -115 |  |
|  |  |  | PGA gain $=8$ | -122 |  |  |
|  |  |  | PGA gain $=16$ | -121 | -113 |  |
|  |  |  | PGA gain = 32 and 64 | -123 |  |  |
| SFDR | Spurious-free dynamic range | $\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$ |  | 115 |  | dB |
|  | Crosstalk | $\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$ |  | -140 |  | dB |

ADS1285

### 6.5 Electrical Characteristics (continued)

minimum and maximum specifications over $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; typical specifications are at $25^{\circ} \mathrm{C}$; all specifications are at AVDD1 $=5 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}$ to 5 V , $\mathrm{AVSS}=0 \mathrm{~V}$, IOVDD $=1.8 \mathrm{~V}, \mathrm{~V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\mathrm{REFN}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{PGA}$ gain $=1$,
$\mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}$ ( 4.096 MHz low-power mode) and $\mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VOLTAGE REFERENCE INPUT |  |  |  |  |  |
|  | Reference input current | High-power mode | 110 |  | $\mu \mathrm{A} / \mathrm{V}$ |
|  |  | Mid-power mode | 110 |  |  |
|  |  | Low-power mode | 80 |  |  |
| FIR DIGITAL FILTER |  |  |  |  |  |
| $\mathrm{f}_{\text {DATA }}$ | Data rate | High-power mode | 250 | 4000 | SPS |
|  |  | Mid-power mode | 250 | 4000 |  |
|  |  | Low-power mode | 125 | 2000 |  |
|  | Pass-band ripple |  | -0.003 | 0.003 | dB |
|  | Pass-band (-0.01 dB) |  | $0.375 \times \mathrm{f}_{\text {DATA }}$ |  | Hz |
|  | Bandwidth ( -3 dB ) |  | $0.413 \times \mathrm{f}_{\text {DATA }}$ |  | Hz |
|  | Stop band |  | $0.5 \times \mathrm{f}_{\text {DATA }}$ |  | Hz |
|  | Stop-band attenuation ${ }^{(1)}$ |  | 135 |  | dB |
|  | Group delay | Minimum phase filter, at dc | $5 / f_{\text {DATA }}$ |  | s |
|  |  | Linear phase filter | 31/f fata |  |  |
|  | Settling time (latency) | Minimum phase filter | $62 / f_{\text {DATA }}$ |  | s |
|  |  | Linear phase filter | $62 / f_{\text {DATA }}$ |  |  |
| IIR DIGITAL FILTER |  |  |  |  |  |
|  | High-pass corner frequency |  | 0.1 | 10 | Hz |
| SAMPLE RATE CONVERTER |  |  |  |  |  |
|  | Clock compensation range |  | -244 | 244 | ppm of $\mathrm{f}_{\mathrm{CLK}}$ |
|  | Resolution |  | 7.45 |  | ppb of $\mathrm{f}_{\mathrm{CLK}}$ |

## DIGITAL INPUT/OUTPUT

| $\mathrm{V}_{\mathrm{OH}}$ | High-level output voltage | $\mathrm{l}_{\mathrm{OH}}=1 \mathrm{~mA}$ |  | $0.8 \times$ IOVDD |  | V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OL }}$ | Low-level output voltage | $\mathrm{l}_{\mathrm{OL}}=-1 \mathrm{~mA}$ |  |  | $0.2 \times 10 \mathrm{VDD}$ | V |
| $\mathrm{l}_{\text {kg }}$ | Input leakage |  |  | -1 | 1 | $\mu \mathrm{A}$ |
| POWER SUPPLY |  |  |  |  |  |  |
| $\mathrm{I}_{\text {AVDD1, }}$ $I_{\text {Avss }}$ | AVDD1, AVSS current | High-power mode AVDD1 $=3.3 \mathrm{~V}$ | PGA operation | 1.4 |  | mA |
|  |  |  | Buffer operation | 0.25 |  |  |
|  |  | Mid-power mode AVDD1 $=3.3 \mathrm{~V}$ | PGA operation | 0.85 |  | mA |
|  |  |  | Buffer operation | 0.25 |  |  |
|  |  | Low-power mode AVDD1 $=3.3 \mathrm{~V}$ | PGA operation | 0.8 |  | mA |
|  |  |  | Buffer operation | 0.2 |  |  |
|  |  | High-power mode AVDD1 $=5 \mathrm{~V}$ | PGA operation | 1.5 | 1.85 | mA |
|  |  |  | Buffer operation | 0.35 | 0.45 |  |
|  |  | Mid-power mode AVDD1 $=5 \mathrm{~V}$ | PGA operation | 0.9 | 1.2 | mA |
|  |  |  | Buffer operation | 0.35 | 0.45 |  |
|  |  | Low-power mode AVDD1 $=5 \mathrm{~V}$ | PGA operation | 0.85 | 1.1 | mA |
|  |  |  | Buffer operation | 0.25 | 0.45 |  |
|  |  | Power-down mode |  | 1 | 5 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {AVDD2 }}$ | AVDD2 current | High-power mode | AVDD2 $=2.5 \mathrm{~V}$ | 1.2 | 1.5 | mA |
|  |  | Mid-power mode |  | 1.2 | 1.5 |  |
|  |  | Low-power mode |  | 0.7 | 0.85 |  |
|  |  | Power-down mode |  | 1 | 5 | $\mu \mathrm{A}$ |

### 6.5 Electrical Characteristics (continued)

minimum and maximum specifications over $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$; typical specifications are at $25^{\circ} \mathrm{C}$; all specifications are at AVDD1 $=5 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}$ to 5 V , AVSS $=0 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{~V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\mathrm{REFN}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}$, PGA gain $=1$,
$\mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}$ (4.096 MHz low-power mode) and $\mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS |  | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IIOVDD | IOVDD current | High-power mode |  | 0.43 | 0.6 | mA |
|  |  | Mid-power mode |  | 0.43 | 0.6 |  |
|  |  | Low-power mode |  | 0.24 | 0.4 |  |
|  |  | Power-down mode |  | 1 | 10 | $\mu \mathrm{A}$ |
|  |  | Standby mode |  | 200 |  |  |
|  | IOVDD additional current | High-power mode | Sample rate converter operation | 1.2 |  | mA |
|  |  | Mid-power mode |  | 1.2 |  |  |
|  |  | Low-power mode |  | 0.6 |  |  |
| $\mathrm{P}_{\mathrm{d}}$ | Power dissipation ${ }^{(2)}$ | High-power mode AVDD1 $=3.3 \mathrm{~V}$ AVDD2 $=2.5 \mathrm{~V}$ | PGA operation | 8.3 |  | mW |
|  |  |  | Buffer operation | 4.5 |  |  |
|  |  | Mid-power mode AVDD1 $=3.3 \mathrm{~V}$ AVDD2 $=2.5 \mathrm{~V}$ | PGA operation | 6.5 |  | mW |
|  |  |  | Buffer operation | 4.5 |  |  |
|  |  | Low-power mode AVDD1 $=3.3 \mathrm{~V}$ AVDD2 $=2.5 \mathrm{~V}$ | PGA operation | 4.8 |  | mW |
|  |  |  | Buffer operation | 2.8 |  |  |
|  |  | High-power mode <br> AVDD1 $=5 \mathrm{~V}$ <br> AVDD2 $=2.5 \mathrm{~V}$ | PGA operation | 11.5 | 14.1 | mW |
|  |  |  | Buffer operation | 5.3 | 6.7 |  |
|  |  | Mid-power mode <br> AVDD1 $=5 \mathrm{~V}$ <br> AVDD2 $=2.5 \mathrm{~V}$ | PGA operation | 8.3 | 10.8 | mW |
|  |  |  | Buffer operation | 5.3 | 6.7 |  |
|  |  | Low-power mode AVDD1 $=5 \mathrm{~V}$ AVDD2 $=2.5 \mathrm{~V}$ | PGA operation | 6.4 | 8.4 | mW |
|  |  |  | Buffer operation | 3.4 | 5.1 |  |

(1) Input frequencies at $\mathrm{N} \times 32 \mathrm{kHz}$ ( 16 kHz low-power mode) $\pm \mathrm{f}_{\text {DATA }} / 2$ (where $N=1,2,3 \ldots$ ) intermodulate with the chopper clock. At these frequencies stop band attenuation $=-90 \mathrm{dBFS}$ (typ).
(2) Excluding current consumed by the voltage reference input or by sample rate converter operation. See voltage reference input current and IOVDD current of sample rate converter operation.

### 6.6 Timing Requirements: $1.65 \mathrm{~V} \leq$ IOVDD $\leq 1.95 \mathrm{~V}$ and $2.7 \mathrm{~V} \leq I O V D D \leq 3.6 \mathrm{~V}$

over operating ambient temperature range (unless otherwise noted)

|  |  |  | MIN | NOM | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CLOCK |  |  |  |  |  |  |
| $\mathrm{t}_{\mathrm{c} \text { (CLK) }}$ | CLK period | High-power mode | 120.5 | 122.07 | 166 | ns |
|  |  | Mid-power mode | 120.5 | 122.07 | 166 |  |
|  |  | Low-power mode | 241 | 244.14 | 332 |  |
| $\mathrm{t}_{\mathrm{w} \text { (CLKH) }}$ | Pulse duration, CLK high | High-power mode | 55 |  |  | ns |
|  |  | Mid-power mode | 55 |  |  |  |
|  |  | Low-power mode | 110 |  |  |  |
| $\mathrm{t}_{\mathrm{w} \text { (CLKL) }}$ | Pulse duration, CLK low | High-power mode | 55 |  |  | ns |
|  |  | Mid-power mode | 55 |  |  |  |
|  |  | Low-power mode | 110 |  |  |  |

## SERIAL INTERFACE

| $\mathrm{t}_{\mathrm{w} \text { (CSH) }}$ | Pulse duration, $\overline{C S}$ high | 20 | ns |
| :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\mathrm{d} \text { (CSSC) }}$ | Delay time, first SCLK rising edge after $\overline{\mathrm{CS}}$ falling edge | 20 | ns |
| $\mathrm{t}_{\mathrm{c}(\mathrm{SCLK})}$ | SCLK period | 120 | ns |
| $\mathrm{t}_{\mathrm{w} \text { (SCH) }}$ | Pulse duration, SCLK high | 50 | ns |
| $\mathrm{t}_{\mathrm{w} \text { (SCL) }}$ | Pulse duration, SCLK low | 50 | ns |
| $\mathrm{t}_{\text {su( }{ }_{\text {d }} \text { ) }}$ | Setup time, DIN valid before SCLK rising edge | 10 | ns |
| $\mathrm{th}_{\mathrm{h} \text { (DI) }}$ | Hold time, DIN valid after SCLK rising edge | 10 | ns |
| $\mathrm{t}_{\text {su }}$ (SRC-W) | Setup time, SRC[1:0] register write before $\overline{\text { DRDY }}$ falling edge | 256 | 1 / f(CLK) |
| SYNC |  |  |  |
| $\mathrm{t}_{\text {W(SYNL) }}$ | Pulse duration, SYNC low | 2 | $1 / \mathrm{f}$ (CLK) |
| $\mathrm{t}_{\mathrm{W} \text { (SYNH) }}$ | Pulse duration, SYNC high | 2 | $1 / \mathrm{f}$ (CLK) |
| $\mathrm{t}_{\text {su(SYNCLK) }}$ | Setup time, SYNC high before CLK rising edge | 10 | ns |
| $\mathrm{th}_{\text {(SYNCLK) }}$ | Hold time, SYNC high after CLK rising edge | 10 | ns |
| RESET |  |  |  |
| $\mathrm{t}_{\mathrm{w} \text { (RSTL) }}$ | Pulse duration, RESET low | 2 | $1 / \mathrm{f}$ (CLK) |
| $\mathrm{t}_{\text {su(RSTCLK) }}$ | Setup time, $\overline{\text { RESET }}$ high before CLK rising edge | 10 | ns |
| $\mathrm{t}_{\text {(RSTCLK) }}$ | Hold time, RESET high after CLK rising edge | 10 | ns |

6.7 Switching Characteristics: $1.65 \mathrm{~V} \leq$ IOVDD $\leq 1.95 \mathrm{~V}$ and $2.7 \mathrm{~V} \leq \mathrm{IOVDD} \leq 3.6 \mathrm{~V}$
over operating ambient temperature range and $\mathrm{C}_{\text {LOAD }}=20 \mathrm{pF}$ (unless otherwise noted)

|  | PARAMETER | MIN | TYP MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| SERIAL INTERFACE |  |  |  |  |
| $\mathrm{t}_{\mathrm{w} \text { (DRH) }}$ | Pulse duration, $\overline{\text { DRDY }}$ high |  | 8 | $1 / \mathrm{f}$ (CLK) |
| $\mathrm{t}_{\mathrm{p} \text { (CSDO) }}$ | Propagation delay time, $\overline{\mathrm{CS}}$ falling edge to DOUT driven valid |  | 50 | ns |
| $\mathrm{t}_{\mathrm{p} \text { (SCDO) }}$ | Propagation delay time, SCLK falling edge to new DOUT valid |  | 50 | ns |
| $\mathrm{th}_{\text {(SCDO) }}$ | Propagation delay time, SCLK falling edge to DOUT invalid | 5 |  | ns |
| SYNC |  |  |  |  |
| $\mathrm{t}_{\text {p(SYNDR) }}$ | Propagation delay time, SYNC rising edge to valid data $\overline{\text { DRDY falling edge }}$ | 62.981 | +930 / fCLK | s |
| RESET |  |  |  |  |
| $\mathrm{t}_{\text {p(RSTDR) }}$ | Propagation delay time, RESET rising edge to DRDY falling edge |  |  | 1/f ${ }_{\text {CLK }}$ |
| PWDN |  |  |  |  |
| $\mathrm{t}_{\mathrm{p} \text { (PDDR) }}$ | Propagation delay time, $\overline{\text { PWDN }}$ rising edge to $\overline{\text { DRDY }}$ falling edge | 62.981 | + $946 / \mathrm{f}_{\text {(CLK) }}$ | S |
| POWER UP |  |  |  |  |
| $\mathrm{t}_{\text {(SUPDR) }}$ | Propagation delay time, power supply and CLK applied to first DRDY pulse |  |  | 1 / fCLK |

### 6.8 Timing Diagrams

CLK


Figure 6-1. Clock Timing Requirements


Figure 6-2. Serial Interface Timing Requirements


Figure 6-3. Serial Interface Switching Characteristics


Figure 6-4. SYNC Timing Requirements and Switching Characteristics


Figure 6-5. RESET Timing Requirements and Switching Characteristics


Figure 6-6. PWDN Switching Characteristics


Figure 6-7. Sample Rate Converter Register-Write Timing Requirements


Figure 6-8. Power-Up Switching Characteristics

### 6.9 Typical Characteristics

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


Figure 6-9. High-Power Mode FFT Spectrum


Figure 6-11. High-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$, PGA gain $=1$
Figure 6-13. High-Power Mode FFT Spectrum


Shorted input, PGA gain $=8$
Figure 6-10. High-Power Mode FFT Spectrum


Figure 6-12. High-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-20 \mathrm{dBFS}$, PGA gain $=1$
Figure 6-14. High-Power Mode FFT Spectrum

### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$, buffer operation

Figure 6-15. High-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$, PGA gain $=8$
Figure 6-17. High-Power Mode FFT Spectrum


Figure 6-19. Mid-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}, \mathrm{PGA}$ gain $=2, \mathrm{~V}_{\mathrm{REF}}=2.5 \mathrm{~V}$, AVDD1 $=3.3 \mathrm{~V}, 2048$ data points
Figure 6-16. High-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-20 \mathrm{dBFS}, \mathrm{PGA}$ gain $=8$
Figure 6-18. High-Power Mode FFT Spectrum


Shorted input, PGA gain = 8
Figure 6-20. Mid-Power Mode FFT Spectrum

### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


Shorted input, PGA gain $=1, \mathrm{~V}_{\text {REF }}=2.5 \mathrm{~V}, \mathrm{AVDD} 1=3.3 \mathrm{~V}$
Figure 6-21. Mid-Power Mode FFT Spectrum


Figure 6-23. Mid-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$, PGA gain $=8$
Figure 6-25. Mid-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$, PGA gain $=1$
Figure 6-22. Mid-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}, \mathrm{PGA}$ gain $=2, \mathrm{~V}_{\mathrm{REF}}=2.5 \mathrm{~V}$, AVDD1 $=3.3 \mathrm{~V}, 2048$ data points

Figure 6-24. Mid-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-20 \mathrm{dBFS}, \mathrm{PGA}$ gain $=8$
Figure 6-26. Mid-Power Mode FFT Spectrum

### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


Figure 6-27. Low-Power Mode FFT Spectrum


Shorted input, PGA gain $=1, \mathrm{~V}_{\mathrm{REF}}=2.5 \mathrm{~V}, \mathrm{AVDD} 1=3.3 \mathrm{~V}$
Figure 6-29. Low-Power Mode FFT Spectrum


Figure 6-31. Low-Power Mode FFT Spectrum


Shorted input, PGA gain $=8$
Figure 6-28. Low-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}$, PGA gain $=1$
Figure 6-30. Low-Power Mode FFT Spectrum

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}, \mathrm{PGA}$ gain $=2, \mathrm{~V}_{\mathrm{REF}}=2.5 \mathrm{~V}$, AVDD1 = $3.3 \mathrm{~V}, 2048$ data points

Figure 6-32. Low-Power Mode FFT Spectrum

### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


Figure 6-35. Channel-to-Channel Crosstalk


Figure 6-37. Dynamic Range vs PGA Gain

$\mathrm{f}_{\mathrm{IN}}=31.25 \mathrm{~Hz}, \mathrm{~V}_{\mathrm{IN}}=-20 \mathrm{dBFS}, \mathrm{PGA}$ gain $=8$
Figure 6-34. Low-Power Mode FFT Spectrum


Figure 6-36. Dynamic Range vs PGA Gain


Figure 6-38. Dynamic Range vs PGA Gain

### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\text {DATA }}=500 \mathrm{SPS}$ (unless otherwise noted)


### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\mathrm{DATA}}=500 \mathrm{SPS}$ (unless otherwise noted)


Figure 6-57. Reference Input Current vs Temperature


Figure 6-59. CMRR vs Common-Mode Input Frequency


Figure 6-61. AVDD1 Current Distribution


Figure 6-58. Reference Input Current Distribution


Figure 6-60. AVDD1 Current Distribution


Figure 6-62. AVDD1 Current vs Temperature

### 6.9 Typical Characteristics (continued)

at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{AVDD} 1=5 \mathrm{~V}, \mathrm{AVSS}=0 \mathrm{~V}, \mathrm{AVDD} 2=2.5 \mathrm{~V}, \mathrm{IOVDD}=1.8 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=8.192 \mathrm{MHz}(4.096 \mathrm{MHz}$ low-power mode $)$, $\mathrm{V}_{\text {REFP }}=4.096 \mathrm{~V}, \mathrm{~V}_{\text {REFN }}=0 \mathrm{~V}, \mathrm{PGA}$ gain $=1, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{f}_{\mathrm{DATA}}=500 \mathrm{SPS}$ (unless otherwise noted)


Figure 6-63. AVDD1 Current vs Temperature


Figure 6-65. AVDD2 Current vs Temperature


Figure 6-64. AVDD2 Current Distribution


Figure 6-66. PSRR vs Power-Supply Frequency


Figure 6-67. IOVDD Current vs Data Rate

## 7 Parameter Measurement Information

### 7.1 Noise Performance

The ADS1285 is a 32-bit ADC providing three power-resolution modes, allowing optimization of noise performance verses device power consumption. The four determining factors of noise performance are the power mode, output data rate, PGA gain setting, and reference voltage selection. The high-power mode operates the PGA and modulator sampling rate at the highest capacity for best overall noise performance. The mid-power mode scales down the PGA quiescent current to reduce power consumption but results in increased PGA noise. The low-power mode reduces both the modulator sampling rate and PGA quiescent current. The result is the low-power mode has the lowest power consumption but the highest level of overall noise.
For all power modes, decreasing the output data rate reduces signal bandwidth, and therefore decreases total noise. Increasing the PGA gain reduces noise when noise is referred to the input. Dynamic range performance decreases when PGA gain is increased because the ratio of input voltage range to input-referred noise also decreases.

Noise performance also depends on the reference voltage. Operation with $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$ or 5 V provides the best noise performance. Operation with $\mathrm{V}_{\mathrm{REF}}=2.5 \mathrm{~V}$ (required when operating AVDD1 $=3.3 \mathrm{~V}$ ) reduces noise performance.

Dynamic range and input noise are equivalent parameters that describe the available resolution of the ADC. Equation 1 derives dynamic range from the input-referred noise data:

$$
\begin{equation*}
\text { Dynamic Range }(\mathrm{dB})=20 \times \log \left[\frac{1.768 \mathrm{~V}}{\text { Gain } \times \mathrm{e}_{\mathrm{n}}}\right] \tag{1}
\end{equation*}
$$

where:

- $e_{n}=$ Input-referred voltage noise (RMS)

Figure 7-1 and Figure 7-2 show dynamic range performance at $f_{\text {DATA }}=500 \mathrm{SPS}$ for operation with $\mathrm{V}_{\text {REF }}=4.096$ V and $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$.


Figure 7-1. Dynamic Range vs PGA Gain


Figure 7-2. Dynamic Range vs PGA Gain

Table 7-1 through Table 7-3 list dynamic range and input-referred noise performance with $\mathrm{V}_{\text {REF }}=4.096 \mathrm{~V}$ and AVDD1 $=5 \mathrm{~V}$, tested with input source resistance $\left(\mathrm{R}_{\mathrm{S}}\right)=0 \Omega$. Table 7-4 through Table 7-6 list dynamic range and input noise performance with $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$ and AVDD1 $=3.3 \mathrm{~V}$, tested with $\mathrm{R}_{\mathrm{S}}=0 \Omega$. Noise data are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ and are representative of typical ADC performance. The data are the standard deviation of 4096 consecutive ADC conversion results with the ADC inputs shorted, measured over the $0.413 \times \mathrm{f}_{\text {DATA }}$ bandwidth. Because of the statistical nature of noise, repeated measurements can yield varying noise performance results.

ADS1285
www.ti.com
Table 7-1. High-Power Mode Noise Performance ( $\mathrm{V}_{\text {REF }}=4.096 \mathrm{~V}$, AVDD1 $=5 \mathrm{~V}, \mathrm{R}_{\mathrm{S}}=0 \Omega$ )

| GAIN | MODE | DYNAMIC RANGE (dB) |  |  |  |  | $e_{\mathrm{n}}$, INPUT-REFERRED NOISE ( $\mu \mathrm{V}_{\text {RMS }}$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  |
|  |  | 250 | 500 | 1000 | 2000 | 4000 | 250 | 500 | 1000 | 2000 | 4000 |
| 1 | Buffer | 135 | 132 | 129 | 126 | 123 | 0.31 | 0.44 | 0.63 | 0.89 | 1.25 |
| 1 | PGA | 137 | 134 | 131 | 128 | 125 | 0.25 | 0.35 | 0.50 | 0.70 | 0.99 |
| 2 | PGA | 136 | 133 | 130 | 127 | 124 | 0.14 | 0.20 | 0.28 | 0.39 | 0.56 |
| 4 | PGA | 134 | 131 | 128 | 125 | 122 | 0.09 | 0.12 | 0.18 | 0.25 | 0.35 |
| 8 | PGA | 130 | 127 | 124 | 121 | 118 | 0.07 | 0.10 | 0.14 | 0.20 | 0.28 |
| 16 | PGA | 126 | 123 | 120 | 117 | 114 | 0.06 | 0.08 | 0.11 | 0.16 | 0.22 |
| 32 | PGA | 120 | 117 | 114 | 111 | 108 | 0.06 | 0.08 | 0.11 | 0.16 | 0.22 |
| 64 | PGA | 114 | 111 | 108 | 105 | 102 | 0.06 | 0.08 | 0.11 | 0.16 | 0.22 |

Table 7-2. Mid-Power Mode Noise Performance ( $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$, AVDD1 $=5 \mathrm{~V}, \mathrm{R}_{\mathrm{S}}=0 \Omega$ )

| GAIN | MODE | DYNAMIC RANGE (dB) |  |  |  |  | $\mathrm{e}_{\mathrm{n}}$, INPUT-REFERRED NOISE ( $\mu \mathrm{V}_{\text {RMS }}$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  |
|  |  | 250 | 500 | 1000 | 2000 | 4000 | 250 | 500 | 1000 | 2000 | 4000 |
| 1 | Buffer | 135 | 132 | 129 | 126 | 123 | 0.31 | 0.44 | 0.63 | 0.89 | 1.25 |
| 1 | PGA | 137 | 134 | 131 | 128 | 125 | 0.25 | 0.35 | 0.50 | 0.70 | 0.99 |
| 2 | PGA | 135 | 132 | 129 | 126 | 123 | 0.16 | 0.22 | 0.31 | 0.44 | 0.63 |
| 4 | PGA | 133 | 130 | 127 | 124 | 121 | 0.10 | 0.14 | 0.20 | 0.28 | 0.39 |
| 8 | PGA | 128 | 125 | 122 | 119 | 116 | 0.09 | 0.12 | 0.18 | 0.25 | 0.35 |
| 16 | PGA | 123 | 120 | 117 | 114 | 111 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |
| 32 | PGA | 117 | 114 | 111 | 108 | 105 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |
| 64 | PGA | 111 | 108 | 105 | 102 | 99 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |

Table 7-3. Low-Power Mode Noise Performance ( $\mathrm{V}_{\text {REF }}=4.096 \mathrm{~V}$, AVDD1 $=5 \mathrm{~V}, \mathrm{R}_{\mathrm{S}}=0 \Omega$ )

| GAIN | MODE | DYNAMIC RANGE (dB) |  |  |  |  | $e_{n}$, INPUT-REFERRED NOISE ( $\mu \mathrm{V}_{\text {RMs }}$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  |
|  |  | 125 | 250 | 500 | 1000 | 2000 | 125 | 250 | 500 | 1000 | 2000 |
| 1 | Buffer | 135 | 132 | 129 | 126 | 123 | 0.31 | 0.44 | 0.63 | 0.89 | 1.25 |
| 1 | PGA | 138 | 135 | 132 | 129 | 126 | 0.22 | 0.31 | 0.44 | 0.63 | 0.89 |
| 2 | PGA | 137 | 134 | 131 | 128 | 125 | 0.12 | 0.18 | 0.25 | 0.35 | 0.50 |
| 4 | PGA | 135 | 132 | 129 | 126 | 123 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |
| 8 | PGA | 131 | 128 | 125 | 122 | 119 | 0.06 | 0.09 | 0.12 | 0.18 | 0.25 |
| 16 | PGA | 126 | 123 | 120 | 117 | 114 | 0.06 | 0.08 | 0.11 | 0.16 | 0.22 |
| 32 | PGA | 120 | 117 | 114 | 111 | 108 | 0.06 | 0.08 | 0.11 | 0.16 | 0.22 |
| 64 | PGA | 114 | 111 | 108 | 105 | 102 | 0.06 | 0.08 | 0.11 | 0.16 | 0.22 |

Table 7-4. High-Power Mode Noise Performance ( $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$, AVDD1 $=3.3 \mathrm{~V}, \mathrm{R}_{\mathrm{S}}=0 \Omega$ )

| GAIN | MODE | DYNAMIC RANGE (dB) |  |  |  |  | $\mathrm{e}_{\mathrm{n}}$, INPUT-REFERRED NOISE ( $\mu \mathrm{V}_{\text {RMS }}$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  |
|  |  | 250 | 500 | 1000 | 2000 | 4000 | 250 | 500 | 1000 | 2000 | 4000 |
| 1 | Buffer | 135 | 132 | 129 | 126 | 123 | 0.31 | 0.44 | 0.63 | 0.89 | 1.25 |
| $1{ }^{11}$ | PGA | 128 | 125 | 122 | 119 | 116 | 0.35 | 0.50 | 0.70 | 0.99 | 1.40 |
| 2 | PGA | 133 | 130 | 127 | 124 | 121 | 0.20 | 0.28 | 0.39 | 0.56 | 0.79 |
| 4 | PGA | 132 | 129 | 126 | 123 | 120 | 0.11 | 0.16 | 0.22 | 0.31 | 0.44 |
| 8 | PGA | 129 | 126 | 123 | 120 | 117 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |
| 16 | PGA | 125 | 122 | 119 | 116 | 113 | 0.06 | 0.09 | 0.12 | 0.18 | 0.25 |
| 32 | PGA | 119 | 116 | 113 | 110 | 107 | 0.06 | 0.09 | 0.12 | 0.17 | 0.25 |
| 64 | PGA | 113 | 110 | 107 | 104 | 101 | 0.06 | 0.09 | 0.12 | 0.17 | 0.25 |

Table 7-5. Mid-Power Mode Noise Performance ( $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$, AVDD1 $=3.3 \mathrm{~V}, \mathrm{R}_{\mathrm{S}}=0 \Omega$ )

| GAIN | MODE | DYNAMIC RANGE (dB) |  |  |  |  | $e_{n}$, INPUT-REFERRED NOISE ( $\mu \mathrm{V}_{\text {RMS }}$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  |
|  |  | 250 | 500 | 1000 | 2000 | 4000 | 250 | 500 | 1000 | 2000 | 4000 |
| 1 | Buffer | 135 | 132 | 129 | 126 | 123 | 0.31 | 0.44 | 0.63 | 0.89 | 1.25 |
| $1{ }^{(1)}$ | PGA | 128 | 125 | 122 | 119 | 116 | 0.35 | 0.50 | 0.70 | 0.99 | 1.40 |
| 2 | PGA | 133 | 130 | 127 | 124 | 121 | 0.20 | 0.28 | 0.39 | 0.56 | 0.79 |
| 4 | PGA | 131 | 128 | 125 | 122 | 119 | 0.12 | 0.18 | 0.25 | 0.35 | 0.50 |
| 8 | PGA | 127 | 124 | 121 | 118 | 115 | 0.10 | 0.14 | 0.20 | 0.28 | 0.39 |
| 16 | PGA | 123 | 120 | 117 | 114 | 111 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |
| 32 | PGA | 117 | 114 | 111 | 108 | 105 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |
| 64 | PGA | 111 | 108 | 105 | 102 | 99 | 0.08 | 0.11 | 0.16 | 0.22 | 0.31 |

