

BQ25756 Standalone/I²C Controlled, 1- to 14-Cell Bidirectional Buck-Boost Battery Charge Controller

1 Features

- Wide input voltage operating range: 4.2V to 70V
- Wide battery voltage operating range: up to 70V with multi-chemistry support:
 - 1- to 14-cell Li-ion charge profile
 - 1- to 16-cell LiFePO₄ charge profile
- Synchronous buck-boost charge controller with NFET drivers
 - Adjustable switching frequency from 200kHz to 600kHz
 - Optional synchronization to external clock
 - Integrated loop compensation with soft start
 - Optional gate driver supply input for optimized efficiency
- Automatic maximum power point tracking (MPPT) for solar charging
- Bidirectional converter operation (Reverse Mode) supporting USB-PD Extended Power Range (EPR)
 - Adjustable input voltage (VAC) regulation from 3.3V to 65V with 20mV/step
 - Adjustable input current regulation (R_{AC_SNS}) from 400mA to 20A with 50mA/step using 2mΩ resistor
- High accuracy
 - ±0.5% charge voltage regulation
 - ±3% charge current regulation
 - ±3% input current regulation
- I²C controlled for optimal system performance with resistor-programmable option
 - Hardware adjustable input and output current limits
- Integrated 16-bit ADC for voltage, current, and temperature monitoring
- High safety integration
 - Adjustable input overvoltage and undervoltage protection
 - Battery Overvoltage and overcurrent protection
 - Charging safety timer
 - Battery short protection
 - Thermal shutdown
- Status outputs
 - Adapter present status (PG)
 - Charger Operation status (STAT1, STAT2)
- Package
 - 36-pin 6mm × 5mm QFN

2 Applications

- [Kick eScooter, eBike](#)
- [Cordless power tool, Garden tool](#)
- [Robotic lawn mower](#)
- [Portable power station](#)
- [Cordless vacuum cleaner, Vacuum robot](#)
- Solar charger
- USB-PD EPR (Extended Power Range)

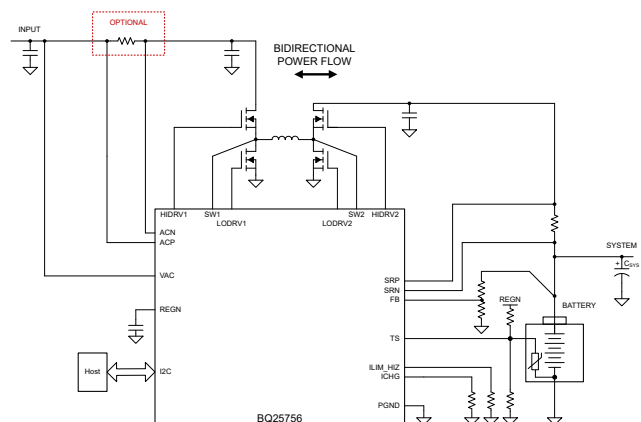
3 Description

The BQ25756 is a wide input voltage, switched-mode buck-boost Li-Ion, Li-polymer, or LiFePO₄ battery charge controller with bidirectional power flow support. The device offers high-efficiency battery charging over a wide voltage range with accurate charge current and charge voltage regulation, in addition to automatic charge preconditioning, termination, and charge status indication. The device integrates all the loop compensation for the buck-boost converter, thereby providing a high density solution with ease of use. In reverse mode, the device draws power from the battery and regulates the input terminal voltage with an added constant current loop for protection, supporting USB-PD EPR power profile.

Package Information

PART NUMBER	PACKAGE ⁽¹⁾	PACKAGE SIZE ⁽²⁾	BODY SIZE (NOM)
BQ25756	VQFN (36)	6.0mm × 5.0mm	6.0 × 5.0mm ²

- (1) For all available packages, see [Section 12](#).
- (2) The package size (length × width) is a nominal value and includes pins, where applicable.



Simplified Schematic



Table of Contents

1 Features	1	7 Application and Implementation	59
2 Applications	1	7.1 Application Information.....	59
3 Description	1	7.2 Typical Applications.....	59
4 Pin Configuration and Functions	3	8 Power Supply Recommendations	70
5 Specifications	6	9 Layout	71
5.1 Absolute Maximum Ratings.....	6	9.1 Layout Guidelines.....	71
5.2 ESD Ratings.....	6	9.2 Layout Example.....	72
5.3 Recommended Operating Conditions.....	7	10 Device and Documentation Support	74
5.4 Thermal Information.....	7	10.1 Device Support.....	74
5.5 Electrical Characteristics.....	8	10.2 Receiving Notification of Documentation Updates..	74
5.6 Timing Requirements.....	14	10.3 Support Resources.....	74
5.7 Typical Characteristics	15	10.4 Trademarks.....	74
6 Detailed Description	18	10.5 Electrostatic Discharge Caution.....	74
6.1 Overview.....	18	10.6 Glossary.....	74
6.2 Functional Block Diagram.....	19	11 Revision History	74
6.3 Feature Description.....	20	12 Mechanical, Packaging, and Orderable	
6.4 Device Functional Modes.....	36	Information	75
6.5 BQ25756 Registers.....	37		

4 Pin Configuration and Functions

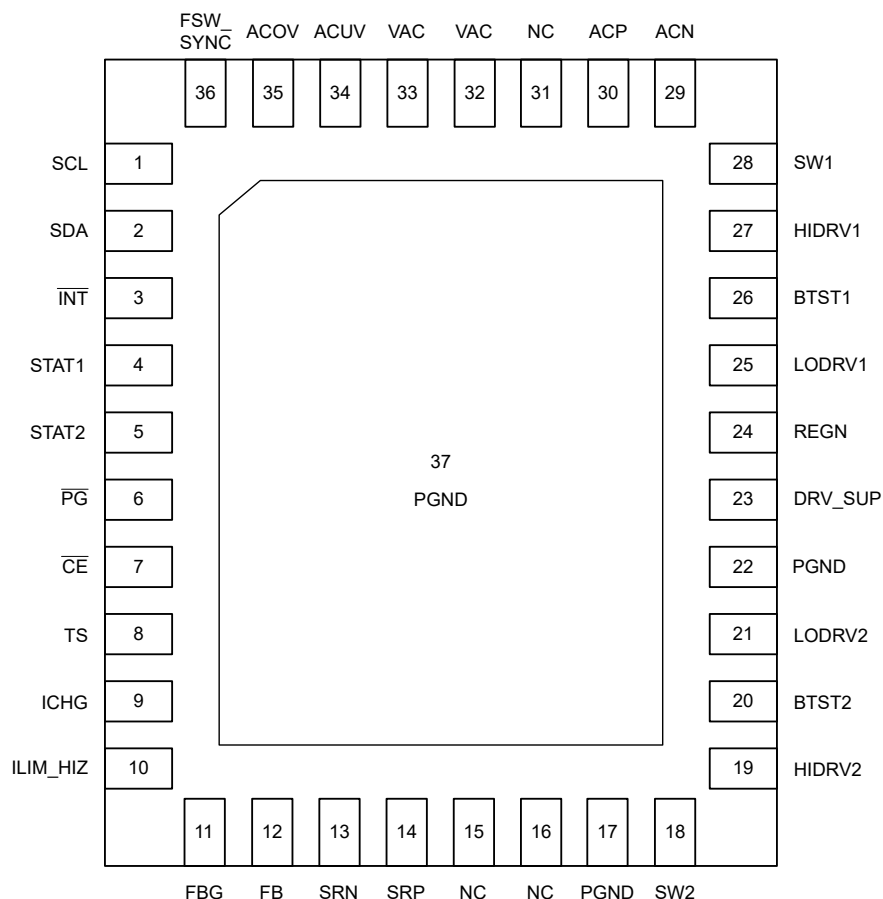


Figure 4-1. BQ25756, RRV Package 36-pin VQFN Top View

Table 4-1. Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
SCL	1	I	I²C Interface Clock – Connect SCL to the logic rail through a 10kΩ resistor.
SDA	2	IO	I²C Interface Data – Connect SDA to the logic rail through a 10kΩ resistor.
INT	3	O	Open Drain Interrupt Output – Connect the INT pin to a logic rail via 10kΩ resistor. The INT pin sends an active low, 256μs pulse to host to report the charger device status and faults.
STAT1	4	O	Open Drain Charge Status 1 Output – STAT1 and STAT2 indicate various charger operations, see Table 6-6 . Connect to the pull up rail via 10kΩ resistor. The STAT1, STAT2 pin functions can be disabled when DIS_STAT_PINS bit is set to 1. When disabled, this pin can be used as a general purpose indicator via the FORCE_STAT1_ON bit.
STAT2	5	O	Open Drain Charge Status 2 Output – STAT1 and STAT2 indicate various charger operations, see Table 6-6 . Connect to the pull up rail via 10kΩ resistor. The STAT1, STAT2 pin functions can be disabled when DIS_STAT_PINS bit is set to 1. When disabled, this pin can be used as a general purpose indicator via the FORCE_STAT2_ON bit.
PG	6	O	Open Drain Active Low Power Good Indicator – Connect to the pull up rail via 10kΩ resistor. LOW indicates a good input source if VAC is within the programmed ACUV / ACOV operating window. The PG pin function can be disabled when DIS_PG_PIN bit is set to 1. When disabled, this pin can be used as a general purpose indicator via the FORCE_STAT3_ON bit.
CE	7	IO	Active Low Charge Enable Pin – Battery charging is enabled when EN_CHG bit is 1 and CE pin is LOW. CE pin must be pulled HIGH or LOW, do not leave floating. The CE pin function can be disabled when DIS_CE_PIN bit is set to 1. When disabled, this pin can be used as a general purpose indicator via the FORCE_STAT4_ON bit.

Table 4-1. Pin Functions (continued)

PIN		I/O	DESCRIPTION
NAME	NO.		
TS	8	I	Temperature Qualification Voltage Input – Connect a negative temperature coefficient thermistor. Program temperature window with a resistor divider from REGN to TS to PGND. Charge suspends when TS pin voltage is out of range. Recommend 103AT-2 10-kΩ thermistor.
ICHG	9	I	Charge Current Limit Setting – ICHG pin sets the maximum charge current, and can be used to monitor the charge current. A programming resistor to PGND is used to set the charge current limit as $I_{CHG} = K_{ICHG} / R_{ICHG}$. When the device is under charge current regulation, the voltage at ICHG pin is V_{REF_ICHG} . When ICHG pin voltage is less than V_{REF_ICHG} , the actual charge current can be calculated as: $I_{BAT} = K_{ICHG} \times V_{ICHG} / (R_{ICHG} \times V_{REF_ICHG})$. The actual charge current limit is the lower of the limits set by ICHG pin or the ICHG_REG register bits. This pin function can be disabled when EN_ICHG_PIN bit is 0. If ICHG pin is not used, this pin must be pulled to PGND, do not leave floating.
ILIM_HIZ	10	I	Input Current Limit Setting and HIZ Mode Control Pin – ILIM_HIZ pin sets the maximum input current limit, can be used to monitor the input current and can be pulled HIGH to force device into HIZ mode. A programming resistor to PGND is used to set the input current limit as $I_{LIM} = K_{ILIM} / R_{ILIM}$. When the device is under input current regulation, the voltage at ILIM_HIZ pin is V_{REF_ILIM} . When ILIM_HIZ pin voltage is less than V_{REF_ILIM} , the actual input current can be calculated as: $I_{AC} = K_{ILIM} \times V_{ILIM} / (R_{ILIM} \times V_{REF_ILIM})$. The actual input current limit is the lower of the limits set by ILIM_HIZ pin or the IAC_DPM register bits. This pin function can be disabled when EN_ILIM_HIZ_PIN bit is 0. If ILIM_HIZ pin is not used, this pin must be pulled to PGND, do not leave floating.
FBG	11	I	Voltage Feedback Divider Return – Connect to the bottom of battery feedback resistor. When charging, this pin is driven to PGND internally. When input voltage is outside of the ACUV / ACOV operating window, this pin is high-impedance, minimizing battery leakage current.
FB	12	I	Charge Voltage Analog Feedback Adjustment – Connect the output of a resistive voltage divider from the battery terminals to this node to adjust the output battery regulation voltage.
SRN	13	I	Charge Current-Sense Resistor, Negative Input – A 0.47-μF ceramic capacitor is placed from SRN to SRP to provide differential-mode filtering. An optional 0.1-μF ceramic capacitor is placed from the SRN pin to PGND for common-mode filtering.
SRP	14	I	Charge Current-Sense Resistor, Positive Input – A 0.47-μF ceramic capacitor is placed from SRN to SRP to provide differential-mode filtering. A 0.1-μF ceramic capacitor is placed from the SRP pin to PGND for common-mode filtering.
NC	15	-	No Connect - Leave this pin floating, do not tie to PGND
NC	16	-	No Connect - Leave this pin floating, do not tie to PGND
PGND	17	-	Tie this pin directly to PGND .
SW2	18	P	Boost Side Half Bridge Switching Node – Connect to the source of boost HS FET and the drain of boost LS FET. Connect the inductor between SW1 and SW2.
HIDRV2	19	O	Boost Side High-Side Gate Driver – Connect to the boost high-side N-channel MOSFET gate.
BTST2	20	P	Boost Side High-Side Power MOSFET Gate Driver Power Supply – Connect a capacitor between BTST2 and SW2 to provide bias to the high-side MOSFET gate driver.
LODRV2	21	O	Boost Side Low-Side Gate Driver – Connect to the boost low-side N-channel MOSFET gate.
PGND	22	P	Power Ground Return – The high current ground connection for the low-side gate drivers.
DRV_SUP	23	P	Charger Gate Drive Supply Input – Voltage on this pin is used to drive the gates of buck-boost converter switching FET. Connect a 4.7μF ceramic capacitor from DRV_SUP to power ground. REGN LDO voltage can be used as the gate driver supply for all switching FETs by connecting REGN to DRV_SUP pin. In high-voltage applications, it is possible to directly provide the DRV_SUP voltage with an external supply up to 12V to achieve higher switching efficiency. See Section 6.3.3.2 for more details.
REGN	24	P	Charger Internal Linear Regulator Output – Connect a 4.7μF ceramic capacitor from REGN to power ground. REGN LDO voltage can be used as the gate driver supply for all switching FETs by connecting REGN to DRV_SUP pin. In high-voltage applications, it is possible to directly provide the DRV_SUP voltage with an external supply up to 12V to achieve higher switching efficiency. See Section 6.3.3.2 for more details.
LODRV1	25	O	Buck Side Low-Side Gate Driver – Connect to the buck low-side N-channel MOSFET gate.
BTST1	26	P	Buck Side High-Side Power MOSFET Gate Driver Power Supply – Connect a capacitor between BTST1 and SW1 to provide bias to the high-side MOSFET gate driver.
HIDRV1	27	O	Buck Side High-Side Gate Driver – Connect to the buck high-side N-channel MOSFET gate.

Table 4-1. Pin Functions (continued)

PIN		I/O	DESCRIPTION
NAME	NO.		
SW1	28	P	Buck Side Half Bridge Switching Node – Connect to the source of buck HS FET and the drain of buck LS FET. Connect the inductor between SW1 and SW2.
ACN	29	I	Adapter Current-Sense Resistor, Negative Input – A 0.47µF ceramic capacitor is placed from ACN to ACP to provide differential-mode filtering. An optional 0.1µF ceramic capacitor is placed from the ACN pin to PGND for common-mode filtering.
ACP	30	I	Adapter Current-Sense Resistor, Positive Input – A 0.47µF ceramic capacitor is placed from ACN to ACP to provide differential-mode filtering. A 0.1µF ceramic capacitor is placed from the ACP pin to PGND for common-mode filtering.
NC	31	-	No Connect - Leave this pin floating, do not tie to PGND
VAC	32	P	Input Voltage Detection and Power – Connect a 1µF capacitor from pin to PGND. Pin 33 is the input bias to power the IC, and ACOV/ACUV resistor divider must be connected relative to pin 33. When Reverse Mode is enabled, pin 32 is regulated to VAC_REV.
	33		
ACUV	34	I	AC Undervoltage Comparator Input – Connect a resistor divider from VAC to PGND to program the undervoltage protection. When this pin falls below V_{REF_ACUV} , the device stops charging. The hardware limit for input voltage regulation reference is V_{ACUV_DPM} . The actual input voltage regulation is the higher of the pin-programmed value and the VAC_DPM register value. If ACUV programming is not used, pull this pin to VAC, do not leave floating.
ACOV	35	I	AC Overvoltage Comparator Input – Connect a resistor divider from VAC to PGND to program the overvoltage protection. When this pin rises above V_{REF_ACOV} , the device stops charging. If ACOV programming is not used, pull this pin to PGND, do not leave floating.
FSW_SYNC	36	I	Switching Frequency and Synchronization Input – An external resistor is connected to the FSW_SYNC pin and PGND to set the nominal switching frequency. This pin can also be used to synchronize the PWM controller to an external clock with 200kHz to 600kHz frequency.
Thermal Pad	37	P	Exposed pad beneath the IC – Always solder the thermal pad to the board, and have vias on the thermal pad plane star-connecting to PGND and ground plane for high-current power converter. It also serves as a thermal pad to dissipate the heat.

5 Specifications

5.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
Voltage	VAC, ACUV, ACOV, ACP, ACN, SRP, SRN, FB, FBG	−0.3	85	V
Voltage	SW1, SW2	−2	85	V
Voltage	SW1, SW2 (40ns transient)	−4	85	V
Voltage	$\overline{PG}$	−0.3	40	V
Voltage	BTST1, HIDRV1 with respect to SW1	−0.3	14	V
Voltage	BTST2, HIDRV2 with respect to SW2	−0.3	14	V
Voltage	ACP with respect to ACN, SRP with respect to SRN	−0.3	0.3	V
Voltage	$\overline{CE}$, FSW_SYNC, ICHG, ILIM_HIZ, $\overline{INT}$, REGN, SCL, SDA, MODE, STAT1, STAT2, TS	−0.3	6	V
Output Sink Current	$\overline{CE}$, $\overline{PG}$, STAT1, STAT2		5	mA
T _J	Junction temperature	−40	150	°C
T _{stg}	Storage temperature	−65	150	°C

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

5.2 ESD Ratings

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins ⁽¹⁾	±2000	V
		Charged device model (CDM), per ANSI/ESDA/JEDEC JS-002, all pins ⁽²⁾	±500	

- (1) JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process.
 (2) JEDEC document JEP157 states that 250V CDM allows safe manufacturing with a standard ESD control process.

