





TEXAS INSTRUMENTS

UCC5350-Q1 SLUSE29E – MAY 2020 – REVISED FEBRUARY 2024

# UCC5350-Q1 Single-Channel Isolated Gate Driver for SiC/IGBT and Automotive Applications

## 1 Features

- 5kV<sub>RMS</sub> and 3kV<sub>RMS</sub> single-channel isolated gate driver
- AEC-Q100 qualified for automotive applications
  - Temperature grade 1
  - HBM ESD classification level H2
  - CDM ESD classification level C6
- Feature options
  - Split outputs, 8V UVLO (UCC5350SB-Q1)
  - Miller clamp, 12V UVLO (UCC5350MC-Q1)
- ±5A minimum peak current drive strength
- 3V to 15V input supply voltage
- Up to 33V driver supply voltage
   8V and 12V UVLO options
- 100V/ns minimum CMTI
- Negative 5V handling capability on input pins
- 100ns (maximum) propagation delay and <25ns part-to-part skew
- 8-pin DWV (8.5mm creepage) and D (4mm creepage) packages
- Isolation barrier life > 40 Years
- Safety-related certifications:
  - 5000V<sub>RMS</sub> DWV and 3000V<sub>RMS</sub> D isolation rating for 1 minute per UL 1577
- CMOS inputs

IN-

IN

GND1

Operating junction temperature: –40°C to +150°C

BARRIER

11

ISOLATION

S Version

UVLO

and

Input

Logic

UVLO

Lev el

Shift

and

Ctrl

Logic

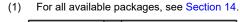
## 2 Applications

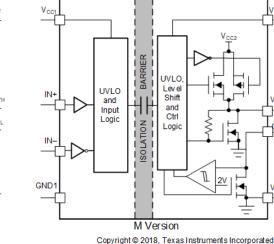
- On-board charger
- Traction inverter for EVs
- DC charging stations
- HVAC
- Heaters

## **3 Description**

The UCC5350-Q1 is a single-channel, isolated gate driver with 5A source and 5A sink minimum peak current designed to drive MOSFETs, IGBTs, and SiC MOSFETs. The UCC5350-Q1 has the option for Miller clamp or Split Outputs. The CLAMP pin is used to connect the transistor gate to an internal FET besides the output to prevent false turn-on caused by Miller current. The split outputs option allows separate control of the rise and fall times of the gate voltage with OUTH and OUTL pins.

PART VERSION	FEATURES	PACKAGE <sup>(1)</sup>	BODY SIZE (NOM)
UCC5350MC-Q1	Miller Clamp,	DWV SOIC-8	7.5mm × 5.85mm
000000000-01	12V UVLO	D SOIC-8	3.91mm x 4.9mm
UCC5350SB-Q1	Split Outputs, 8V UVLO	D SOIC-8	3.91mm x 4.9mm





### Functional Block Diagram (S and M Versions)

An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, intellectual property matters and other important disclaimers. PRODUCTION DATA.



## **Table of Contents**

1 Features1	
2 Applications1	
3 Description1	
4 Description (continued)	3
5 Pin Configuration and Function4	
6 Specifications	
6.1 Absolute Maximum Ratings	
6.2 ESD Ratings	
6.3 Recommended Operating Conditions	5
6.4 Thermal Information	5
6.5 Power Ratings6	5
6.6 Insulation Specifications for D Package	5
6.7 Insulation Specifications for DWV Package	3
6.8 Safety-Related Certifications For D Package	)
6.9 Safety-Related Certifications For DWV Package	)
6.10 Safety Limiting Values	
6.11 Electrical Characteristics10	)
6.12 Switching Characteristics11	
6.13 Insulation Characteristics Curves12	
6.14 Typical Characteristics13	3
7 Parameter Measurement Information16	5
7.1 Propagation Delay, Inverting, and Noninverting	
Configuration16	
8 Detailed Description18	3

8.1 Overview	. 18
8.2 Functional Block Diagram	
8.3 Feature Description.	
8.4 Device Functional Modes	
9 Application and Implementation	
9.1 Application Information	
9.2 Typical Application	
10 Power Supply Recommendations	
11 Layout	
11.1 Layout Guidelines	. 31
11.2 Layout Example	
11.3 PCB Material	. 34
12 Device and Documentation Support	35
12.1 Device Support	. 35
12.2 Documentation Support	. 35
12.3 Certifications	. 35
12.4 Receiving Notification of Documentation Updates	35
12.5 Support Resources	. 35
12.6 Trademarks	
12.7 Electrostatic Discharge Caution	35
12.8 Glossary	35
13 Revision History	. 36
14 Mechanical, Packaging, and Orderable	
Information	. 36



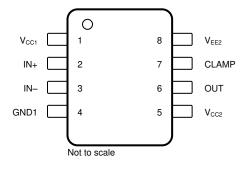
## 4 Description (continued)

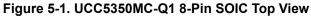
The UCC5350-Q1 is available in a 4mm SOIC-8 (D) or 8.5mm wide body SOIC-8 (DWV) package and can support isolation voltage up to  $3kV_{RMS}$  and  $5kV_{RMS}$ , respectively. The input side is isolated from the output side with SiO2 capacitive isolation technology with longer than 40 years isolation barrier lifetime. The UCC5350-Q1 is a good fit for driving IGBTs or MOSFETs in applications such as high-voltage traction inverters and on-board chargers.

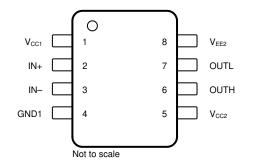
Compared to an optocoupler, the UCC5350-Q1 device has lower part-to-part skew, lower propagation delay, higher operating temperature, and higher CMTI.

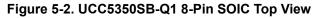


## **5** Pin Configuration and Function









	PIN				
NAME	NO.	NO.	TYPE <sup>(1)</sup>	DESCRIPTION	
NAME	UCC5350MC-Q1	UCC5350SB-Q1	1		
CLAMP	7	_	I	Active Miller-clamp input used to prevent false turn-on of the power switches found on the 'M' version.	
GND1	4	4	G	Input ground. All signals on the input side are referenced to this ground.	
IN+	2	2	I	Noninverting gate-drive voltage-control input. The IN+ pin has a CMOS input threshold. This pin is pulled low internally if left open. Use Table 8-4 to understand the input and output logic of these devices.	
IN–	3	3	I	Inverting gate-drive voltage control input. The IN– pin has a CMOS input threshold. This pin is pulled high internally if left open. Use Table 8-4 to understand the input and output logic of these devices.	
OUT	6	—	0	Gate-drive output found on the 'M' version	
OUTH	_	6	0	Gate-drive pullup output found on the 'S' version	
OUTL	_	7	0	Gate-drive pulldown output found on the 'S' version	
V <sub>CC1</sub>	1	1	Р	Input supply voltage. Connect a locally decoupled capacitor to GND1. Use a low-ESR or ESL capacitor located as close to the device as possible.	
V <sub>CC2</sub>	5	5	Р	Positive output supply rail. Connect a locally decoupled capacitor to $V_{\text{EE2}}$ . Use a low-ESR or ESL capacitor located as close to the device as possible.	
V <sub>EE2</sub>	8	8	G	Ground pin. Connect to MOSFET source or IGBT emitter. Connect a locally decoupled capacitor from $V_{CC2}$ to $V_{EE2}.$ Use a low-ESR or ESL capacitor located as close to the device as possible.	

#### Table 5-1. Pin Functions

(1) P = Power, G = Ground, I = Input, O = Output



## **6** Specifications

### 6.1 Absolute Maximum Ratings

Over operating free air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Input bias pin supply voltage	V <sub>CC1</sub> – GND1	GND1 – 0.3	18	V
Driver bias supply	V <sub>CC2</sub> – V <sub>EE2</sub>	-0.3	35	V
Output signal voltage	$V_{OUTH} - V_{EE2}, V_{OUTL} - V_{EE2}, V_{OUT} - V_{EE2}, V_{CLAMP} - V_{EE2}$	V <sub>EE2</sub> - 0.3	V <sub>CC2</sub> + 0.3	V
Input signal voltage	V <sub>IN+</sub> – GND1, V <sub>IN-</sub> – GND1	GND1 – 5	V <sub>CC1</sub> + 0.3	V
Junction temperature, T <sub>J</sub> <sup>(2)</sup>		-40	150	°C
Storage temperature, T <sub>stg</sub>		-65	150	°C

(1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

(2) To maintain the recommended operating conditions for  $T_J$ , see the Thermal Information table.

## 6.2 ESD Ratings

			VALUE	UNIT	
V	Electrostatic	Human-body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±4000	V	
V <sub>(ESD)</sub>	discharge	Charged-device model (CDM), per AEC Q100-011	±1500	v	

(1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

### 6.3 Recommended Operating Conditions

Over operating free-air temperature range (unless otherwise noted)

		MIN	NOM MAX	UNIT
V <sub>CC1</sub>	Supply voltage, input side	3	15	V
V <sub>CC2</sub>	Positive supply voltage output side ( $V_{CC2} - V_{EE2}$ ), UCC5350MC	13.2	33	V
V <sub>CC2</sub>	Positive supply voltage output side ( $V_{CC2} - V_{EE2}$ ), UCC5350SB	9.5	33	V
TJ	Junction Temperature	-40	150	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		UCC53	UCC5350-Q1		
		D	DWV	UNIT	
		8 PINS	8 PINS		
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	109.5	119.8	°C/W	
R <sub>0JC(top)</sub>	Junction-to-case (top) thermal resistance	43.1	64.1	°C/W	
R <sub>θJB</sub>	Junction-to-board thermal resistance	51.2	65.4	°C/W	
$\Psi_{JT}$	Junction-to-top characterization parameter	18.3	37.6	°C/W	
$\Psi_{JB}$	Junction-to-board characterization parameter	50.7	63.7	°C/W	

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics Application Report.