Table 7-6. Low-Power Mode Noise Performance ( $\mathrm{V}_{\mathrm{REF}}=2.5 \mathrm{~V}$, AVDD1 $=3.3 \mathrm{~V}, \mathrm{R}_{\mathrm{S}}=0 \Omega$ )

| GAIN | MODE | DYNAMIC RANGE (dB) |  |  |  |  | $\mathrm{e}_{\mathrm{n}}$, INPUT-REFERRED NOISE ( $\mu \mathrm{V}_{\text {RMS }}$ ) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  | $\mathrm{f}_{\text {DATA }}$ |  |  |  |  |
|  |  | 125 | 250 | 500 | 1000 | 2000 | 125 | 250 | 500 | 1000 | 2000 |
| 1 | Buffer | 135 | 132 | 129 | 126 | 123 | 0.31 | 0.44 | 0.63 | 0.89 | 1.25 |
| $1^{(1)}$ | PGA | 129 | 126 | 123 | 120 | 117 | 0.31 | 0.44 | 0.83 | 0.89 | 1.25 |
| 2 | PGA | 134 | 131 | 128 | 125 | 122 | 0.18 | 0.25 | 0.35 | 0.50 | 0.70 |
| 4 | PGA | 133 | 130 | 127 | 124 | 121 | 0.10 | 0.14 | 0.20 | 0.28 | 0.39 |
| 8 | PGA | 130 | 127 | 124 | 121 | 118 | 0.07 | 0.10 | 0.14 | 0.20 | 0.28 |
| 16 | PGA | 125 | 122 | 119 | 116 | 113 | 0.06 | 0.09 | 0.12 | 0.17 | 0.25 |
| 32 | PGA | 119 | 116 | 113 | 110 | 107 | 0.06 | 0.09 | 0.12 | 0.17 | 0.25 |
| 64 | PGA | 113 | 110 | 107 | 104 | 101 | 0.06 | 0.09 | 0.12 | 0.17 | 0.25 |

(1) Because of the limited input headroom with AVDD1 $=3.3 \mathrm{~V}$ operation, the available input range with PGA gain operation $=1$ is $\pm 1.35$ $\mathrm{V}_{\mathrm{PP}}$. The dynamic range data for PGA gain $=1$ and $\mathrm{AVDD} 1=3.3 \mathrm{~V}$ reflects the reduced input range .

## 8 Detailed Description

### 8.1 Overview

The ADS1285 is a high-resolution, low-power analog-to-digital converter (ADC) designed for applications in energy exploration, geology, and seismic monitoring where low-power consumption and high resolution are required. The converter provides 32 bits of resolution spanning data rates from 125 SPS to 4000 SPS. The programmable gain amplifier (PGA) expands the system dynamic range by accepting signals ranging from $\pm 2.5$ $\mathrm{V}_{\mathrm{PP}}$ to $\pm 0.039 \mathrm{~V}_{\mathrm{Pp}}$.
As illustrated in the Functional Block Diagram, the ADC consists of the following sections: input multiplexer (MUX), programmable gain amplifier (PGA), unity-gain buffer, delta-sigma ( $\Delta \Sigma$ ) modulator, sample rate converter, infinite impulse response (IIR) high-pass filter (HPF), finite impulse response (FIR) low-pass filter (LPF), and an SPI-compatible serial interface used for both device configuration and conversion data readback.
The input multiplexer selects between inputs 1 and 2, and internal options designed for self-test, including an input-short option used to test offset and noise.
The input multiplexer is followed by a low-noise PGA. The PGA gain range is 1 to 16, with gains 32 and 64 provided as digital gains. The PGA is chopper-stabilized to reduce $1 / \mathrm{f}$ noise and input offset voltage. The PGA output connects to a buffer which drives the modulator. An external 10-nF capacitor, connected to PGA output pins CAPP and CAPN, provides an antialias filter for the input signal.

The PGA can be disabled to lower device power consumption by operating the ADC with the unity-gain buffer. External 47-nF capacitors connected to each buffer output filters the modulator sampling pulses.
The $\Delta \Sigma$ modulator measures the differential input signal $\left(\mathrm{V}_{\mathrm{IN}}\right)$ against the differential reference voltage $\left(\mathrm{V}_{\text {REF }}\right)$. The modulator provides three reference voltage options ( $2.5 \mathrm{~V}, 4.096 \mathrm{~V}$, or 5 V ). The reference voltage is programmed by the user.

Modulator data are processed by the digital filter providing the final conversion result. The digital filter consists of a sinc filter followed by a programmable phase, FIR low-pass filter, and an IIR high-pass filter. The high-pass filter removes dc and low-frequency components from the data.
The sample rate converter (SRC) compensates clock frequency error by resampling the output data. The clock frequency compensation range is $\pm 244$ ppm with $7-\mathrm{ppb}$ resolution.

User-programmable gain and offset calibration registers correct offset and gain errors.
The SYNC pin synchronizes the ADC. Synchronization has two modes of operation: pulse synchronization and continuous synchronization. The RESET pin resets the ADC, including user configuration settings. The pins are noise-resistant, Schmitt-trigger inputs to increase reliability in high-noise environments.
The $\overline{\text { PWDN }}$ pin powers down the ADC when not in use. The software power-down mode (STANDBY) is available through the serial interface
The 4-wire, SPI-compatible, serial interface reads conversion data and reads or writes device register data.
Two general-purpose digital I/Os are available for system level control.
Power for the PGA and buffer is supplied by AVDD1 and AVSS. A charge pump voltage regulator increases the input voltage range of the buffer that follows the PGA. Power for the modulator is supplied by AVDD2. IOVDD supplies the digital logic core through a 1.8-V low-dropout regulator (LDO). IOVDD is the digital I/O supply.

### 8.2 Functional Block Diagram



### 8.3 Feature Description

### 8.3.1 Analog Input

Figure 8-1 shows the analog input circuit and input multiplexer.


Figure 8-1. Analog Input and Multiplexer
Electrostatic discharge (ESD) diodes are incorporated to protect the ADC inputs from ESD events that occur during device manufacturing and printed circuit board (PCB) assembly process when assembled in an ESDcontrolled environment. For system-level protection, consider using external ESD protection devices to protect the input that are exposed to ESD events.

If the inputs are driven below AVSS -0.3 V , or above AVDD1 +0.3 V , the protection diodes can conduct. If these conditions are possible, use external clamp diodes, series resistors, or both to limit input current to the specified maximum value. Overdriving an unused input channel can affect the conversion results of the active input channel. Clamp the overdriven voltage with Schottky diodes to prevent channel crosstalk.
The ADC incorporates two differential input channels The multiplexer selects between the two differential inputs for measurement. A test mode to measure noise and offset is also provided by the multiplexer. The shorted input test configuration is available with or without the $400-\Omega$ resistors to simulate the thermal noise generated by an $800-\Omega$ geophone. Table $8-1$ summarizes the multiplexer configurations.

Table 8-1. Input Multiplexer Modes

| MUX[2:0] BITS | SWITCHES | DESCRIPTION |
| :---: | :--- | :--- |
| 000 | $\mathrm{~S}_{1}, \mathrm{~S}_{5}$ | Input AIN1P, AIN1N connection |
| 001 | $\mathrm{~S}_{2}, \mathrm{~S}_{6}$ | Input AIN2P, AIN2N connection |
| 010 | $\mathrm{~S}_{3}, \mathrm{~S}_{4}$ | $400-\Omega$ input-short test mode for offset and noise test. |
| 011 | $\mathrm{~S}_{1}, \mathrm{~S}_{5}, \mathrm{~S}_{2}, \mathrm{~S}_{6}$ | Cross-connection test mode. Inputs AIN1P, AIN2P and AIN2P, AIN2N are connected |
| 100 | - | Reserved |
| 101 | $\mathrm{~S}_{3}, \mathrm{~S}_{4}, \mathrm{~S}_{7}$ | $0-\Omega$ input-short test mode for offset and noise test. |

To test geophone THD performance, apply a test signal to the test channel through series resistors. The series resistors are typically half the value of the geophone impedance. Select the multiplexer for the cross-connection test mode (MUX[2:0] = 011b). In cross-connection mode, the test signal is cross-fed to the geophone input.

Geophone THD test performance can be affected by the nonlinear on-resistance of the multiplexer ( $\mathrm{R}_{\mathrm{sw}}$ ). Figure $8-2$ shows a model of the input multiplexer resistance for the geophone THD test. Figure 8-3 shows THD performance versus a test resistor ( $\mathrm{R}_{\text {LOAD }}$ ) used to simulate geophone resistance. Small amplitude test signals (such as, $\mathrm{V}_{\mathbb{I N}}=0.221 \mathrm{~V}$ ), shows less THD performance degradation for geophone resistance $<500 \Omega$.


Figure 8-2. THD versus R $_{\text {LOAD }}$ Test Circuit


Figure 8-3. THD Performance vs R $_{\text {LOAD }}$

### 8.3.2 PGA and Buffer

Figure 8-4 shows the simplified PGA and buffer block diagram.


Figure 8-4. PGA and Buffer Block Diagram
The device can be operated with the PGA or the unity-gain buffer. Buffer operation disables the PGA bias, reducing device power consumption. Because of the limited input headroom for PGA gain = 1 when operating with AVDD1 $=3.3 \mathrm{~V}$, the buffer must be used under this condition.

### 8.3.2.1 Programmable Gain Amplifier (PGA)

The PGA is a low-noise, chopper-stabilized differential amplifier that extends the ADC dynamic range performance. The PGA provides analog gains from 1 to 16 , with gains of 32 and 64 provided by digital scaling. The PGA output signal is routed to the CAPP and CAPN pins through $270-\Omega$ resistors. Connect an external $10-\mathrm{nF}, \mathrm{COG}$-dielectric capacitor across these pins. An antialias filter is formed by these components to attenuate the signal level at the modulator aliasing frequency ( $f_{\text {MOD }}$ ).

As shown in Figure 8-4, the buffer is used between the PGA and the modulator. Connect two 47-nF, C0Gdielectric capacitors from each buffer output to AVSS (CAPBP and CAPBN). A voltage charge pump increases
the buffer input voltage headroom. Connect an external 4.7-nF capacitor between CAPC and AGND for charge pump operation.
The PGA gain is programmed by the GAIN[2:0] bits of the CONFIG1 register. Table 8-2 shows the PGA gain settings and buffer selection. The PGA gains and input signal range are irrespective of the voltage reference.

Table 8-2. PGA Gains

| GAIN[2:0] REGISTER BITS | PGA GAIN | INPUT SIGNAL RANGE (VPP) |
| :---: | :---: | :---: |
| 000 | 1 | $\pm 2.5$ |
| 001 | 2 | $\pm 1.25$ |
| 010 | 4 | $\pm 0.625$ |
| 011 | 8 | $\pm 0.3125$ |
| 100 | 16 | $\pm 0.15625$ |
| 101 | 32 | $\pm 0.078125$ |
| 110 | 64 | $\pm 0.0390625$ |
| 111 | Buffer mode, gain $=1$ | $\pm 2.5$ |

Observe the PGA input and output voltage headroom specification. Figure $8-5$ shows the input and output voltage headroom when operating with AVDD1 $=5 \mathrm{~V}$, an input common-mode voltage $\left(\mathrm{V}_{\mathrm{CM}}\right)=2.5 \mathrm{~V}$, a differential input voltage $= \pm 2.5 \mathrm{~V}_{\mathrm{PP}}$, and at gain $=1$. The absolute minimum and maximum PGA input voltage ( 1.25 V and 3.75 V ) is $\pm 1 / 2$ of the differential signal voltage plus the common-mode voltage. The PGA provides $0.15-\mathrm{V}$ input voltage margin at the negative peak and $0.4-\mathrm{V}$ input voltage margin at the positive peak. As shown in the figure, the PGA gain increases by $\times 1.5$ when the ADC is operated with $4.096-\mathrm{V}$ or $5-\mathrm{V}$ voltage references. The PGA provides $0.475-\mathrm{V}$ output voltage margin at the positive and negative peaks.


Figure 8-5. PGA Headroom (AVDD1 = 5 V, PGA Gain = 1)
When operating with AVDD1 $=3.3 \mathrm{~V}$, the PGA cannot support $\pm 2.5-\mathrm{V}_{\mathrm{PP}}$ input signals. Use the buffer for $\pm 2.5-\mathrm{V}_{\mathrm{PP}}$ input signals. For $\pm 1.25-\mathrm{V}_{\mathrm{PP}}$ input signals (PGA gain $=2$ ), the input headroom is increased by increasing the common-mode voltage by 0.1 V to AVSS +1.75 V . Figure $8-6$ illustrates the input and output operating headroom for AVDD1 $=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=1.75 \mathrm{~V}$, input signal $= \pm 1.25 \mathrm{~V}_{\mathrm{PP}}$, and gain $=2$. The PGA uses normal gain scaling when $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$.

SBAS559A - MAY 2022 - REVISED DECEMBER 2022


Figure 8-6. PGA Headroom ( AVDD1 $=3.3 \mathrm{~V}$, Gain $=2$ )

### 8.3.2.2 Buffer Operation (PGA Bypass)

The ADC provides a buffer option, bypassing the PGA. Bypassing the PGA reduces device power consumption. Use the buffer for $\pm 2.5-\mathrm{V}_{\mathrm{PP}}$ input signals when operating AVDD1 at 3.3 V . Buffer operation is enabled by setting the GAIN[2:0] bits $=111 \mathrm{~b}$ of the CONFIG1 register.
Figure $8-7$ shows the buffer voltage headroom with AVDD1 $=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=1.65 \mathrm{~V}$, and the input signal $= \pm 2.5$ $V_{\mathrm{PP}}$. The buffer has sufficient voltage headroom for $\pm 2.5-\mathrm{V}_{\mathrm{PP}}$ input signals when operating with AVDD1 $=3.3 \mathrm{~V}$.


Figure 8-7. Buffer Headroom (3.3-V Operation Shown)
Regardless of PGA or buffer operation, connect two 47-nF, C0G-dielectric capacitors from each buffer output to AVSS (CAPBP and CAPBN). The voltage charge pump increases the buffer input operating headroom. Connect an external $4.7-\mathrm{nF}$ capacitor between CAPC and AGND for the charge pump operation.

### 8.3.3 Voltage Reference Input

The ADC requires a reference voltage for operation. The reference voltage input is differential, defined as the voltage between the REFP and REFN pins: $\mathrm{V}_{\text {REF }}=\mathrm{V}_{\text {REFP }}-\mathrm{V}_{\text {REFN }}$. Because of the differential input, the VREFN trace can be routed to the voltage reference ground terminal to avoid ground noise pickup.
The device offers the choice of three reference voltages: $5 \mathrm{~V}, 4.096 \mathrm{~V}$, or 2.5 V . Maximum dynamic range performance is achieved using $\mathrm{V}_{\text {REF }}=5 \mathrm{~V}$ or 4.096 V , which requires AVDD1 $=5 \mathrm{~V}$ for operation. If AVDD1 $=3.3$ V , the reference voltage is limited to 2.5 V . Program the reference voltage to match the physical voltage by the $\operatorname{REF}[1: 0]$ bits of the CONFIG1 register. Use a precision voltage reference with low noise, optimally less than 0.5 $\mu \mathrm{V}_{\text {RMS }}$ over the measurement bandwidth.