5.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V _{AC}	Input voltage	4.2		70	V
V _{BAT}	Battery voltage	0		70	V
V _{DRV_SUP}	DRV_SUP pin direct drive voltage range	4.0		12	V
F _{SW}	Switching Frequency	200		600	kHz
T _J	Junction temperature	–40		125	°C
T _A	Ambient temperature	–40		105	°C
C _{VAC}	VAC capacitor	1			μF
C _{IN}	Buck input capacitance (minimum value after derating)	80			μF
C _{OUT}	Buck output capacitance (minimum value after derating)	80			μF
C _{REGN}	REGN capacitor (nominal value before derating)	4.7			μF
C _{DRV_SUP}	DRV_SUP capacitor (nominal value before derating)	4.7			μF
L	Switched Inductor	2.2		15	μH
R _{DCR}	Inductor DC resistance	1.75		60	mΩ
R _{AC_SNS}	Input current sense resistor	0 ⁽¹⁾	5	10	mΩ
R _{BAT_SNS}	Battery current sense resistor		5		mΩ
R _{ICHG}	ICHG programming pulldown resistor	0.0 ⁽²⁾		100	kΩ
R _{ILIM_HIZ}	ILIM_HIZ programming pulldown resistor	0.0 ⁽³⁾		50	kΩ

(1) When R_{AC_SNS} is 0mΩ, input current limit function is disabled

(2) When R_{ICHG} is pulled to GND, the hardware charge current limit is disabled, actual charge current is controlled by the ICHG_REG register setting

(3) When R_{ILIM_HIZ} is pulled to GND, the hardware input current limit is disabled, actual input current is controlled by the IAC_DPM register setting

5.4 Thermal Information

THERMAL METRIC ⁽¹⁾		BQ25756	UNIT
		RRV	
		36 PINS	
R _{θJA}	Junction-to-ambient thermal resistance (JEDEC ⁽¹⁾)	29.4	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	18.8	°C/W
R _{θJB}	Junction-to-board thermal resistance	9.9	°C/W
Ψ _{JT}	Junction-to-top characterization parameter	0.2	°C/W
Ψ _{JB}	Junction-to-board characterization parameter	9.8	°C/W
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	2.5	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application note.

5.5 Electrical Characteristics

VAC = ACP = ACN = SYS = SRP = SRN = 28V, $T_J = -40^{\circ}\text{C}$ to $+125^{\circ}\text{C}$, and $T_J = 25^{\circ}\text{C}$ for typical values (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
QUIESCENT CURRENTS						
I_{Q_BAT}	Quiescent battery current with BATFET on ($I_{SRN} + I_{SRP}$)	$V_{BAT} = 28\text{V}$, $VAC = 0\text{V}$, $ADC_EN = 0$, $T_J < 105^{\circ}\text{C}$	17			μA
		$V_{BAT} = 28\text{V}$, $VAC = 0\text{V}$, $ADC_EN = 1$, $T_J < 105^{\circ}\text{C}$	500	700		μA
I_{Q_VAC}	Quiescent input current (I_{VAC})	Not switching	0.75	1		mA
I_{Q_REV}	Quiescent battery current in Reverse mode ($I_{SRN} + I_{SRP}$)	Not switching	0.75	1		mA
VAC / BAT POWER UP						
V_{VAC_OP}	VAC operating range		4.2		70	V
V_{VAC_OK}	VAC converter enable threshold	VAC rising, no battery	4.2			V
V_{VAC_OKZ}	VAC converter disable threshold	VAC falling, no battery			3.5	V
V_{REF_ACUV}	ACUV comparator threshold to enter VAC_UVP	V_{ACUV} falling	1.095	1.1	1.106	V
$V_{REF_ACUV_HYS}$	ACUV comparator threshold hysteresis	V_{ACUV} rising		50		mV
$V_{VAC_INT_OV}$	VAC internal threshold to enter VAC_OVP	IN rising	72	74	76	V
$V_{VAC_INT_OVZ}$	VAC internal thresholds to exit VAC_OVP	IN falling	69	71	73	V
V_{REF_ACOV}	ACOV comparator threshold to enter VAC_OVP	V_{ACOV} rising	1.184	1.2	1.206	V
$V_{REF_ACOV_HYS}$	ACOV comparator threshold hysteresis	V_{ACOV} falling		50		mV
CHARGE VOLTAGE REGULATION						
V_{VFB_RANGE}	Feedback voltage range		1.504		1.566	V
V_{VFB_NOM}	Nominal feedback voltage	$V_{FB_REG} = 0 \times 10$		1.536		V
V_{VFB_ACC}	Feedback voltage regulation accuracy	$T_J = 0^{\circ}\text{C}$ to 85°C	-0.5		0.5	%
		$T_J = -40^{\circ}\text{C}$ to 125°C	-0.7		0.7	%
R_{FBG}	FBG resistance to PGND	$I_{FBG} = 1\text{mA}$		33	55	Ω
FAST CHARGE CURRENT REGULATION						
$I_{CHG_REG_RANGE}$	Charge current regulation range		0.4		20	A
$I_{CHG_REG_ACC}$	$I^2\text{C}$ setting charge current regulation accuracy	$R_{BAT_SNS} = 5\text{m}\Omega$, $V_{BAT} = 12\text{V}$, 36V, 55V. $ICHG_REG = 0 \times 012\text{C}$	15			A
			-3		3	%
		$R_{BAT_SNS} = 5\text{m}\Omega$, $V_{BAT} = 12\text{V}$, 36V, 55V. $ICHG_REG = 0 \times 0064$	5			A
			-3		3	%
K_{ICHG}	Hardware charge current limit set factor (Amperes of charge current per $\text{k}\Omega$ on ICHG pin)	$R_{BAT_SNS} = 5\text{m}\Omega$, $V_{BAT} = 12\text{V}$, 36V, 55V. $ICHG_REG = 0 \times 0028$	2			A
			-5		5	%
K_{ICHG}		$R_{BAT_SNS} = 5\text{m}\Omega$, $R_{ICHG} = 10\text{k}\Omega$, 5k Ω , and 3.33k Ω	48	50	52	A $\times$ k Ω
V_{REF_ICHG}	ICHG pin voltage when ICHG pin is in regulation		2.0			V
PRE-CHARGE CURRENT REGULATION						
I_{PRECHG_RANGE}	Precharge current regulation range	$V_{FB} < V_{BAT_LOWV} * V_{VFB_REG}$	0.25		10	A

5.5 Electrical Characteristics (continued)

VAC = ACP = ACN = SYS = SRP = SRN = 28V, T_J = -40°C to +125°C, and T_J = 25°C for typical values (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
I _{PRECHG_ACC}	I ² C setting precharge current accuracy	R _{BAT_SNS} = 5mΩ, V _{FB} < V _{BAT_LOWV} * V _{VFB_REG} . IPRECHG = 0x003C	3.0			A	
			−4		4	%	
		R _{BAT_SNS} = 5mΩ, V _{FB} < V _{BAT_LOWV} * V _{VFB_REG} . IPRECHG[1:0] = 0x0014	1.0			A	
			−10		10	%	
		R _{BAT_SNS} = 5mΩ, V _{FB} < V _{BAT_LOWV} * V _{VFB_REG} . IPRECHG[1:0] = 0x000A	0.50			A	
−30			30	%			
CHARGE TERMINATION							
I _{TERM_RANGE}	Termination current range	V _{FB} = V _{VFB_REG}	0.25		10	A	
I _{TERM_ACC}	Termination current accuracy	R _{BAT_SNS} = 5mΩ, VBAT = 12V, 36V, 55V. ITERM = 0x001E	1.5			A	
			−7		7	%	
		R _{BAT_SNS} = 5mΩ, VBAT = 12V, 36V, 55V. ITERM = 0x000A	0.50			A	
			−20		20	%	
		R _{BAT_SNS} = 5mΩ, VBAT = 12V, 36V, 55V. ITERM = 0x0005	0.250			A	
−50		50	%				
BATTERY VOLTAGE COMPARATORS							
V _{BAT_SHORT}	Trickle charge to pre-charge transition	V _{SRN} rising	2.8	3	3.2	V	
	Pre-charge to trickle charge transition	V _{SRN} falling	2.2	2.4	2.6	V	
V _{BAT_LOWV}	Pre-charge to fast-charge transition	V _{FB} rising, as percentage of V _{FB_REG} , VBAT_LOWV[2:0] = 3	69.0	71.7	73.8	%	
		V _{FB} rising, as percentage of V _{FB_REG} , VBAT_LOWV[2:0] = 2	64.3	66.7	69.0	%	
		V _{FB} rising, as percentage of V _{FB_REG} , VBAT_LOWV[2:0] = 1	52	55	58	%	
		V _{FB} rising, as percentage of V _{FB_REG} , VBAT_LOWV[2:0] = 0	27	30	33	%	
V _{BAT_LOWV_HYS}	BAT_LOWV hysteresis		5			%	
V _{RECHG}	Battery recharge threshold for Li-Ion and LiFePO ₄	V _{FB} falling, as percentage of V _{FB_REG} , VRECHG[1:0] = 3	97.6			%	
		V _{FB} falling, as percentage of V _{FB_REG} , VRECHG[1:0] = 2	95.2			%	
		V _{FB} falling, as percentage of V _{FB_REG} , VRECHG[1:0] = 1	94.3			%	
		V _{FB} falling, as percentage of V _{FB_REG} , VRECHG[1:0] = 0	93.0			%	
INPUT CURRENT REGULATION							
I _{I²C_DPM_ACC}	I ² C setting input current regulation accuracy in forward mode	R _{AC_SNS} = 2mΩ, IAC_DPM = 0x00A0	20			A	
			−3		3	%	
		R _{AC_SNS} = 2mΩ, IAC_DPM = 0x0050	10			A	
			−4		4	%	
		R _{AC_SNS} = 2mΩ, IAC_DPM = 0x0028	5			A	
−7			7	%			
K _{ILIM}	Hardware input current limit set factor (Amperes of input current per kΩ on ILIM_HIZ pin)	R _{AC_SNS} = 2mΩ, R _{ILIM} = 5kΩ, 2.5kΩ, and 1.67kΩ	48	50	52	A x kΩ	

5.5 Electrical Characteristics (continued)

VAC = ACP = ACN = SYS = SRP = SRN = 28V, T_J = -40°C to +125°C, and T_J = 25°C for typical values (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
V _{REF_ILIM_HIZ}	ILIM_HIZ pin voltage when ILIM_HIZ pin is in regulation		2.0			V	
V _{IH_ILIM_HIZ}	ILIM_HIZ input high threshold to enter HIZ mode	V _{ILIM_HIZ} rising	3.7			V	
INPUT VOLTAGE REGULATION							
V _{VREG_DPM_RANGE}	Input voltage DPM regulation range		4.2		65	V	
V _{VREG_DPM_ACC}	I ² C setting input voltage regulation accuracy	VAC_DPM = 0x076C	38			V	
			-2	2	%		
V _{VREG_DPM_ACC}	I ² C setting input voltage regulation accuracy in forward mode	VAC_DPM = 0x04E2	25			V	
			-2	2	%		
		VAC_DPM = 0x03B6	19			V	
			-2	2	%		
V _{ACUV_DPM}	ACUV pin voltage when in VDPM regulation		1.198	1.210	1.222	V	
REVERSE MODE VOLTAGE REGULATION							
V _{REV_RANGE}	VAC Voltage regulation range in Reverse mode		3.3		65	V	
V _{REV_ACC}	Voltage regulation accuracy in Reverse mode	VAC_REV = 0x0960	48			V	
			-2	2	%		
		VAC_REV = 0x0578	28			V	
			-2	2	%		
V _{REV_ACC}	VAC Voltage regulation accuracy in Reverse mode	VAC_REV = 0x02EE	15			V	
			-2	2	%		
		VAC_REV = 0x00FA	5			V	
			-2	2	%		
REVERSE MODE CURRENT REGULATION							
I _{IREV_ACC}	Input current regulation accuracy in Reverse mode	R _{AC_SNS} = 2mΩ, IAC_REV = 0x00A0	20			A	
			-3.5	3.5	%		
		R _{AC_SNS} = 2mΩ, IAC_REV = 0x0028	5			A	
			-5.5	5.5	%		
CHARGE MODE BATTERY-PACK NTC MONITOR							
V _{T1_RISE}	TS pin voltage rising T1 threshold, charge suspended above this voltage.	As Percentage to REGN, TS_T1=0°C w/ 103AT	72.75	73.25	73.85	%	
V _{T1_FALL}	TS pin voltage falling T1 threshold, charge re-enabled below this voltage.	As Percentage to REGN, TS_T1=0°C w/ 103AT	71.5	72	72.5	%	
V _{T2_RISE}	TS pin voltage rising T2 threshold, charge back to reduced ICHG above this voltage	As Percentage to REGN, TS_T2=10°C w/ 103AT	67.75	68.25	68.75	%	
V _{T2_FALL}	TS pin voltage falling T2 threshold. Charge back to normal below this voltage	As Percentage to REGN, TS_T2=10°C w/ 103AT	66.45	66.95	67.45	%	
V _{T3_FALL}	TS pin voltage falling T3 threshold, charge to ICHG and reduced V _{FB_REG} below this voltage.	As Percentage to REGN, TS_T3=45°C w/ 103AT	44.25	44.75	45.25	%	

5.5 Electrical Characteristics (continued)

VAC = ACP = ACN = SYS = SRP = SRN = 28V, T_J = -40°C to +125°C, and T_J = 25°C for typical values (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
V _{T3_RISE}	TS pin voltage rising T3 threshold. Charge back to normal above this voltage.	As Percentage to REGN, TS_T3=45°C w/ 103AT	45.55	46.05	46.55	%	
V _{T5_FALL}	TS pin voltage falling T5 threshold, charge suspended below this voltage	As Percentage to REGN, TS_T5=60°C w/ 103AT	33.875	34.375	34.875	%	
V _{T5_RISE}	TS pin voltage rising T5 threshold. Charge back to ICHG and reduced V _{FB_REG} above this voltage.	As Percentage to REGN, TS_T5=60°C w/ 103AT	35	35.5	36	%	
REVERSE MODE BATTERY-PACK NTC MONITOR							
V _{BCOLD_RISE}	TS pin voltage rising TCOLD threshold. Reverse mode suspended above this voltage	As Percentage to REGN (BCOLD = -20°C w/ 103AT)	79.45	80.0	80.55	%	
V _{BCOLD_RISE}	TS pin voltage rising TCOLD threshold. Reverse mode suspended above this voltage	As Percentage to REGN (BCOLD = -10°C w/ 103AT)	76.65	77.15	77.65	%	
V _{BCOLD_FALL}	TCOLD comparator falling threshold.	As Percentage to REGN (-20°C w/ 103AT)	78.2	78.7	79.2	%	
V _{BCOLD_FALL}	TCOLD comparator falling threshold.	As Percentage to REGN (-10°C w/ 103AT)	75.5	75.6	76.5	%	
V _{BHOT_FALL}	TS pin voltage falling THOT threshold. Reverse mode suspends below this voltage	As Percentage to REGN, (BHOT = 55°C w/ 103AT)	37.2	37.7	38.2	%	
V _{BHOT_FALL}	TS pin voltage falling THOT threshold. Reverse mode suspends below this voltage	As Percentage to REGN, (BHOT = 60°C w/ 103AT)	33.875	34.375	34.875	%	
V _{BHOT_FALL}	TS pin voltage falling THOT threshold. Reverse mode suspends below this voltage	As Percentage to REGN, (BHOT 65°C w/ 103AT)	30.75	31.25	31.75	%	
V _{BHOT_RISE}	TS pin voltage rising THOT threshold. Reverse mode allowed above this voltage	As Percentage to REGN, (BHOT = 55°C w/ 103AT)	38.5	39.0	39.95	%	
V _{BHOT_RISE}	TS pin voltage rising THOT threshold. Reverse mode allowed above this voltage	As Percentage to REGN, (BHOT = 60°C w/ 103AT)	35	35.5	36	%	
V _{BHOT_RISE}	TS pin voltage rising THOT threshold. Reverse mode allowed above this voltage	As Percentage to REGN, (BHOT 65°C w/ 103AT)	32.0	32.5	33.0	%	
BATTERY CHARGER PROTECTION							
V _{BAT_OV}	Battery overvoltage threshold	V _{FB} rising, as percentage of V _{FB_REG}	102.5	104	105.5	%	
V _{BAT_OVZ}	Battery overvoltage falling threshold	V _{FB} falling, as percentage of V _{FB_REG}	100.5	102	103.5	%	
V _{ICHG_OC}	Battery charge over-current threshold	V _{SRP} - V _{SRN} rising	120		170	mV	
THERMAL SHUTDOWN							
T _{SHUT}	Thermal shutdown rising threshold	Temperature increasing		150		°C	
	Thermal shutdown falling threshold	Temperature decreasing		135		°C	
REGN REGULATOR AND GATE DRIVE SUPPLY (DRV_SUP)							
V _{REGN}	REGN LDO output voltage	I _{REGN} = 20mA	4.8	5	5.2	V	
		VAC = 5V, I _{REGN} = 20mA	4.35	4.6		V	
I _{REGN}	REGN LDO current limit	V _{REGN} = 4.5V	70			mA	

5.5 Electrical Characteristics (continued)

VAC = ACP = ACN = SYS = SRP = SRN = 28V, $T_J = -40^{\circ}\text{C}$ to $+125^{\circ}\text{C}$, and $T_J = 25^{\circ}\text{C}$ for typical values (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
V _{REGN_OK}	REGN OK threshold to allow switching	REGN rising	3.55			V	
V _{DRV_UVPZ}	DRV_SUP under-voltage threshold to allow switching	DRV_SUP rising	3.7			V	
V _{DRV_OVP}	DRV_SUP over-voltage threshold to disable switching	DRV_SUP rising	12.8	13.2	13.6	V	
I _{AC_LOAD}	VAC discharge load current		16			mA	
I _{BAT_LOAD}	Battery (SRP) discharge load current		16			mA	
SWITCHING FREQUENCY AND SYNC							
f _{SW}	Switching Frequency	R _{FSW_SYNC} = 133kΩ	212	250	288	kHz	
		R _{FSW_SYNC} = 50kΩ	425	500	575	kHz	
V _{IH_SYNC}	FSW_SYNC input high threshold		1.3			V	
V _{IL_SYNC}	FSW_SYNC input low threshold		0.4			V	
PW _{SYNC}	FSW_SYNC input pulse width		80			ns	
PWM DRIVERS							
R _{HIDRV1_ON}	Buck side high-side turnon resistance	V _{BTST1} - V _{SW1} = 5V	3.4			Ω	
R _{HIDRV1_OFF}	Buck side high-side turnoff resistance	V _{BTST1} - V _{SW1} = 5V	1.0			Ω	
V _{BTST1_REFRESH}	Bootstrap refresh comparator threshold voltage	BTST1 falling, V _{BTST1} - V _{SW1} when low-side refresh pulse is requested	2.7	3.1	3.9	V	
R _{LODRV1_ON}	Buck side low-side turnon resistance	V _{REGN} = 5V	3.4			Ω	
R _{LODRV1_OFF}	Buck side low-side turnoff resistance	V _{REGN} = 5V	1.0			Ω	
t _{DT1}	Buck side dead time, both edges		45			ns	
R _{HIDRV2_ON}	Boost side high-side turnon resistance	V _{BTST2} - V _{SW2} = 5V	3.4			Ω	
R _{HIDRV2_OFF}	Boost side high-side turnoff resistance	V _{BTST2} - V _{SW2} = 5V	1.0			Ω	
V _{BTST2_REFRESH}	Bootstrap refresh comparator threshold voltage	BTST2 falling, V _{BTST2} - V _{SW2} when low-side refresh pulse is requested	2.7	3.1	3.9	V	
R _{LODRV2_ON}	Boost side low-side turnon resistance	V _{REGN} = 5V	3.4			Ω	
R _{LODRV2_OFF}	Boost side low-side turnoff resistance	V _{REGN} = 5V	1.0			Ω	
t _{DT2}	Boost side dead time, both edges		45			ns	
ANALOG-TO-DIGITAL CONVERTER (ADC)							
t _{ADC_CONV}	Conversion-time, each measurement	ADC_SAMPLE[1:0] = 00	24			ms	
		ADC_SAMPLE[1:0] = 01	12			ms	
		ADC_SAMPLE[1:0] = 10	6			ms	
ADC _{RES}	Effective resolution	ADC_SAMPLE[1:0] = 00	14	15	bits		
		ADC_SAMPLE[1:0] = 01	13	14	bits		
		ADC_SAMPLE[1:0] = 10	12	13	bits		
ADC MEASUREMENT RANGE AND LSB							