## 6.5 Power Ratings

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT			
D Pacl	D Package (UCC5350MC-Q1)								
PD	Maximum power dissipation on input and output	V <sub>CC1</sub> = 15 V, V <sub>CC2</sub> = 15 V, f = 2.1-MHz,			1.14	W			
P <sub>D1</sub>	Maximum input power dissipation	50% duty cycle, square wave, 2.2-nF load			0.05	W			
P <sub>D2</sub>	Maximum output power dissipation				1.09	W			
D Pacl	(age (UCC5350SB-Q1)								
P <sub>D</sub>	Maximum power dissipation on input and output	V <sub>CC1</sub> = 15 V, V <sub>CC2</sub> = 15 V, f = 1.8-MHz,			0.99	W			
P <sub>D1</sub>	Maximum input power dissipation	50% duty cycle, square wave, 2.2-nF load			0.05	W			
P <sub>D2</sub>	Maximum output power dissipation				0.94	W			
DWV F	Package (UCC5350MC-Q1)	· · · · ·							
PD	Maximum power dissipation on input and output	V <sub>CC1</sub> = 15 V, V <sub>CC2</sub> = 15 V, f = 1.9-MHz,			1.04	W			
P <sub>D1</sub>	Maximum input power dissipation	50% duty cycle, square wave, 2.2-nF load			0.05	W			
P <sub>D2</sub>	Maximum output power dissipation				0.99	W			

## 6.6 Insulation Specifications for D Package

	PARAMETER	TEST CONDITIONS	VALUE	
	PARAMETER	TEST CONDITIONS	D	
CLR	External Clearance <sup>(1)</sup>	Shortest pin–to-pin distance through air	≥ 4	mm
CPG	External Creepage <sup>(1)</sup>	Shortest pin–to-pin distance across the package surface	≥ 4	mm
DTI	Distance through the insulation	Minimum internal gap (internal clearance)	> 21	μm
CTI	Comparative tracking index	DIN EN 60112 (VDE 0303–11); IEC 60112	> 400	V
	Material Group	According to IEC 60664–1	II	
Overvelte		Rated mains voltage ≤ 150 <sub>VRMS</sub>	I-IV	
Overvoita	age category per IEC 60664-1	Rated mains voltage ≤ 300 <sub>VRMS</sub>	1-111	
	DE 0884–11: 2017–01 <sup>(2)</sup>			
V <sub>IORM</sub>	Maximum repetitive peak isolation voltage	AC voltage (bipolar)	990 <sup>(6)</sup>	V <sub>PK</sub>
V <sub>IOWM</sub>	Maximum isolation working	AC voltage (sine wave); time dependent dielectric breakdown (TDDB) test	700 <sup>(6)</sup>	V <sub>RMS</sub>
IOWM	voltage	DC Voltage	990 <sup>(6)</sup>	V <sub>DC</sub>
V <sub>IOTM</sub>	Maximum transient isolation voltage	$V_{\text{TEST}} = V_{\text{IOTM}}, t = 60 \text{ s (qualification)};$ $V_{\text{TEST}} = 1.2 \times V_{\text{IOTM}}, t = 1 \text{ s (100\% production)}$	4242	V <sub>PK</sub>
V <sub>IOSM</sub>	Maximum surge isolation voltage <sup>(3)</sup>	Test method per IEC 62368-1, 1.2/50-µs waveform, V <sub>TEST</sub> = 1.3 × V <sub>IOSM</sub> (qualification)	4242	V <sub>PK</sub>
			≤ 5	
q <sub>pd</sub>	Apparent charge <sup>(4)</sup>		≤ 5	рС
		$\label{eq:constraint} \begin{array}{l} \mbox{Method b1: At routine test (100\% production) and} \\ \mbox{preconditioning (type test),} \\ \mbox{V}_{ini} = 1.2 \ x \ V_{IOTM}, \ t_{ini} = 1 \ s; \\ \mbox{V}_{pd(m)} = 1.5 \ x \ V_{IORM}, \ t_m = 1 \ s \end{array}$	≤ 5	
C <sub>IO</sub>	Barrier capacitance, input to output <sup>(5)</sup>	$V_{IO}$ = 0.4 × sin (2 $\pi$ ft), f = 1 MHz	1.2	pF



## 6.6 Insulation Specifications for D Package (continued)

PARAMETER		TEST CONDITIONS	VALUE		UNIT
	FARAMETER	TEST CONDITIONS	D		UNIT
		V <sub>IO</sub> = 500 V, T <sub>A</sub> = 25°C	> 1	0 <sup>12</sup>	
R <sub>IO</sub> Isolation resistance, input to	Isolation resistance, input to output <sup>(5)</sup>	$V_{IO} = 500 \text{ V}, \ 100^{\circ}\text{C} \le \text{T}_{A} \le 125^{\circ}\text{C}$	> 1	0 <sup>11</sup>	Ω
	- up at	V <sub>IO</sub> = 500 V at T <sub>S</sub> = 150°C	> 1	10 <sup>9</sup>	
	Pollution degree		2	2	
	Climatic category		40/12	25/21	
UL 1577					
V <sub>ISO</sub>	Withstand isolation voltage	V <sub>TEST</sub> = V <sub>ISO</sub> , t = 60 s (qualification); V <sub>TEST</sub> = 1.2 > (100% production)	< V <sub>ISO</sub> , t = 1 s	3000	V <sub>RMS</sub>

(1) Creepage and clearance requirements should be applied according to the specific equipment isolation standards of an application. Care should be taken to maintain the creepage and clearance distance of a board design to ensure that the mounting pads of the isolator on the printed-circuit board do not reduce this distance. Creepage and clearance on a printed-circuit board become equal in certain cases. Techniques such as inserting grooves, ribs, or both on a printed circuit board are used to help increase these specifications.

(2) This coupler is suitable for basic electrical insulation only within the maximum operating ratings. Compliance with the safety ratings shall be ensured by means of suitable protective circuits.

(3) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.

(4) Apparent charge is electrical discharge caused by a partial discharge (pd).

(5) All pins on each side of the barrier tied together creating a two-pin device.

(6) System isolation working voltages need to be verified according to application parameters.



### 6.7 Insulation Specifications for DWV Package

PARAMETER			VALUE	UNIT	
		TEST CONDITIONS	DWV		
CLR	External Clearance <sup>(1)</sup>	Shortest pin–to-pin distance through air	≥ 8.5	mm	
CPG	External Creepage <sup>(1)</sup>	Shortest pin–to-pin distance across the package surface	≥ 8.5	mm	
DTI	Distance through the insulation	Minimum internal gap (internal clearance)	> 21	μm	
СТІ	Comparative tracking index	DIN EN 60112 (VDE 0303-11); IEC 60112	> 600	V	
	Material Group	According to IEC 60664–1	I		
O		Rated mains voltage ≤ 600 <sub>VRMS</sub>	1-111		
Overvoitag	e category per IEC 60664-1	Rated mains voltage ≤ 1000 <sub>VRMS</sub>	I-II		
DIN V VDE	E 0884–11: 2017–01 <sup>(2)</sup>				
V <sub>IORM</sub>	Maximum repetitive peak isolation voltage	AC voltage (bipolar)	2121	V <sub>PK</sub>	
V <sub>IOWM</sub>	Maximum isolation working	AC voltage (sine wave); time dependent dielectric breakdown (TDDB) test	1500	V <sub>RMS</sub>	
10111	voltage	DC Voltage	2121	V <sub>DC</sub>	
V <sub>IOTM</sub>	Maximum transient isolation voltage	$V_{\text{TEST}} = V_{\text{IOTM}}$ , t = 60 s (qualification) ; $V_{\text{TEST}} = 1.2 \times V_{\text{IOTM}}$ , t = 1 s (100% production)	7000	V <sub>PK</sub>	
V <sub>IOSM</sub>	Maximum surge isolation voltage <sup>(3)</sup>	Test method per IEC 62368-1, 1.2/50-µs waveform, V <sub>TEST</sub> = 1.6 × V <sub>IOSM</sub> (qualification)	8000	V <sub>PK</sub>	
			≤5		
q <sub>pd</sub>	Apparent charge <sup>(4)</sup>	Method a: After environmental tests subgroup 1, $V_{ini} = V_{IOTM}, t_{ini} = 60 \text{ s};$ $V_{pd(m)} = 1.6 \times V_{IORM}, t_m = 10 \text{ s}$	≤5 p	рС	
		Method b1: At routine test (100% production) and preconditioning (type test), $V_{ini} = 1.2 \times V_{IOTM}$ , $t_{ini} = 1 \text{ s}$ ; $V_{pd(m)} = 1.875 \times V_{IORM}$ , $t_m = 1 \text{ s}$	≤5		
C <sub>IO</sub>	Barrier capacitance, input to output <sup>(5)</sup>	$V_{IO} = 0.4 \times \sin (2\pi ft), f = 1 MHz$	1.2	pF	
		V <sub>IO</sub> = 500 V, T <sub>A</sub> = 25°C	> 10 <sup>12</sup>		
R <sub>IO</sub>	Isolation resistance, input to output <sup>(5)</sup>	$V_{IO} = 500 \text{ V}, \ 100^{\circ}\text{C} \le \text{T}_{A} \le 125^{\circ}\text{C}$	> 10 <sup>11</sup>	Ω	
	ouput	V <sub>IO</sub> = 500 V at T <sub>S</sub> = 150°C	> 10 <sup>9</sup>		
	Pollution degree		2		
	Climatic category		40/125/21		
UL 1577		· I			
V <sub>ISO</sub>	Withstand isolation voltage	$V_{\text{TEST}} = V_{\text{ISO}}$ , t = 60 s (qualification); $V_{\text{TEST}} = 1.2 \times V_{\text{ISO}}$ , t = 1 s (100% production)	5000	V <sub>RMS</sub>	

(1) Creepage and clearance requirements should be applied according to the specific equipment isolation standards of an application. Care should be taken to maintain the creepage and clearance distance of a board design to ensure that the mounting pads of the isolator on the printed-circuit board do not reduce this distance. Creepage and clearance on a printed-circuit board become equal in certain cases. Techniques such as inserting grooves, ribs, or both on a printed circuit board are used to help increase these specifications.

(2) This coupler is suitable for safe electrical insulation only within the safety ratings. Compliance with the safety ratings shall be ensured by means of suitable protective circuits.

(3) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.

(4) Apparent charge is electrical discharge caused by a partial discharge (pd).

(5) All pins on each side of the barrier tied together creating a two-pin device.



### 6.8 Safety-Related Certifications For D Package

UL			
Recognized under UL 1577 Component Recognition Program			
Single protection, 3000 V <sub>RMS</sub>			
File Number: E181974			

### 6.9 Safety-Related Certifications For DWV Package

UL Recognized under UL 1577 Component Recognition Program			
File Number: E181974			

### 6.10 Safety Limiting Values

Safety limiting intends to minimize potential damage to the isolation barrier upon failure of input or output circuitry.