Figure 8-8 illustrates a simplified reference input circuit. Similar to the analog inputs, the reference inputs are protected by ESD diodes. If the reference inputs are driven below AVSS -0.3 V or above AVDD1 +0.3 V , the protection diodes can conduct. If these conditions are possible, use external clamp diodes, series resistors, or both to limit the reference input current to the specified value.


Figure 8-8. Simplified Voltage Reference Input Circuit
The ADC samples the reference voltage by an internal capacitor ( $\mathrm{C}_{\mathrm{REF}}$ ) and then discharges the capacitor at the modulator sampling frequency ( $\mathrm{f}_{\mathrm{MOD}}$ ). The sampling operation results in transient current flow into the reference inputs. The transient current is filtered by a $0.1-\mu \mathrm{F}$ ceramic capacitor placed directly at the reference pins with a larger $10-\mu \mathrm{F}$ to $47-\mu \mathrm{F}$ capacitor at the voltage reference output. In applications where the voltage reference drives multiple ADCs, use $0.1-\mu \mathrm{F}$ capacitors at each ADC.
The external capacitor filters the current transients, resulting in an average reference current. The average reference current is $110 \mu \mathrm{~A} / \mathrm{V}$ for high- and mid-power operating modes and $80 \mu \mathrm{~A} / \mathrm{V}$ for low-power operating mode. For example, with $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$, the reference input current is $110 \mu \mathrm{~A} / \mathrm{V} \times 4.096 \mathrm{~V}=451 \mu \mathrm{~A}$.

### 8.3.4 IOVDD Power Supply

The IOVDD digital supply operates in two voltage ranges: 1.65 V to 1.95 V and 2.7 V to 3.6 V . If operating IOVDD in the $1.65-\mathrm{V}$ to $1.95-\mathrm{V}$ range, connect IOVDD directly to the CAPD pin. Figure $8-9$ shows the required connection if IOVDD is operating in the $1.65-\mathrm{V}$ to $1.95-\mathrm{V}$ range. Otherwise, if operating IOVDD in the $2.7-\mathrm{V}$ to $3.6-\mathrm{V}$ range, do not connect these pins together.


Figure 8-9. IOVDD Power-Supply Connection

### 8.3.5 Modulator

The modulator is a multibit delta-sigma architecture featuring low power and outstanding dynamic range performance with very low levels of spurious tones in the frequency spectrum. The modulator shapes the quantization noise of the internal quantizer to an out-of-band frequency range where the noise is removed by the digital filter. Noise remaining within the pass-band region is thermal noise with constant density (white noise). The integrated noise within the pass band is determined by the digital filter OSR.

### 8.3.5.1 Modulator Overdrive

The modulator is an inherently stable design and, therefore exhibits predictable recovery from input overdrive. If the modulator is overdriven at the peaks of the input signal, the filter output data may or may not clip depending on the duration of the signal overdrive resulting from the data averaging of the digital filter. If the modulator is

SBAS559A - MAY 2022 - REVISED DECEMBER 2022
heavily overdriven, then the likelihood of clipped conversion data increases. Be aware the group delay of the digital filter delays the occurrence of an input overdrive event from appearing in the output data.

### 8.3.6 Digital Filter

The digital filter decimates and filters the modulator data to provide the high-resolution output data. By adjusting the amount of filtering though the OSR, trade-offs can be made between total noise and bandwidth. Increasing the OSR lowers total noise while decreasing the signal bandwidth.

As shown in Figure 8-10, the sample rate converter (SRC) receives data from the modulator prior to input to the digital filter block. See the Sample Rate Converter section for details.


Figure 8-10. Digital Filter Block Diagram
The digital filter is comprised of three sections: a variable-decimation sinc filter; a variable-coefficient, fixeddecimation FIR filter; and a programmable high-pass filter (IIR). The desired filter path is selected by the FILTER[1:0] bits of the CONFIG0 register. The sinc filter provides partially filtered data, bypassing the FIR and HPF filters and user calibration. For fully filtered data, select the FIR filter option. The IIR filter stage removes dc and low-frequency data The FIR and the combined FIR + IIR filter are routed to the user calibration block and output code clipping block. See the Offset and Gain Calibration section for details of user calibration.

### 8.3.6.1 Sinc Filter Section

The first section of the digital filter is a variable-decimation, fifth-order sinc filter ( $\sin \mathrm{x} / \mathrm{x}$ ). Modulator data are passed through the sample rate converter to the sinc filter at the nominal rate of $f_{\text {MOD }}=f_{\text {CLK }} / 4=2.048 \mathrm{MHz}$ (1.024-MHz low-power mode). The sinc filter partially filters the data for the FIR filter that produces the final frequency response. The sinc filter data are intended to be used with post-processing filters to shape the final frequency response.

Table 8-3 shows the decimation ratio and the resulting output data rate of the sinc filter. The sinc filter data rate is programmed by the DR[2:0] bits of the CONFIG0 register.

Table 8-3. Sinc Filter Data Rates

| DR[2:0] BITS |  | DATA RATE (SPS) |  |
| :---: | :---: | :---: | :---: |
|  | SINC DECIMATION RATIO (N) | HIGH- AND MID-POWER MODES | LOW-POWER MODE |
|  | 256 | 8,000 | 4,000 |
| 001 | 128 | 16,000 | 8,000 |
| 010 | 64 | 32,000 | 16,000 |
| 011 | 32 | 64,000 | 32,000 |
| 100 | 16 | 128,000 | 64,000 |

Equation 2 shows the Z-domain transfer function of the sinc filter.

$$
\begin{equation*}
H(Z)=\left[\frac{1-Z^{-N}}{N\left(1-Z^{-1}\right)}\right]^{5} \tag{2}
\end{equation*}
$$

where:

- $\mathrm{N}=$ Decimation ratio of Table 8-3

Equation 3 shows the frequency domain transfer function of the sinc filter.

$$
\begin{equation*}
|H(f)|=\left|\frac{\sin \left(\frac{\pi N \times f}{f_{M O D}}\right)}{N \sin \left(\frac{\pi \times f}{f_{M O D}}\right)}\right|^{5} \tag{3}
\end{equation*}
$$

where:

- $\mathrm{N}=$ Decimation ratio shown in Table 8-3
- $f=$ Input signal frequency
- $f_{\text {MOD }}=$ Modulator sampling frequency $=f_{\text {CLK }} / 4$ (sample rate converter disabled)

The sinc filter frequency response has notches (or zeros) occurring at the output data rate and multiples thereof. At these frequencies, the filter has zero gain. Figure $8-11$ shows the wide-band frequency response of the sinc filter and Figure $8-12$ shows details of the $-3-\mathrm{dB}$ response.


Figure 8-11. Sinc Filter Frequency Response


Figure 8-12. Sinc Filter -3-dB Response

Figure $8-13$ illustrates the sinc filter frequency response at $f_{\text {DATA }}=32 \mathrm{kSPS}$. The tones at 1 kHz and harmonics are the result of dither added to the modulator input to suppress idle tones. The frequency of the dither signal is $f_{\text {MOD }}$ divided by the combined decimation ratio shown in Table $8-4$. The rise of the noise floor at 2 kHz is resultant of modulator noise shaping. For sinc filter decimation $\mathrm{N}=64$ (data rate $=32 \mathrm{kSPS}$ ), the usable bandwidth by the use of external post filtering is 500 Hz .


Figure 8-13. FFT Output of the Sinc Filter (f${ }_{\text {DATA }}=\mathbf{3 2} \mathbf{k S P S}$ )
The sinc filter data bypasses the data scaling, clip stage, and user calibration, and as a result, the sinc filter data are scaled differently compared to the FIR filter. See the Conversion Data Format section for details of sinc filter data scaling.

### 8.3.6.2 FIR Filter Section

The second section of the digital filter is a multistage, FIR low-pass filter. Partially filtered data from the sinc filter are input to the FIR filter. The FIR filter determines the final frequency and phase response of the data. Figure 8-14 shows that the FIR filter consists of four stages.


Figure 8-14. FIR Filter
The first two FIR stages are half-band filters with decimation $=2$ for each stage. The third and fourth FIR stages determine the final frequency and phase response. Decimation is 4 and 2, for FIR stages three and four. The overall decimation ratio of the FIR filter is 32 . Unique coefficient sets in stage 3 and 4 determine linear and minimum phase filter response. The phase response is selected by the PHASE bit of the CONFIGO register. Table 8-4 lists the combined decimation ratio of the sinc and FIR filter stages and the corresponding FIR filter data rate.

Table 8-4. FIR Filter Data Rate

|  |  | DATA RATE (SPS) |  |
| :---: | :---: | :---: | :---: |
| DR[2:0] BITS | COMBINED DECIMATION RATIO | HIGH- AND MID-POWER MODES | LOW-POWER MODE |
| 000 | 8192 | 250 | 125 |
| 001 | 4096 | 500 | 250 |
| 010 | 2048 | 1000 | 500 |
| 011 | 1024 | 2000 | 1000 |
| 100 | 512 | 4000 | 2000 |

Table 8-5 lists the FIR filter coefficients and the data scaling for the linear and minimum phase coefficients.

ADS1285
www.ti.com
SBAS559A - MAY 2022 - REVISED DECEMBER 2022
Table 8-5. FIR Filter Coefficients

| COEFFICIENT | STAGE 1 | STAGE 2 | STAGE 3 |  | STAGE 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SCALE $=1 / 512$ | SCALE $=1 / 8388608$ | SCALE $=1 / 134217728$ |  | SCALE $=1 / 134217728$ |  |
|  | LINEAR PHASE | LINEAR PHASE | LINEAR PHASE | MINIMUM PHASE | LINEAR PHASE | MINIMUM PHASE |
| $\mathrm{b}_{0}$ | 3 | -10944 | 0 | 819 | -132 | 11767 |
| $\mathrm{b}_{1}$ | 0 | 0 | 0 | 8211 | -432 | 133882 |
| $\mathrm{b}_{2}$ | -25 | 103807 | -73 | 44880 | -75 | 769961 |
| $\mathrm{b}_{3}$ | 0 | 0 | -874 | 174712 | 2481 | 2940447 |
| $\mathrm{b}_{4}$ | 150 | -507903 | -4648 | 536821 | 6692 | 8262605 |
| $\mathrm{b}_{5}$ | 256 | 0 | -16147 | 1372637 | 7419 | 17902757 |
| $\mathrm{b}_{6}$ | 150 | 2512192 | -41280 | 3012996 | -266 | 30428735 |
| $\mathrm{b}_{7}$ | 0 | 4194304 | -80934 | 5788605 | -10663 | 40215494 |
| $\mathrm{b}_{8}$ | -25 | 2512192 | -120064 | 9852286 | -8280 | 39260213 |
| $\mathrm{b}_{9}$ | 0 | 0 | -118690 | 14957445 | 10620 | 23325925 |
| $\mathrm{b}_{10}$ | 3 | -507903 | -18203 | 20301435 | 22008 | -1757787 |
| $\mathrm{b}_{11}$ |  | 0 | 224751 | 24569234 | 348 | -21028126 |
| $\mathrm{b}_{12}$ |  | 103807 | 580196 | 26260385 | -34123 | -21293602 |
| $\mathrm{b}_{13}$ |  | 0 | 893263 | 24247577 | -25549 | -3886901 |
| $\mathrm{b}_{14}$ |  | -10944 | 891396 | 18356231 | 33460 | 14396783 |
| $\mathrm{b}_{15}$ |  |  | 293598 | 9668991 | 61387 | 16314388 |
| $\mathrm{b}_{16}$ |  |  | -987253 | 327749 | -7546 | 1518875 |
| $\mathrm{b}_{17}$ |  |  | -2635779 | -7171917 | -94192 | -12979500 |
| $\mathrm{b}_{18}$ |  |  | -3860322 | -10926627 | -50629 | -11506007 |
| $\mathrm{b}_{19}$ |  |  | -3572512 | -10379094 | 101135 | 2769794 |
| $\mathrm{b}_{20}$ |  |  | -822573 | -6505618 | 134826 | 12195551 |
| $\mathrm{b}_{21}$ |  |  | 4669054 | -1333678 | -56626 | 6103823 |
| $\mathrm{b}_{22}$ |  |  | 12153698 | 2972773 | -220104 | -6709466 |
| $\mathrm{b}_{23}$ |  |  | 19911100 | 5006366 | -56082 | -9882714 |
| $\mathrm{b}_{24}$ |  |  | 25779390 | 4566808 | 263758 | -353347 |
| $\mathrm{b}_{25}$ |  |  | 27966862 | 2505652 | 231231 | 8629331 |
| $\mathrm{b}_{26}$ |  |  | 25779390 | 126331 | -215231 | 5597927 |
| $\mathrm{b}_{27}$ |  |  | 19911100 | -1496514 | -430178 | -4389168 |
| $\mathrm{b}_{28}$ |  |  | 12153698 | -1933830 | 34715 | -7594158 |
| $\mathrm{b}_{29}$ |  |  | 4669054 | -1410695 | 580424 | -428064 |
| $\mathrm{b}_{30}$ |  |  | -822573 | -502731 | 283878 | 6566217 |
| $\mathrm{b}_{31}$ |  |  | -3572512 | 245330 | -588382 | 4024593 |
| $\mathrm{b}_{32}$ |  |  | -3860322 | 565174 | -693209 | -3679749 |
| $\mathrm{b}_{33}$ |  |  | -2635779 | 492084 | 366118 | -5572954 |
| $\mathrm{b}_{34}$ |  |  | -987253 | 231656 | 1084786 | 332589 |
| $\mathrm{b}_{35}$ |  |  | 293598 | -9196 | 132893 | 5136333 |
| $\mathrm{b}_{36}$ |  |  | 891396 | -125456 | -1300087 | 2351253 |
| $\mathrm{b}_{37}$ |  |  | 893263 | -122207 | -878642 | -3357202 |
| $\mathrm{b}_{38}$ |  |  | 580196 | -61813 | 1162189 | -3767666 |
| $\mathrm{b}_{39}$ |  |  | 224751 | -4445 | 1741565 | 1087392 |
| $\mathrm{b}_{40}$ |  |  | -18203 | 22484 | -522533 | 3847821 |
| $\mathrm{b}_{41}$ |  |  | -118690 | 22245 | -2490395 | 919792 |
| $\mathrm{b}_{42}$ |  |  | -120064 | 10775 | -688945 | -2918303 |
| $\mathrm{b}_{43}$ |  |  | -80934 | 940 | 2811738 | -2193542 |
| $\mathrm{b}_{44}$ |  |  | -41280 | -2953 | 2425494 | 1493873 |
| $\mathrm{b}_{45}$ |  |  | -16147 | -2599 | -2338095 | 2595051 |
| $\mathrm{b}_{46}$ |  |  | -4648 | -1052 | -4511116 | -79991 |
| $\mathrm{b}_{47}$ |  |  | -874 | -43 | 641555 | -2260106 |
| $\mathrm{b}_{48}$ |  |  | -73 | 214 | 6661730 | -963855 |
| $\mathrm{b}_{49}$ |  |  | 0 | 132 | 2950811 | 1482337 |
| $\mathrm{b}_{50}$ |  |  | 0 | 33 | -8538057 | 1480417 |
| $\mathrm{b}_{51}$ |  |  | 0 | 0 | -10537298 | -586408 |
| $\mathrm{b}_{52}$ |  |  |  |  | 9818477 | -1497356 |