5.5 Electrical Characteristics (continued)

V_{AC} = ACP = ACN = SYS = SRP = SRN = 28V, T_J = -40°C to +125°C, and T_J = 25°C for typical values (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
I _{AC_ADC}	Input current ADC reading (positive or negative)	Range with 2mΩ R _{AC_SNS}	-50000		50000	mA	
		LSB with 2mΩ R _{AC_SNS}		2		mA	
I _{BAT_ADC}	Battery current ADC reading (positive or negative)	Range with 5mΩ R _{BAT_SNS}	-20000		20000	mA	
		LSB with 5mΩ R _{BAT_SNS}		2		mA	
V _{AC_ADC}	Input voltage ADC reading	Range	0		65534	mV	
		LSB		2		mV	
V _{BAT_ADC}	Battery voltage ADC reading	Range	0		65534	mV	
		LSB		2		mV	
TS _{ADC}	TS voltage ADC reading, as percentage of REGN	Range	0		99.9	%	
		LSB		0.098		%	
V _{FB_ADC}	FB voltage ADC reading	Range	0		2047	mV	
		LSB		1		mV	
I ² C INTERFACE (SCL, SDA)							
V _{IH}	Input high threshold level		1.3			V	
V _{IL}	Input low threshold level				0.4	V	
V _{OL}	Output low threshold level	Sink current = 5mA			0.4	V	
I _{IN_BIAS}	High-level leakage current	Pull up rail 3.3V			1	μA	
LOGIC I/O PIN (CE, PG , STAT1, STAT2)							
V _{IH}	Input high threshold level (CE)		1.3			V	
V _{OL}	Output low threshold level (CE, PG, STAT1, STAT2)	Sink current = 5mA			0.4	V	
V _{IL}	Input low threshold level (CE)				0.4	V	
I _{OUT_BIAS}	High-level leakage current (CE, PG, STAT1, STAT2)	Pull up rail 3.3V			1	μA	

5.6 Timing Requirements

		MIN	NOM	MAX	UNIT
VAC / BAT POWER UP					
t_{ACOV_DGL}	Enter ACOV deglitch time, ACOV rising		100		μ s
t_{ACOVZ_DGL}	Exit ACOV deglitch time, ACOV falling		12		ms
t_{ACUV_DGL}	Enter ACUV deglitch time, ACUV falling		100		μ s
t_{ACUVZ_DGL}	Exit ACUV deglitch time, ACUV rising		12		ms
BATTERY CHARGER					
t_{TERM_DGL}	Deglitch time for charge termination, $V_{SRP} - V_{SRN}$ falling		220		ms
t_{RECHG_DGL}	Deglitch time for recharge threshold, VFB falling		200		ms
t_{PRECHG}	Pre-charge safety timer accuracy	1.7	2	2.3	hr
t_{SAFETY}	Fast-charge safety timer accuracy, CHG_TMR = 8hr	6.8	8	9.2	hr
t_{TOPOFF}	Top-off timer accuracy, TOPOFF_TMR = 30 min	25.5	30	34.5	min
BATTERY-PACK NTC MONITOR					
t_{TS_DGL}	Deglitch time for TS threshold crossing		25		ms
MPPT TIMERS					
t_{FULL_SWEEP}	Full Panel Sweep timer accuracy, FULL_SWEEP_TMR = 10 min	8.5	10	11.5	min
I²C INTERFACE					
f_{SCL}	SCL clock frequency			1000	kHZ
DIGITAL CLOCK AND WATCHDOG					
t_{LP_WDT}	I ² C Watchdog reset time (EN_HIZ = 1, WATCHDOG[1:0] = 160s)	100	160		s
t_{WDT}	I ² C Watchdog reset time (EN_HIZ = 0, WATCHDOG[1:0] = 160s)	130	160		s

5.7 Typical Characteristics

$C_{VAC} = 160\mu F$, $C_{OUT} = 160\mu F$, $f_{SW} = 250kHz$, $L = 10\mu H$, $T_A = 25^\circ C$ (unless otherwise specified)

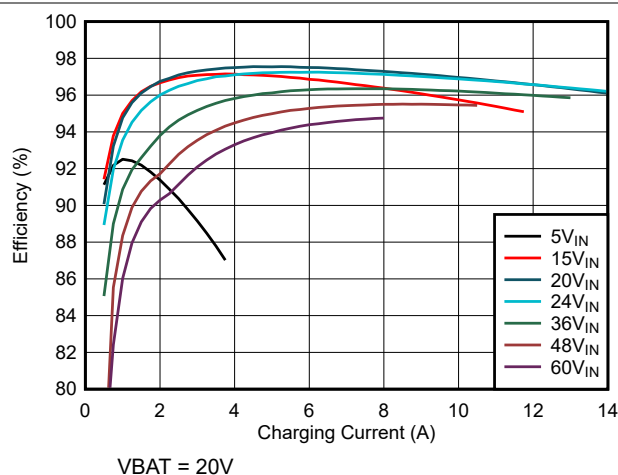


Figure 5-1. Charge Efficiency vs Charge Current (5s battery configuration)

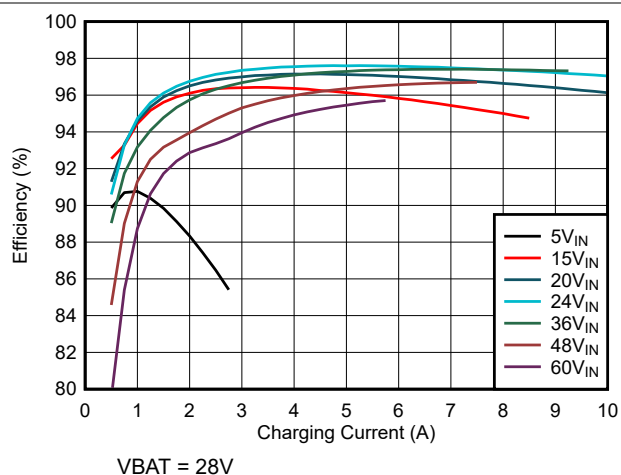


Figure 5-2. Charge Efficiency vs Charge Current (7s battery configuration)

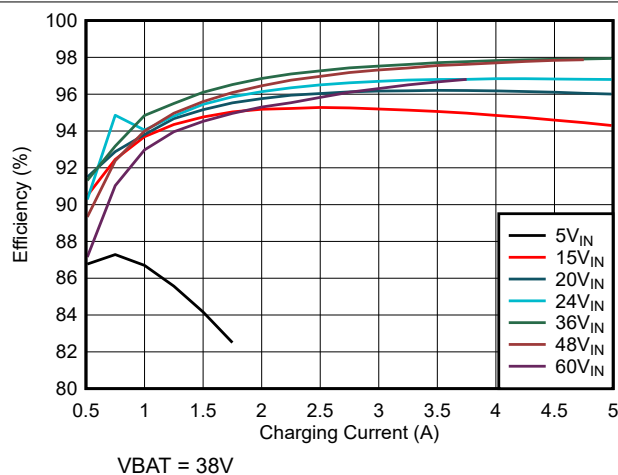


Figure 5-3. Charge Efficiency vs Charge Current (10s battery configuration)

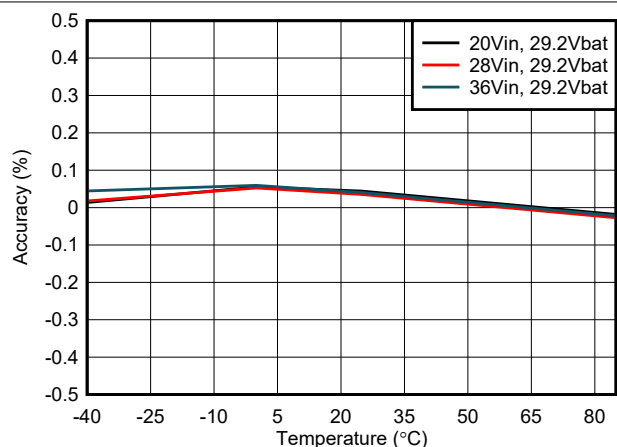


Figure 5-4. Charge Voltage Accuracy vs Temperature

5.7 Typical Characteristics (continued)

$C_{VAC} = 160\mu F$, $C_{OUT} = 160\mu F$, $f_{SW} = 250kHz$, $L = 10\mu H$, $T_A = 25^\circ C$ (unless otherwise specified)

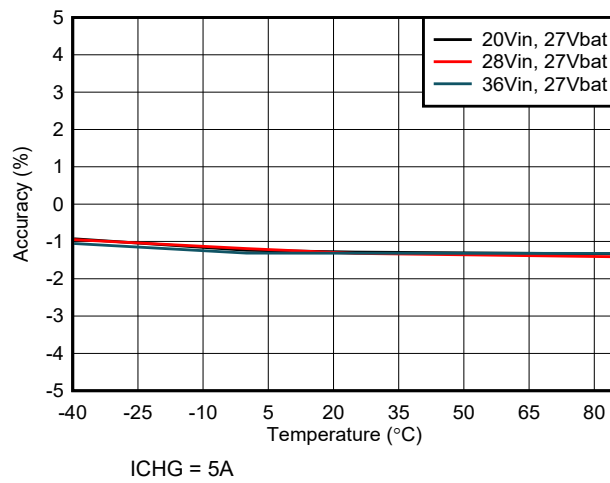


Figure 5-5. Charge Current Accuracy vs Temperature

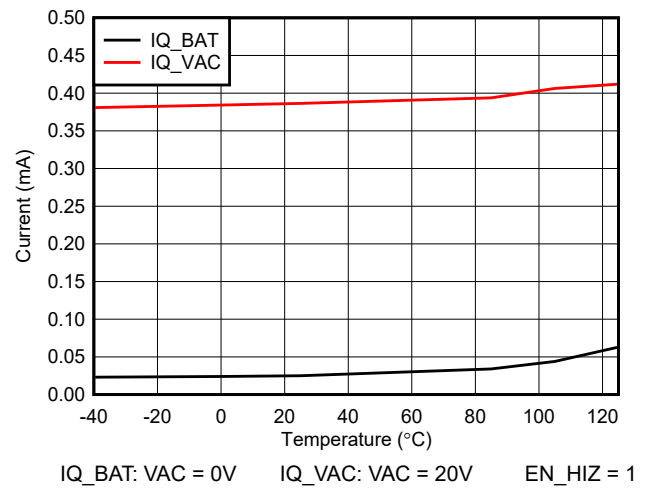


Figure 5-6. Battery and Input Quiescent Current vs Temperature with VBAT = 28V

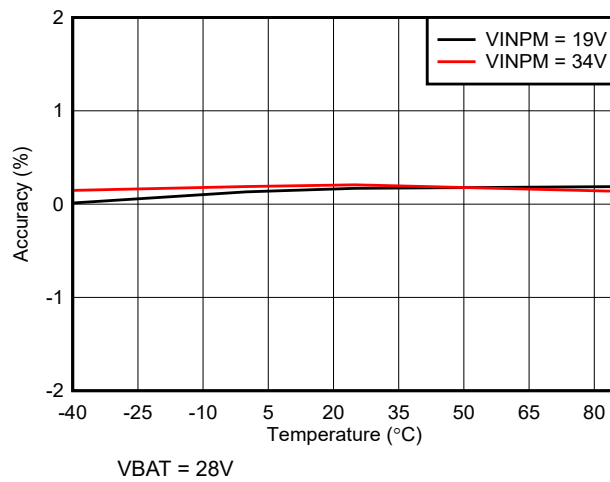


Figure 5-7. Input Voltage (VAC_DPM) Regulation Accuracy vs Temperature

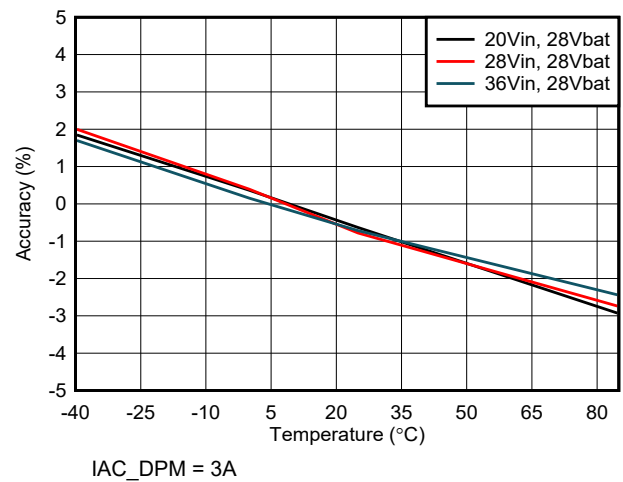


Figure 5-8. Input Current (IAC_DPM) Regulation Accuracy vs Temperature

5.7 Typical Characteristics (continued)

$C_{VAC} = 160\mu F$, $C_{OUT} = 160\mu F$, $f_{SW} = 250kHz$, $L = 10\mu H$, $T_A = 25^\circ C$ (unless otherwise specified)

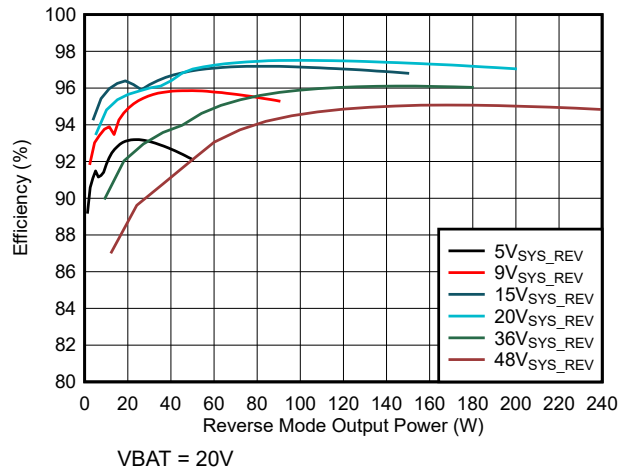


Figure 5-9. Reverse Mode Efficiency (5s battery configuration)

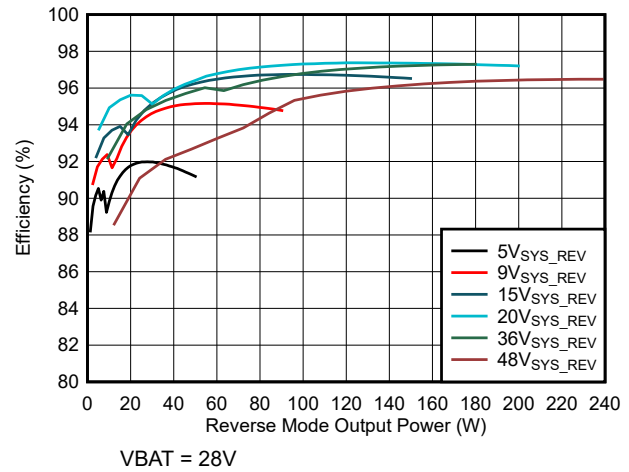


Figure 5-10. Reverse Mode Efficiency (7s battery configuration)

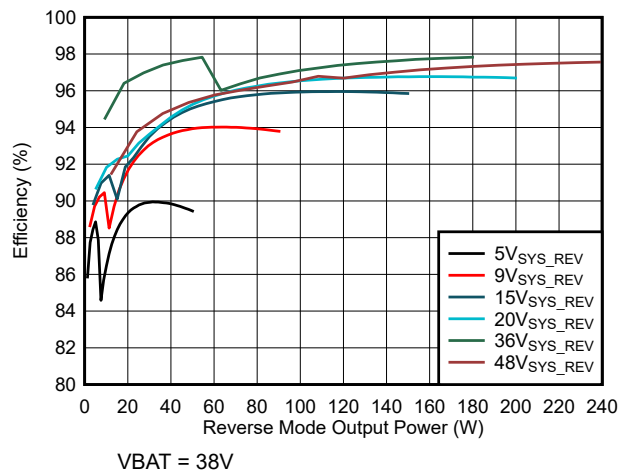


Figure 5-11. Reverse Mode Efficiency (10s battery configuration)

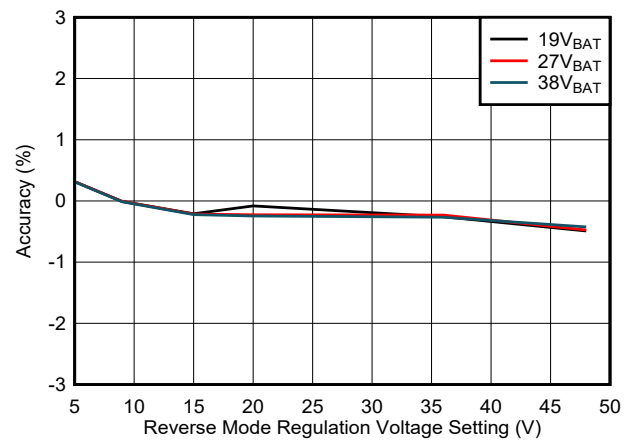


Figure 5-12. Reverse Mode Output Voltage Accuracy vs VAC_REV Setting

6 Detailed Description

6.1 Overview

The BQ25756 is a wide input voltage, Li-Ion, Li-polymer, LiFePO₄ bi-directional switched-mode buck-boost battery charge controller. The device offers high-efficiency battery charging over a wide voltage range with accurate and programmable charge current and charge voltage regulation, in addition to automatic charge preconditioning, termination, and charge status indication. The device integrates all the loop compensation and 5V gate drivers for the buck converter, thereby providing a high density solution with ease of use. The switching frequency of the device can be programmed or forced to follow an external clock frequency via the FSW_SYNC pin. While switching under light-load the device offers an optional Pulse Frequency Modulation (PFM) mode to increase efficiency. The charger has a digital state machine that advances the charger's states as the converter analog feedback loops hand off control to each other. It also manages the fault protection comparators. The loops regulate and comparators compare against reference values in the I²C registers, unless clamped by external resistors.

Besides the I²C host-controlled charging mode, the device also supports autonomous charging mode via resistor programmable limits. Input current, charge current and charge voltage regulation targets can be changed via the ILIM_HIZ, ICHG, and FB pins, respectively. The device can complete a charging cycle without any software intervention. Charging function is controlled via the $\overline{CE}$ pin.

For Li-Ion and LiFePO₄ chemistries, the device checks battery voltage and charges the battery in different phases accordingly: trickle charging, pre-charging, constant current (CC) charging and constant voltage (CV) charging. At the end of the charging cycle, the charger automatically terminates when the charge current is below the termination current limit in the constant voltage phase. When the full battery falls below the recharge threshold, the charger automatically starts a new charge cycle.

The input operating window is programmed via the ACUV and ACOV pins. When the input voltage is outside the programmed window, the device automatically stops the charger, and the $\overline{PG}$ pin pulls HIGH.

The charger provides various safety features for battery charging and system operation, including battery temperature negative thermistor (NTC) monitoring, charge timers and over-voltage/over-current protections on battery and input. The thermal shutdown prevents charging when the junction temperature exceeds the T_{SHUT} limit.

The device supports buck-boost reverse power direction to deliver power from the battery to the input when the adapter is not present. In reverse mode, the regulation voltage and current can be programmed via the I²C interface (VAC_REV and IAC_REV) to provide a CC/CV profile supporting the USB-PD Extended Power Range (EPR).