	PARAMETER	TEST CONDITIONS		MIN	TYP	MAX	UNIT
D PAC	KAGE (UCC5350MC-Q1)						
		$R_{\theta,JA} = 109.5^{\circ}C/W, V_{CC2} = 15 V, T_{J} = 150^{\circ}C, T_{A} = 25^{\circ}C, \text{ see Figure 6-2}$	Output side			73	mA
I <sub>S</sub>	Salety output supply current	$R_{\theta,JA} = 109.5^{\circ}C/W, V_{CC2} = 30 V, T_{J} = 150^{\circ}C, T_{A} = 25^{\circ}C, \text{ see Figure 6-2}$	Output side			36	ША
			Input side			0.05	
Ps	Safety output supply power	$ R_{\theta JA}  = 109.5^{\circ}C/W, T_{J} = 150^{\circ}C, T_{A} = 25^{\circ}C,$ see Figure 6-4	Output side			1.09	1.09 W
		Total	1.14				
Τs	Maximum safety temperature <sup>(1)</sup>					150	°C
D PAC	KAGE (UCC5350SB-Q1)	•					
		$R_{\theta JA} = 109.5^{\circ}C/W, V_{CC2} = 15 V, T_{J} = 150^{\circ}C, T_{A} = 25^{\circ}C, \text{ see Figure 6-2}$	Output side			63	mA
I <sub>S</sub>	Safety output supply current	$\begin{array}{c} R_{\theta JA} = 109.5^{\circ}\text{C/W}, V_{CC2} = 30 \text{ V}, T_{J} = 150^{\circ}\text{C}, \\ T_{A} = 25^{\circ}\text{C}, \text{ see Figure 6-2} \end{array} \qquad \text{Output side}$		31			
			Input side			0.05	
Ps	Safety output supply power	$R_{\theta JA} = 109.5^{\circ}C/W, T_{J} = 150^{\circ}C, T_{A} = 25^{\circ}C,$ see Figure 6-4	Output side			0.94	W
			Total		0.99		
Τs	Maximum safety temperature <sup>(1)</sup>					150	°C
DWV I	PACKAGE (UCC5350MC-Q1)	•					
, Safety input, output, or supply		R <sub>0JA</sub> = 119.8°C/W, V <sub>I</sub> = 15 V, T <sub>J</sub> = 150°C, T <sub>A</sub> = 25°C, see Figure 6-1	Output side			66	mA
I <sub>S</sub>	current	R <sub>0JA</sub> = 119.8°C/W, V <sub>I</sub> = 30 V, T <sub>J</sub> = 150°C, T <sub>A</sub> = 25°C, see Figure 6-1	Output side			33	ШA
			Input side			0.05	
Ps	Safety input, output, or total power	$R_{\theta JA} = 119.8^{\circ}C/W, T_J = 150^{\circ}C, T_A = 25^{\circ}C,$ see Figure 6-3	Output side			0.99	W
	power		Total			1.04	
Τs	Maximum safety temperature <sup>(1)</sup>					150	°C

(1) The maximum safety temperature, T<sub>S</sub>, has the same value as the maximum junction temperature, T<sub>J</sub>, specified for the device. The I<sub>S</sub> and P<sub>S</sub> parameters represent the safety current and safety power respectively. The maximum limits of I<sub>S</sub> and P<sub>S</sub> should not be exceeded. These limits vary with the ambient temperature, T<sub>A</sub>.

The junction-to-air thermal resistance,  $R_{\theta JA}$ , in the Thermal Information table is that of a device installed on a high-K test board for leaded surface-mount packages. Use these equations to calculate the value for each parameter:

 $T_J = T_A + R_{\theta JA} \times P$ , where P is the power dissipated in the device.

 $T_{J(max)} = T_S = T_A + R_{\theta JA} \times P_S$ , where  $T_{J(max)}$  is the maximum allowed junction temperature.

 $P_S = I_S \times V_I$ , where  $V_I$  is the maximum input voltage.

### **6.11 Electrical Characteristics**

 $V_{CC1}$  = 3.3 V or 5 V, 0.1- $\mu$ F capacitor from  $V_{CC1}$  to GND1,  $V_{CC2}$ = 15 V, 1- $\mu$ F capacitor from  $V_{CC2}$  to  $V_{EE2}$ ,  $C_L$  = 100-pF,  $T_J$  = -40°C to +125°C (UCC5350MC-Q1),  $T_J$  = -40°C to +150°C (UCC5350SB-Q1), (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY CU	RRENTS					
I <sub>VCC1</sub>	Input supply quiescent current			1.67	2.4	mA
I <sub>VCC2</sub>	Output supply quiescent current			1.1	1.8	mA
SUPPLY VO	LTAGE UNDERVOLTAGE THRES	SHOLDS				
V <sub>IT+(UVLO1)</sub>	VCC1 Positive-going UVLO threshold voltage			2.6	2.8	V
V <sub>IT- (UVLO1)</sub>	VCC1 Negative-going UVLO threshold voltage		2.4	2.5		V
V <sub>hys(UVLO1)</sub>	VCC1 UVLO threshold hysteresis			0.1		V
OUTPUT SU	JPPLY VOLTAGE UNDERVOLTAG	SE THRESHOLDS (UCC5350MC-Q1)				
V <sub>IT+(UVLO2)</sub>	VCC2 Positive-going UVLO threshold voltage			12	13	V
V <sub>IT–(UVLO2)</sub>	VCC2 Negative-going UVLO threshold voltage		10.3	11		V
V <sub>hys(UVLO2)</sub>	VCC2 UVLO threshold voltage hysteresis			1		V
OUTPUT SU	JPPLY VOLTAGE UNDERVOLTAG	SE THRESHOLDS (UCC5350SB-Q1)			I	
V <sub>IT+(UVLO2)</sub>	VCC2 Positive-going UVLO threshold voltage			8.7	9.4	V
V <sub>IT–(UVLO2)</sub>	VCC2 Negative-going UVLO threshold voltage		7.3	8.0		V
V <sub>hys(UVLO2)</sub>	VCC2 UVLO threshold voltage hysteresis			0.7		V
LOGIC I/O						
V <sub>IT+(IN)</sub>	Positive-going input threshold voltage (IN+, IN–)			0.55 × V <sub>CC1</sub>	0.7 × V <sub>CC1</sub>	V
V <sub>IT–(IN)</sub>	Negative-going input threshold voltage (IN+, IN–)		0.3 × V <sub>CC1</sub>	0.45 × V <sub>CC1</sub>		V
V <sub>hys(IN)</sub>	Input hysteresis voltage (IN+, IN–)			0.1 × V <sub>CC1</sub>		V
I <sub>IH</sub>	High-level input leakage at IN+	IN+ = V <sub>CC1</sub>		40	240	μA
I <sub>IL</sub>	Low-level input leakage at IN–	IN– = GND1	-240	-40		μA
		IN– = GND1 – 5 V	-310	-80		μ, ,
GATE DRIVE		1				
V <sub>OH</sub>	High-level output voltage (VCC2 - OUT) and (VCC2 - OUTH)	I <sub>OUT</sub> = –20 mA	100	240		mV
V <sub>OL</sub>	Low level output voltage (OUT and OUTL)	IN+ = low, IN– = high; I <sub>OUT</sub> = 20 mA	5	7		mV
I	Peak source current	UCC5350MC, IN+ = high, IN- = low	5	10		А
I <sub>OH</sub>	FEAN SOUICE CUITEIIL	UCC5350SB, IN+ = high, IN- = low	5	8.5		А

### 6.11 Electrical Characteristics (continued)

 $V_{CC1}$  = 3.3 V or 5 V, 0.1-µF capacitor from  $V_{CC1}$  to GND1,  $V_{CC2}$ = 15 V, 1-µF capacitor from  $V_{CC2}$  to  $V_{EE2}$ ,  $C_L$  = 100-pF,  $T_J$  = -40°C to +125°C (UCC5350MC-Q1),  $T_J$  = -40°C to +150°C (UCC5350SB-Q1), (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
V <sub>CLAMP</sub>	Low-level clamp voltage	I <sub>CLAMP</sub> = 20 mA		7	10	mV
ICLAMP	Clamp low-level current	V <sub>CLAMP</sub> = V <sub>EE2</sub> + 15 V	5	10		А
I <sub>CLAMP(L)</sub>	Clamp low-level current for low output voltage	V <sub>CLAMP</sub> = V <sub>EE2</sub> + 2 V	5	10		А
V <sub>CLAMP-TH</sub>	Clamp threshold voltage			2.1	2.3	V
SHORT CIR	CUIT CLAMPING				•	
V <sub>CLP-OUT</sub>	Clamping voltage (V <sub>OUT</sub> –V <sub>CC2</sub> )	IN+ = high, IN- = low, $t_{CLAMP}$ = 10 $\mu$ s, I <sub>OUT</sub> = 500 mA		1	1.3	V
M	Clamping voltage ( V <sub>EE2</sub> – V <sub>OUT</sub> )	IN+ = low, IN– = high, $t_{CLAMP}$ = 10 $\mu$ s, I <sub>OUT</sub> = -500 mA		1.5		V
V <sub>CLP-OUT</sub>		IN+ = Iow, IN- = high, $I_{OUT} = -20 mA$		0.9	1	v
ACTIVE PUI	LLDOWN					
V <sub>OUTSD</sub>	Active pulldown voltage on OUT	$I_{OUT} = 0.1 \times I_{OUT(typ)}, V_{CC2} = open$		1.8	2.5	V
		1				

### 6.12 Switching Characteristics

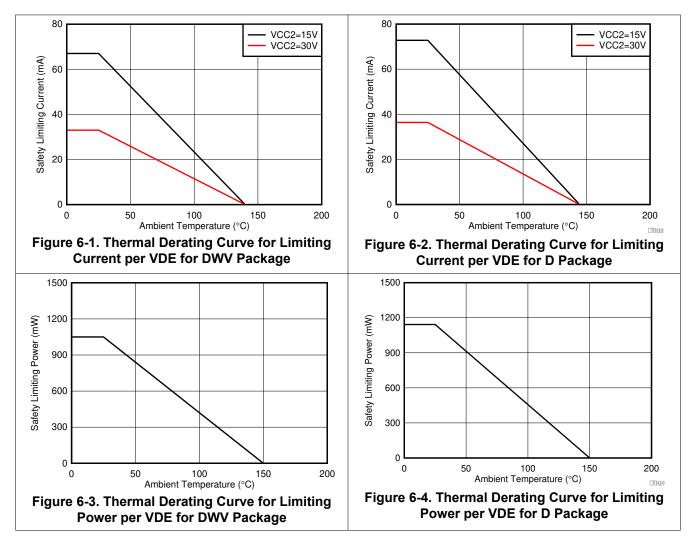
 $V_{CC1}$  = 3.3 V or 5 V, 0.1-µF capacitor from  $V_{CC1}$  to GND1,  $V_{CC2}$ = 15 V, 1-µF capacitor from  $V_{CC2}$  to  $V_{EE2}$ ,  $T_J$  = -40°C to +125°C, (unless otherwise noted)

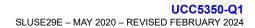
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t <sub>r</sub>	Output-signal rise time	C <sub>LOAD</sub> = 1 nF		10	26	ns
t <sub>f</sub>	Output-signal fall time	C <sub>LOAD</sub> = 1 nF		10	22	ns
t <sub>PLH</sub>	Propagation delay, high	C <sub>LOAD</sub> = 100 pF		65	100	ns
t <sub>PHL</sub>	Propagation delay, low	C <sub>LOAD</sub> = 100 pF		65	100	ns
t <sub>UVLO1_rec</sub>	UVLO recovery delay of $V_{CC1}$	See Figure 8-7.		30		μs
t <sub>UVLO2_rec</sub>	UVLO recovery delay of $V_{\text{CC2}}$	See Figure 8-7.		50		μs
t <sub>PWD</sub>	Pulse width distortion  t <sub>PHL</sub> – t <sub>PLH</sub>	C <sub>LOAD</sub> = 100 pF		1	20	ns
t <sub>sk(pp)</sub>	Part-to-part skew <sup>(1)</sup>	C <sub>LOAD</sub> = 100 pF		1	25	ns
t <sub>PWmin1</sub>	No response at OUT where OUT <10% × $V_{CC2}$	C <sub>LOAD</sub> = 100 pF	8			ns
t <sub>PWmin2</sub>	No response at OUT where OUT ≥90% × V <sub>CC2</sub>	C <sub>LOAD</sub> = 100 pF			38	ns
CMTI	Common-mode transient immunity	PWM is tied to GND or $V_{CC1}$ , $V_{CM}$ = 1200 V	100	120		kV/μs

(1) t<sub>sk(pp)</sub> is the magnitude of the difference in propagation delay times between the output of different devices switching in the same direction while operating at identical supply voltages, temperature, input signals and loads guaranteed by characterization.