ADS1285
Table 8-5. FIR Filter Coefficients (continued)

| COEFFICIENT | STAGE 1 | STAGE 2 | STAGE 3 |  | STAGE 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SCALE $=1 / 512$ | SCALE $=1 / 8388608$ | SCALE $=1 / 134217728$ |  | SCALE $=1 / 134217728$ |  |
|  | LINEAR PHASE | LINEAR PHASE | LINEAR PHASE | MINIMUM PHASE | LINEAR PHASE | MINIMUM PHASE |
| $\mathrm{b}_{53}$ |  |  |  |  | 41426374 | -168417 |
| $\mathrm{b}_{54}$ |  |  |  |  | 56835776 | 1166800 |
| $\mathrm{b}_{55}$ |  |  |  |  | 41426374 | 644405 |
| $\mathrm{b}_{56}$ |  |  |  |  | 9818477 | -675082 |
| $\mathrm{b}_{57}$ |  |  |  |  | -10537298 | -806095 |
| $\mathrm{b}_{58}$ |  |  |  |  | -8538057 | 211391 |
| $\mathrm{b}_{59}$ |  |  |  |  | 2950811 | 740896 |
| $\mathrm{b}_{60}$ |  |  |  |  | 6661730 | 141976 |
| $\mathrm{b}_{61}$ |  |  |  |  | 641555 | -527673 |
| $\mathrm{b}_{62}$ |  |  |  |  | -4511116 | -327618 |
| $\mathrm{b}_{63}$ |  |  |  |  | -2338095 | 278227 |
| $\mathrm{b}_{64}$ |  |  |  |  | 2425494 | 363809 |
| $\mathrm{b}_{65}$ |  |  |  |  | 2811738 | -70646 |
| $\mathrm{b}_{66}$ |  |  |  |  | -688945 | -304819 |
| $\mathrm{b}_{67}$ |  |  |  |  | -2490395 | -63159 |
| $\mathrm{b}_{68}$ |  |  |  |  | -522533 | 205798 |
| $\mathrm{b}_{69}$ |  |  |  |  | 1741565 | 124363 |
| $\mathrm{b}_{70}$ |  |  |  |  | 1162189 | -107173 |
| $\mathrm{b}_{71}$ |  |  |  |  | -878642 | -131357 |
| $\mathrm{b}_{72}$ |  |  |  |  | -1300087 | 31104 |
| $\mathrm{b}_{73}$ |  |  |  |  | 132893 | 107182 |
| $\mathrm{b}_{74}$ |  |  |  |  | 1084786 | 15644 |
| $\mathrm{b}_{75}$ |  |  |  |  | 366118 | -71728 |
| $\mathrm{b}_{76}$ |  |  |  |  | -693209 | -36319 |
| $\mathrm{b}_{77}$ |  |  |  |  | -588382 | 38331 |
| $\mathrm{b}_{78}$ |  |  |  |  | 283878 | 38783 |
| $\mathrm{b}_{79}$ |  |  |  |  | 580424 | -13557 |
| $\mathrm{b}_{80}$ |  |  |  |  | 34715 | -31453 |
| $\mathrm{b}_{81}$ |  |  |  |  | -430178 | -1230 |
| $\mathrm{b}_{82}$ |  |  |  |  | -215231 | 20983 |
| $\mathrm{b}_{83}$ |  |  |  |  | 231231 | 7729 |
| $\mathrm{b}_{84}$ |  |  |  |  | 263758 | -11463 |
| $\mathrm{b}_{85}$ |  |  |  |  | -56082 | -8791 |
| $\mathrm{b}_{86}$ |  |  |  |  | -220104 | 4659 |
| $\mathrm{b}_{87}$ |  |  |  |  | -56626 | 7126 |
| $\mathrm{b}_{88}$ |  |  |  |  | 134826 | -732 |
| $\mathrm{b}_{89}$ |  |  |  |  | 101135 | -4687 |
| $\mathrm{b}_{90}$ |  |  |  |  | -50629 | -976 |
| $\mathrm{b}_{91}$ |  |  |  |  | -94192 | 2551 |
| $\mathrm{b}_{92}$ |  |  |  |  | -7546 | 1339 |
| $\mathrm{b}_{93}$ |  |  |  |  | 61387 | -1103 |
| $\mathrm{b}_{94}$ |  |  |  |  | 33460 | -1085 |
| $\mathrm{b}_{95}$ |  |  |  |  | -25549 | 314 |
| $\mathrm{b}_{96}$ |  |  |  |  | -34123 | 681 |
| $\mathrm{b}_{97}$ |  |  |  |  | 348 | 16 |
| $\mathrm{b}_{98}$ |  |  |  |  | 22008 | -349 |
| $\mathrm{b}_{99}$ |  |  |  |  | 10620 | -96 |
| $\mathrm{b}_{100}$ |  |  |  |  | -8280 | 144 |
| $\mathrm{b}_{101}$ |  |  |  |  | -10663 | 78 |
| $\mathrm{b}_{102}$ |  |  |  |  | -266 | -46 |
| $\mathrm{b}_{103}$ |  |  |  |  | 7419 | -42 |
| $\mathrm{b}_{104}$ |  |  |  |  | 6692 | 9 |
| $\mathrm{b}_{105}$ |  |  |  |  | 2481 | 16 |

Table 8-5. FIR Filter Coefficients (continued)

| COEFFICIENT | STAGE 1 | STAGE 2 | STAGE 3 |  | STAGE 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SCALE $=1 / 512$ | SCALE $=1 / 8388608$ | SCALE $=1 / 134217728$ |  | SCALE $=1 / 134217728$ |  |
|  | LINEAR PHASE | LINEAR PHASE | LINEAR PHASE | MINIMUM PHASE | LINEAR PHASE | MINIMUM PHASE |
| $\mathrm{b}_{106}$ |  |  |  |  | -75 | 0 |
| $\mathrm{b}_{107}$ |  |  |  |  | -432 | -4 |
| $\mathrm{b}_{108}$ |  |  |  |  | -132 | 0 |
| $\mathrm{b}_{109}$ |  |  |  |  | 0 | 0 |

Figure $8-15$ shows the FIR pass-band frequency response to $0.375 \times \mathrm{f}_{\text {DATA }}$ with $\pm 0.003-\mathrm{dB}$ pass-band ripple. Figure $8-16$ shows the pass-band, transition-band, and stop-band performance from 0 Hz to f DATA. The filter is designed for $-135-\mathrm{dB}$ stop-band attenuation at the Nyquist frequency.


Figure 8-15. FIR Filter Pass-Band Response


Figure 8-16. FIR Filter Transition Band Response

As with many sampled systems, the filter response repeats at multiples of the modulator sample rate ( $\mathrm{f}_{\mathrm{MOD}}$ ). The filter response repeats at frequencies $=N \times f_{M O D} \pm f_{0}$, where $N=1,2$, and so on, and $f_{0}=$ filter pass-band). These frequencies, if not filtered and are otherwise present in the signal, fold back (or alias) into the pass-band causing errors. A low-pass input filter reduces the aliasing error. For a band-limited signal typical of many geophones, a single-pole filter at the PGA output is sufficient to suppress the aliasing frequencies.

### 8.3.6.3 Group Delay and Step Response

The FIR filter offers linear and minimum phase filter options. The pass-band, transition band, and stop-band responses of the linear and minimum phase filters are the same but differ in phase and step response behavior.

### 8.3.6.3.1 Linear Phase Response

A linear phase filter has the unique property that the delay from input to output is constant across all input frequencies (that is, constant group delay). The constant delay property is independent of the nature of the input signal (impulse or swept-tone), and therefore the phase is linear across frequency, which can be important when analyzing multitone signals. However, as depicted in Figure 8-17, the group delay is longer for the linear phase filter compared to minimum phase. For both the linear and minimum filters, fully settled data are available 62 conversions after a step input change occurs.


Figure 8-17. FIR Step Response

### 8.3.6.3.2 Minimum Phase Response

The minimum phase filter provides a short group delay for data from filter input to filter output. Figure 8-18 shows the group delay for minimum and linear phase filters. The group delay of the minimum phase filter is a function of signal frequency. The PHASE bit of the CONFIG0 register programs the filter phase.


Figure 8-18. FIR Group Delay ( $\mathrm{f}_{\text {DATA }}=\mathbf{5 0 0}$ SPS)

### 8.3.6.4 HPF Stage

The last stage of the digital filter is the high-pass filter (HPF). The high-pass filter is implemented as a firstorder, IIR filter. The high-pass filter removes dc and low frequencies from the data. The HPF is enabled by programming the FILTR[1:0] bits $=11 \mathrm{~b}$ of the CONFIG0 register.
Equation 4 shows the $z$-domain transfer function of the filter:

$$
\begin{equation*}
H(z)=\frac{2-a}{2} \frac{1-z^{-1}}{1-(1-a) z^{-1}} \tag{4}
\end{equation*}
$$

where:

$$
a=\frac{2 \sin \left(\omega_{N}\right)}{\cos \left(\omega_{N}\right)+\sin \left(\omega_{N}\right)}
$$

- $\omega_{N}=\pi \times f_{C} / f_{\text {DATA }}$ (normalized corner frequency, radians)
- $\mathrm{f}_{\mathrm{C}}=$ Corner frequency (Hz)
- $\mathrm{f}_{\text {DATA }}=$ Output data rate $(\mathrm{Hz})$

Be aware the corner frequency programming is a function of $f_{\text {DATA }}$. As shown by Equation 5 , the value written to the HPF1, HPF0 registers is value a, computed by Equation 4, $\times 2^{16}$.

$$
\begin{equation*}
\operatorname{HPF}[15: 0]=a \times 2^{16} \tag{5}
\end{equation*}
$$

Table 8-6 shows examples of the high-pass filter programming.
Table 8-6. High-Pass Filter Value Examples

| HPF[15:0] | $\mathbf{f c}_{\mathbf{C}}(\mathbf{H z})$ | $\mathbf{f}_{\text {DATA }}$ (SPS) |
| :---: | :---: | :---: |
| 0332h | 0.5 | 250 |
| 0332h | 1.0 | 500 |
| 019Ah | 1.0 | 1000 |

The HPF accumulates data to perform the high-pass function. Similar to the operation of an analog HPF after a dc step change is applied to the input, the filter takes time to accumulate data to remove dc from the signal. The lower the corner frequency, the longer the filter takes to settle.
To shorten the HPF settling time, the offset register is used as a seed value for the HPF accumulator. The accumulator is loaded with the offset register each time the HPF state is changed from disabled to enabled. The offset register can be preset with an estimated value, or a calibrated value if the dc level is known. To improve accuracy, scale the offset value by the inverse value of GAIN[3:0] / 400000h. The normal offset operation is disabled when the HPF is enabled.

To initialize the HPF accumulator with the OFFSET[2:0] registers:

1. Disable the HPF.
2. Write the desired value to the OFFSET[2:0] registers.
3. Enable the HPF. OFFSET[2:0] is loaded to the HPF data accumulator.
4. The HPF tracks the remaining dc value from the signal.

Subsequent writes to the OFFSET[2:0] registers are ignored. To reload the contents of the OFFSET[2:0] registers to the HPF, disable and re-enable the HPF.

### 8.3.7 Clock Input

A clock signal is required for operation. The clock signal is applied to the CLK pin at $\mathrm{f}_{\text {CLK }}=8.192 \mathrm{MHz}$ for highand mid-power modes and 4.096 MHz for low-power mode. As with many precision data converters, a low-jitter clock is required to achieve data sheet performance. Avoid the use of R-C clock oscillators. A crystal-based clock source is recommended. Avoid ringing on the clock signal by placing a series resistor in the clock PCB trace to source-terminate. Keep the clock signal routed away from other clock signals, input pins, and analog components.

### 8.3.8 GPIO

The ADC provides two general-purpose I/O (GPIO) pins that can be used as digital inputs or outputs. The GPIO voltage levels are IOVDD and DGND. Figure 8-19 illustrates the GPIO block diagram.
The GPIOs are programmed by the GPIO register. The GPIOs are programmed as an input or output by the GPIOx_DIR bits. The GPIO state is read or written by the GPIOx_DAT bits. When programmed as an output, reading the GPIOx_DAT bits returns the register bit value previously written. If the GPIOs are unused, terminate the GPIOs with pulldown resistors to prevent the pins from floating.


Figure 8-19. GPIO Operation

### 8.4 Device Functional Modes

### 8.4.1 Power Modes

There are three power-resolution modes offering trade-offs between power consumption and dynamic range. The modes are high power, mid power, and low power. See the Noise Performance section for details of noise performance. The MODE[1:0] bits of the CONFIG0 register selects the power mode. The clock frequency for low-power mode is 4.096 MHz (half-speed clock); therefore, the output data rates are also scaled by one half.

### 8.4.2 Power-Down Mode

Power-down is engaged by taking the PWDN pin low, or by software control, by sending the STANDBY command. To exit power-down, take PWDN high or send the WAKEUP command to exit software power-down (with the clock running). Power-down disables the analog circuit; however, the digital LDO (CAPD pin) remains biased, drawing a small bias current from IOVDD. In comparison, software power-down draws larger IOVDD bias current. In both power-down modes, the ac signals of the digital outputs are stopped but remain driven high or low. The digital inputs must not be allowed to float; otherwise, leakage current can flow from the IOVDD supply. Reset the ADC if the clock is interrupted in power-down. Synchronization is lost in power-down; therefore, resynchronize the ADC.

### 8.4.3 Reset

The ADC is reset by three methods: power-on reset (POR), the RESET pin, or the RESET command. Poweron reset occurs when the power-supply voltages cross the respective thresholds. See Power-Up Switching Characteristics for details. To reset the ADC by pin, drive RESET low for at least two f fLK cycles and return high for reset. By command, reset takes effect on the next rising $\mathrm{f}_{\text {CLK }}$ edge after the eighth rising edge of SCLK of the reset command. At reset, the filter is restarted and the user registers reset to default. Reset timing is illustrated in Figure 6-5.

### 8.4.4 Synchronization

The ADC is synchronized by the SYNC pin or by the SYNC command, resulting in restart of the digital filter cycle. Synchronization by the pin occurs on the next rising edge of CLK after SYNC is taken high on the falling edge of CLK. Synchronization by the SYNC command occurs on the rising edge of CLK following the eighth bit of the command.