The device has three status pins (STAT1, STAT2, and $\overline{PG}$) to indicate the charging status and input voltage status. These pins can be used to drive LEDs or communicate with a host processor. If needed, these pins can also be used as general purpose indicators and their status controlled directly by the I²C interface. In addition, the $\overline{CE}$ pin can also be used as a general purpose indicator. The $\overline{INT}$ pin immediately notifies host when the device status changes, including faults.

The device also provides a 16-bit analog-to-digital converter (ADC) for monitoring input current, charge current and input/battery/thermistor voltages (IAC, IBAT, VAC, VBAT, TS).

The device comes with a 36-pin 5mm × 6mm QFN package with 0.5mm pin pitch.

The diagram illustrates the internal architecture of the BQ25756, a high-precision, low-power, and high-accuracy battery charger and system monitor. The chip is organized into several main functional blocks:

- Input and Reference Section:** This section handles external inputs and reference voltages. It includes comparators for V_{ACOV} (overvoltage) and V_{ACUV} (undervoltage) against their respective references V_{REF_ACOV} and V_{REF_ACUV} . It also features a V_{SRN} input and a V_{ILIM_HIZ} input for high-impedance current limiting. The $REGN$ LDO (Low Dropout Regulator) is connected to the V_{SRN} input and provides a regulated output $V_{O,REF}$.
- Current and Voltage Regulation Section:** This section manages the charging current and voltage. It includes comparators for I_{CHG} (charging current) and I_{AC} (average current) against their respective references V_{REF_ICHG} and $V_{REF_ILIM_HIZ}$. The V_{FB} (feedback) input is used for voltage regulation, with comparators for V_{BAT_OV} (battery overvoltage), V_{BAT_OC} (battery overcurrent), V_{DRV_SUP} (driver supply), V_{DRV_OVP} (driver supply overvoltage), V_{DRV_UVP} (driver supply undervoltage), and V_{SYS_OVP} (system overvoltage).
- Control and Monitoring Section:** This section contains the **CONVERTER CONTROL**, **ADC** (Analog-to-Digital Converter), and **CHARGE CONTROL** blocks. The **CONVERTER CONTROL** block manages the V_{FB_REG} , I_{CHG_REG} , I_{AC_DPM} , and V_{AC_DPM} signals. The **ADC** block converts analog signals to digital, and the **CHARGE CONTROL** block manages the V_{BAT_LOWV} (battery low voltage), BAT_SHORT (battery short), and $TS_SUSPEND$ (thermal shutdown) signals. The **STATUS PIN CNTRL** block manages the $STAT2$, $STAT1$, and FBG signals.
- Output and Protection Section:** This section handles the output of the converter and provides protection. It includes comparators for V_{BAT_OV} , V_{BAT_OC} , V_{DRV_SUP} , V_{DRV_OVP} , V_{DRV_UVP} , and V_{SYS_OVP} . The **BUCK-BOOST CONTROLLER** block manages the V_{BAT_OV} , V_{BAT_OC} , V_{DRV_SUP} , V_{DRV_OVP} , V_{DRV_UVP} , and V_{SYS_OVP} signals. The **OSCILLATOR** block provides a clock signal CLK to the **BUCK-BOOST CONTROLLER**. The **BATTERY THERMISTOR SENSING** block provides a temperature signal TS to the **CHARGE CONTROL** block.

The diagram also shows the external connections for the BQ25756, including the VAC , $ACOV$, $ACUV$, $ILIM_HIZ$, $ICHG$, SRP , SRN , ACP , ACN , FB , SCL , SDA , INT , $\overline{CE}$, PG , $STAT2$, $STAT1$, FBG , $REGN$, DRV_SUP , $BTST1$, $HIDRV1$, $SW1$, $LODRV1$, $BTST2$, $HIDRV2$, $SW2$, $LODRV2$, FSW_SYNC , $PGND$, and TS pins.

6.3 Feature Description

6.3.1 Device Power-On-Reset

The internal bias circuits are powered from either VAC or SRN. When VAC rises above V_{VAC_OK} , charging is allowed. When BAT rises above 3V, reverse mode operation is allowed.

A POR occurs when one of these supplies rises above its corresponding V_{OK} level, while the other supply is below its corresponding V_{OK} level. After the POR, I²C interface is ready for communication and all the registers are reset to default value. The host can access all the registers after POR.

6.3.2 Device Power-Up From Battery Without Input Source

If only the battery is present and the voltage is above 3V threshold, the device is ready for I²C communication. The REGN LDO stays off to minimize the quiescent current. The ADC can be used to monitor all system parameters.

6.3.3 Device Power Up from Input Source

When a valid input source ($V_{VAC_OK} < VAC$ and VAC within the ACUV and ACOV operating window) is detected, the $\overline{PG}$ pin pulls LOW. If charging is enabled, the device proceeds to enable the REGN LDO and power up the buck-boost converter.

6.3.3.1 VAC Operating Window Programming (ACUV and ACOV)

The VAC operating window can be programmed via the ACUV and ACOV pins using a three-resistor divider from VAC to PGND as shown in Figure 6-1.

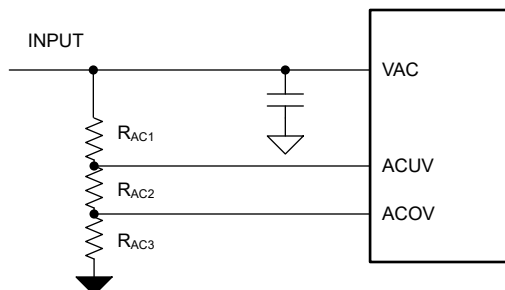


Figure 6-1. ACUV and ACOV Programming

When V_{ACUV} falls and reaches V_{ACUV_DPM} , the device enters input voltage regulation, thereby reducing the charge current. V_{ACUV} continues falling below V_{REF_ACUV} , the device automatically stops the converter and the $\overline{PG}$ pin pulls high.

System Note: if VAC_DPM register is programmed to a value higher than POR, the device regulates the VAC voltage to the higher of VAC_DPM register or V_{ACUV_DPM} pin voltage. Refer to Section 6.3.5.1.2 for more information.

When V_{ACOV} rises above V_{REF_ACOV} , the device automatically stops the converter and the $\overline{PG}$ pin pulls high.

The following equations govern the relationship between the resistor divider and the target operating voltage window programmed by ACOV and ACUV pins:

$$V_{ACOV_TARGET} = V_{REF_ACOV} \times \frac{R_{AC1} + R_{AC2} + R_{AC3}}{R_{AC3}} \quad (1)$$

$$V_{ACUV_TARGET} = V_{REF_ACUV} \times \frac{R_{AC1} + R_{AC2} + R_{AC3}}{R_{AC2} + R_{AC3}} \quad (2)$$

If unused, tie ACUV to VAC and ACOV to PGND to apply the internal VAC operating window (V_{VAC_OP}).

6.3.3.2 REGN Regulator (REGN LDO)

The REGN LDO regulator provides a regulated bias supply for the IC and the TS external resistors. Additionally, REGN voltage can be used to drive the buck switching FETs directly by tying the DRV_SUP pin to REGN. The pull-up rail of $\overline{PG}$, STAT1, and STAT2 can be connected to REGN as well. The REGN LDO is enabled when below conditions are valid:

1. VAC voltage above V_{VAC_OK} and charge is enabled in forward mode.
2. BAT voltage above 3.8V in Reverse mode and Reverse Mode is enabled (EN_REV = 1)

At high input voltages and/or large gate drive requirements, the power loss from gate driving via the REGN LDO can be excessive. This power for the gate drivers can be provided externally by directly driving the DRV_SUP pin with a high efficiency supply ranging from 4.5V to 12V. This supply must be able to provide at least 50mA or more as required to drive the switching FET gate charge. When the converter is disabled, the DRV_SUP supply needs to be disabled such that BTST1/BTST2 and DRV_SUP pins are not biased.

The power dissipation for driving the gates via the REGN LDO is: $P_{REGN} = (V_{AC} - V_{REGN}) \times Q_{G(TOT)1,2} \times f_{SW}$, where $Q_{G(TOT)1,2}$ is the sum of the total gate charge for all switching FETs and f_{SW} is the programmed switching frequency. The Safe Operating Area (SOA) below is based on a 1W power loss limit.

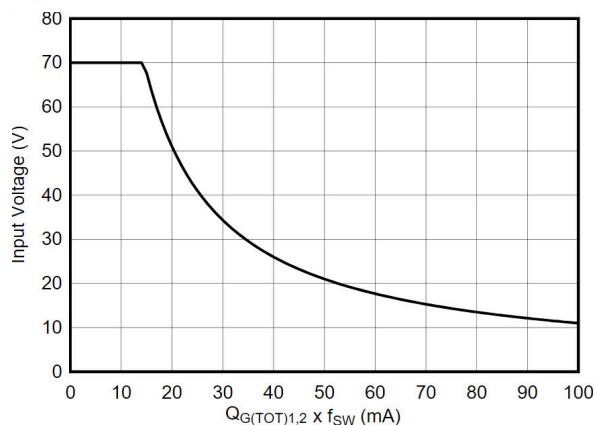


Figure 6-2. REGN LDO Safe Operating Area (SOA)

6.3.3.3 Compensation-Free Buck-Boost Converter Operation

The device integrates all the loop compensation, thereby providing a high density solution with ease of use. At startup, the device toggles the SW node for about 40ms to determine the correct compensation values for a given set of passives. If the battery is above VBAT_LOWV, then SW2 is toggled. SW1 is toggled otherwise.

The charger employs a synchronous buck-boost converter that allows charging from a wide range of input voltage sources. The charger operates in buck, buck-boost or boost mode. The converter can operate uninterruptedly and continuously across the three operation modes. During buck-boost mode, the converter alternates a SW1 pulse with a SW2 pulse, with effective switching frequency interleaved among these pulses for highest efficiency operation.

During boost mode operation, the HS FET is forced to turn on for 225ns in each switching cycle to ensure inductor energy is delivered to the output, effectively limiting the maximum boosting ratio. For example, when device is configured to switch at 500kHz, the switching period is 2μs, yielding a duty cycle limit of $(1 - 0.225\mu s / 2\mu s) = 88.75\%$. Given a 5V input, this translates to a maximum 44V output assuming 100% efficiency. The true output will be lower than this ideal limit. At lower switching frequencies, the maximum duty cycle increases, making the limitation less significant.

Table 6-1. Switching MOSFET Operation

MODE	BUCK	BUCK-BOOST	BOOST
HS BUCK FET	Switching at f_{SW}	Switching (f_{SW} interleaved between SW1 and SW2)	ON

Table 6-1. Switching MOSFET Operation (continued)

MODE	BUCK	BUCK-BOOST	BOOST
LS BUCK FET	Switching at f_{SW}	Switching (f_{SW} interleaved between SW1 and SW2)	OFF
LS BOOST FET	OFF	Switching (f_{SW} interleaved between SW1 and SW2)	Switching at f_{SW}
HS BOOST FET	ON	Switching (f_{SW} interleaved between SW1 and SW2)	Switching at f_{SW}

6.3.3.4 Light-Load Operation

To improve converter light-load efficiency, the device switches to Pulse Frequency Modulation (PFM) control at light load when the EN_PFM bit is set to 1. The effective switching frequency decreases accordingly when output load decreases.

EN_PFM bit is automatically cleared to 0 every time the converter starts and a valid SYNC clock input is detected on the FSW_SYNC pin, for fixed frequency operation regardless of output current. The bit can be overwritten to 1 to allow PFM after startup even when SYNC signal is present.

Light-load PFM mode can be disabled by clearing the EN_PFM bit. In this case, the device switches in PWM mode at a fixed switching frequency. It is recommended to disable PFM mode (EN_PFM = 0) when termination is enabled and set lower than 2A.

6.3.3.5 Switching Frequency and Synchronization (FSW_SYNC)

The device switching frequency can be programmed between 200kHz to 600kHz using a resistor from the FSW_SYNC pin to PGND. The R_{FSW} resistor is related to the nominal switching frequency (f_{SW}) by the equation:

$$R_{FSW} = \frac{1}{10 \times (f_{SW} \times 5 \times 10^{-12} - 500 \times 10^{-9})} \quad (3)$$

This pin must be pulled to PGND using a R_{FSW} , do not leave floating. In addition to programming the nominal switching frequency, the FSW_SYNC pin can also be used to synchronize the internal oscillator to an external clock signal. The synchronization feature works over the same range as the switching frequency: 200kHz to 600kHz range.

Table 6-2. Common R_{FSW} and Switching Frequency Values

R_{FSW} (k Ω)	SWITCHING FREQUENCY (kHz)
200	200
133	250
100	300
80	350
66.67	400
57.1	450
50	500
44.4	550
40	600

6.3.3.6 Device HIZ Mode

When a valid input supply is present, it is possible to force the device into HIZ Mode which disables switching and disables the REGN LDO. The charger enters HIZ Mode when EN_HIZ bit is set to 1 or the ILIM_HIZ pin is pulled above $V_{IH_ILIM_HIZ}$ (refer to [Section 6.3.5.1.1.1](#)).

If the device is operating in reverse mode with the converter turned on, and the device enters HIZ mode (EN_HIZ bit is set to 1 or ILIM_HIZ pin is pulled above $V_{IH_ILIM_HIZ}$), switching stops. Once HIZ mode condition is cleared by the host, the device resumes reverse mode operation.

The device exits HIZ Mode when the EN_HIZ bit is cleared to 0 and the ILIM_HIZ pin is pulled below 0.4V.

6.3.4 Battery Charging Management

The device charges 1-cell up-to 14-cell Li-Ion batteries and 1-cell up-to 16-cell LiFePO₄ batteries. The charge cycle is autonomous and requires no host interaction.

6.3.4.1 Autonomous Charging Cycle

When battery charging is enabled (EN_CHG bit =1 and $\overline{CE}$ pin is LOW), the device autonomously completes a charging cycle without host involvement. The device charging parameters can be set by hardware through the FB pin to set regulation voltage and the ICHG pin to set charging current. The host can always control the charging operation and optimize the charging parameters by writing to the corresponding registers through I²C.

Table 6-3. Li-Ion & LiFePO₄ Charging Parameter Default Settings

PARAMETER	VALUE
Charge Stages	Precharge → Fast Charge (CC) → Taper Charge (CV) → Termination → Recharge
FB Voltage Regulation Target (VFB_REG)	1.536V
Battery Low Voltage (VBAT_LOWV)	66.7% x VFB_REG = 1.0245V
Recharge Voltage (VRECHG)	97.6% x VFB_REG =1.4991V
Charging Current HW Limit (ICHG pin)	ICHG = K _{ICHG} / R _{ICHG}
Pre-Charge Current HW Limit (ICHG pin)	20% x ICHG
Termination Current HW Limit (ICHG pin)	10% x ICHG
NTC Temperature Profile	JEITA
Safety Timer	12 hours

A new charge cycle starts when the following conditions are valid:

- VAC is within the ACUV and ACOV operating window
- Device is not in HIZ mode (EN_HIZ = 0 and ILIM_HIZ pin voltage is below V_{IH_ILIM_HIZ})
- REGN is above V_{REGN_OK}
- Battery charging is enabled (EN_CHG = 1 and $\overline{CE}$ pin is LOW)
- No thermistor fault on TS
- No safety timer fault

For lithium-ion battery charging, the charger device automatically terminates the charging cycle when the charging current is below termination threshold, charge voltage is above recharge threshold, and device is not in DPM mode. When a full battery voltage is discharged below recharge threshold (threshold selectable via VRECHG[1:0] bits), the device automatically starts a new charging cycle. After the charge is done, toggle either $\overline{CE}$ pin or EN_CHG bit can initiate a new charging cycle.

The status register (CHARGE_STAT) indicates the different charging phases as:

- 000 – Not Charging
- 001 – Trickle Charge (VFB < V_{BAT_SHORT})
- 010 – Pre-charge (V_{BAT_SHORT} < VFB < V_{BAT_LOWV})
- 011 – Fast-charge (CC mode)
- 100 – Taper Charge (CV mode)
- 101 – Reserved
- 110 – Top-off Timer Active Charging
- 111 – Charge Termination Done

When the charger transitions to any of these states, including when charge cycle is completed, an INT pulse is asserted to notify the host.

Supercapacitors do not require Trickle Charge or Pre-charge regions when the voltage is low. For supercapacitor charging, setting the EN_PRECHG bit to 0 can disable both of these charging regions. In this case, the charger

outputs ICHG current as long as the feedback voltage (V_{FB}) is below V_{FB_REG} . The following settings are recommended for supercapacitor charging:

- $EN_PRECHG = 0$
- $EN_TERM = 0$
- $EN_CHG_TMR = 0$

6.3.4.1.1 Charge Current Programming (ICHG pin and ICHG_REG)

There are two distinct thresholds to limit the charge current (if both are enabled, the lowest limit of these will apply):

1. ICHG pin pull down resistor (hardware control)
2. ICHG_REG register bits (host software control)

To set the maximum charge current using the ICHG pin, a pull-down resistor to PGND is used. It is required to use a 5-m Ω R_{BAT_SNS} sense resistor. The charge current limit is controlled by:

$$I_{CHG_MAX} = \frac{K_{ICHG}}{R_{ICHG}} \quad (4)$$

The precharge current limit is defined as $I_{PRECHG_MAX} = 20\% \times I_{CHG_MAX}$, and the termination current is $I_{TERM} = 10\% \times I_{CHG_MAX}$.

The actual charge current limit is the lower value between ICHG pin setting and I²C register setting (ICHG_REG). For example, if the register setting is 10 A (0xC8), and ICHG pin has a 10k Ω resistor ($K_{ICHG} = 50\text{Ak}\Omega$) to ground for 5A, the actual charge current limit is 5A. The device regulates ICHG pin at V_{REF_ICHG} . If ICHG pin voltage exceeds V_{REF_ICHG} , the device enters charge current regulation.

The ICHG pin can also be used to monitor charge current when device is not in charge current regulation. When not in charge current regulation, the voltage on ICHG pin (V_{ICHG}) is proportional to the actual charging current. ICHG pin can be used to monitor battery current with the following relationship:

$$I_{BAT} = \frac{K_{ICHG} \times V_{ICHG}}{R_{ICHG} \times V_{REF_ICHG}} \quad (5)$$

For example, if ICHG pin is set with 10-k Ω resistor, and the ICHG voltage 1.0V, the actual charge current is between 2.4A to 2.6A (based on K_{ICHG} specified).

If ICHG pin is shorted to PGND, the charge current limit is set by the ICHG_REG register. If hardware charge current limit function is not needed, it is recommended to short this pin to PGND. The ICHG pin function can be disabled by setting the EN_ICHG_PIN bit to 0 (recommended when pin is shorted to PGND). When the pin is disabled, charge current limit and monitoring functions via ICHG pin are not available.

To set the maximum charge current using the ICHG_REG register bits, write to the ICHG_REG register bits. The charge current limit range is from 400mA to 20,000mA with 50mA/step. The default ICHG_REG is set to maximum code, allowing ICHG pin to limit the current in hardware.

6.3.4.2 Li-Ion Battery Charging Profile

The device charges the battery in five phases: trickle charge, pre-charge, constant current, constant voltage, and top-off trickle charging (optional). At the beginning of a charging cycle, the device checks the battery voltage and regulates current/voltage accordingly.