#### 6.13 Insulation Characteristics Curves

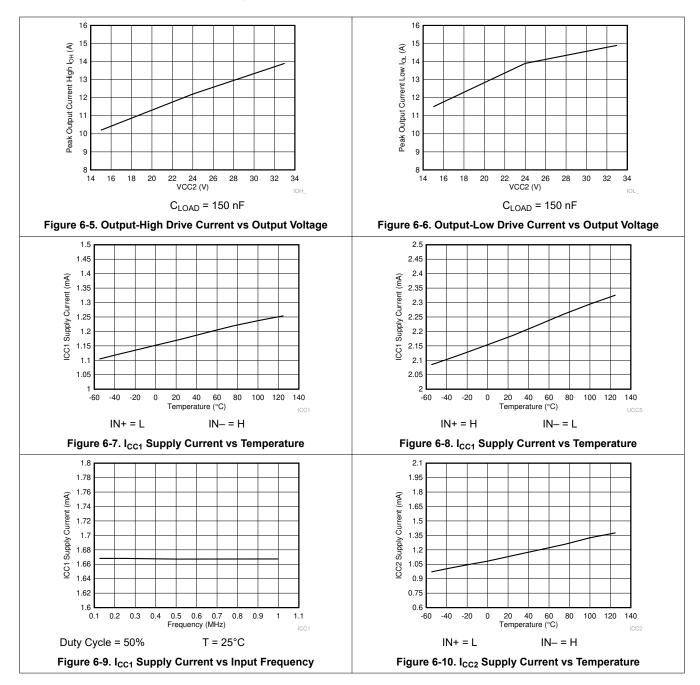






## 6.14 Typical Characteristics

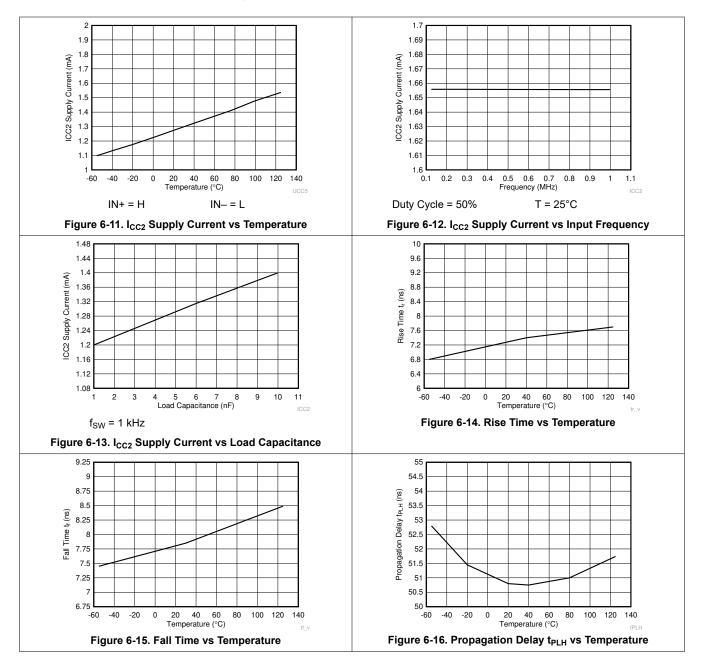
 $V_{CC1}$  = 3.3 V or 5 V, 0.1-µF capacitor from  $V_{CC1}$  to GND1,  $V_{CC2}$ = 15 V, 1-µF capacitor from  $V_{CC2}$  to  $V_{EE2}$ ,  $C_{LOAD}$  = 1 nF,  $T_J$  = -40°C to +125°C, (unless otherwise noted)





## 6.14 Typical Characteristics (continued)

 $V_{CC1}$  = 3.3 V or 5 V, 0.1- $\mu$ F capacitor from  $V_{CC1}$  to GND1,  $V_{CC2}$ = 15 V, 1- $\mu$ F capacitor from  $V_{CC2}$  to  $V_{EE2}$ ,  $C_{LOAD}$  = 1 nF,  $T_J$  = -40°C to +125°C, (unless otherwise noted)

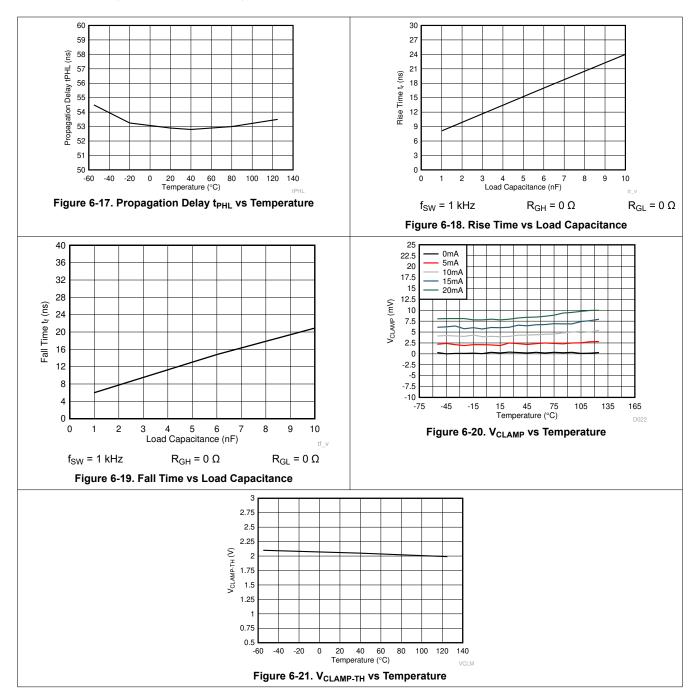






## 6.14 Typical Characteristics (continued)

 $V_{CC1}$  = 3.3 V or 5 V, 0.1- $\mu$ F capacitor from  $V_{CC1}$  to GND1,  $V_{CC2}$ = 15 V, 1- $\mu$ F capacitor from  $V_{CC2}$  to  $V_{EE2}$ ,  $C_{LOAD}$  = 1 nF,  $T_J$  = -40°C to +125°C, (unless otherwise noted)





## 7 Parameter Measurement Information

### 7.1 Propagation Delay, Inverting, and Noninverting Configuration

Figure 7-1 shows the propagation delay for noninverting configurations. Figure 7-2 shows the propagation delay with the inverting configuration. These figures also demonstrate the method used to measure the rise ( $t_r$ ) and fall ( $t_f$ ) times.

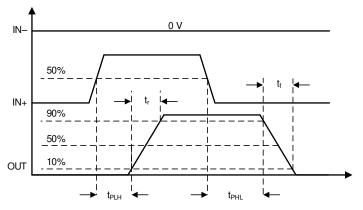


Figure 7-1. Propagation Delay, Noninverting Configuration

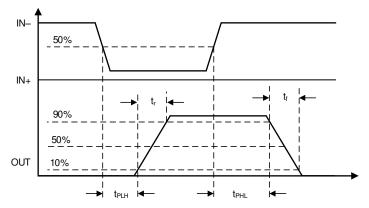
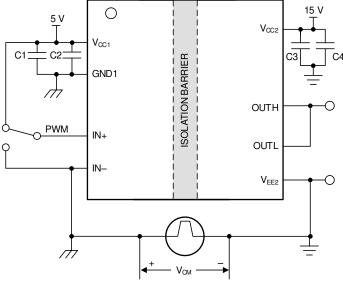


Figure 7-2. Propagation Delay, Inverting Configuration



## 7.1.1 CMTI Testing

Figure 7-3 and Figure 7-4 are simplified diagrams of the CMTI testing configuration.



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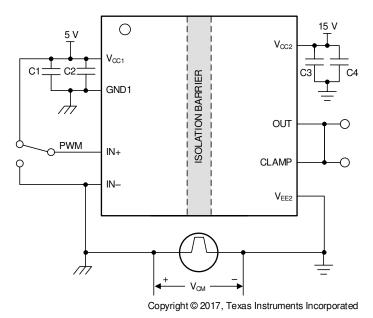


Figure 7-4. CMTI Test Circuit for Miller Clamp (UCC5350MC)



## 8 Detailed Description

## 8.1 Overview

The UCC5350-Q1 family of isolated gate drivers has two variations: split output, and Miller clamp. The isolation inside the UCC5350-Q1 is implemented with high-voltage SiO<sub>2</sub>-based capacitors. The signal across the isolation has an on-off keying (OOK) modulation scheme to transmit the digital data across a silicon dioxide based isolation barrier (see Figure 8-2). The transmitter sends a high-frequency carrier across the barrier to represent one digital state and sends no signal to represent the other digital state. The receiver demodulates the signal after advanced signal conditioning and produces the output through a buffer stage. The UCC5350-Q1 also incorporates advanced circuit techniques to maximize the CMTI performance and minimize the radiated emissions from the high frequency carrier and IO buffer switching. The conceptual block diagram of a digital capacitive isolator, Figure 8-1, shows a functional block diagram of a typical channel. Figure 8-2 shows a conceptual detail of how the OOK scheme works.

Figure 8-1 shows how the input signal passes through the capacitive isolation barrier through modulation (OOK) and signal conditioning.

## 8.2 Functional Block Diagram

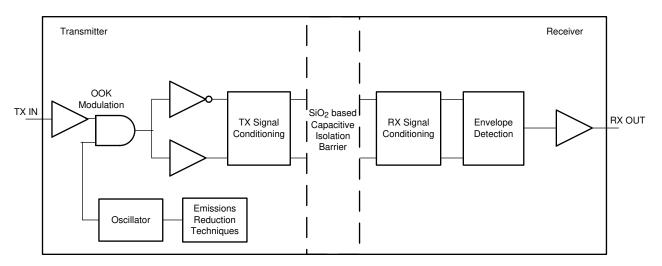


Figure 8-1. Conceptual Block Diagram of a Capacitive Data Channel

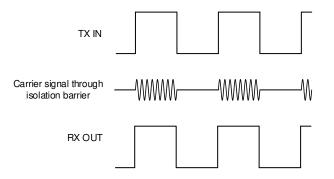
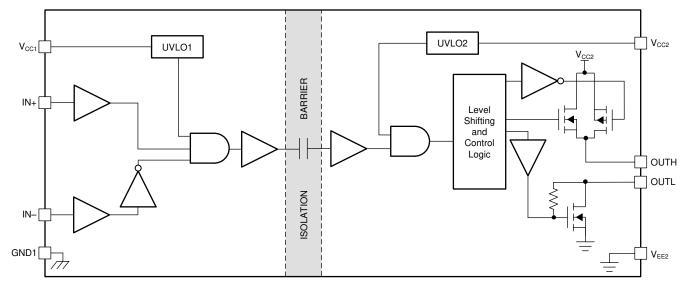
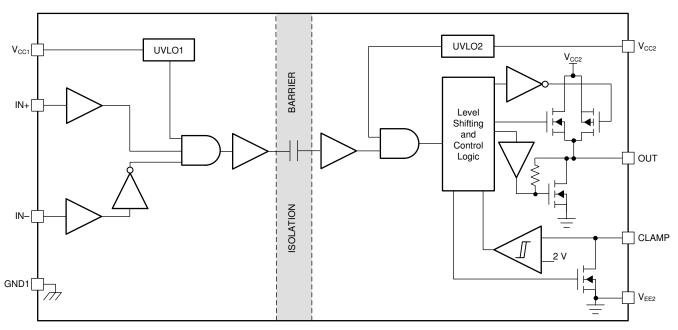


Figure 8-2. On-Off Keying (OOK) Based Modulation Scheme











## 8.3 Feature Description

## 8.3.1 Power Supply

The V<sub>CC1</sub> input power supply supports a wide voltage range from 3 V to 15 V and the V<sub>CC2</sub> output supply supports a voltage range from 13.2 V to 33 V (UCC5350MC) or 9.5 V to 33 V (UCC5350SB).