The following results in loss of synchronization:

- Power-up cycle, ADC reset, or when hardware or software power down modes are entered
- The following mode changes:
- DR[2:0] (data rate)
- PHASE (filter phase)
- MODE[1:0] (power mode)
- SYNC (synchronization mode)
- SRC[1:0] (sample rate converter enabled or disabled)

There are two synchronization control modes: pulse sync and continuous sync. The synchronization mode is programmed by the SYNC bit of the ID/SYNC register.

### 8.4.4.1 Pulse-Sync Mode

The pulse-sync mode unconditionally synchronizes the ADC on the rising edge of SYNC. When synchronized, the internal filter memory is reset, DRDY goes high, and the filter cycle restarts. The following 63 DRDY periods are disabled to allow for digital filter settling. DRDY asserts low when the conversion data are ready. See Figure 6-4 for synchronization timing details.

### 8.4.4.2 Continuous-Sync Mode

The continuous-sync mode offers the option of accepting a continuous clock signal to the SYNC pin. The ADC compares the period of the SYNC clock signal to $N$ periods of the $\overline{\text { DRDY }}$ signal to qualify resynchronization. Initially, the first SYNC positive edge synchronizes the ADC. Resynchronization occurs only when the time period between rising edges of SYNC over $N$ multiple DRDY periods differ by at least $\pm$ one f fLK cycle, where $N=1,2,3$ and so on. Otherwise, the SYNC clock period is in synchronization with the existing DRDY pulses, so no resynchronization occurs. Be aware the continuous sync mode cannot be used when the sample rate converter is enabled.

After synchronization, $\overline{\text { DRDY }}$ continues to pulse; however, data are held low for 63 data periods to allow for the digital filter to settle. See Figure 6-4 for the DRDY behavior. Because of the initial delay of the digital filter, the SYNC input signal and the DRDY pulses exhibit an offset time. The offset time is a function of the data rate.

### 8.4.5 Sample Rate Converter

The sample rate converter (SRC) compensates clock frequency error by resampling the modulator data at a new rate set by the compensation factor written to the SRC registers. The frequency compensation range is $\pm 244$ ppm with $7.45-\mathrm{ppb}\left(1 / 2^{27}\right)$ resolution.

Clock frequency error is compensated by writing a value to the SCR0 and SRC1 registers. The register value is in 2's-complement format for positive and negative frequency error compensation. Positive register data values decrease the data rate frequency (increases the period). The new data rate frequency is observed by the frequency of the $\overline{\mathrm{DRDY}}$ signal.
Table 8-7 shows example values of frequency compensation. 8000h disables the sample rate converter. 0000 h passes the data through with no compensation but adds an $8 / \mathrm{f}_{\text {CLK }}$ delay to the time delay of SYNC input to the DRDY pulses.

Table 8-7. Example SRC Values

| SRC[15:0] VALUE | COMPENSATION FACTOR |
| :---: | :---: |
| 7FFFh | $\left(1-32,767 / 2^{27}\right) \times f_{\text {DATA }}$ |
| 0001 h | $\left(1-1 / 2^{27}\right) \times f_{\text {DATA }}$ |
| 0000 h | $1 \times \mathrm{f}_{\text {DATA }}$ |
| 7 FFFh | $\left(1+1 / 2^{27}\right) \times \mathrm{f}_{\text {DATA }}$ |
| 8001 h | $\left(1+32,767 / 2^{27}\right) \times \mathrm{f}_{\text {DATA }}$ |
| 8000 h | $1 \times \mathrm{f}_{\text {DATA }}(\mathrm{SRC}$ disabled $)$ |

Resynchronize the ADC after the sample rate converter is enabled or disabled.

Because the SRC is a digital function, operation is deterministic without error. The SRC trim value can be written all at the same time, or written incrementally up to a target value to minimize the step change of frequency. Use the multibyte command operation to write to the SRC registers and complete the write operation 256 CLK cycles before the DRDY falling edge. This procedure loads the high and low bytes simultaneously before they are internally processed. See Figure 6-7 for details.

### 8.4.6 Offset and Gain Calibration

The ADC integrates calibration registers to correct offset and gain errors. As shown in Equation 6 and Figure 8-20, the 24-bit offset value (OFFSET[23:0]) is subtracted from the filter data before multiplication by the 24-bit gain value (GAIN[23:0]), divided by 400000 h . The data are clipped to 32 bits to yield the final output. The offset operation is bypassed when the high-pass filter is enabled.

$$
\begin{equation*}
\text { Output }=\left(\text { Input }- \text { OFFSET[23:0]) } \cdot \frac{\text { GAIN[23:0] }}{400000 \mathrm{~h}}\right. \tag{6}
\end{equation*}
$$



Figure 8-20. Calibration Block Diagram

### 8.4.6.1 OFFSET Register

Offset correction is by a 24-bit word consisting of three 8-bit registers (high address is the MSB). The offset value is left-justified to align to the 32-bit data. The offset value is 2 's-complement coding with a maximum positive value of 7FFFFFh and a maximum negative value of 800000 h . OFFSET is subtracted from the conversion data; see Table 8-8. Offset error is corrected by the offset calibration command with the input-short multiplexer option, or by collecting shorted-input ADC data and writing the value to the registers.
Although the offset correction range is from -FS to +FS , the sum of offset and gain correction must not exceed $106 \%$ of the uncalibrated range.

When the high-pass filter is enabled, offset correction is disabled. The offset value is used instead as a starting value to shorten the high-pass filter settling time. To reload the offset value to the HPF, disable and re-enable the high-pass filter. See the HPF Stage section for more details.

Table 8-8. Offset Calibration Values

| OFFSET[31:0] | CALIBRATED OUTPUT CODE $^{(1)}$ |
| :---: | :---: |
| 00007 Fh | FFFF8100h |
| 000000 h | 00000000 h |
| FFFF7Fh | 00008100 h |

(1) Ideal code value with no offset error.

### 8.4.6.2 GAIN Register

Gain correction is through a 24-bit word, consisting of three 8-bit registers (high address $=$ MSB). The gain value is 24 bits, coded in straight binary and normalized to 1.0 for GAIN[23:0] equal to 400000 h . With a calibration signal applied, gain error is calibrated by either the gain calibration command, or by collecting ADC data and writing a computed value to the gain registers. Table 8-9 lists examples of the GAIN[23:0] register values. Although the range of gain values can be much greater or less than 1, the sum of offset and gain correction must not exceed $106 \%$ of the uncalibrated range.

Table 8-9. Gain Calibration Values

| GAIN[31:0] | GAIN CORRECTION FACTOR |
| :---: | :---: |
| 433333 h | 1.05 |
| 400000 h | 1.00 |
| $3 C C C C C h$ | 0.95 |

### 8.4.6.3 Calibration Procedure

ADC calibration can be performed using the ADC calibration commands or by performing manual calibration. The calibration procedure is as follows:

1. Select the PGA or buffer operation, input channel, and PGA gain condition for calibration.
2. Preset the OFFSET register $=000000 \mathrm{~h}$ and the GAIN register $=400000 \mathrm{~h}$.
3. Disable the high-pass filter for offset calibration. Short the inputs to the system, or use the input MUX to provide the input short. A system-level input short can yield more accurate calibration. After the input settles, either send the OFSCAL command or perform a manual calibration.
a. OFSCAL command. After the command is sent, DRDY is driven low 81 conversion periods later to indicate calibration is complete. The OFFSET register is updated with the new calibration value. As shown in Figure 8-21, the first data output uses the new OFFSET value.
b. Manual calibration. Wait at least 64 conversions for the digital filter to settle then average a number of data points to improve calibration accuracy. Write the value to the 24-bit OFFSET register.
4. Apply a gain calibration voltage. After the input settles, either send the GANCAL command or perform a manual calibration.
a. GANCAL command. Apply a positive dc full-scale calibration voltage. After the command is sent, DRDY is driven low 81 conversion periods later to indicate calibration is complete. The ADC calculates GAIN such that the full-scale code is equal to the applied calibration signal. As shown in Figure 8-21, the first data output uses the new GAIN value.
b. Manual calibration. Apply an ac signal coherent to the sample rate or dc calibration signal that are slightly below full-scale (for example, 2.4 V for gain $=1$ ). Using a calibration signal less than full-scale range prevents clipped output codes that otherwise lead to incorrect calibration. Wait 64 conversions for the digital filter to settle then average a number of data points to improve calibration accuracy. For ac-signal calibration, use a number of coherent signal periods to compute the RMS value.

Equation 7 computes the value of GAIN for manual calibration.

$$
\begin{equation*}
\operatorname{GAIN}[23: 0]=400000 \mathrm{~h} \cdot \frac{\text { Expected Output Code }}{\text { Actual Output Code }} \tag{7}
\end{equation*}
$$



Figure 8-21. Calibration Command

### 8.5 Programming

### 8.5.1 Serial Interface

Conversion data are read and ADC configuration is made through the SPI-compatible serial interface. The interface consists of four signals: $\overline{C S}$, SCLK, DIN, and DOUT. DRDY asserts low when conversion data are ready. The serial interface is passive (peripheral mode), where the serial clock (SCLK) is an input. The ADC operates in SPI mode 0 , where CPOL $=0$ and CPHA $=0$. In mode 0 , SCLK idles low and data are updated on the SCLK falling edges and are read on the SCLK rising edges.

### 8.5.1.1 Chip Select ( $\overline{C S}$ )

$\overline{C S}$ is an active-low input that selects the serial interface for communication. A communication frame is started by taking $\overline{\mathrm{CS}}$ low and is ended by taking $\overline{\mathrm{CS}}$ high. Because only one command per frame is permitted, toggle $\overline{\mathrm{CS}}$ between commands. Taking $\overline{\mathrm{CS}}$ high before the command is completed resets the operation and blocks further SCLK inputs. CS high forces DOUT to a high-impedance state. DRDY remains active regardless of the state of $\overline{\mathrm{CS}}$.

### 8.5.1.2 Serial Clock (SCLK)

SCLK is the serial clock input that shifts data into and out of the ADC. The ADC latches DIN data on the rising edge of SCLK. DOUT data are shifted out on the falling edge of SCLK. Keep SCLK low when not active. The SCLK pin is a Schmidt-trigger input that reduces sensitivity to SCLK noise. However, keep the SCLK signal as noise free as possible to prevent inadvertent shifting of the data.

### 8.5.1.3 Data Input (DIN)

DIN is used to input data to the ADC. DIN data are latched on the rising edge of SCLK.

### 8.5.1.4 Data Output (DOUT)

DOUT is the data output pin. Data are shifted out on the falling edge of SCLK and are latched by the host on the rising edge. Because the conversion data MSB is on DOUT when $\overline{\mathrm{CS}}$ is driven low ( $\overline{\mathrm{DRDY}}$ low), the MSB of the data is read on the first rising edge of SCLK. Minimize trace length to reduce load capacitance on the pin. Place a series termination resistor close to the pin to terminate the PCB trace impedance. Taking $\overline{\mathrm{CS}}$ high forces DOUT to a high-impedance state.

### 8.5.1.5 Data Ready ( $\overline{\mathrm{DRDY}})$

$\overline{\mathrm{DRDY}}$ is an active-low output that indicates conversion data are ready. $\overline{\mathrm{DRDY}}$ is active regardless of the state of CS. DRDY is driven high on the first falling edge of SCLK, regardless if data is being read or a command is input. As shown in Figure 8-22, if data are not retrieved, DRDY pulses high for eight $\mathrm{f}_{\mathrm{CLK}}$ periods.


Figure 8-22. DRDY With No Data Retrieval

ADS1285

### 8.5.2 Conversion Data Format

As listed in Table 8-10, the conversion data are coded in 32-bit, 2's-complement format to represent positive and negative numbers. If desired, the data read operation can be shortened to 24 bits by taking $\overline{\mathrm{CS}}$ high. Data scaling from the Sinc filter is dependent on the value of $\mathrm{V}_{\text {REF }}$ and whether PGA or buffer operation.

Table 8-10. Output Data Format

| $\mathrm{V}_{\text {IN }}(\mathrm{V})$ | CONVERSION CODES ${ }^{(1)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | FIR FILTER$\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}, 4.096 \mathrm{~V} \text { or } 5 \mathrm{~V}$ | SINC FILTER ${ }^{(2)}$ |  |  |
|  |  | $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$ | $\mathrm{V}_{\text {REF }}=4.096 \mathrm{~V}$ | $\mathrm{V}_{\text {REF }}=5 \mathrm{~V}$ |
| $\geq 2.5 \mathrm{~V} \times\left(2^{31}-1\right) / 2^{31} /$ Gain | 7FFFFFFFh | 3FFFFFFFFh | 3A980000h | 30000000h |
| $2.5 \mathrm{~V} /\left(\right.$ Gain $\left.\times\left(2^{31}-1\right)\right)$ | 00000001h | <00000001h | <00000001h | <00000001h |
| 0 | 00000000h | 00000000h | 00000000h | 00000000h |
| $-2.5 \mathrm{~V} /\left(\right.$ Gain $\left.\times 2^{31}\right)$ | FFFFFFFFh | >FFFFFFFFFh | >FFFFFFFFFh | >FFFFFFFFFh |
| $\leq-2.5 \mathrm{~V} / \mathrm{Gain}$ | 80000000h | C0000000h | C5680000h | D0000000h |

(1) Excluding the effects of reference voltage error, noise, linearity, offset, and gain errors.
(2) In buffer operation when $\mathrm{V}_{\mathrm{REF}}=4.096 \mathrm{~V}$ or 5 V , the data from the sinc filter are scaled $66.6 \%$ compared to PGA mode. Because of the relatively low value of OSR, full 32-bit resolution is not available in sinc filter operation. When overdriven, the sinc filter continues to output code values beyond nominal $\pm$ full-scale until the point of modulator saturation.

### 8.5.3 Commands

Table 8-11 lists the commands for the ADC. Most commands are one byte in length. However, the number of bytes for the register read and write commands depend on the amount of register data specified in the command.

Table 8-11. Command Descriptions

| MNEMONIC | TYPE | DESCRIPTION | BYTE 1 $^{(1)}$ | BYTE 2 |
| :--- | :--- | :--- | :--- | :---: |
| WAKEUP | Control | Wake from standby mode or NOP | $0000000 \times(00 \mathrm{~h}$ or 01h $)$ | - |
| STANDBY | Control | Enter standby (software power-down mode) | $0000001 \times(02 \mathrm{~h}$ or 03h) | - |
| SYNC | Control | Synchronize | $0000010 \times(04 \mathrm{~h}$ or 5 h$)$ | - |
| RESET | Control | Reset | $0000011 \times(06 \mathrm{~h}$ or 07 h$)$ | - |
| RDATA | Data | Read conversion data | $00010010(12 \mathrm{~h})$ | - |
| RREG | Register | Read $n n n n$ registers beginning at address $r r r r$ | $0010 r r r r(20 \mathrm{~h}+r r r r)^{(2)}$ | $0000 \mathrm{nnnn}(00 \mathrm{~h}+n n n n)^{(3)}$ |
| WREG | Register | Write $n n n n$ registers beginning at address $r r r r$ | $0100 r r r(40 \mathrm{~h}+r r r)^{(2)}$ | $0000 n n n n(00 \mathrm{~h}+n n n n)^{(3)}$ |
| OFSCAL | Calibration | Offset calibration | $01100000(60 \mathrm{~h})$ | - |
| GANCAL | Calibration | Gain calibration | $01100001(61 \mathrm{~h})$ | - |

(1) $x=$ Don't care.
(2) $\quad$ rrrr $=$ Starting address for register read and write commands.
(3) $n n n n=$ Number of registers to be read or written -1 . For example, to read or write three registers, $n n n n=2$.