Table 6-4. Recommended Li-Ion Charge Settings

PARAMETER	I ² C REGISTER BITS	VALUE	EQUIVALENT PER 4.2V CHARGE (V)
Battery Low Voltage	VBAT_LOWV	$0x3 = 71.4\% \times V_{FB_REG}$	3.0V
Recharge Voltage	VRECHG	$0x3 = 97.6\% \times V_{FB_REG}$	4.1V

If the charger device is in DPM regulation during charging, the actual charging current will be less than the programmed value. In this case, termination is temporarily disabled and the charging safety timer is counted at half the clock rate, as explained in Charging Safety Timer.

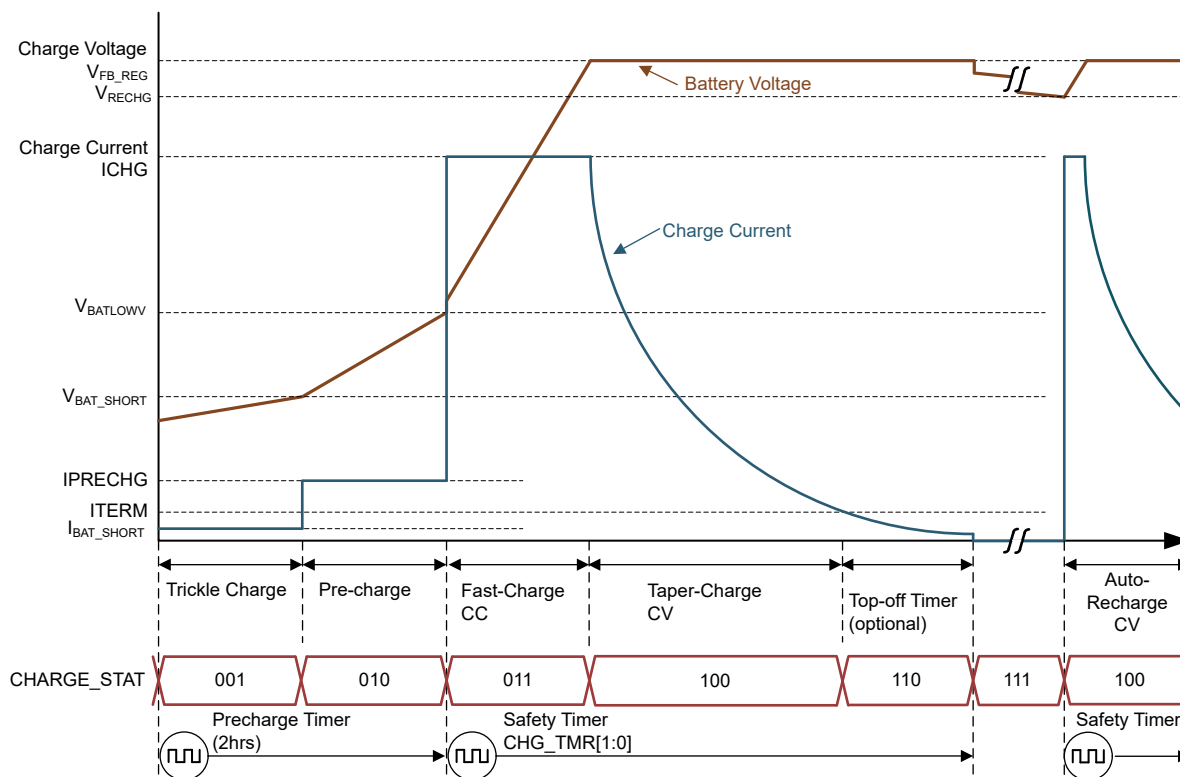


Figure 6-3. Typical Li-Ion Battery Charging Profile

6.3.4.3 LiFePO₄ Battery Charging Profile

The device charges the battery in five phases: trickle charge, pre-charge, constant current, constant voltage, and top-off trickle charging (optional). At the beginning of a charging cycle, the device checks the battery voltage and regulates current/voltage accordingly.

Table 6-5. Recommended LiFePO₄ Charge Settings

PARAMETER	I ² C REGISTER BITS	VALUE	EQUIVALENT PER 3.6V CHARGE (V)
Battery Low Voltage	VBAT_LOWV	0x1 = 55% x VFB_REG	1.98V
Recharge Voltage	VRECHG	0x0 = 93% x VFB_REG	3.35V

If the charger device is in DPM regulation during charging, the actual charging current will be less than the programmed value. In this case, termination is temporarily disabled and the charging safety timer is counted at half the clock rate, as explained in Charging Safety Timer. The typical charging cycle for LiFePO₄ follows the same profile as [Typical Li-Ion Battery Charging Profile](#).

6.3.4.4 Charging Termination for Li-ion and LiFePO₄

The device terminates a charge cycle when the battery voltage is above recharge threshold, and the current is below termination current. The termination current threshold is controlled by the lower option between 10% x ICHG pin setting or the ITERM register setting.

In standalone applications using the ICHG pin to program the current, the termination threshold is set at 10% of the ICHG pin value (10A ICHG pin programming results in 1A termination).

In host-controlled applications, the termination current can be programmed using the ITERM register bits. The ICHG pin can still be used to set a hardware limit for the charge current.

After the charging cycle is completed, the buck converter turns off. When termination occurs, the status register CHARGE_STAT is set to 111, and an INT pulse is asserted to the host. Termination is temporarily disabled when the charger device is in input current, or input voltage regulation. Termination can be permanently disabled by writing 0 to EN_TERM.

At low termination currents, due to the comparator offset, the actual termination current can be up to 20% higher than the termination target. To compensate for comparator offset, a programmable top-off timer (default disabled) can be applied after termination is detected. The top-off timer follows safety timer constraints, such that if safety timer is suspended, so is the top-off timer. Similarly, if safety timer is doubled, so is the top-off timer. CHARGE_STAT reports whether the top off timer is active via the 110 code. Once the Top-Off timer expires, the CHARGE_STAT register is set to 111 and an INT pulse is asserted to the host.

6.3.4.5 Charging Safety Timer

The device has built-in safety timer to prevent extended charging cycle due to abnormal battery conditions. The user can program fast charge safety timer through I²C (CHG_TMR bits). When safety timer expires, the fault register CHG_TMR_STAT bit is set to 1, and an INT pulse is asserted to the host. The safety timer feature can be disabled by clearing EN_CHG_TMR bit.

During input voltage or input current regulation, the safety timer counts at half clock rate as the actual charge current is likely to be below the programmed setting. For example, if the charger is in input current regulation (IAC_DPM_STAT=1) throughout the whole charging cycle, and the safety timer is set to 5 hours, then the timer will expire in 10 hours. The timer also counts at half clock rate for TS pin events which reduce charge current (refer to [JEITA Guideline Compliance in Charge Mode](#) section). This half clock rate feature can be disabled by setting EN_TMR2X = 0.

During faults which disable charging, timer is suspended. Once the fault goes away, safety timer resumes. If the charging cycle is stopped and started again, the timer gets reset (toggle CE pin or EN_CHG bit restarts the timer).

The pre-charge safety timer is a fixed 2 hour counter that runs when $V_{BAT} < V_{BAT_LOWV}$. The pre-charge safety timer is disabled when EN_PRECHG bit is 0.

6.3.4.6 Thermistor Qualification

The charger device provides a single thermistor input for battery temperature monitor.

6.3.4.6.1 JEITA Guideline Compliance in Charge Mode

To improve the safety of charging Li-ion batteries, JEITA guideline released on April 20, 2007. The guideline emphasized the importance of avoiding a high charge current and high charge voltage at certain low and high temperature ranges.

To initiate a charge cycle, the voltage on TS pin must be within the VT1 to VT5 thresholds. If TS voltage exceeds the T1 to T5 range, the controller suspends charging and waits until the battery temperature is within the T1 to T5 range.

At cool temperature, T1 to T2, JEITA recommends the charge current to be reduced to half of the charge current or lower. The device allows charge current in the cool temperature region to be programmed to 20%, 40% or 100% of the charge current at T2 to T3 or charge suspend, which is controlled by the register bits JEITA_ISETC. If charge current is reduced in the cool temperature region, the safety timer counts at half clock rate when EN_TMR2X = 1.

At warm temperature, T3 to T5, JEITA recommends charge voltage less than 4.1V / cell. The device provides the programmability of the charge voltage at T3-T5, to be with a voltage offset less than charge voltage at T2 to T3 or charge suspend, which is controlled by the register bits JEITA_VSET.

The charger also provides flexible voltage/current settings beyond the JEITA requirements. The charge current setting at warm temperature T3 to T5 can be configured to be 40%, or 100% of the programmed charge current

or charge suspend, which is programmed by the register bit JEITA_ISETH. If charge current is reduced in the JEITA warm region, the safety timer counts at half clock rate when EN_TMR2X = 1.

The default charging profile for JEITA is shown in the figure below, in which the blue line is the default setting and the red dash line is the programmable options.

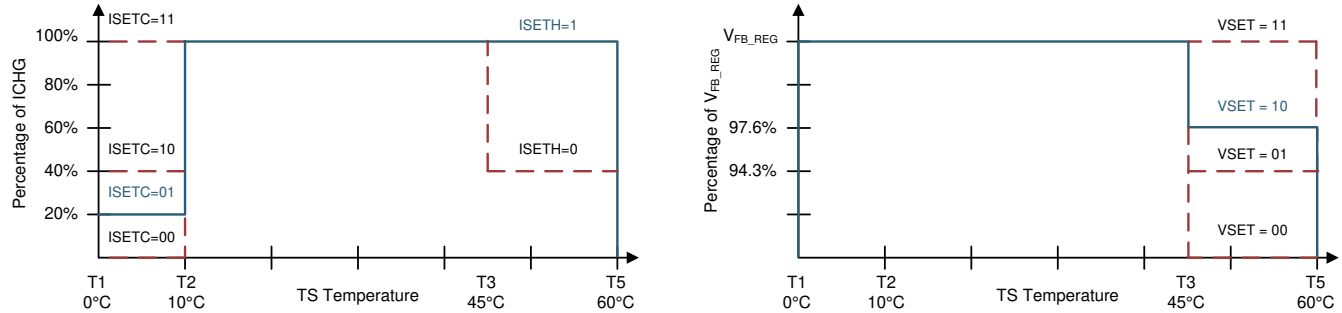
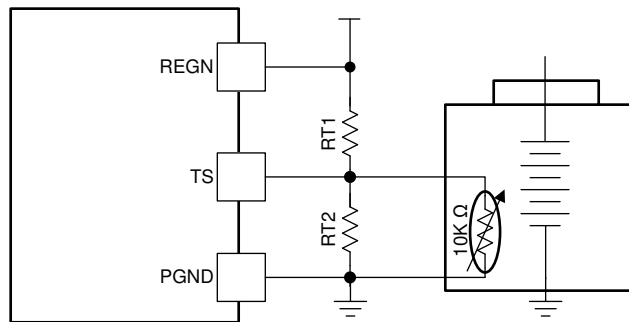


Figure 6-4. TS Charging Values



Assuming a 103AT NTC thermistor on the battery pack as shown above, the value of RT1 and RT2 can be determined by:

$$RT2 = \frac{R_{THCOLD} \times R_{THHOT} \times \left(\frac{1}{VT1} - \frac{1}{VT5} \right)}{R_{THHOT} \times \left(\frac{1}{VT5} - 1 \right) - R_{THCOLD} \times \left(\frac{1}{VT1} - 1 \right)} \quad (6)$$

$$RT1 = \frac{\frac{1}{VT1} - 1}{\frac{1}{RT2} + \frac{1}{R_{THCOLD}}} \quad (7)$$

Select 0°C to 60°C range for Li-ion or Li-polymer battery:

$$R_{THT1} = 27.28k\Omega$$

$$R_{THT5} = 3.02k\Omega$$

$$RT1 = 5.24k\Omega$$

$$RT2 = 30.31k\Omega$$

The device also offers programmability for all the thresholds via the TS Charging Threshold Control register (REG0x1B). This flexibility can help to change the charger's operating window in software.

The JEITA profile can be disabled by clearing the EN_JEITA register bit. In this case, the device still limits the charging window from T1 to T5, but no special charge profile is employed within the Cool (T1 to T2) or Warm (T3 to T5) regions.

The NTC monitoring window can be disabled by clearing the EN_TS register bit. In this case, the TS pin voltage is ignored, and the device always reports normal TS status. If EN_TS is set to 0, TS pin can be floated or connected to PGND.

6.3.4.6.2 Cold/Hot Temperature Window in Reverse Mode

For battery protection during reverse or auto-reverse mode operation, the device monitors the battery temperature to be within the VBCOLD to VBHOT thresholds. When temperature is outside of the thresholds, the reverse mode is shut off. In addition, the EN_REV and REVERSE_STAT bits are cleared to 0 and corresponding TS_STAT is reported (TS Cold or TS Hot). The temperature protection in reverse mode can be completely disabled by clearing the EN_TS bit to 0.

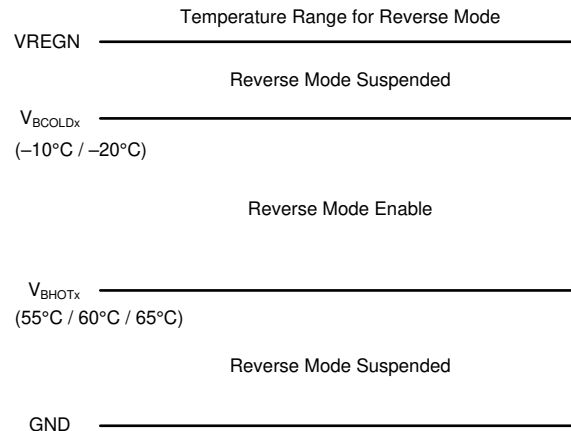


Figure 6-5. TS Pin Thermistor Sense Threshold in Reverse Mode

6.3.5 Power Management

The device accommodates a wide range of input sources from 4.4V up to 70V.

6.3.5.1 Dynamic Power Management: Input Voltage and Input Current Regulation

The device features Dynamic Power Management (DPM), which continuously monitors the input current and input voltage. When input source is over-loaded, either the current exceeds the input current limit (lower of IAC_DPM or ILIM_HIZ pin setting), or the voltage falls below the input voltage limit (higher of VAC_DPM or ACUV pin setting, V_{ACUV_DPM}). The device then reduces the charge current until the input current falls below the input current limit and the input voltage rises above the input voltage limit.

When the charge current is reduced to zero, but the input source is still overloaded, the input voltage continues to drop. Once the input voltage drops below the ACUV limit ($V_{ACUV} < V_{REF_ACUV}$), the charger stops switching.

6.3.5.1.1 Input Current Regulation

The total input current is a function of the system supply current and the battery charging current. System current normally fluctuates as portions of the systems are powered up or down. Without DPM, the source must be able to supply the maximum system current and the maximum charger input current simultaneously. By using DPM, the battery charger reduces the charging current when the input current exceeds the input current limit set by the lower of IAC_DPM register bits, or ILIM_HIZ pin. This allows the current capability of the input source to be lowered, reducing system cost.

There are two thresholds to limit the input current (if both are enabled, the lower limit of these two will apply):

1. IAC_DPM register bits (host software control)
2. ILIM_HIZ pull down resistor (hardware control)

The default IAC_DPM is set to maximum code, allowing ILIM_HIZ pin to limit the current in hardware.

To set the maximum current using the ILIM_HIZ pin, refer to [Section 6.3.5.1.1.1](#).

For example, using a 5mΩ resistor yields programmability from 400mA to 20A with 50mA/step.

6.3.5.1.1.1 ILIM_HIZ Pin

To set the maximum input current using the ILIM_HIZ pin, a pull-down resistor to PGND is used. When using a 2mΩ R_{AC_SNS} resistor, the input current limit is controlled by: $I_{AC_MAX} = K_{ILIM} / R_{ILIM_HIZ}$.

The actual input current limit is the lower value between ILIM_HIZ pin setting and register setting (IAC_DPM). For example, if the register setting is 20A, and ILIM_HIZ pin has a 5kΩ resistor ($K_{ILIM} = 50A \times k\Omega$) to ground for 10A, the actual input current limit is 10A. ILIM_HIZ pin can be used to set the input current limit when EN_ILIM_HIZ_PIN bit is set to 1. The device regulates the pin at V_{REF_ILIM_HIZ}. If pin voltage exceeds V_{REF_ILIM_HIZ}, the device enters input current regulation. Entering input current regulation through the pin sets the IAC_DPM_STAT and FLAG bits, and produces an interrupt to host. The interrupt can be masked via the IAC_DPM_MASK bit.

The ILIM_HIZ pin can also be used to monitor input current. When not in input current regulation, the voltage on ILIM_HIZ pin (V_{ILIM_HIZ}) is proportional to the input current. Pin voltage can be used to monitor input current with the following relationship: $IAC = K_{ILIM} \times V_{ILIM_HIZ} / (R_{ILIM_HIZ} \times V_{REF_ILIM_HIZ})$.

If ILIM_HIZ pin is shorted, the input current limit is set by the IAC_DPM register. If hardware input current limit function is not needed, it is recommended to short this pin to GND. If ILIM_HIZ pin is pulled above V_{IH_ILIM_HIZ}, the device enters HIZ mode (refer to [Section 6.3.3.6](#)). The ILIM_HIZ pin function can be disabled by setting the EN_ILIM_HIZ_PIN bit to 0. When the pin is disabled, input current limit and monitoring functions as well as HIZ mode control via the pin are not available.

K_{ILIM} is defined as 50A×kΩ referenced to a 2mΩ sense resistor. A larger sense resistor provides a larger sense voltage and higher regulation accuracy, but changes the gain from the ILIM_HIZ pin. For example, using a 5mΩ resistor yields $K_{ILIM} = 50 (A \times k\Omega) \times 2 (m\Omega) / 5 (m\Omega) = 20 (A \times k\Omega)$.

6.3.5.1.2 Input Voltage Regulation

In addition to input current regulation, the device also offers input voltage regulation to limit the input power. This is especially useful when dealing with input sources such as solar panels, where the operating voltage must be controlled to extract the maximum power. Alternatively, if the input source current limitation is not known, input voltage regulation can be used to limit the power draw from the input source. By using input voltage regulation, the battery charger reduces the charging current when the input voltage falls below the input voltage limit set by the higher of VAC_DPM register bits, or ACUV pin.

There are two thresholds to limit the input voltage (the higher limit of these will apply)

1. VAC_DPM register bits (host software control)
2. ACUV pin falling threshold (hardware control)

To set the minimum input voltage using the VAC_DPM register bits, write the desired value directly to the VAC_DPM register bits. The default VAC_DPM is set to minimum code, allowing ACUV pin to limit the input voltage in hardware.

To set the minimum input voltage using the ACUV pin, refer to [Section 6.3.3.1](#).

6.3.5.1.2.1 Max Power Point Tracking (MPPT) for Solar PV Panel

When EN_MPPT bit is 1, the device provides a maximum power point tracking (MPPT) algorithm for solar PV panel input sources. The Input Power Maximizer algorithm finds and tracks the maximum power point with full panel sweeps.