For operation with unipolar supply, the  $V_{CC2}$  supply is connected to 15 V with respect to VEE2 for IGBTs, and 20 V for SiC MOSFETs. The  $V_{EE2}$  supply is connected to 0 V. In this use case, the Miller clamp helps to prevent a false turn-on of the power switch without a negative voltage rail. The Miller clamping function is implemented by adding a low impedance path between the gate of the power device and the  $V_{EE2}$  supply. Miller current sinks through the clamp pin, which clamps the gate voltage to be lower than the turn-on threshold value for the gate.

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### 8.3.2 Input Stage

The input pins (IN+ and IN–) of the UCC5350-Q1 are based on CMOS-compatible input-threshold logic that is completely isolated from the V<sub>CC2</sub> supply voltage. The input pins are easy to drive with logic-level control signals (such as those from 3.3-V microcontrollers), because the UCC5350-Q1 has a typical high threshold (V<sub>IT+(IN)</sub>) of 0.55 × V<sub>CC1</sub> and a typical low threshold of 0.45 × V<sub>CC1</sub>. A wide hysteresis (V<sub>hys(IN)</sub>) of 0.1 × V<sub>CC1</sub> makes for good noise immunity and stable operation. If either of the inputs are left open, 128 k $\Omega$  of internal pull-down resistance forces the IN+ pin low and 128 k $\Omega$  of internal resistance pulls IN– high. However, TI still recommends grounding an input or tying to VCC1 if it is not being used for improved noise immunity.

Because the input side of the UCC5350-Q1 is isolated from the output driver, the input signal amplitude can be larger or smaller than  $V_{CC2}$  provided that it does not exceed the recommended limit. This feature allows greater flexibility when integrating the gate-driver with control signal sources and allows the user to choose the most efficient  $V_{CC2}$  for any gate. However, the amplitude of any signal applied to IN+ or IN– must never be at a voltage higher than  $V_{CC1}$ .

#### 8.3.3 Output Stage

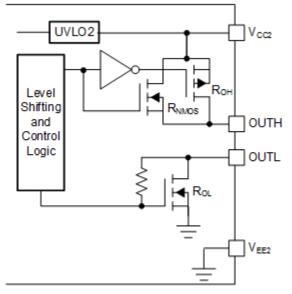
The output stage of the UCC5350-Q1 features a pull-up structure that delivers the highest peak-source current when it is most needed which is during the Miller plateau region of the power-switch turn-on transition (when the power-switch drain or collector voltage experiences dV/dt). The output stage pull-up structure features a P-channel MOSFET and an additional pull-up N-channel MOSFET in parallel. The function of the N-channel MOSFET is to provide a brief boost in the peak-sourcing current, which enables fast turn-on. Fast turn-on is accomplished by briefly turning on the N-channel MOSFET during a narrow instant when the output is changing states from low to high. Table 8-1 lists the typical internal resistance values of the pull-up and pull-down structure.

DEVICE OPTION	R <sub>NMOS</sub>	R <sub>OH</sub>	R <sub>OL</sub>	R <sub>CLAMP</sub>	UNIT
UCC5350MC-Q1	1.54	12	0.26	0.26	Ω
UCC5350SB-Q1	1.54	12	0.26	Not applicable	Ω

#### Table 8-1. UCC5350-Q1 On-Resistance

The  $R_{OH}$  parameter is a DC measurement and is representative of the on-resistance of the P-channel device only. This parameter is only for the P-channel device, because the pull-up N-channel device is held in the OFF state in DC condition and is turned on only for a brief instant when the output is changing states from low to high. Therefore, the effective resistance of the UCC5350-Q1 pull-up stage during this brief turn-on phase is much lower than what is represented by the R<sub>OH</sub> parameter, which yields a faster turn-on. The turn-on-phase output resistance is the parallel combination  $R_{OH} \parallel R_{NMOS}$ .

The pull-down structure in the UCC5350-Q1 is simply composed of an N-channel MOSFET. The output of the UCC5350-Q1 is capable of delivering, or sinking, 5-A peak current pulses. The output voltage swing between  $V_{CC2}$  and  $V_{EE2}$  provides rail-to-rail operation because of the MOS-out stage which delivers very low dropout.





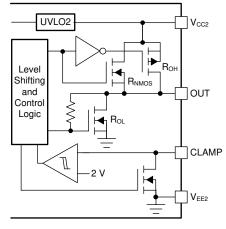


Figure 8-6. Output Stage—M Version

### 8.3.4 Protection Features

### 8.3.4.1 Undervoltage Lockout (UVLO)

UVLO functions are implemented for both the V<sub>CC1</sub> and V<sub>CC2</sub> supplies between the V<sub>CC1</sub> and GND1, and V<sub>CC2</sub> and V<sub>EE2</sub> pins to prevent an underdriven condition on IGBTs and MOSFETs. When V<sub>CC</sub> is lower than V<sub>IT+ (UVLO)</sub> at device start-up or lower than V<sub>IT-(UVLO)</sub> after start-up, the voltage-supply UVLO feature holds the effected output low, regardless of the input pins (IN+ and IN–) as shown in Table 8-2. The V<sub>CC</sub> UVLO protection has a hysteresis feature (V<sub>hys(UVLO)</sub>). This hysteresis prevents chatter when the power supply produces ground noise; this allows the device to permit small drops in bias voltage, which occurs when the device starts switching and operating current consumption increases suddenly. Figure 8-7 shows the UVLO functions.

CONDITION	INP	INPUTS			
CONDITION	IN+	IN–	OUT		
	н	H L L			
V = CND1 < V during device start up	L	Н	L		
$V_{CC1} - GND1 < V_{IT+(UVLO1)}$ during device start-up	Н	Н	L		
	L	L	L		

#### Table 8-2. UCC5350-Q1 V<sub>CC1</sub> UVLO Logic



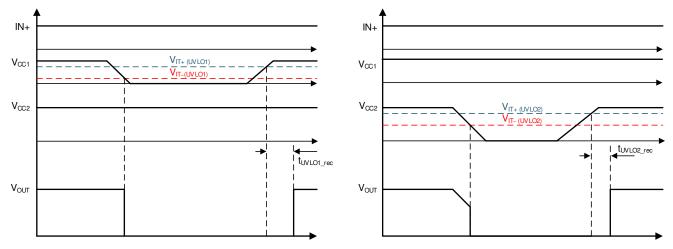
CONDITION	INP	INPUTS		
CONDITION	IN+	IN–	OUT	
	Н	L	L	
(0,0)	L	Н	L	
$V_{CC1} - GND1 < V_{IT-(UVLO1)}$ after device start-up	Н	Н	L	
	L	L	L	

### Table 8-2. UCC5350-Q1 V<sub>CC1</sub> UVLO Logic (continued)

### Table 8-3. UCC5350-Q1 V<sub>CC2</sub> UVLO Logic

CONDITION	INP	INPUTS	
CONDITION	IN+	IN-	OUT
	н	L	L
V = V = c V during device start up	L	Н	L
$V_{CC2} - V_{EE2} < V_{IT+(UVLO2)}$ during device start-up	Н	Н	L
	L	L	L
	н	L	
V = V = c V after device start up	L	Н	L
$V_{CC2} - V_{EE2} < V_{IT-(UVLO2)}$ after device start-up	Н	Н	L
	L	L	L

When  $V_{CC1}$  or  $V_{CC2}$  drops below the UVLO1 or UVLO2 threshold, a delay,  $t_{UVLO1\_rec}$  or  $t_{UVLO2\_rec}$ , occurs on the output when the supply voltage rises above  $V_{IT+(UVLO2)}$  or  $V_{IT+(UVLO2)}$  again. Figure 8-7 shows this delay.





### 8.3.4.2 Active Pulldown

The active pull-down function is used to pull the IGBT or MOSFET gate to the low state when no power is connected to the  $V_{CC2}$  supply. This feature prevents false IGBT and MOSFET turn-on on the OUT and CLAMP pins by clamping the output to approximately 2 V.

When the output stages of the driver are in an unbiased or UVLO condition, the driver outputs are held low by an active clamp circuit that limits the voltage rise on the driver outputs. In this condition, the upper PMOS is resistively held off by a pull-up resistor while the lower NMOS gate is tied to the driver output through a 500-k $\Omega$ resistor. In this configuration, the output is effectively clamped to the threshold voltage of the lower NMOS device, which is approximately 1.5 V when no bias power is available.



#### 8.3.4.3 Short-Circuit Clamping

The short-circuit clamping function is used to clamp voltages at the driver output and pull the active Miller clamp pins slightly higher than the  $V_{CC2}$  voltage during short-circuit conditions. The short-circuit clamping function helps protect the IGBT or MOSFET gate from overvoltage breakdown or degradation. The short-circuit clamping function is implemented by adding a diode connection between the dedicated pins and the  $V_{CC2}$  pin inside the driver. The internal diodes can conduct up to 500-mA current for a duration of 10 µs and a continuous current of 20 mA. Use external Schottky diodes to improve current conduction capability as needed.

#### 8.3.4.4 Active Miller Clamp

The active Miller-clamp function helps to prevent a false turn-on of the power switches caused by Miller current in applications where a unipolar power supply is used. The active Miller-clamp function is implemented by adding a low impedance path between the power-switch gate terminal and ground ( $V_{EE2}$ ) to sink the Miller current. With the Miller-clamp function, the power-switch gate voltage is clamped to less than 2 V during the off state. Figure 9-2 shows a typical application circuit of this function.

### 8.4 Device Functional Modes

Table 8-5 lists the functional modes for the UCC5350-Q1 assuming  $V_{CC1}$  and  $V_{CC2}$  are in the recommended range.

Table 6-4. Function Table for OCC5350SB-Q1							
IN+	IN–	OUTH	OUTL				
Low	Х	Hi-Z	Low				
Х	High	Hi-Z	Low				
High	Low	High	High-Z				

### Table 8-4. Function Table for UCC5350SB-Q1

#### Table 8-5. Function Table for UCC5350MC-Q1

IN+	IN–	OUT		
Low	X	Low		
X	High	Low		
High	Low	High		

#### 8.4.1 ESD Structure

Figure 8-9 shows the multiple diodes involved in the ESD protection components of the UCC5350-Q1 device. This provides pictorial representation of the absolute maximum rating for the device.