### 8.5.3.1 Single Byte Command

Figure $8-23$ shows the general format of a single byte command (for the response bytes of the RDATA command, see the RDATA command).


Figure 8-23. Single Byte Command Format

SBAS559A - MAY 2022 - REVISED DECEMBER 2022

### 8.5.3.2 WAKEUP: Wake Command

The WAKEUP command exits standby mode to resume normal operation. If the ADC is already powered, the command is no operation (NOP). When exiting standby mode, the ADC requires resynchronization. See the Power-Down Mode section for details of power-down mode.

### 8.5.3.3 STANDBY: Software Power-Down Command

The STANDBY command enters the software power-down mode. The ADC exits software power-down mode by the WAKEUP command. See the Power-Down Mode section for details of power-down mode.

### 8.5.3.4 SYNC: Synchronize Command

The SYNC command synchronizes the ADC. Synchronization occurs at the eighth bit of the SYNC command byte. When synchronized, the current conversion is stopped and restarted. In order to synchronize multiple ADCs by software command, send the command simultaneously to all devices. The SYNC pin must be high when using the command. See the Synchronization section for details of synchronization.

### 8.5.3.5 RESET: Reset Command

The RESET command resets the ADC. See the Reset section for details of the reset operation.

### 8.5.3.6 Read Data Direct

There are two methods in which to read conversion data: read data direct and read data by command.
Read data direct does not require a command, instead after $\overline{\mathrm{DRDY}}$ falls low, simply apply SCLK to read the data. Figure $8-24$ shows the read data direct operation. When $\overline{\text { DRDY }}$ falls low, take $\overline{\mathrm{CS}}$ low to start the read operation. $\overline{\mathrm{CS}}$ low causes DOUT to transition from tri-state mode to the output of the data MSB. Data are read on the rising edge of SCLK and updated on the falling edge of SCLK. DRDY returns high on the first falling edge of SCLK. DOUT is low after 32 data bits are read. To read the same data again before new data are available, use the RDATA command.

Keep DIN low when reading conversion data. If the RDATA (read conversion data) or RREG (read register data) command is sent, output data are interrupted in response to the command. If DRDY falls low during the read operation, the new data are lost unless a minimum of three bytes of the old data are read.


Figure 8-24. Read Data Direct

### 8.5.3.7 RDATA: Read Conversion Data Command

The RDATA command (Figure 8-25) is useful to re-read data within the same conversion period or to read data interrupted by a read register command. In both cases, $\overline{\text { DRDY }}$ is high because $\overline{\text { DRDY }}$ is driven high on the first SCLK of the previous operation. If $\overline{\mathrm{DRDY}}$ is high, the first output byte is zero followed by data. If low, the first output byte is byte 1 of the conversion data, which is restarted for output byte 2 .

ADS1285
www.ti.com


Figure 8-25. Read Conversion Data by Command

### 8.5.3.8 RREG: Read Register Command

The RREG command reads register data. The command is comprised of two bytes followed by output of the designated number of register bytes. The ADC auto-increments the address up to the number of registers specified in byte 2 of the command. The incrementing address does not wrap. The first byte of the command is the opcode added to the register starting address, and the second byte is the number of registers to read minus one.

- First command byte: 0010 rrrr, where $r$ rrr is the starting register address
- Second command byte: 0000 nnnn, where nnnn is the number of registers to read minus one

Figure $8-26$ shows an example of a three-register read operation starting at register address 01 h . The first register data appears on DOUT at the 16th falling edge of SCLK. The data are latched on the rising edge of SCLK.


Figure 8-26. Read Register Data

### 8.5.3.9 WREG: Write Register Command

The WREG command is used to write register data. The command is two bytes followed by the designated number of register bytes to be written. The ADC auto-increments the address up to the number of registers specified in the command. The incrementing address does not wrap. The first byte of the command is the opcode added to the register starting address, and the second byte is the number of registers to write minus one.

First command byte: 0100 rrrr , where $r$ rrr is the starting address of the first register.
Second command byte: 0000 nnnn, where nnnn is the number of registers to write minus one.
Data bytes: Depending on the number of registers specified.

Figure 8-27 shows an example of a three-register write operation starting at register address 01 h .


Figure 8-27. Write Register Data

### 8.5.3.10 OFSCAL: Offset Calibration Command

The OFSCAL command performs offset calibration. See the Calibration Procedure section for details of operation.

### 8.5.3.11 GANCAL: Gain Calibration Command

The GANCAL command performs a gain calibration. See the Calibration Procedure section for details of operation.

### 8.6 Register Map

Collectively, the registers contain all the information needed to configure the device (such as data rate, filter mode, specific reference voltage, and so on). The registers are accessed by the read and write commands (RREG and WREG). Registers can be accessed individually, or accessed in multiples given by the number of registers specified in the command field.
Changes made to certain register bits result in a filter reset, thus requiring resynchronization of the ADC. See the Synchronization section for details.

Table 8-12. Register Map

| ADDRESS | REG LINK | RESET | BIT 7 | BIT 6 | BIT 5 | BIT 4 | BIT 3 | BIT 2 | BIT 1 | BIT 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 00h | ID/SYNC | xxxx0000b | REVID[3:0] |  |  |  | DEVID[2:0] |  |  | SYNC |
| 01h | CONFIG0 | 00010010b | MODE[1:0] |  | DR[2:0] |  |  | PHASE | FILTR[1:0] |  |
| 02h | CONFIG1 | 00000000b | MUX[2:0] |  |  | REF[1:0] |  | GAIN[2:0] |  |  |
| 03h | HPF0 | 00110010h | HPF[7:0] |  |  |  |  |  |  |  |
| 04h | HPF1 | 00000011b | HPF[15:8] |  |  |  |  |  |  |  |
| 05h | OFFSET0 | 00000000b | OFFSET[7:0] |  |  |  |  |  |  |  |
| 06h | OFFSET1 | 00000000b | OFFSET[15:8] |  |  |  |  |  |  |  |
| 07h | OFFSET2 | 00000000b | OFFSET[23:16] |  |  |  |  |  |  |  |
| 08h | GAIN0 | 00000000b | GAIN[7:0] |  |  |  |  |  |  |  |
| 09h | GAIN1 | 00000000b | GAIN[15:8] |  |  |  |  |  |  |  |
| OAh | GAIN2 | 01000000b | GAIN[23:16] |  |  |  |  |  |  |  |
| OBh | GPIO | 000xx000b | RESERVED |  |  | GPIO1_DAT | GPIO0_DAT | GPIO1_DIR | GPIO0_DIR | RESERVED |
| OCh | SRC0 | 00000000b | SRC[7:0] |  |  |  |  |  |  |  |
| ODh | SRC1 | 10000000b | SRC[15:8] |  |  |  |  |  |  |  |

### 8.6.1 Register Descriptions

Table 8-13 shows the register access codes for the ADS1285 registers.
Table 8-13. ADS1285 Access Codes

| Access Type | Code | Description |
| :--- | :--- | :--- |
| R | R | Read |
| R-W | R/W | Read or write |
| W | W | Write |
| $-n$ |  | Value after reset or the default value |

ADS1285

### 8.6.1.1 ID/SYNC: Device ID, SYNC Register (Address = 00h) [Reset = xxxx0000b]

Figure 8-28. ID/SYNC Register

| 7 | 6 | 4 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: |
|  | REVID[3:0] |  | DEVID[2:0] | 0 |
|  | R-xxxxb | R-000b | SYNC |  |

Table 8-14. ID/SYNC Register Field Descriptions

| Bit | Field | Type | Reset | Description |
| :---: | :--- | :--- | :--- | :--- |
| $7: 4$ | REVID[3:0] | R | xxxxb | Factory-programmed die revision. <br> These bits identify the revision of the die. The die revision is <br> subject to change without notification. |
| $3: 1$ | DEVID[2:0] | R | 000 b | Factory-programmed device identification. <br> These bits identify the ADC. <br> 000b = ADS1285 |
| 0 | SYNC | R/W | 0 b | Synchronization mode selection. <br> See the Synchronization section for details. <br> 0b Pulse-sync mode <br> $1 \mathrm{~b}=$ Continuous-sync mode |

### 8.6.1.2 CONFIGO: Configuration Register 0 (Address $=01 \mathrm{~h})$ [Reset $=12 \mathrm{~h}]$

Figure 8-29. CONFIGO Register

| 7 | 6 | 5 | 4 | 3 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MODE[1:0] | DR[2:0] | PHASE | FILTR[1:0] |  |  |  |
| R/W-00b | R/W-010b | R/W-0b | R/W-10b |  |  |  |

Table 8-15. CONFIGO Register Field Descriptions

| Bit | Field | Type | Reset | Description |
| :---: | :---: | :---: | :---: | :---: |
| 7:6 | MODE[1:0] | R/W | 00b | Power mode selection. <br> See the Power Modes section for details. $\begin{aligned} & 00 \mathrm{~b}=\text { High } \\ & 01 \mathrm{~b}=\text { Mid } \\ & 10 \mathrm{~b}=\text { Low } \\ & 11 \mathrm{~b}=\text { Reserved } \end{aligned}$ |
| 5:3 | DR[2:0] | R/W | 010b | Data rate selection. <br> See the Digital Filter section for details. 000b $=250$ SPS ( 125 SPS in low-power mode) 001b $=500$ SPS (250 SPS in low-power mode) $010 b=1000$ SPS (500 SPS in low-power mode) 011b $=2000$ SPS (1000 SPS in low-power mode) $100 b=4000$ SPS (2000 SPS in low-power mode) 101b-111b = Reserved |
| 2 | PHASE | R/W | Ob | FIR filter phase selection. <br> See the Digital Filter section for details. <br> $\mathrm{Ob}=$ Linear phase <br> $1 \mathrm{~b}=$ Minimum phase |
| 1:0 | FILTR[1:0] | R/W | 10b | Digital filter configuration. <br> See the Digital Filter section for details. <br> 00b $=$ Reserved <br> 01b $=$ Sinc filter output <br> 10b = FIR filter output <br> $11 \mathrm{~b}=$ FIR + IIR filter output |

### 8.6.1.3 CONFIG1: Configuration Register 1 (Address $=02 \mathrm{~h})$ [Reset $=00 \mathrm{~h}]$

Figure 8-30. CONFIG1 Register

| 7 | 6 | 5 | 4 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUX[2:0] | RE[1:0] | GAIN[2:0] |  |  |
| R/W-000b | R/W-00b | R/W-000b |  |  |  |

Table 8-16. CONFIG1 Register Field Descriptions

| Bit | Field | Type | Reset | Description |
| :---: | :---: | :---: | :---: | :---: |
| 7:5 | MUX[2:0] | R/W | 000b | Input MUX selection. <br> See the Analog Input section for details. <br> 000b $=$ Input 1 <br> $001 \mathrm{~b}=\ln$ nut 2 <br> $010 \mathrm{~b}=$ Internal short with a $400-\Omega$ resistor <br> 011b $=$ Input 1 and input 2 <br> 100b $=$ Reserved <br> $101 \mathrm{~b}=$ Internal short with a $0-\Omega$ resistor <br> 110b, 111b = Reserved |
| 4:3 | REF[1:0] | R/W | 00b | Select reference voltage operation. <br> See the Voltage Reference Input section for details. $\begin{aligned} & 00 \mathrm{~b}=5 \mathrm{~V} \\ & 01 \mathrm{~b}=4.096 \mathrm{~V} \\ & 10 \mathrm{~b}=2.5 \mathrm{~V} \\ & 11 \mathrm{~b}=\text { Reserved } \end{aligned}$ |
| 2:0 | GAIN[2:0] | R/W | 000b | PGA gain selection. <br> See the PGA and Buffer section for details. $\begin{aligned} & 000 b=1 \\ & 001 b=2 \\ & 010 b=4 \\ & 011 b=8 \\ & 100 b=16 \\ & 101 b=32 \\ & 110 b=64 \\ & 111 b=\text { Buffer operation } \end{aligned}$ |

### 8.6.1.4 HPFO, HPF1: High-Pass Filter Registers (Address = 03h, 04h) [Reset = 32h, 03h]

Figure 8-31. HPFO Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HPF[7:0] |  |  |  |  |  |  |  |
| R/W-32h |  |  |  |  |  |  |  |

Figure 8-32. HPF1 Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table 8-17. HPF0, HPF1 Registers Field Description

| Bit | Field | Type | Reset | Description |
| :---: | :--- | :--- | :--- | :--- |
| $15: 0$ | HPF[15:0] | R/W | 0332h | High-pass filter programming. <br> These registers program the corner frequency of the high-pass <br> filter. See the HPF Stage section for details. |

### 8.6.1.5 OFFSETO, OFFSET1, OFFSET2: Offset Calibration Registers (Address $=05 \mathrm{~h}, 06 \mathrm{~h}, 07 \mathrm{~h})$ [Reset $=00 \mathrm{~h}, 00 \mathrm{~h}, 00 \mathrm{~h}]$

Figure 8-33. OFFSETO Register

| 7 | 5 | 4 | 3 | 2 | 1 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |  |

Figure 8-34. OFFSET1 Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Figure 8-35. OFFSET2 Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Table 8-18. OFFSET0, OFFSET1, OFFSET2 Registers Field Description

| Bit | Field | Type | Reset | Description |
| :---: | :--- | :--- | :--- | :--- |
| $23: 0$ | OFFSET[23:0] | R/W | 000000 h | Offset calibration. <br> These bits are the 24-bit offset calibration word. The format is <br> 2's-complement coding. The ADC subtracts the value of offset <br> from the conversion result prior to the gain calibration operation. <br> See the Offset and Gain Calibration section for details. |

8.6.1.6 GAINO, GAIN1, GAIN2: Gain Calibration Registers
(Address $=08 \mathrm{~h}, 09 \mathrm{~h}, 0 \mathrm{Ah}$ ) [Reset $=00 \mathrm{~h}, 00 \mathrm{~h}, 40 \mathrm{~h}]$
Figure 8-36. GAINO Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GAIN[7:0] |  |  |  |  |  |  |  |
| R/W-00h |  |  |  |  |  |  |  |

Figure 8-37. GAIN1 Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Figure 8-38. GAIN2 Register

| 7 | 6 | 5 | 3 | 2 | 1 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  | GAIN[23:16] |

Table 8-19. GAIN0, GAIN1, GAIN2 Registers Field Description

| Bit | Field | Type | Reset | Description |
| :---: | :--- | :--- | :--- | :--- |
| $23: 0$ | GAIN[23:0] | R/W | 400000 h | Gain calibration. <br> These bits are the 24-bit, gain calibration word. Gain calibration <br> is straight binary coding. The register value is divided by <br> $400000 \mathrm{~h}\left(2^{22}\right)$ and multiplied with the conversion data. The gain <br> operation occurs after the offset operation. See the Offset and <br> Gain Calibration section for details. |