The full panel sweep is used to find the input operating voltage which delivers the maximum charge current to the battery. Before running a full panel sweep, the device momentarily enters HIZ mode to measure input source open-circuit voltage (V_{OC}). The device proceeds to reduce the input voltage regulation target, measuring the charge current output at each setting. The VAC_DPM register is used to program the minimum voltage to exit the full panel sweep. After the sweep is complete, the device updates the VAC_MPP register to the input voltage regulation value producing the maximum charge current. The device then waits for a period of

FULL_SWEEP_TMR[1:0] before performing a new full panel sweep. A full panel sweep can be forced at any time by setting the FORCE_SWEEP bit to 1. Note that EN_MPPT = 1 is required for FORCE_SWEEP to work. The FORCE_SWEEP bit is automatically cleared to 0 after the full panel sweep is completed. Note that the device uses the internal ADC to determine the charge current at each step of the full panel sweep, therefore writes to the IBAT_ADC_DIS bit are ignored while MPPT is enabled (EN_MPPT = 1).

Note that when the system is directly connected to the input supply, the device cannot limit the system load. Therefore, the MPPT algorithm may not find and track the true MPP under all conditions. To enable MPPT operation, it is recommended to connect the system load directly in parallel to the battery pack.

6.3.6 Reverse Mode Power Direction

The device supports buck-boost reverse power direction with CC/CV profile to deliver power from the battery to the input when the adapter is not present. The reverse mode output voltage regulation is set in VAC_REV register bits. The reverse mode also offers output current regulation via the R_{AC_SNS} resistor. This parameter is controlled by the IAC_REV register bits. The reverse mode operation can be enabled if the following conditions are valid:

1. SRN above 3.8V.
2. DRV_SUP voltage within valid operating window ($V_{DRV_UVP} < V_{DRV} < V_{DRV_OVP}$).
3. Reverse mode operation is enabled (EN_REV = 1)
4. Voltage at TS (thermistor) pin is within range configured by Reverse Temperature Monitor as configured by BHOT and BCOLD register bits

While the reverse mode is active, the device sets the REVERSE_STAT bit to 1. Host can disable the reverse operation at any time by setting EN_REV bit to 0.

The charger also monitors and regulates the battery discharging current in reverse mode. When the battery discharge current rises above the IBAT_REV register setting, the charger reduces the reverse mode power flow to limit the discharge current.

A minimum of 3.8V is needed to start the reverse mode successfully. However, once already in reverse mode, the VBAT side can be reduced up to 2.5V before the reverse mode turns off.

6.3.7 Integrated 16-Bit ADC for Monitoring

The device includes a 16-bit ADC to monitor critical system information based on the device's modes of operation. The ADC is allowed to operate if either the $V_{VAC} > V_{VAC_OK}$ or $V_{BAT} > V_{REGN_OK}$ is valid. The ADC_EN bit provides the ability to enable and disable the ADC to conserve power. The ADC_RATE bit allows continuous conversion or one-shot behavior. After a one-shot conversion finishes, the ADC_EN bit is cleared, and must be re-asserted to start a new conversion.

The ADC_SAMPLE bits control the resolution and sample speed of the ADC. By default, ADC channels will be converted in one-shot or continuous conversion mode unless disabled in the ADC Function Disable register. If an ADC parameter is disabled by setting the corresponding bit, then the read-back value in the corresponding register will be from the last valid ADC conversion or the default POR value (all zeros if no conversions have taken place). If an ADC parameter is disabled in the middle of an ADC measurement cycle, the device will finish the conversion of that parameter, but will not convert the parameter starting the next conversion cycle. If all channels are disabled in one-shot conversion mode, the ADC_EN bit is cleared.

The ADC_DONE_STAT and ADC_DONE_FLAG bits signal when a conversion is complete in one-shot mode only. This event produces an INT pulse, which can be masked with ADC_DONE_MASK. During continuous conversion mode, the ADC_DONE_STAT bit has no meaning and will be '0'. The ADC_DONE_FLAG bit will remain unchanged in continuous conversion mode.

ADC conversion operates independently of the faults present in the device. ADC conversion will continue even after a fault has occurred (such as one that causes the power stage to be disabled), and the host must set ADC_EN = '0' to disable the ADC. ADC readings are only valid for DC states and not for transients. When host

writes `ADC_EN = 0`, the ADC stops immediately, and ADC measurement values correspond to last valid ADC reading.

If the host wants to exit ADC more gracefully, it is possible to do either of the following:

1. Write `ADC_RATE` to one-shot, and the ADC will stop at the end of a complete cycle of conversions, or
2. Disable all ADC conversion channels, and the ADC will stop at the end of the current measurement.

When the system load is powered from the battery (the input source is removed, or the device is in HIZ mode), enabling the ADC automatically powers up REGN and increases the quiescent current. To keep the battery leakage low, it is recommended to duty cycle or completely disable the ADC.

6.3.8 Status Outputs ($\overline{PG}$, `STAT1`, `STAT2`, and $\overline{INT}$)

6.3.8.1 Power Good Indicator ($\overline{PG}$)

The `PG_STAT` bit goes HIGH and the $\overline{PG}$ pin pulls LOW to indicate a good input source when a valid VAC voltage is detected. The $\overline{PG}$ pin can drive an LED. All conditions must be met to indicate power good:

1. $V_{VAC_OK} < V_{VAC} < V_{VAC_INT_OV}$
2. $V_{ACUV} > V_{REF_ACUV}$
3. $V_{ACOV} < V_{REF_ACOV}$
4. Device not in HIZ mode

The $\overline{PG}$ pin can be disabled via the `DIS_PG_PIN` bit. When disabled, this pin can be controlled to pull LOW using the `FORCE_STAT3_ON` bit.

6.3.8.2 Charging Status Indicator (`STAT1`, `STAT2` Pins)

The device indicates charging state on the open drain `STAT1` and `STAT2` pins. The `STAT1`, `STAT2` pins can drive LEDs.

Table 6-6. `STAT1`, `STAT2` Pin State

CHARGING STATE	<code>STAT1</code>	<code>STAT2</code>
Charge in progress (including recharge)	ON	OFF
Charge done	OFF	ON
Charging fault detected (TS out of range, safety timer fault, etc.)	ON	ON
Charge disabled (<code>EN_CHG = 0</code> , or $\overline{CE}$ pin high)	OFF	OFF

The `STAT1`, `STAT2` pin function can be disabled via the `DIS_STAT_PINS` bit. When disabled, these pins can be controlled to independently pull LOW using the `FORCE_STAT1_ON` and `FORCE_STAT2_ON` bits. The `STAT` pins are not affected by the Reverse mode and remain OFF during this mode.

6.3.8.3 Interrupt to Host ($\overline{INT}$)

In some applications, the host does not always monitor the charger operation. The $\overline{INT}$ pin notifies the system host on the device operation. By default, the following events will generate an active-low, 256- μ s `INT` pulse.

1. Valid input source conditions detected (see conditions for $\overline{PG}$ pin)
2. Valid input source conditions removed (see conditions for $\overline{PG}$ pin)
3. Entering `IAC_DPM` regulation through register or `ILIM_HIZ` pin
4. Entering `VAC_DPM` regulation through register or `ACUV` pin
5. I²C Watchdog timer expired
6. Charger status changes state (`CHARGE_STAT` value change), including Charge Complete
7. `TS_STAT` changes state (`TS_STAT` value change)
8. Junction temperature shutdown (`TSHUT`)
9. Battery overvoltage detected (`BATOV`)
10. Charge safety timer expired
11. A rising edge on any of the `*_STAT` bits

Each one of these INT sources can be masked off to prevent INT pulses from being sent out when they occur. Three bits exist for each one of these events:

- The STAT bit holds the *current status* of each INT source
- The FLAG bit holds information on which source produced an INT, regardless of the current status
- The MASK bit is used to prevent the device from sending out INT for each particular event

When one of the above conditions occurs (a rising edge on any of the *_STAT bits), the device sends out an INT pulse and keeps track of which source generated the INT via the FLAG registers. The FLAG register bits are automatically reset to zero after the host reads them, and a new edge on STAT bit is required to re-assert the FLAG.

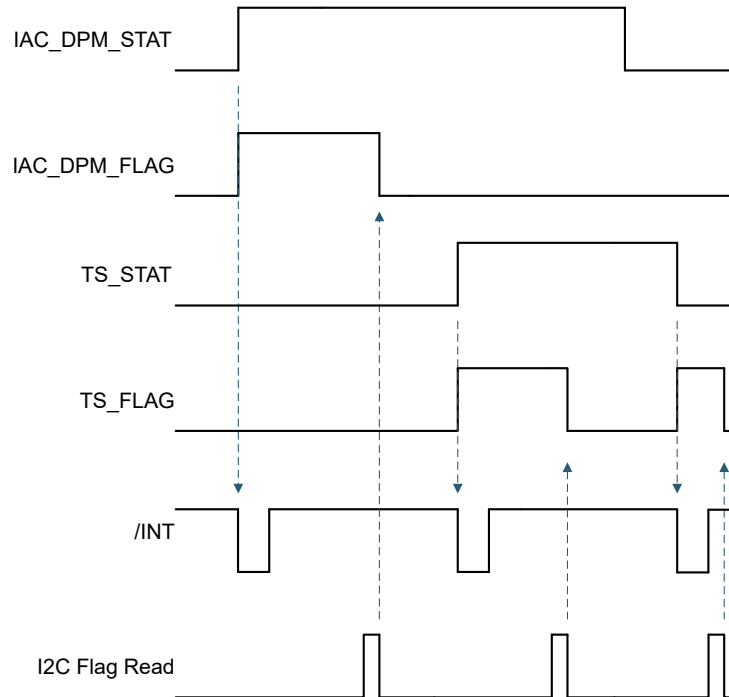


Figure 6-6. INT Generation Behavior Example

6.3.9 Protections

The device closely monitors the input and battery voltage, as well as switching FET currents for safe switch-mode operation.

6.3.9.1 Voltage and Current Monitoring

6.3.9.1.1 VAC Over-voltage Protection (VAC_OVP)

To protect downstream devices on the system rail, the input over-voltage threshold can be programmed with the ACOV pin as $V_{VACOV} = V_{REF_ACOV}$ (refer to [Section 6.3.3.1](#)). The device also features an internal over-voltage protection preset at $V_{VAC_INT_OV}$. When the input voltage rises above the lower of these two thresholds, the device disables the charger. During input over-voltage, an INT pulse is asserted to signal the host, and the VAC_OV_STAT, and _FLAG bits are set. Additionally, the PG_STAT bit is cleared and the PG pin pulls HIGH. The device automatically resumes charging operation when the over-voltage condition goes away.

6.3.9.1.2 VAC Under-voltage Protection (VAC_UVP)

To maintain a minimum operating voltage on the system rail, the input under-voltage threshold can be programmed with the ACUV pin as $V_{VACUV} = V_{REF_ACUV}$ (refer to [Section 6.3.3.1](#)). The device also features an internal under-voltage protection preset at V_{VAC_OK} . When the input voltage falls below the higher of these two thresholds, the device disables the charger. During input under-voltage, an INT pulse is asserted to signal the

host, and the VAC_UV_STAT, and _FLAG bits are set. Additionally, the PG_STAT bit is cleared and the $\overline{\text{PG}}$ pin pulls HIGH. The device automatically resumes charging operation when the under-voltage condition goes away.

6.3.9.1.3 Battery Over-voltage Protection (BAT_OVP)

The device protects against battery over-charge using the BAT_OVP comparator. When the FB voltage exceeds $V_{\text{BAT_OV}}$, the converter stops switching immediately and prevents the high-side FETs to turn on until the battery feedback voltage falls below $V_{\text{BAT_OVZ}}$. This allows one-cycle response to an overvoltage condition, such as occurs when the load is removed or the battery is disconnected. During the BAT_OVP event, the $I_{\text{BAT_LOAD}}$ turns on and sinks current from SRN to GND, allowing for the discharge of stored energy in the output capacitors. BAT_OVP also suspends the safety timer and top-off timer.

6.3.9.1.4 Battery Over-current Protection (BAT_OCP)

The device protects the battery against over-current condition using the BAT_OCP comparator. The device monitors the charge current and prevents the current from exceeding $V_{\text{ICHG_OC}}$ over $R_{\text{BAT_SNS}}$. If the $V_{\text{ICHG_OC}}$ threshold is reached, the device stops charging and attempts to restart after one second.

6.3.9.1.5 Reverse Mode Over-voltage Protection (REV_OVP)

While operating the converter in reverse mode, the device monitors the reverse voltage, V_{VAC} . When V_{VAC} rises above the regulation target and exceeds $V_{\text{REV_OVP}}$, the device stops switching, and waits for the voltage to fall below the threshold to resume switching. An INT pulse is asserted to the host.

6.3.9.1.6 Reverse Mode Under-voltage Protection (REV_UVP)

While operating the converter in reverse mode, the device monitors the reverse voltage, V_{VAC} . When V_{VAC} falls below the undervoltage threshold (programmable via SYSREV_UV register bit), the device stops switching, clears the EN_REV bit, and exits Reverse mode. During the under-voltage event duration, the REVERSE_STAT bit is cleared and the REVERSE_FLAG bit is set to indicate a fault in reverse mode. An INT pulse is also asserted to the host.

6.3.9.1.7 DRV_SUP Under-voltage and Over-voltage Protection (DRV_OKZ)

The DRV_SUP pin must maintain a valid voltage between DRV_UVP and DRV_OVP for proper operation of the switching power converter stage. This is true both in charging mode and in reverse mode.

When DRV_SUP pin voltage falls below DRV_UVP threshold, the switching converter stops operation, an INT pulse is asserted to signal the host, the DRV_OKZ_STAT, and DRV_OKZ_FLAG bits are set to signal the fault. Additionally, the STAT1 and STAT2 pins will change to reflect the charger function is disabled.

When DRV_SUP pin voltage rises above DRV_OVP threshold, the switching converter stops operation, an INT pulse is asserted to signal the host, the DRV_OKZ_STAT, and DRV_OKZ_FLAG bit are set to signal the fault. Additionally the STAT1 and STAT2 pins will change to reflect the charger function is disabled.

When the DRV pin returns to normal operating range, the device automatically resumes switching in either charging or reverse mode as configured before the fault.

6.3.9.1.8 REGN Under-voltage Protection (REGN_OKZ)

The REGN pin is driven by an internal regulator, and must maintain a voltage above REGN_OKZ for proper device operation. This is true both in charging mode and in reverse mode, and for the ADC to function in battery only mode.

If the internal regulator is overloaded externally, the pin voltage may drop. When REGN falls below REGN_OKZ threshold, the switching converter stops operation. Additionally, the STAT1 and STAT2 pins will change to reflect the charger function is disabled. When the fault is removed, the REGN voltage recovers automatically and switching resumes in either charging or reverse mode as configured before the fault.

6.3.9.2 Thermal Shutdown (TSHUT)

The device has thermal shutdown to turn off the converter when IC surface temperature exceeds TSHUT. The fault register bits TSHUT_STAT and TSHUT_FLAG are set and an INT pulse is asserted to the host. The

converter turns back on when IC temperature is below TSHUT_HYS. Note that TSHUT protection is active both in charging and reverse mode of operation.

6.3.10 Serial Interface

The device uses I²C compatible interface for flexible charging parameter programming and instantaneous device status reporting. I²C is a bi-directional 2-wire serial interface. Only two open-drain bus lines are required: a serial data line (SDA), and a serial clock line (SCL). Devices can be considered as controllers or targets when performing data transfers. A controller is a device which initiates a data transfer on the bus and generates the clock signals to permit that transfer. At that time, any device addressed is considered a target.

The device operates as a target device with address 0x6B, receiving control inputs from the controller device like a micro-controller or digital signal processor through the registers defined in the Register Map. Registers read outside those defined in the map, return 0xFF. The I²C interface supports standard mode (up to 100 kbits/s), fast mode (up to 400 kbits/s), and fast mode plus (up to 1 Mbit/s). When the bus is free, both lines are HIGH. The SDA and SCL pins are open drain and must be connected to the positive supply voltage via a current source or pull-up resistor.

System Note: All 16-bit registers are defined as Little Endian, with the most-significant byte allocated to the higher address. 16-bit register writes must be done sequentially and are recommended to be programmed using multi-write approach described in the [Section 6.3.10.7](#).

6.3.10.1 Data Validity

The data on the SDA line must be stable during the HIGH period of the clock. The HIGH or LOW state of the data line can only change when the clock signal on SCL line is LOW. One clock pulse is generated for each data bit transferred.

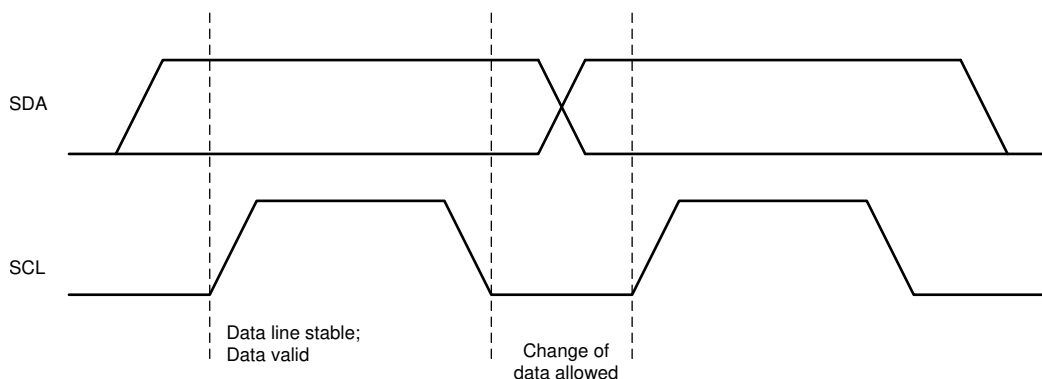


Figure 6-7. Bit Transfers on the I²C Bus

6.3.10.2 START and STOP Conditions

All transactions begin with a START (S) and are terminated with a STOP (P). A HIGH to LOW transition on the SDA line while SCL is HIGH defines a START condition. A LOW to HIGH transition on the SDA line when the SCL is HIGH defines a STOP condition.

START and STOP conditions are always generated by the controller. The bus is considered busy after the START condition, and free after the STOP condition. When timeout condition is met, for example START condition is active for more than 2 seconds and there is no STOP condition triggered, the charger I²C communication will automatically reset and communication lines are free for another transmission.

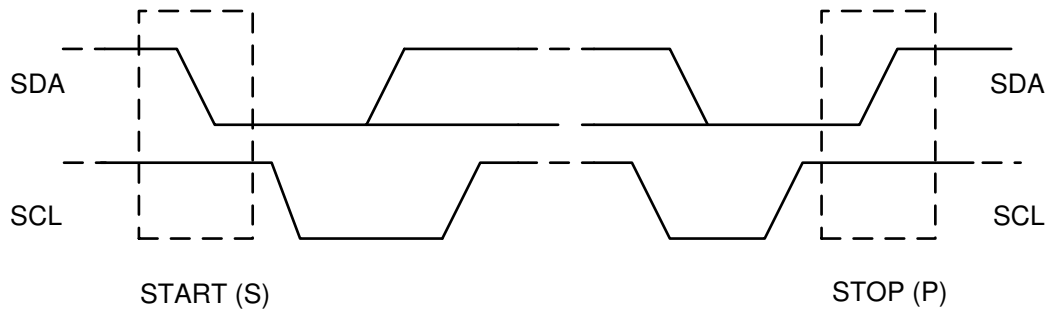


Figure 6-8. START and STOP Conditions on the I²C Bus

6.3.10.3 Byte Format

Every byte on the SDA line must be 8 bits long. The number of bytes to be transmitted per transfer is unrestricted. Each byte has to be followed by an ACKNOWLEDGE (ACK) bit. Data is transferred with the Most Significant Bit (MSB) first.