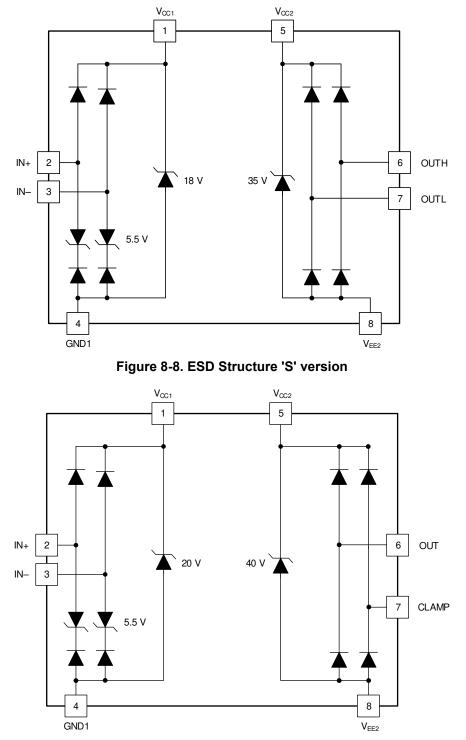


Figure 8-9. ESD Structure ' M' Version



## 9 Application and Implementation

#### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 9.1 Application Information

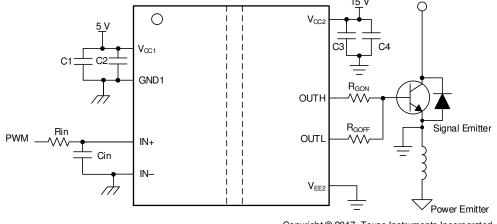
The UCC5350-Q1 is a simple, isolated gate driver for power semiconductor devices, such as MOSFETs, IGBTs, or SiC MOSFETs. The family of devices is intended for use in applications such as motor control, solar inverters, switched-mode power supplies, and industrial inverters.

The UCC5350-Q1 has two pinout configurations, featuring split outputs and Miller clamp. The split outputs, OUTH and OUTL, are used to separately decouple the power transistor turn on and turn off commutations.

The M version features active Miller clamping, which can be used to prevent false turn-on of the power transistors induced by the Miller current. The device comes in an 8-pin D and 8-pin DWV package and has creepage, or clearance, of 4 mm and 8.5 mm, respectively, which is suitable for applications where basic or reinforced isolation is required. The UCC5350-Q1 offers a 5-A minimum drive current.

### 9.2 Typical Application

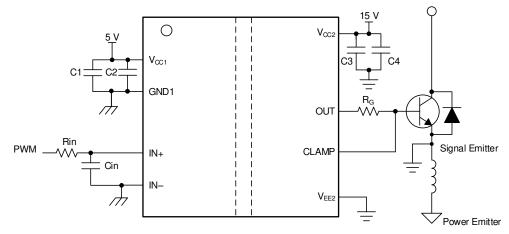
The circuits in Figure 9-1 and Figure 9-2 show a typical application for driving IGBTs.



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### Figure 9-2. Typical Application Circuit for UCC5350MC-Q1 to Drive IGBT

#### 9.2.1 Design Requirements

Table 9-1. UCC5350-Q1 Design Re	equirements	

PARAMETER	VALUE	UNIT
V <sub>CC1</sub>	3.3	V
V <sub>CC2</sub> – V <sub>EE2</sub>	18	V
IN+	3.3	V
IN-	GND1	-
Switching frequency	150	kHz
Gate Charge of Power Device	126	nC

### 9.2.2 Detailed Design Procedure

#### 9.2.2.1 Designing IN+ and IN– Input Filter

TI recommends that users avoid shaping the signals to the gate driver in an attempt to slow down (or delay) the signal at the output. However, a small input filter,  $R_{IN}$ - $C_{IN}$ , can be used to filter out the ringing introduced by nonideal layout or long PCB traces.

Such a filter should use an R<sub>IN</sub> resistor with a value from 0  $\Omega$  to 100  $\Omega$  and a C<sub>IN</sub> capacitor with a value from 10 pF to 1000 pF. In the example, the selected value for R<sub>IN</sub> is 51  $\Omega$  and C<sub>IN</sub> is 33 pF, with a corner frequency of approximately 100 MHz.

When selecting these components, pay attention to the trade-off between good noise immunity and propagation delay.

#### 9.2.2.2 Gate-Driver Output Resistor

The external gate-driver resistors,  $R_{G(ON)}$  and  $R_{G(OFF)}$  are used to:

- 1. Limit ringing caused by parasitic inductances and capacitances
- 2. Limit ringing caused by high voltage or high current switching dv/dt, di/dt, and body-diode reverse recovery
- 3. Fine-tune gate drive strength, specifically peak sink and source current to optimize the switching loss
- 4. Reduce electromagnetic interference (EMI)

The output stage has a pull-up structure consisting of a P-channel MOSFET and an N-channel MOSFET in parallel. The combined typical peak source current is 10 A for UCC5350-Q1. Use Equation 1 to estimate the peak source current.



(1)

$$I_{OH} = \frac{V_{CC2} - V_{EE2}}{R_{NMOS} ||R_{OH} + R_{GON} + R_{GFET\_Int}}$$

where

- $R_{ON}$  is the external turn-on resistance, which is 2.2  $\Omega$  in this example.
- R<sub>GFET\_Int</sub> is the power transistor internal gate resistance, found in the power transistor data sheet. We will assume 1.8Ω for our example.
- I<sub>OH</sub> is the typical peak source current which is the minimum value between 10 A, the gate-driver peak source current, and the calculated value based on the gate-drive loop resistance.

In this example, the peak source current is approximately 3.36 A as calculated in Equation 2.

$$I_{OH} = \frac{V_{CC2} - V_{EE2}}{R_{NMOS} ||R_{OH} + R_{GON} + R_{GFET\_Int}} = \frac{18 V}{1.54\Omega ||12\Omega + 2.2\Omega + 1.8\Omega} \approx 3.36A$$
(2)

Similarly, use Equation 3 to calculate the peak sink current.

$$I_{OL} = \frac{V_{CC2} - V_{EE2}}{R_{OL} + R_{GOFF} + R_{GFET\_Int}}$$
(3)

where

- $R_{OFF}$  is the external turn-off resistance, which is 2.2  $\Omega$  in this example.
- I<sub>OL</sub> is the typical peak sink current which is the minimum value between 10 A, the gate-driver peak sink current, and the calculated value based on the gate-drive loop resistance.

In this example, the peak sink current is the minimum value between Equation 4 and 10 A.

$$I_{OL} = \frac{V_{CC2} - V_{EE2}}{R_{OL} + R_{GOFF} + R_{GFET\_Int}} = \frac{18V}{0.26\Omega + 2.2\Omega + 1.8\Omega} \approx 4.23A$$
(4)

Note

The estimated peak current is also influenced by PCB layout and load capacitance. Parasitic inductance in the gate-driver loop can slow down the peak gate-drive current and introduce overshoot and undershoot. Therefore, TI strongly recommends that the gate-driver loop should be minimized. Conversely, the peak source and sink current is dominated by loop parasitics when the load capacitance ( $C_{ISS}$ ) of the power transistor is very small (typically less than 1 nF) because the rising and falling time is too small and close to the parasitic ringing period.

#### 9.2.2.3 Estimate Gate-Driver Power Loss

The total loss,  $P_{G}$ , in the gate-driver subsystem includes the power losses ( $P_{GD}$ ) of the UCC5350-Q1 device and the power losses in the peripheral circuitry, such as the external gate-drive resistor.

The P<sub>GD</sub> value is the key power loss which determines the thermal safety-related limits of the UCC5350-Q1 device, and it can be estimated by calculating losses from several components.

The first component is the static power loss,  $P_{GDQ}$ , which includes quiescent power loss on the driver as well as driver self-power consumption when operating with a certain switching frequency. The  $P_{GDQ}$  parameter is measured on the bench with no load connected to the OUT pins at a given  $V_{CC1}$ ,  $V_{CC2}$ , switching frequency, and ambient temperature. In this example,  $V_{CC1}$  is 3.3V and  $V_{CC2}$  is 18 V. The current on each power supply, with PWM switching from 0 V to 3.3 V at 150 kHz, is measured to be  $I_{CC1} = 1.67$  mA and  $I_{CC2} = 1.11$  mA. Therefore, use Equation 5 to calculate  $P_{GDQ}$ .

$$\mathsf{P}_{\mathsf{GDQ}} = \mathsf{V}_{\mathsf{CC1}} \times \mathsf{I}_{\mathsf{VCC1}} + (\mathsf{V}_{\mathsf{CC2}} - \mathsf{V}_{\mathsf{EE2}}) \times \mathsf{I}_{\mathsf{CC2}} \approx 23.31 \text{mW}$$

(5)



$$P_{GSW} = (V_{CC2} - V_{EE2}) \times Q_G \times f_{SW}$$

where

Q<sub>G</sub> is the gate charge of the power transistor at V<sub>CC2</sub>.

So, for this example application the total dynamic loss from load switching is approximately 340 mW as calculated in Equation 7.

$$P_{GSW} = 18 \text{ V} \times 126 \text{ nC} \times 150 \text{ kHz} = 340 \text{ mW}$$
 (7)

Q<sub>G</sub> represents the total gate charge of the power transistor and is subject to change with different testing conditions. The UCC5350-Q1 gate-driver loss on the output stage, PGDO, is part of PGSW. PGDO is equal to PGSW if the external gate-driver resistance and power-transistor internal resistance are 0  $\Omega$ , and all the gate driver-loss will be dissipated inside the UCC5350-Q1. If an external turn-on and turn-off resistance exists, the total loss is distributed between the gate driver pull-up/down resistance, external gate resistance, and power-transistor internal resistance. Importantly, the pull-up/down resistance is a linear and fixed resistance if the source/sink current is not saturated to 10 A, however, it will be non-linear if the source/sink current is saturated. The gate driver loss will be estimated in the case in which it is not saturated as given in Equation 8.

$$P_{GDO} = \frac{P_{GSW}}{2} \left( \frac{R_{OH} || R_{NMOS}}{R_{OH} || R_{NMOS} + R_{GON} + R_{GFET\_Int}} + \frac{R_{OL}}{R_{OL} + R_{GOFF} + R_{GFET\_Int}} \right)$$
(8)

In this design example, all the predicted source and sink currents are less than 10 A, therefore, use Equation 9 to estimate the gate-driver loss.

$$\mathsf{P}_{\mathsf{GDO}} = \frac{340 \text{ mW}}{2} \left( \frac{12 \Omega \| 1.54 \Omega}{12 \Omega \| 1.54 \Omega + 2.2 \Omega + 1.8 \Omega} + \frac{0.26 \Omega}{0.26 \Omega + 2.2 \Omega + 1.8 \Omega} \right) \approx 53.66 \text{ mW}$$
(9)

where

V<sub>OUTH/L(t)</sub> is the gate-driver OUT pin voltage during the turnon and turnoff period. In cases where the output is saturated for some time, this value can be simplified as a constant-current source (10 A at turnon and turnoff) charging or discharging a load capacitor. Then, the V<sub>OUTH/L(t)</sub> waveform will be linear and the T<sub>R Svs</sub> and T<sub>F Svs</sub> can be easily predicted.