### 8.6.1.7 GPIO: Digital Input/Output Register (Address = 0Bh) [Reset = 000xx000b]

Figure 8-39. GPIO Register

| 7 | 6 | 5 | 4 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RESERVED | GPIO1_DAT | GPIO0_DAT | GPIO1_DIR | GPIO0_DIR | RESERVED |
| R/W-000b | R/W-xb | R/W-xb | R/W-0b | R/W-0b | R/W-0b |  |

Table 8-20. GPIO Register Field Descriptions

| Bit | Field | Type | Reset | Description |
| :---: | :---: | :---: | :---: | :---: |
| 7:5 | RESERVED | R/W | 000b | Always write 000b. |
| 4 | GPIO1_DAT | R/W | xb | GPIO1 data. <br> See the GPIO section for details. <br> $0 \mathrm{~b}=$ GPIO1 is low <br> $1 b=$ GPIO1 is high |
| 3 | GPIOO_DAT | R/W | xb | GPIO0 data. <br> Ob = GPIOO is low <br> $1 \mathrm{~b}=$ GPIOO is high |
| 2 | GPIO1_DIR | R/W | 0b | GPIO1 direction. <br> 0b = GPIO1 is an input <br> $1 \mathrm{~b}=$ GPIO1 is an output |
| 1 | GPIO0_DIR | R/W | 0b | GPIO0 direction. <br> $0 \mathrm{~b}=$ GPIOO is an input <br> $1 \mathrm{~b}=$ GPIOO is an output |
| 0 | RESERVED | R/W | Ob | Always write 0b. |

### 8.6.1.8 SRCO, SRC1: Sample Rate Converter Registers (Address $=0 C h, 0 D h)$ [Reset $=00 \mathrm{~h}, 80 \mathrm{~h}]$

Figure 8-40. SRC0 Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SRC[7:0] |  |  |  |  |  |  |  |
| R/W-00h |  |  |  |  |  |  |  |

Figure 8-41. SRC1 Register

| 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Table 8-21. SRC0, SRC1 Registers Field Description

| Bit | Field | Type | Reset | Description |
| :---: | :--- | :--- | :--- | :--- |
| $15: 0$ | SRC[15:0] | R/W | 8000 h | Sample rate converter. <br> These registers program the sample rate converter. See the <br> Sample Rate Converter section for details of operation. <br> 8000h = SRC function is disabled |

## 9 Application and Implementation

## Note

Information in the following applications sections is not part of the TI component specification, and Tl does not warrant its accuracy or completeness. Tl's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 9.1 Application Information

The ADS1285 is a high-resolution ADC designed for low-power seismic data acquisition equipment. Optimizing performance requires special attention to the support circuitry and printed-circuit board (PCB) layout. As much as possible, locate noisy circuit components (such as microcontrollers, oscillators, switching regulators, and so forth) away from the ADC input circuit components, reference voltage, and the ADC clock signal.

### 9.2 Typical Application



Figure 9-1. Geophone Input Application Example

### 9.2.1 Design Requirements

Figure 9-1 depicts a typical application of a geophone input circuit. The application shows the ADC operating with a $5-\mathrm{V}$ power supply and a $2.5-\mathrm{V}$ level-shift voltage applied to the ADC inputs. The goal of this evaluation is to analyze the effect of noise resulting from source resistance. The source resistance is the sum of the series input resistors and the geophone output resistance.

### 9.2.2 Detailed Design Procedure

Referring to Figure 9-1, Schottky diodes (BAS70 or equivalent) protect the ADC inputs from voltage overloads. The ADC inputs are protected from ESD events by the optional ESD protection diodes (TVSO701). The geophone signal is level-shifted to mid-supply by driving the input termination resistors ( $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ ) common point to 2.5 V . The level-shift voltage is derived from the reference voltage and is buffered by the OPA391 op amp. The input termination resistors also provide the input bias current return path for the ADC inputs.

The input signal is filtered to reduce out-of-band noise. The filter is comprised of common-mode and differential sections. The common-mode section filters noise common to both inputs, consisting of $R_{3}, R_{4}, C_{1}$, and $C_{2}$. The differential section filters differential noise, consisting of $R_{3}$ through $R_{6}$ and $C_{3}$. The resistor values are kept low to reduce thermal noise.

The REF6241 4.096-V voltage reference is used. The ADC must be programmed to match the value of the reference voltage. The optional noise filter consisting of $R_{7}$ and $C_{3}$ reduces reference noise. Resistor $R_{7}$ increases gain error resulting from the impedance of the reference input.
The AVDD1 power supply voltage $=5 \mathrm{~V}$, with AVSS connected to AGND. The AVDD2 voltage is 2.5 V to minimize power consumption. If IOVDD $=1.8 \mathrm{~V}$, connect the CAPD pin to IOVDD.

Besides the power supply pins, place additional capacitors at certain pins. Capacitors are required between CAPP - CAPN, REFP - REFN, and at the CAPBP, CAPBN, CAPI, CAPR, CAPC, and CAPD pins with the capacitance values given in Figure 9-1. The CAPP - CAPN, CAPBP, and CAPBN capacitors are C0G type.

The DAC1282 provides a low-distortion signal to test THD performance, and through the DAC1282 dc test mode, test geophone impulse response. Increase the value of the DAC1282 capacitors CAPP and CAPN to 10 nF to optimize the ADS1285 THD test performance. See the DAC1282 data sheet for additional circuit details.

### 9.2.3 Application Curves

Table 9-1 lists the effect of source resistance ( $\mathrm{R}_{\mathrm{S}}$ ) and device input current noise on dynamic range performance. Selected values of $R_{S}$ and input current noise, obtained from the input current noise distribution of Figure $9-2(1.5 \mathrm{pA} / \sqrt{\mathrm{Hz}}$ and $3 \mathrm{pA} / \sqrt{\mathrm{Hz}})$, are evaluated. Thermal noise voltage of the source resistance, input current noise $\times$ source resistance, and ADC input-referred noise voltage are summed as RMS values to derive the total noise. Dynamic range is calculated from the total noise result.


Figure 9-2. PGA Input Current Noise Distribution

Table 9-1. Source Resistance Noise

| $\mathrm{R}_{\mathrm{S}}(\Omega)$ | GAIN | $\mathrm{i}_{\mathrm{n}}$ NOISE ( $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ ) | R ${ }_{\text {NOIS }}(\mu \mathrm{V}$ ) | $i_{n} \times R_{S}$ NOISE ( $\mu \mathrm{V}$ ) | ADC SELF-NOISE ( $\mu \mathrm{V}$ ) | TOTAL NOISE ( $\mu \mathrm{V}$ ) | DR (dB) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1 | 1.5 | 0 | 0 | 0.44 | 0.44 | 132.1 |
|  |  | 3 |  | 0 |  | 0.44 | 132.1 |
|  | 16 | 1.5 |  | 0 | 0.11 | 0.11 | 120.1 |
|  |  | 3 |  | 0 |  | 0.11 | 120.1 |
| 1000 | 1 | 1.5 | 0.06 | 0.024 | 0.44 | 0.445 | 132.0 |
|  |  | 3 |  | 0.048 |  | 0.446 | 132.0 |
|  | 16 | 1.5 |  | 0.024 | 0.11 | 0.127 | 118.8 |
|  |  | 3 |  | 0.048 |  | 0.134 | 118.4 |
| 5000 | 1 | 1.5 | 0.13 | 0.11 | 0.44 | 0.472 | 131.5 |
|  |  | 3 |  | 0.22 |  | 0.508 | 130.8 |
|  | 16 | 1.5 |  | 0.11 | 0.11 | 0.202 | 114.8 |
|  |  | 3 |  | 0.21 |  | 0.277 | 112.0 |

Data for the analysis is shown for low-power mode operation over a $206-\mathrm{Hz}$ noise bandwidth ( $f_{\text {DATA }}=500 \mathrm{SPS}$ ). For PGA gain $=1,5000-\Omega$ source resistance has a minor effect on dynamic range performance. However, at PGA gain $=16$, dynamic range performance can degrade from -5 dB to -8 dB depending on the level of device input current noise. $1000-\Omega$ source resistance has $1.6-\mathrm{dB}$ degradation at gain $=16$ for input current noise density $=3 \mathrm{pA} / \sqrt{\mathrm{Hz}}$.

### 9.3 Power Supply Recommendations

The ADC has four power supplies: AVDD1, AVDD2, AVSS, and IOVDD. Among the power-supply options, the number of power supplies can be reduced to a single 3.3-V supply used for AVDD1, AVDD2, and IOVDD, with AVSS connected to ground. Be aware that 3.3-V operation limits the reference voltage to 2.5 V and requires using the buffer for gain $=1$.

The power supplies can be sequenced in any order. The ADC is held in reset until the power supplies have crossed the retrospective power-on voltage thresholds and the clock signal is applied (see Figure 6-8 for details of the voltage thresholds).

### 9.3.1 Analog Power Supplies

The ADC has three analog power supplies, AVDD1, AVDD2, and AVSS, all of which must be well regulated and free from switching power-supply noise (voltage ripple $<1 \mathrm{mV}$ ). The AVDD1 power-supply voltage is relative to AVSS and powers the PGA and buffer. AVSS is the negative power supply. The ADC can be configured for single-supply operation with AVDD1 $=5 \mathrm{~V}$ or 3.3 V with AVSS connected to ground. Because the minimum voltage of AVDD1 to AGND $=2.375 \mathrm{~V}$, dual-supply operation is only possible when AVDD1 $-\mathrm{AVSS}= \pm 2.5 \mathrm{~V}$. Single-power supply operation requires a level-shift voltage at the geophone input through the input termination resistors. The level-shift voltage is typically equal to AVDD1 / 2. Bypass AVDD1 with $1-\mu \mathrm{F}$ and $0.1-\mu \mathrm{F}$ parallel capacitors to AVSS.

The AVDD2 power supply powers the modulator. To simplify system power management, AVDD2 can be connected AVDD1, regardless whether AVDD1 and AVSS are configured for single- or dual-supply operation (AVDD2 voltage range is 2.375 V to 5.25 V with respect to AGND). Bypass AVDD2 with $1-\mu \mathrm{F}$ and $0.1-\mu \mathrm{F}$ parallel capacitors to AGND.

### 9.3.2 Digital Power Supply

IOVDD is the digital power supply. IOVDD is the digital pin I/O voltage and also powers the digital core by an $1.8-\mathrm{V}$ low-dropout regulator (LDO). The LDO output is the CAPD pin and is bypassed with a $0.22-\mu \mathrm{F}$ capacitor to DGND. Do not externally load the CAPD voltage output. Bypass the IOVDD pin with 1- $\mu \mathrm{F}$ and $0.1-\mu \mathrm{F}$ parallel capacitors to DGND.

ADS1285
www.ti.com
If IOVDD is in the range of 1.65 V to 1.95 V , tie the IOVDD and CAPD pins together. This connection forces the internal LDO off, thereby the IOVDD voltage now directly powers the digital core. Pay close attention to the absolute maximum voltage rating of IOVDD driving the CAPD pin to avoid damaging the device.

### 9.3.3 Grounds

The ADC has two ground pins, AGND and DGND. Connect the AGND and DGND pins together at the ADC to a single ground plane using short direct connections.

### 9.3.4 Thermal Pad

The thermal pad does not carry device current but must be soldered and connected to the most negative power-supply voltage (AVSS). Because of the low power dissipation, PCB thermal vias can be omitted to provide space for bottom layer components under the device.

### 9.4 Layout

### 9.4.1 Layout Guidelines

Figure 9-3 shows the layout of the geophone input application example of Figure 9-1. In most cases, a single unbroken ground plane connecting the grounds of the analog and digital components is preferred. A four-layer PCB is used, with the inner layers dedicated for ground and power-supply planes. Low resistance power-supply planes are necessary to maintain THD performance.
Connect the REFN pin of the ADC directly to the ground terminal of the voltage reference to avoid ground noise coupling. Similarly, avoid ground noise between the tie-points of termination resistors $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ by connecting the resistors together first, then connect to ground (dual-supply operation).
Place the smaller of the parallel power-supply bypass capacitors closest to the device supply pins. The thermal pad of the package connects to the most negative power-supply voltage (AVSS). Figure 9-3 shows single-supply operation, with AVSS tied to AGND. In this case, the thermal pad connects to AGND. For dual-supply operation, connect the thermal pad to AVSS.

### 9.4.2 Layout Example



Figure 9-3. Example Layout

## 10 Device and Documentation Support

### 10.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on Subscribe to updates to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 10.2 Support Resources

TI E2E ${ }^{T M}$ support forums are an engineer's go-to source for fast, verified answers and design help - straight from the experts. Search existing answers or ask your own question to get the quick design help you need.
Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

### 10.3 Trademarks

TI E2E ${ }^{\text {TM }}$ is a trademark of Texas Instruments.
All trademarks are the property of their respective owners.

### 10.4 Electrostatic Discharge Caution

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.
ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 10.5 Glossary

TI Glossary This glossary lists and explains terms, acronyms, and definitions.

## 11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

INSTRUMENTS

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material <br> (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ADS1285IRHBR | ACTIVE | VQFN | RHB | 32 | 3000 | RoHS \& Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | $\begin{aligned} & \text { ADS } \\ & 1285 \end{aligned}$ | Samples |
| ADS1285IRHBT | ACTIVE | VQFN | RHB | 32 | 250 | RoHS \& Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | $\begin{aligned} & \text { ADS } \\ & 1285 \end{aligned}$ | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: Tl defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the $<=1000$ ppm threshold requirement.
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a " $\sim$ " will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

Important Information and Disclaimer:The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall Tl's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by Tl to Customer on an annual basis.

TAPE AND REEL INFORMATION


TAPE DIMENSIONS


| A0 | Dimension designed to accommodate the component width |
| :---: | :--- |
| B0 | Dimension designed to accommodate the component length |
| K0 | Dimension designed to accommodate the component thickness |
| W | Overall width of the carrier tape |
| P1 | Pitch between successive cavity centers |

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter (mm) | Reel Width W1 (mm) | $\begin{gathered} \mathrm{AO} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \text { B0 } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \mathrm{KO} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \text { P1 } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} W \\ (\mathrm{~mm}) \end{gathered}$ | Pin1 <br> Quadrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ADS1285IRHBR | VQFN | RHB | 32 | 3000 | 330.0 | 12.4 | 5.3 | 5.3 | 1.1 | 8.0 | 12.0 | Q2 |
| ADS1285IRHBT | VQFN | RHB | 32 | 250 | 180.0 | 12.4 | 5.3 | 5.3 | 1.1 | 8.0 | 12.0 | Q2 |


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ADS1285IRHBR | VQFN | RHB | 32 | 3000 | 367.0 | 367.0 | 35.0 |
| ADS1285IRHBT | VQFN | RHB | 32 | 250 | 210.0 | 185.0 | 35.0 |



Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.


NOTES: (continued)
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.


SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL
EXPOSED PAD 33:
75\% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE
SCALE:20X

NOTES: (continued)
6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

## IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.
These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.
These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other Tl intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

Tl's products are provided subject to Tl's Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter Tl's applicable warranties or warranty disclaimers for TI products.
TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265
Copyright © 2023, Texas Instruments Incorporated