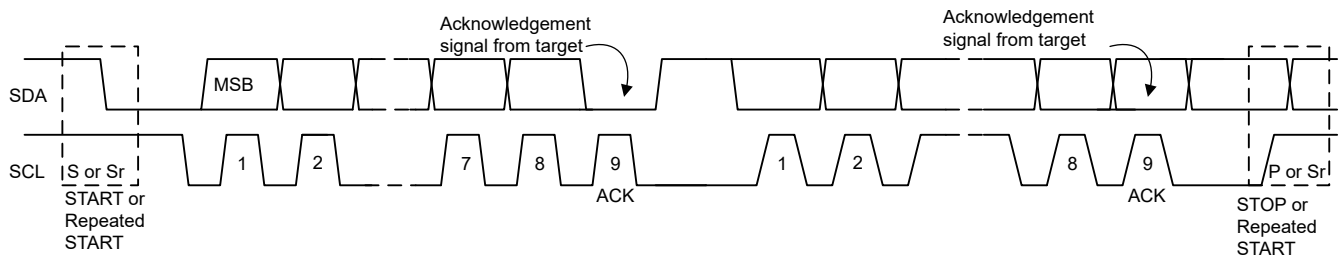


Figure 6-9. Data Transfer on the I²C Bus

6.3.10.4 Acknowledge (ACK) and Not Acknowledge (NACK)

The ACK signaling takes place after each byte. The ACK bit allows the target to signal the controller that the byte was successfully received and another byte may be sent. All clock pulses, including the acknowledge 9th clock pulse, are generated by the controller.

The controller releases the SDA line during the acknowledge clock pulse so the target can pull the SDA line LOW and it remains stable LOW during the HIGH period of this 9th clock pulse.

A NACK is signaled when the SDA line remains HIGH during the 9th clock pulse. The controller can then generate either a STOP to abort the transfer or a repeated START to start a new transfer.

6.3.10.5 Target Address and Data Direction Bit

After the START signal, a target address is sent. This address is 7 bits long, followed by the 8 bit as a data direction bit (bit R/ $\bar{W}$). A zero indicates a transmission (WRITE) and a one indicates a request for data (READ). The device 7-bit address is defined as 1101 011' (0x6B) by default.

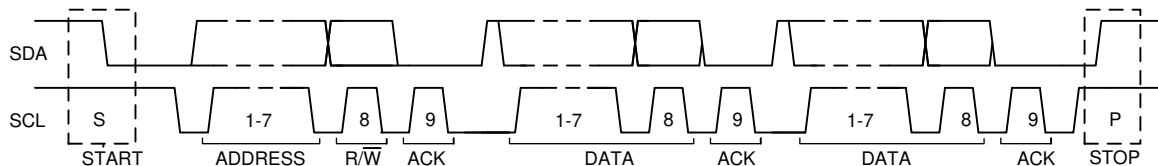


Figure 6-10. Complete Data Transfer on the I²C Bus

6.3.10.6 Single Write and Read

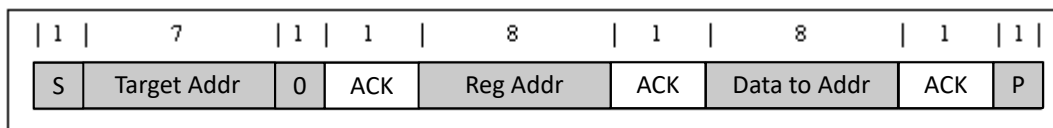


Figure 6-11. Single Write

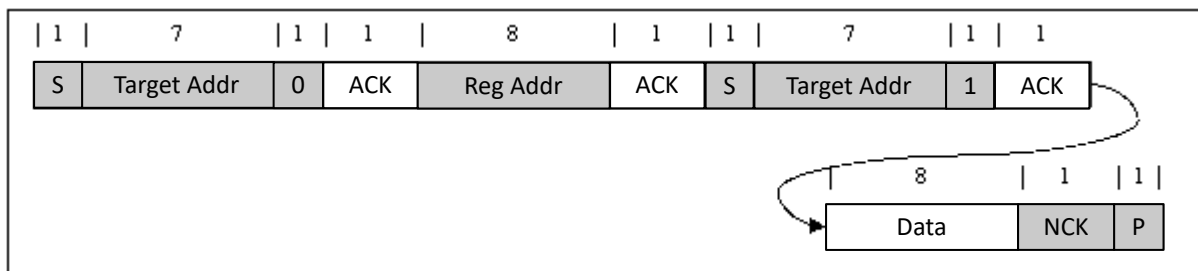


Figure 6-12. Single Read

If the register address is not defined, the charger IC sends back NACK and returns to the idle state.

6.3.10.7 Multi-Write and Multi-Read

The charger device supports multi-read and multi-write of all registers.

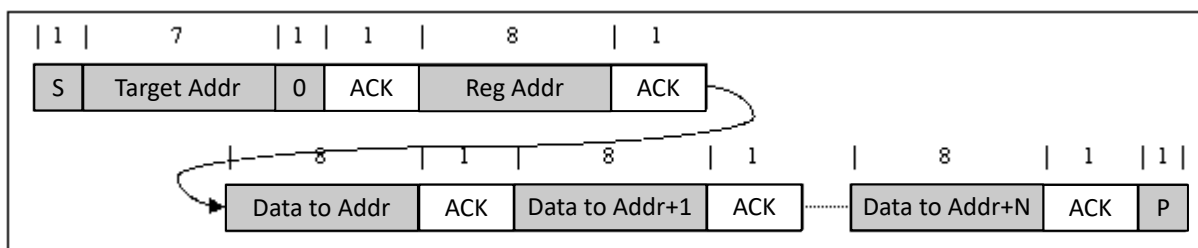


Figure 6-13. Multi-Write

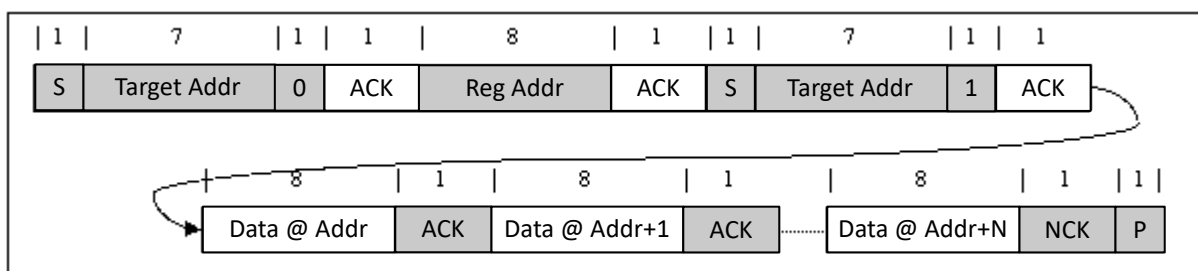


Figure 6-14. Multi-Read

6.4 Device Functional Modes

6.4.1 Host Mode and Default Mode

The device is a host controlled charger, but it can operate in default mode without host management. In default mode, the device can be used as an autonomous charger with no host or while host is in sleep mode. When the charger is in default mode, WD_STAT bit becomes HIGH, WD_FLAG is set to 1, and a $\overline{\text{INT}}$ is asserted low to alert the host (unless masked by WD_MASK). The WD_FLAG bit would read as a '1' upon the first read and then '0' upon subsequent reads. When the charger is in host mode, WD_STAT bit is LOW.

After power-on-reset, the device starts in default mode with watchdog timer expired. All the registers are in the default settings.

In default mode, the device keeps charging the battery with default 2-hour pre-charging safety timer and the 12-hour fast charging safety timer. At the end of the 2-hour or 12-hour timer expiration, the charging is stopped if termination has not been detected.

A write to any I²C register transitions the charger from default mode to host mode, and initiates the watchdog timer. All the device parameters can be programmed by the host. To keep the device in host mode, the host has to reset the watchdog timer by writing 1 to WD_RST bit before the watchdog timer expires (WD_STAT bit is set), or disable watchdog timer by setting WATCHDOG bits = 00.

When the watchdog timer is expired, the device returns to default mode and select registers are reset to default values as detailed in the Register Map section. The Watchdog timer will be reset on any write if the watchdog timer has expired. When watchdog timer expires, WD_STAT and WD_FLAG is set to 1, and /INT is asserted low to alert the host (unless masked by WD_MASK).

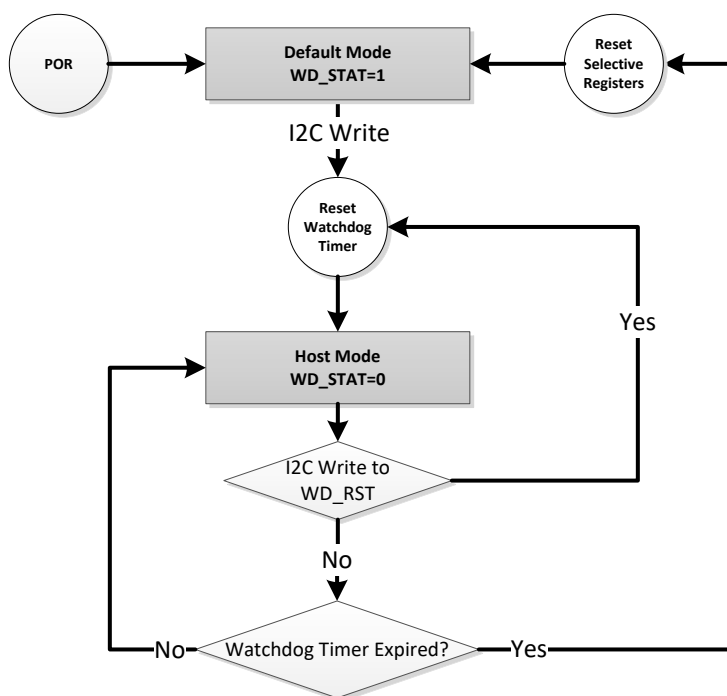


Figure 6-15. Watchdog Timer Flow Chart

6.4.2 Register Bit Reset

Besides the register reset by the watchdog timer in the default mode, the registers and the timer can be reset to the default value by writing the REG_RST bit to 1. The register bits which can be reset by the REG_RST bit are noted in the Register Map section. After the register reset, the REG_RST bit will go back from 1 to 0 automatically.

6.5 BQ25756 Registers

Section 6.5 lists the memory-mapped registers for the BQ25756 registers. All register offset addresses not listed in Table 6-7 must be considered as reserved locations and the register contents must not be modified.

Table 6-7. BQ25756 Registers

Address	Acronym	Register Name	Section
0x0	REG0x00_Charge_Voltage_Limit	Charge Voltage Limit	Go
0x2	REG0x02_Charge_Current_Limit	Charge Current Limit	Go

Table 6-7. BQ25756 Registers (continued)

Address	Acronym	Register Name	Section
0x6	REG0x06_Input_Current_DPM_Limit	Input Current DPM Limit	Go
0x8	REG0x08_Input_Voltage_DPM_Limit	Input Voltage DPM Limit	Go
0xA	REG0x0A_Reverse_Mode_Input_Current_Limit	Reverse Mode Input Current Limit	Go
0xC	REG0x0C_Reverse_Mode_Input_Voltage_Limit	Reverse Mode Input Voltage Limit	Go
0x10	REG0x10_Precharge_Current_Limit	Precharge Current Limit	Go
0x12	REG0x12_Termination_Current_Limit	Termination Current Limit	Go
0x14	REG0x14_Precharge_and_Termination_Control	Precharge and Termination Control	Go
0x15	REG0x15_Timer_Control	Timer Control	Go
0x16	REG0x16_Three-Stage_Charge_Control	Three-Stage Charge Control	Go
0x17	REG0x17_Charger_Control	Charger Control	Go
0x18	REG0x18_Pin_Control	Pin Control	Go
0x19	REG0x19_Power_Path_and_Reverse_Mode_Control	Power Path and Reverse Mode Control	Go
0x1A	REG0x1A_MPPT_Control	MPPT Control	Go
0x1B	REG0x1B_TS_Charging_Threshold_Control	TS Charging Threshold Control	Go
0x1C	REG0x1C_TS_Charging_Region_Behavior_Control	TS Charging Region Behavior Control	Go
0x1D	REG0x1D_TS_Reverse_Mode_Threshold_Control	TS Reverse Mode Threshold Control	Go
0x1E	REG0x1E_Reverse_Undervoltage_Control	Reverse Undervoltage Control	Go
0x1F	REG0x1F_VAC_Max_Power_Point_Detected	VAC Max Power Point Detected	Go
0x21	REG0x21_Charger_Status_1	Charger Status 1	Go
0x22	REG0x22_Charger_Status_2	Charger Status 2	Go
0x23	REG0x23_Charger_Status_3	Charger Status 3	Go
0x24	REG0x24_Fault_Status	Fault Status	Go
0x25	REG0x25_Charger_Flag_1	Charger Flag 1	Go
0x26	REG0x26_Charger_Flag_2	Charger Flag 2	Go
0x27	REG0x27_Fault_Flag	Fault Flag	Go
0x28	REG0x28_Charger_Mask_1	Charger Mask 1	Go
0x29	REG0x29_Charger_Mask_2	Charger Mask 2	Go
0x2A	REG0x2A_Fault_Mask	Fault Mask	Go
0x2B	REG0x2B_ADC_Control	ADC Control	Go
0x2C	REG0x2C_ADC_Channel_Control	ADC Channel Control	Go
0x2D	REG0x2D_IAC_ADC	IAC ADC	Go
0x2F	REG0x2F_IBAT_ADC	IBAT ADC	Go
0x31	REG0x31_VAC_ADC	VAC ADC	Go
0x33	REG0x33_VBAT_ADC	VBAT ADC	Go
0x37	REG0x37_TS_ADC	TS ADC	Go
0x39	REG0x39_VFB_ADC	VFB ADC	Go
0x3B	REG0x3B_Gate_Driver_Strength_Control	Gate Driver Strength Control	Go
0x3C	REG0x3C_Gate_Driver_Dead_Time_Control	Gate Driver Dead Time Control	Go

Table 6-7. BQ25756 Registers (continued)

Address	Acronym	Register Name	Section
0x3D	REG0x3D_Part_Information	Part Information	Go
0x62	REG0x62_Reverse_Mode_Battery_Discharge_Current	Reverse Mode Battery Discharge Current	Go

Complex bit access types are encoded to fit into small table cells. [Table 6-8](#) shows the codes that are used for access types in this section.

Table 6-8. BQ25756 Access Type Codes

Access Type	Code	Description
Read Type		
R	R	Read
Write Type		
W	W	Write
Reset or Default Value		
-n		Value after reset or the default value

6.5.1 REG0x00_Charge_Voltage_Limit Register (Address = 0x0) [Reset = 0x0010]

REG0x00_Charge_Voltage_Limit is shown in [Table 6-9](#).

Return to the [Summary Table](#).

I2C REG0x01=[15:8], I2C REG0x00=[7:0]

Table 6-9. REG0x00_Charge_Voltage_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:5	RESERVED	R	0x0		Reserved
4:0	VFB_REG	R/W	0x10	Reset by: REG_RESET	FB Voltage Regulation Limit: POR: 1536mV (10h) Range: 1504mV-1566mV (0h-1Fh) Bit Step: 2mV Offset: 1504mV

6.5.2 REG0x02_Charge_Current_Limit Register (Address = 0x2) [Reset = 0x0640]

REG0x02_Charge_Current_Limit is shown in [Table 6-10](#).

Return to the [Summary Table](#).

I2C REG0x03=[15:8], I2C REG0x02=[7:0]

Table 6-10. REG0x02_Charge_Current_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:11	RESERVED	R	0x0		Reserved
10:2	ICHG_REG	R/W	0x190	Reset by: REG_RESET WATCHDOG	Fast Charge Current Regulation Limit with 5mΩ RBAT_SNS: Actual charge current is the lower of ICHG_REG and ICHG pin POR: 20000mA (190h) Range: 400mA-20000mA (8h-190h) Clamped Low Clamped High Bit Step: 50mA

Table 6-10. REG0x02_Charge_Current_Limit Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
1:0	RESERVED	R	0x0		Reserved

6.5.3 REG0x06_Input_Current_DPM_Limit Register (Address = 0x6) [Reset = 0x0640]

REG0x06_Input_Current_DPM_Limit is shown in [Table 6-11](#).

Return to the [Summary Table](#).

I2C REG0x07=[15:8], I2C REG0x06=[7:0]

Table 6-11. REG0x06_Input_Current_DPM_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:11	RESERVED	R	0x0		Reserved
10:2	IAC_DPM	R/W	0x190	Reset by: REG_RESET	Input Current DPM Regulation Limit with 5mΩ RAC_SNS: Actual input current limit is the lower of IAC_DPM and ILIM_HIZ pin POR: 20000mA (190h) Range: 400mA-20000mA (8h-190h) Clamped Low Clamped High Bit Step: 50mA
1:0	RESERVED	R	0x0		Reserved

6.5.4 REG0x08_Input_Voltage_DPM_Limit Register (Address = 0x8) [Reset = 0x0348]

REG0x08_Input_Voltage_DPM_Limit is shown in [Table 6-12](#).

Return to the [Summary Table](#).

I2C REG0x09=[15:8], I2C REG0x08=[7:0]

Table 6-12. REG0x08_Input_Voltage_DPM_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:14	RESERVED	R	0x0		Reserved
13:2	VAC_DPM	R/W	0xD2	Reset by: REG_RESET	Input Voltage Regulation Limit: Note if EN_MPPT = 1, the Full Sweep method uses this limit as the lower search window for Full Panel Sweep POR: 4200mV (D2h) Range: 4200mV-65000mV (D2h-CB2h) Clamped Low Clamped High Bit Step: 20mV
1:0	RESERVED	R	0x0		Reserved

6.5.5 REG0x0A_Reverse_Mode_Input_Current_Limit Register (Address = 0xA) [Reset = 0x0640]

REG0x0A_Reverse_Mode_Input_Current_Limit is shown in [Table 6-13](#).

Return to the [Summary Table](#).

I2C REG0x0B=[15:8], I2C REG0x0A=[7:0]

Table 6-13. REG0x0A_Reverse_Mode_Input_Current_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:11	RESERVED	R	0x0		Reserved
10:2	IAC_REV	R/W	0x190	Reset by: REG_RESET	Input Current Regulation in Reverse Mode with 5mΩ RAC_SNS: POR: 20000mA (190h) Range: 400mA-20000mA (8h-190h) Clamped Low Clamped High Bit Step: 50mA
1:0	RESERVED	R	0x0		Reserved

6.5.6 REG0x0C_Reverse_Mode_Input_Voltage_Limit Register (Address = 0xC) [Reset = 0x03E8]

REG0x0C_Reverse_Mode_Input_Voltage_Limit is shown in [Table 6-14](#).

Return to the [Summary Table](#).

I2C REG0x0D=[15:8], I2C REG0x0C=[7:0]

Table 6-14. REG0x0C_Reverse_Mode_Input_Voltage_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:14	RESERVED	R	0x0		Reserved
13:2	VAC_REV	R/W	0xFA	Reset by: REG_RESET	VAC Voltage Regulation in Reverse Mode: POR: 5000mV (FAh) Range: 3300mV-6500mV (A5h-CB2h) Clamped Low Clamped High Bit Step: 20mV
1:0	RESERVED	R	0x0		Reserved

6.5.7 REG0x10_Precharge_Current_Limit Register (Address = 0x10) [Reset = 0x0140]

REG0x10_Precharge_Current_Limit is shown in [Table 6-15](#).