Use Equation 10 to calculate the total gate-driver loss dissipated in the UCC5350-Q1 gate driver, P<sub>GD</sub>.

$$P_{GD} = P_{GDQ} + P_{GDO} = 25.31 \text{mW} + 53.66 \text{mW} = 78.97 \text{mW}$$
(10)

#### 9.2.2.4 Estimating Junction Temperature

Use the equation below to estimate the junction temperature  $(T_1)$  of the UCC5350-Q1 family.

$$T_{J} = T_{C} + \Psi_{JT} \times P_{GD}$$
<sup>(11)</sup>

where

- $T_{\rm C}$  is the UCC5350-Q1 case-top temperature measured with a thermocouple or some other instrument.
- $\Psi_{\rm JT}$  is the junction-to-top characterization parameter from the Thermal Information table.

Using the junction-to-top characterization parameter ( $\Psi_{JT}$ ) instead of the junction-to-case thermal resistance  $(R_{\theta,JC})$  can greatly improve the accuracy of the junction temperature estimation. The majority of the thermal

(6)

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energy of most ICs is released into the PCB through the package leads, whereas only a small percentage of the total energy is released through the top of the case (where thermocouple measurements are usually conducted). The R<sub>θJC</sub> resistance can only be used effectively when most of the thermal energy is released through the case, such as with metal packages or when a heat sink is applied to an IC package. In all other cases, use of R<sub>θJC</sub> will inaccurately estimate the true junction temperature. The  $\Psi_{JT}$  parameter is experimentally derived by assuming that the dominant energy leaving through the top of the IC will be similar in both the testing environment and the application environment. As long as the recommended layout guidelines are observed, junction temperature estimations can be made accurately to within a few degrees Celsius.

### 9.2.3 Selecting V<sub>CC1</sub> and V<sub>CC2</sub> Capacitors

Bypass capacitors for the  $V_{CC1}$  and  $V_{CC2}$  supplies are essential for achieving reliable performance. TI recommends choosing low-ESR and low-ESL, surface-mount, multi-layer ceramic capacitors (MLCC) with sufficient voltage ratings, temperature coefficients, and capacitance tolerances.

#### Note

DC bias on some MLCCs will impact the actual capacitance value. For example, a 25-V, 1- $\mu$ F X7R capacitor is measured to be only 500 nF when a DC bias of 15-V<sub>DC</sub> is applied.

#### 9.2.3.1 Selecting a V<sub>CC1</sub> Capacitor

A bypass capacitor connected to the V<sub>CC1</sub> pin supports the transient current required for the primary logic and the total current consumption, which is only a few milliamperes. Therefore, a 50-V MLCC with over 100 nF is recommended for this application. If the bias power-supply output is located a relatively long distance from the V<sub>CC1</sub> pin, a tantalum or electrolytic capacitor with a value greater than 1  $\mu$ F should be placed in parallel with the MLCC.

#### 9.2.3.2 Selecting a V<sub>CC2</sub> Capacitor

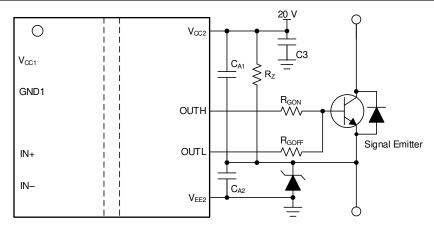
A 50-V, 10- $\mu$ F MLCC and a 50-V, 0.22- $\mu$ F MLCC are selected for the C<sub>VCC2</sub> capacitor. If the bias power supply output is located a relatively long distance from the V<sub>CC2</sub> pin, a tantalum or electrolytic capacitor with a value greater than 10  $\mu$ F should be used in parallel with C<sub>VCC2</sub>.

#### 9.2.3.3 Application Circuits with Output Stage Negative Bias

When parasitic inductances are introduced by nonideal PCB layout and long package leads (such as TO-220 and TO-247 type packages), ringing in the gate-source drive voltage of the power transistor could occur during high di/dt and dv/dt switching. If the ringing is over the threshold voltage, unintended turn-on and shoot-through could occur. Applying a negative bias on the gate drive is a popular way to keep such ringing below the threshold. A few examples of implementing negative gate-drive bias follow.

Figure 9-3 shows the first example with negative bias turn-off on the output using a Zener diode on the isolated power-supply output stage. The negative bias is set by the Zener diode voltage. If the isolated power supply is equal to 20 V, the turn-off voltage is -5.1 V and the turn-on voltage is 20 V - 5.1 V  $\approx 15$  V.





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Figure 9-3. Negative Bias With Zener Diode on Iso-Bias Power-Supply Output

Figure 9-4 shows another example which uses two supplies (or single-input, double-output power supply). The power supply across  $V_{CC2}$  and the emitter determines the positive drive output voltage and the power supply across  $V_{EE2}$  and the emitter determines the negative turn-off voltage. This solution requires more power supplies than the first example, however, it provides more flexibility when setting the positive and negative rail voltages.

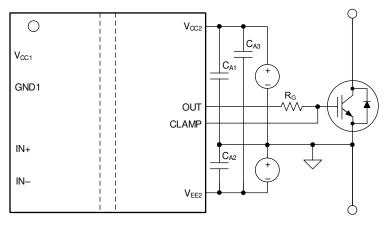


Figure 9-4. Negative Bias With Two Iso-Bias Power Supplies



### 9.2.4 Application Curve

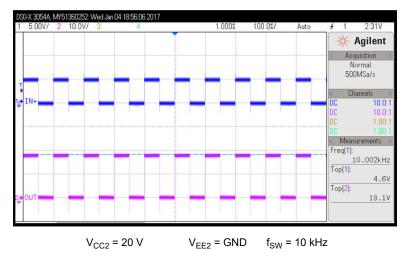


Figure 9-5. PWM Input and Gate Voltage Waveform

## **10 Power Supply Recommendations**

The recommended input supply voltage ( $V_{CC1}$ ) for the UCC5350-Q1 device is from 3 V to 15 V. The lower limit of the range of output bias-supply voltage ( $V_{CC2}$ ) is determined by the internal UVLO protection feature of the device. The  $V_{CC1}$  and  $V_{CC2}$  voltages should not fall below their respective UVLO thresholds for normal operation, or else the gate-driver outputs can become clamped low for more than 50 µs by the UVLO protection feature. For more information on UVLO, see Section 8.3.4.1. The higher limit of the  $V_{CC2}$  range depends on the maximum gate voltage of the power device that is driven by the UCC5350-Q1 device, and should not exceed the recommended maximum  $V_{CC2}$  of 33 V. A local bypass capacitor should be placed between the  $V_{CC2}$  and  $V_{EE2}$  pins, with a value of 220-nF to 10-µF for device biasing. TI recommends placing an additional 100-nF capacitor in parallel with the device biasing capacitor for high frequency filtering. Both capacitors should be positioned as close to the device as possible. Low-ESR, ceramic surface-mount capacitors are recommended. Similarly, a bypass capacitor should also be placed between the  $V_{CC1}$  and GND1 pins. Given the small amount of current drawn by the logic circuitry within the input side of the UCC5350-Q1 device, this bypass capacitor has a minimum recommended value of 100 nF.

## 11 Layout

## **11.1 Layout Guidelines**

Designers must pay close attention to PCB layout to achieve optimum performance for the UCC5350-Q1. Some key guidelines are:

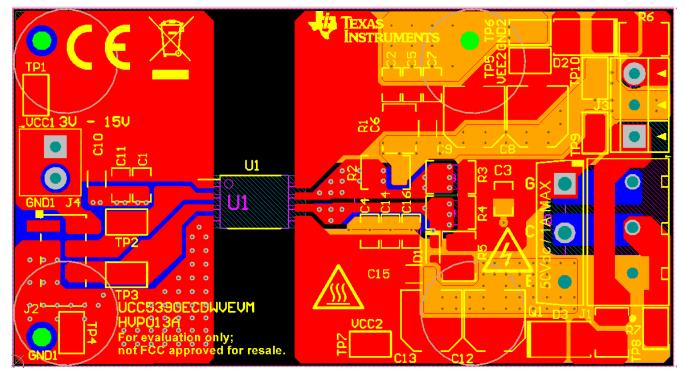
- Component placement:
  - Low-ESR and low-ESL capacitors must be connected close to the device between the V<sub>CC1</sub> and GND1
    pins and between the V<sub>CC2</sub> and V<sub>EE2</sub> pins to bypass noise and to support high peak currents when turning
    on the external power transistor.
  - To avoid large negative transients on the V<sub>EE2</sub> pins connected to the switch node, the parasitic inductances between the source of the top transistor and the source of the bottom transistor must be minimized.
- Grounding considerations:
  - Limiting the high peak currents that charge and discharge the transistor gates to a minimal physical area is essential. This limitation decreases the loop inductance and minimizes noise on the gate terminals of the transistors. The gate driver must be placed as close as possible to the transistors.
- High-voltage considerations:



- To ensure isolation performance between the primary and secondary side, avoid placing any PCB traces or copper below the driver device. A PCB cutout or groove is recommended in order to prevent contamination that may compromise the isolation performance.
- Thermal considerations:
  - A large amount of power may be dissipated by the UCC5350-Q1 if the driving voltage is high, the load is heavy, or the switching frequency is high (for more information, see Section 9.2.2.3). Proper PCB layout can help dissipate heat from the device to the PCB and minimize junction-to-board thermal impedance (θ<sub>JB</sub>).
  - Increasing the PCB copper connecting to the V<sub>CC2</sub> and V<sub>EE2</sub> pins is recommended, with priority on
    maximizing the connection to V<sub>EE2</sub>. However, the previously mentioned high-voltage PCB considerations
    must be maintained.
  - If the system has multiple layers, TI also recommends connecting the V<sub>CC2</sub> and V<sub>EE2</sub> pins to internal ground or power planes through multiple vias of adequate size. These vias should be located close to the IC pins to maximize thermal conductivity. However, keep in mind that no traces or coppers from different high voltage planes are overlapping.

### **11.2 Layout Example**

Figure 11-1 shows a PCB layout example with the signals and key components labeled. The UCC5390ECDWV evaluation module (EVM) is given as an example, available in the same DWV package as the UCC5350-Q1. The UCC5390EC has a split emitter versus Miller clamp so although the layout is not exactly the same, general guidelines and practices still apply. The evaluation board can be configured for the Miller clamp version, as well, as described in the *UCC5390ECDWV Isolated Gate Driver Evaluation Module User's Guide*.



A. No PCB traces or copper are located between the primary and secondary side, which ensures isolation performance.

### Figure 11-1. Layout Example

Figure 11-2 and Figure 11-3 show the top and bottom layer traces and copper.



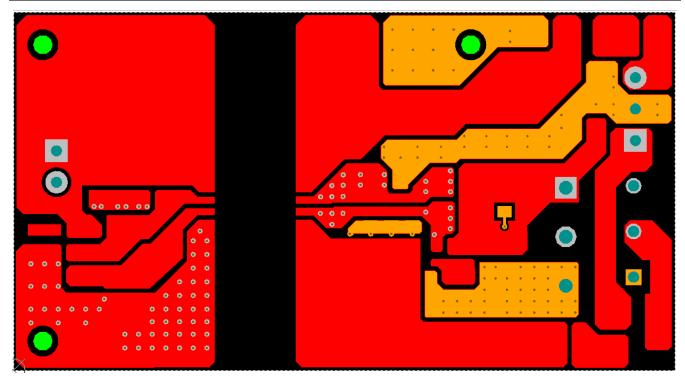


Figure 11-2. Top-Layer Traces and Copper

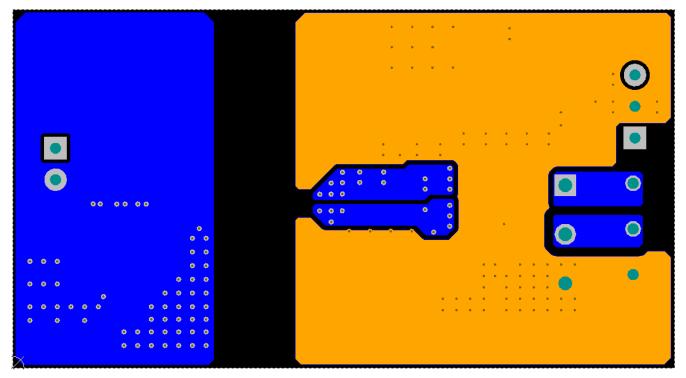


Figure 11-3. Bottom-Layer Traces and Copper (Flipped)

Figure 11-4 shows the 3D layout of the top view of the PCB.

UCC5350-Q1 SLUSE29E - MAY 2020 - REVISED FEBRUARY 2024



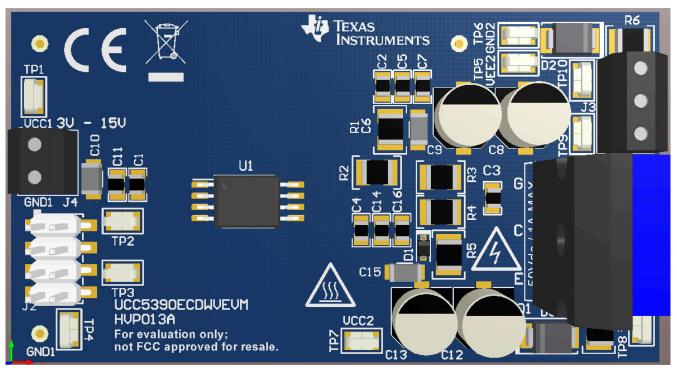
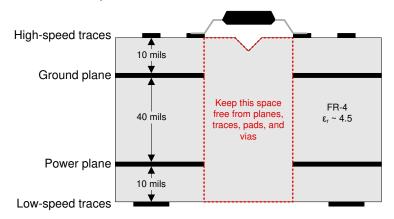


Figure 11-4. 3-D PCB View

## 11.3 PCB Material

Use standard FR-4 UL94V-0 printed circuit board. This PCB is preferred over cheaper alternatives because of lower dielectric losses at high frequencies, less moisture absorption, greater strength and stiffness, and the self-extinguishing flammability-characteristics.

Figure 11-5 shows the recommended layer stack.







## 12 Device and Documentation Support

### 12.1 Device Support

#### 12.1.1 Third-Party Products Disclaimer

TI'S PUBLICATION OF INFORMATION REGARDING THIRD-PARTY PRODUCTS OR SERVICES DOES NOT CONSTITUTE AN ENDORSEMENT REGARDING THE SUITABILITY OF SUCH PRODUCTS OR SERVICES OR A WARRANTY, REPRESENTATION OR ENDORSEMENT OF SUCH PRODUCTS OR SERVICES, EITHER ALONE OR IN COMBINATION WITH ANY TI PRODUCT OR SERVICE.

#### **12.2 Documentation Support**

#### 12.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, Digital Isolator Design Guide
- Texas Instruments, *Isolation Glossary*
- Texas Instruments, SN6501 Transformer Driver for Isolated Power Supplies data sheet
- Texas Instruments, SN6505A Low-Noise 1-A Transformer Drivers for Isolated Power Supplies data sheet
- Texas Instruments, UCC5390ECDWV Isolated Gate Driver Evaluation Module user's guide
- Texas Instruments, UCC53x0xD Evaluation Module user's guide

### 12.3 Certifications

UL Online Certifications Directory, "FPPT2.E181974 Nonoptical Isolating Devices - Component" Certificate Number: 20170718-E181974,

#### **12.4 Receiving Notification of Documentation Updates**

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

#### **12.5 Support Resources**

TI E2E<sup>™</sup> support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

#### 12.6 Trademarks

TI E2E<sup>™</sup> is a trademark of Texas Instruments.

All trademarks are the property of their respective owners.

#### 12.7 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### 12.8 Glossary

TI Glossary This glossary lists and explains terms, acronyms, and definitions.



## 13 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision D (August 2022) to Revision E (February 2024)		Page
•	Changed CTI and Material Group values in insulation specifications and added table note	6

Changes from Revision C (June 2022) to Revision D (August 2022)		Page
•	Changed UCC5350SB-Q1 from Advance Information to Production Data	1

Changes from Revision B (June 2020) to Revision C (June 2022)		
Added the Advance Information for the UCC5350SBQDRQ1 device	1	
Added Section 4		
Added the UCC5350SB device to Section 5		
Added SB-Q1 D package power ratings		
Added SB-Q1 insulation specs		
Added the UL certificate number for the D package		
Added the UL certificate number for the DWV package		
Added SB-Q1 D package safety limiting values		
Added SB-Q1 parameters		
Added minimum pulse width specs		
Added Table 8-4		
Added SB-Q1 ESD figure		
Added typical application circuit for SB-Q1		

## 14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	•	Pins	•	Eco Plan	Lead finish/	MSL Peak Temp	Op Temp (°C)	Device Marking	Samples
	(1)		Drawing		Qty	(2)	Ball material	(3)		(4/5)	
PUCC5350MCQDWVQ1	OBSOLETE	SOIC	DWV	8		TBD	(6) Call TI	Call TI			
UCC5350MCQDQ1	LIFEBUY	SOIC	D	8	75	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	5350Q	
UCC5350MCQDRQ1	ACTIVE	SOIC	D	8	2500	RoHS & Green	Call TI   NIPDAU	Level-2-260C-1 YEAR	-40 to 125	5350Q	Gammalaa
											Samples
UCC5350MCQDWVQ1	LIFEBUY	SOIC	DWV	8	64	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 125	5350MCQ	
UCC5350MCQDWVRQ1	ACTIVE	SOIC	DWV	8	1000	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 125	5350MCQ	Samples
UCC5350SBQDRQ1	ACTIVE	SOIC	D	8	2500	RoHS & Green	Call TI   NIPDAU	Level-3-260C-168 HR	-40 to 125	5350Q	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.



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### PACKAGE OPTION ADDENDUM

12-Apr-2024

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

#### OTHER QUALIFIED VERSIONS OF UCC5350-Q1 :

• Catalog : UCC5350

NOTE: Qualified Version Definitions:

• Catalog - TI's standard catalog product

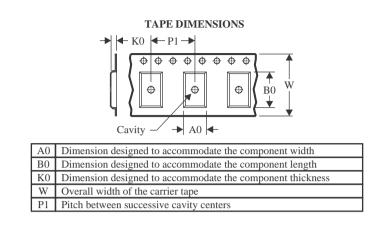


Texas

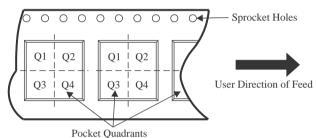
STRUMENTS

#### TAPE AND REEL INFORMATION





#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
UCC5350MCQDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
UCC5350MCQDWVRQ1	SOIC	DWV	8	1000	330.0	16.4	12.05	6.15	3.3	16.0	16.0	Q1
UCC5350SBQDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1



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# PACKAGE MATERIALS INFORMATION

25-Apr-2024



\*All dimensions are nominal

Device	Device Package Type		Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
UCC5350MCQDRQ1	SOIC	D	8	2500	356.0	356.0	35.0
UCC5350MCQDWVRQ1	SOIC	DWV	8	1000	350.0	350.0	43.0
UCC5350SBQDRQ1	SOIC	D	8	2500	356.0	356.0	35.0

#### TEXAS INSTRUMENTS

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25-Apr-2024

#### TUBE



#### - B - Alignment groove width

#### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	Τ (μm)	B (mm)
UCC5350MCQDQ1	D	SOIC	8	75	506.6	8	3940	4.32
UCC5350MCQDQ1	D	SOIC	8	75	505.46	6.76	3810	4
UCC5350MCQDWVQ1	DWV	SOIC	8	64	505.46	13.94	4826	6.6

# DWV0008A



#### SOIC - 2.8 mm max height

SOIC



- NOTES:
- 1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing
- Per ASME Y14.5M.
   This drawing is subject to change without notice.
   This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm, per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm, per side.

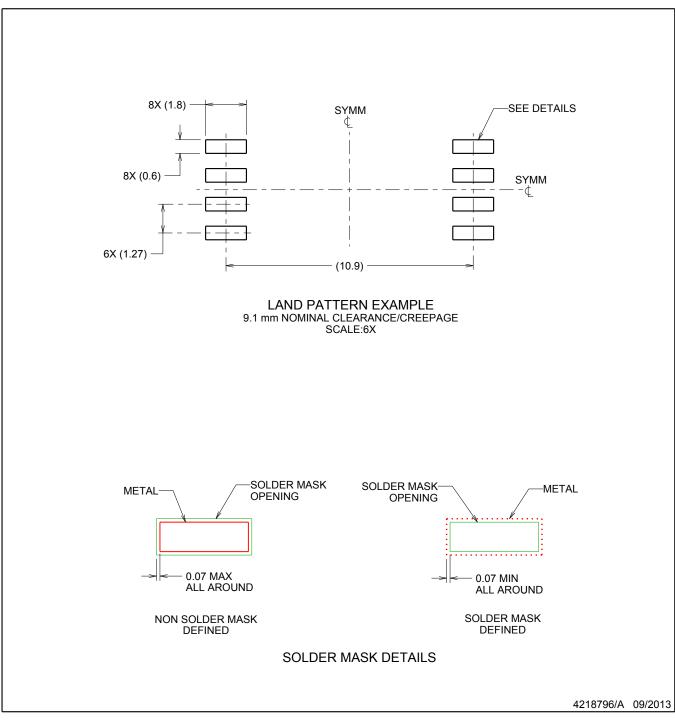


# DWV0008A

# EXAMPLE BOARD LAYOUT

### SOIC - 2.8 mm max height

SOIC



NOTES: (continued)

5. Publication IPC-7351 may have alternate designs.

6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



# EXAMPLE STENCIL DESIGN

# DWV0008A

### SOIC - 2.8 mm max height

SOIC



NOTES: (continued)



<sup>7.</sup> Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

<sup>8.</sup> Board assembly site may have different recommendations for stencil design.

# D0008A



# **PACKAGE OUTLINE**

#### SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



#### NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



# D0008A

# **EXAMPLE BOARD LAYOUT**

### SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



## D0008A

# **EXAMPLE STENCIL DESIGN**

### SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.



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