Return to the [Summary Table](#).

I2C REG0x11=[15:8], I2C REG0x10=[7:0]

Table 6-15. REG0x10_Precharge_Current_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:10	RESERVED	R	0x0		Reserved
9:2	IPRECHG	R/W	0x50	Actual pre-charge current is the lower of IPRECHG and ICHG pin Reset by: REG_RESET	Pre-charge current regulation limit with 5mΩ RBAT_SNS: POR: 4000mA (50h) Range: 250mA-10000mA (5h-C8h) Clamped Low Clamped High Bit Step: 50mA
1:0	RESERVED	R	0x0		Reserved

6.5.8 REG0x12_Termination_Current_Limit Register (Address = 0x12) [Reset = 0x00A0]

REG0x12_Termination_Current_Limit is shown in [Table 6-16](#).

Return to the [Summary Table](#).

I2C REG0x13=[15:8], I2C REG0x12=[7:0]

Table 6-16. REG0x12_Termination_Current_Limit Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:10	RESERVED	R	0x0		Reserved
9:2	ITERM	R/W	0x28	Actual termination current is the lower of ITERM and ICHG pin if both functions enabled Reset by: REG_RESET	Termination Current Threshold with 5mΩ RBAT_SNS: POR: 2000mA (28h) Range: 250mA-10000mA (5h-C8h) Clamped Low Clamped High Bit Step: 50mA
1:0	RESERVED	R	0x0		Reserved

6.5.9 REG0x14_Precharge_and_Termination_Control Register (Address = 0x14) [Reset = 0x0F]

REG0x14_Precharge_and_Termination_Control is shown in [Table 6-17](#).

Return to the [Summary Table](#).

Table 6-17. REG0x14_Precharge_and_Termination_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:4	RESERVED	R	0x0		Reserved
3	EN_TERM	R/W	0x1	Reset by: REG_RESET	Enable termination control 0b = Disable 1b = Enable
2:1	VBAT_LOWV	R/W	0x3	Reset by: REG_RESET	Battery threshold for PRECHG to FASTCHG transition, as percentage of VFB_REG: 00b = 30% x VFB_REG 01b = 55% x VFB_REG 10b = 66.7% x VFB_REG 11b = 71.4% x VFB_REG
0	EN_PRECHG	R/W	0x1	Reset by: REG_RESET	Enable pre-charge and trickle charge functions: 0b = Disable 1b = Enable

6.5.10 REG0x15_Timer_Control Register (Address = 0x15) [Reset = 0x1D]

REG0x15_Timer_Control is shown in [Table 6-18](#).

Return to the [Summary Table](#).

Table 6-18. REG0x15_Timer_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	TOPOFF_TMR	R/W	0x0	Reset by: REG_RESET	Top-off timer control: 00b = Disable 01b = 15 mins 10b = 30 mins 11b = 45 mins
5:4	WATCHDOG	R/W	0x1	Reset by: REG_RESET	Watchdog timer control: 00b = Disable 01b = 40s 10b = 80s 11b = 160s
3	EN_CHG_TMR	R/W	0x1	Reset by: REG_RESET WATCHDOG	Enable charge safety timer: 0b = Disable 1b = Enable

Table 6-18. REG0x15_Timer_Control Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
2:1	CHG_TMR	R/W	0x2	Reset by: REG_RESET	Charge safety timer setting: 00b = 5hr 01b = 8hr 10b = 12hr 11b = 24hr
0	EN_TMR2X	R/W	0x1	Reset by: REG_RESET	Charge safety timer speed in DPM: 0b = Timer always counts normally 1b = Timer slowed by 2x during input DPM

6.5.11 REG0x16_Three-Stage_Charge_Control Register (Address = 0x16) [Reset = 0x00]

REG0x16_Three-Stage_Charge_Control is shown in [Table 6-19](#).

Return to the [Summary Table](#).

Table 6-19. REG0x16_Three-Stage_Charge_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	RESERVED	R	0x0		Reserved
5	RESERVED	R	0x0		Reserved
4	RESERVED	R	0x0		Reserved
3:0	RESERVED	R	0x0		Reserved

6.5.12 REG0x17_Charger_Control Register (Address = 0x17) [Reset = 0xC9]

REG0x17_Charger_Control is shown in [Table 6-20](#).

Return to the [Summary Table](#).

Table 6-20. REG0x17_Charger_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	VRECHG	R/W	0x3	Reset by: REG_RESET	Battery auto-recharge threshold, as percentage of VFB_REG: 00b = 93.0% x VFB_REG 01b = 94.3% x VFB_REG 10b = 95.2% x VFB_REG 11b = 97.6% x VFB_REG
5	WD_RST	R/W	0x0	Reset by: REG_RESET	I2C Watchdog timer reset control: 0b = Normal 1b = Reset (bit goes back to 0 after timer reset)
4	DIS_CE_PIN	R/W	0x0	Reset by: REG_RESET	/CE pin function disable: 0b = /CE pin enabled 1b = /CE pin disabled
3	EN_CHG_BIT_RES ET_BEHAVIOR	R/W	0x1	Reset by: REG_RESET	Controls the EN_CHG bit behavior when WATCHDOG expires: 0b = EN_CHG bit resets to 0 1b = EN_CHG bit resets to 1
2	EN_HIZ	R/W	0x0	Reset by: REG_RESET WATCHDOG Adapter Plug In	HIZ mode enable: 0b = Disable 1b = Enable

Table 6-20. REG0x17_Charger_Control Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
1	EN_IBAT_LOAD	R/W	0x0	Sinks current from SRN to GND. Recommend to disable IBAT ADC (IBAT_ADC_DIS = 1) while this bit is active. Reset by: REG_RESET WATCHDOG	Battery Load (IBAT_LOAD) Enable: 0b = Disabled 1b = Enabled
0	EN_CHG	R/W	0x1	Reset by: REG_RESET WATCHDOG	Charge enable control: 0b = Disable 1b = Enable

6.5.13 REG0x18_Pin_Control Register (Address = 0x18) [Reset = 0xC0]

REG0x18_Pin_Control is shown in [Table 6-21](#).

Return to the [Summary Table](#).

Table 6-21. REG0x18_Pin_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	EN_ICHG_PIN	R/W	0x1	Reset by: REG_RESET WATCHDOG	ICHG pin function enable: 0b = ICHG pin disabled 1b = ICHG pin enabled
6	EN_ILIM_HIZ_PIN	R/W	0x1	Reset by: REG_RESET WATCHDOG	ILIM_HIZ pin function enable: 0b = ILIM_HIZ pin disabled 1b = ILIM_HIZ pin enabled
5	DIS_PG_PIN	R/W	0x0	Reset by: REG_RESET	PG pin function disable: 0b = PG pin enabled 1b = PG pin disabled
4	DIS_STAT_PINS	R/W	0x0	Reset by: REG_RESET	STAT1, STAT2 pin function disable: 0b = STAT pins enabled 1b = STAT pins disabled
3	FORCE_STAT4_ON	R/W	0x0	Reset by: REG_RESET	CE_STAT4 pin override: Can only be forced on if DIS_CE_PIN = 1 0b = CE_STAT4 open-drain off 1b = CE_STAT4 pulls LOW
2	FORCE_STAT3_ON	R/W	0x0	Reset by: REG_RESET	PG_STAT3 pin override: Can only be forced on if DIS_PG_PIN = 1 0b = PG_STAT3 open-drain off 1b = PG_STAT3 pulls LOW
1	FORCE_STAT2_ON	R/W	0x0	Reset by: REG_RESET	STAT2 pin override: Can only be forced on if DIS_STAT_PINS = 1 0b = STAT2 open-drain off 1b = STAT2 pulls LOW
0	FORCE_STAT1_ON	R/W	0x0	Reset by: REG_RESET	STAT1 pin override: Can only be forced on if DIS_STAT_PINS = 1 0b = STAT1 open-drain off 1b = STAT1 pulls LOW

6.5.14 REG0x19_Power_Path_and_Reverse_Mode_Control Register (Address = 0x19) [Reset = 0x20]

REG0x19_Power_Path_and_Reverse_Mode_Control is shown in [Table 6-22](#).

Return to the [Summary Table](#).

Table 6-22. REG0x19_Power_Path_and_Reverse_Mode_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	REG_RST	R/W	0x0	Reset by: REG_RESET	Register reset to default values: 0b = Not reset 1b = Reset (bit goes back to 0 after register reset)
6	EN_IAC_LOAD	R/W	0x0	Reset by: REG_RESET WATCHDOG	VAC Load (IAC_LOAD) Enable: 0b = Disabled 1b = Enabled
5	EN_PFM	R/W	0x1	It is recommended to disable PFM when ITERM < 2A Reset by: REG_RESET	Enable PFM mode in light-load: Note this bit is reset upon a valid SYNC signal detection on FSW_SYNC pin. Host can set this bit back to 1 to force PFM operation even with a valid SYNC input 0b = Disable (Fixed-frequency DCM operation) 1b = Enable (PFM operation)
4	RESERVED	R	0x0		Reserved
3	RESERVED	R	0x0		Reserved
2	RESERVED	R	0x0		Reserved
1	RESERVED	R	0x0		Reserved
0	EN_REV	R/W	0x0	Reset by: REG_RESET WATCHDOG Adapter Plug In	Reverse Mode control: 0b = Disable 1b = Enable

6.5.15 REG0x1A_MPPT_Control Register (Address = 0x1A) [Reset = 0x20]

REG0x1A_MPPT_Control is shown in [Table 6-23](#).

Return to the [Summary Table](#).

Table 6-23. REG0x1A_MPPT_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	FORCE_SWEEP	R/W	0x0	Reset by: REG_RESET	Force Full Panel Sweep and reset MPPT timers: 0b = Normal 1b = Start Full Panel Sweep (bit goes back to 0 after Full Panel Sweep complete)
6:5	P_AND_O_TMR	R/W	0x1	Reset by: REG_RESET	Perturb and Observe timer control: 00b = Disable Perturb & Observe 01b = 0.5s 10b = 1s 11b = 10s
4:3	RESERVED	R	0x0		Reserved
2:1	FULL_SWEEP_TMR	R/W	0x0	Reset by: REG_RESET	Full Panel Sweep timer control: 00b = 3 min 01b = 10 min 10b = 15 min 11b = 20 min
0	EN_MPPT	R/W	0x0	When MPPT is enabled, the ADC is controlled by the device, writes to REG0x2B are ignored Reset by: REG_RESET	MPPT algorithm control: 0b = Disable MPPT 1b = Enable MPPT

6.5.16 REG0x1B_TS_Charging_Threshold_Control Register (Address = 0x1B) [Reset = 0x96]

REG0x1B_TS_Charging_Threshold_Control is shown in [Table 6-24](#).

Return to the [Summary Table](#).

Table 6-24. REG0x1B_TS_Charging_Threshold_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	TS_T5	R/W	0x2	Reset by: REG_RESET	TS T5 (HOT) threshold control: 00b = 41.2% (50C) 01b = 37.7% (55C) 10b = 34.375% (60C) 11b = 31.25% (65C)
5:4	TS_T3	R/W	0x1	Reset by: REG_RESET	JEITA TS T3 (WARM) threshold control: 00b = 48.4% (40C) 01b = 44.8% (45C) 10b = 41.2% (50C) 11b = 37.7% (55C)
3:2	TS_T2	R/W	0x1	Reset by: REG_RESET	JEITA TS T2 (COOL) threshold control: 00b = 71.1% (5C) 01b = 68.4% (10C) 10b = 65.5% (15C) 11b = 62.4% (20C)
1:0	TS_T1	R/W	0x2	Reset by: REG_RESET	TS T1 (COLD) threshold control: 00b = 77.15% (-10C) 01b = 75.32% (-5C) 10b = 73.25% (0C) 11b = 71.1% (5C)

6.5.17 REG0x1C_TS_Charging_Region_Behavior_Control Register (Address = 0x1C) [Reset = 0x57]

REG0x1C_TS_Charging_Region_Behavior_Control is shown in [Table 6-25](#).

Return to the [Summary Table](#).

Table 6-25. REG0x1C_TS_Charging_Region_Behavior_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	RESERVED	R	0x0		Reserved
6:5	JEITA_VSET	R/W	0x2	Reset by: REG_RESET	JEITA Warm (T3 < TS < T5) regulation voltage setting, as percentage of VFB_REG: 00b = Charge Suspend 01b = 94.3% x VFB_REG 10b = 97.6% x VFB_REG 11b = 100% x VFB_REG
4	JEITA_ISETH	R/W	0x1	Reset by: REG_RESET	JEITA Warm (T3 < TS < T5) regulation current setting, as percentage of ICHG_REG: 0b = 40% x ICHG_REG 1b = 100% x ICHG_REG
3:2	JEITA_ISETC	R/W	0x1	Reset by: REG_RESET	JEITA Cool (T1 < TS < T2) regulation current setting, as percentage of ICHG_REG: 00b = Charge Suspend 01b = 20% x ICHG_REG 10b = 40% x ICHG_REG 11b = 100% x ICHG_REG
1	EN_JEITA	R/W	0x1	Reset by: REG_RESET	JEITA profile control: 0b = Disabled (COLD/HOT control only) 1b = Enabled (COLD/COOL/WARM/HOT control)

Table 6-25. REG0x1C_TS_Charging_Region_Behavior_Control Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
0	EN_TS	R/W	0x1	Reset by: REG_RESET	TS pin function control (applies to forward charging and reverse discharging modes): 0b = Disabled (ignore TS pin) 1b = Enabled

6.5.18 REG0x1D_TS_Reverse_Mode_Threshold_Control Register (Address = 0x1D) [Reset = 0x40]

REG0x1D_TS_Reverse_Mode_Threshold_Control is shown in [Table 6-26](#).

Return to the [Summary Table](#).

Table 6-26. REG0x1D_TS_Reverse_Mode_Threshold_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	BHOT	R/W	0x1	Reset by: REG_RESET	Reverse Mode TS HOT temperature threshold control: 00b = 37.7% (55C) 01b = 34.2% (60C) 10b = 31.25%(65C) 11b = Disable
5	BCOLD	R/W	0x0	Reset by: REG_RESET	Reverse Mode TS COLD temperature threshold control: 0b = 77.15% (-10C) 1b = 80% (-20C)
4:0	RESERVED	R	0x0		Reserved

6.5.19 REG0x1E_Reverse_Undervoltage_Control Register (Address = 0x1E) [Reset = 0x00]

REG0x1E_Reverse_Undervoltage_Control is shown in [Table 6-27](#).

Return to the [Summary Table](#).

Table 6-27. REG0x1E_Reverse_Undervoltage_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	RESERVED	R	0x0		Reserved
6	RESERVED	R	0x0		Reserved
5	VAC_REV	R/W	0x0	Reset by: REG_RESET	Reverse Mode System UVP: 0b = 80% of VAC_REV target 1b = Fixed at 3.3V
4	RESERVED	R	0x0		Reserved
3	RESERVED	R	0x0		Reserved
2	RESERVED	R	0x0		Reserved
1	RESERVED	R	0x0		Reserved
0	RESERVED	R	0x0		Reserved

6.5.20 REG0x1F_VAC_Max_Power_Point_Detected Register (Address = 0x1F) [Reset = 0x0000]

REG0x1F_VAC_Max_Power_Point_Detected is shown in [Table 6-28](#).

Return to the [Summary Table](#).

I2C REG0x20=[15:8], I2C REG0x1F=[7:0]

Table 6-28. REG0x1F_VAC_Max_Power_Point_Detected Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:14	RESERVED	R	0x0		Reserved
13:2	VAC_MPP	R	0x0		Input Voltage for Max Power Point detected: POR: 0mV (0h) Range: 0mV-60000mV (0h-BB8h) Clamped High Bit Step: 20mV
1:0	RESERVED	R	0x0		Reserved

6.5.21 REG0x21_Charger_Status_1 Register (Address = 0x21) [Reset = 0x00]

REG0x21_Charger_Status_1 is shown in [Table 6-29](#).

Return to the [Summary Table](#).

Table 6-29. REG0x21_Charger_Status_1 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	ADC_DONE_STAT	R	0x0		ADC conversion status (in one-shot mode only): 0b = Conversion not complete 1b = Conversion complete
6	IAC_DPM_STAT	R	0x0		Input Current regulation status: 0b = Normal 1b = In Input Current regulation (ILIM pin or IAC_DPM)
5	VAC_DPM_STAT	R	0x0		Input Voltage regulation status: 0b = Normal 1b = In Input Voltage regulation (VAC_DPM or VSYS_REV)
4	RESERVED	R	0x0		Reserved
3	WD_STAT	R	0x0		I2C Watchdog timer status: 0b = Normal 1b = WD timer expired
2:0	CHARGE_STAT	R	0x0		Charge cycle status: 000b = Not charging 001b = Trickle Charge (VBAT < VBAT_SHORT) 010b = Pre-Charge (VBAT < VBAT_LOWV) 011b = Fast Charge (CC mode) 100b = Taper Charge (CV mode) 101b = Reserved 110b = Top-off Timer Charge 111b = Charge Termination Done

6.5.22 REG0x22_Charger_Status_2 Register (Address = 0x22) [Reset = 0x00]

REG0x22_Charger_Status_2 is shown in [Table 6-30](#).

Return to the [Summary Table](#).

Table 6-30. REG0x22_Charger_Status_2 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	PG_STAT	R	0x0		Input Power Good status: 0b = Not Power Good 1b = Power Good

Table 6-30. REG0x22_Charger_Status_2 Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
6:4	TS_STAT	R	0x0		TS (Battery NTC) status: 000b = Normal 001b = TS Warm 010b = TS Cool 011b = TS Cold 100b = TS Hot
3:2	RESERVED	R	0x0		Reserved
1:0	MPPT_STAT	R	0x0		Max Power Point Tracking Algorithm status: 00b = MPPT Disabled 01b = MPPT Enabled, But Not Running 10b = Full Panel Sweep In Progress 11b = Max Power Voltage Detected

6.5.23 REG0x23_Charger_Status_3 Register (Address = 0x23) [Reset = 0x00]

REG0x23_Charger_Status_3 is shown in [Table 6-31](#).

Return to the [Summary Table](#).

Table 6-31. REG0x23_Charger_Status_3 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	RESERVED	R	0x0		Reserved
5:4	FSW_SYNC_STAT	R	0x0		FSW_SYNC pin status: 00b = Normal, no external clock detected 01b = Valid ext. clock detected 10b = Pin fault (frequency out-of-range) 11b = Reserved
3	RESERVED	R	0x0		Reserved
2	REVERSE_STAT	R	0x0		Converter Reverse Mode status: 0b = Reverse Mode off 1b = Reverse Mode On
1	RESERVED	R	0x0		Reserved
0	RESERVED	R	0x0		Reserved

6.5.24 REG0x24_Fault_Status Register (Address = 0x24) [Reset = 0x00]

REG0x24_Fault_Status is shown in [Table 6-32](#).

Return to the [Summary Table](#).

Table 6-32. REG0x24_Fault_Status Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	VAC_UV_STAT	R	0x0		Input under-voltage status: 0b = Input Normal 1b = Device in Input under-voltage protection
6	VAC_OV_STAT	R	0x0		Input over-voltage status: 0b = Input Normal 1b = Device in Input over-voltage protection
5	IBAT_OCP_STAT	R	0x0		Battery over-current status: 0b = Battery current normal 1b = Battery over-current detected

Table 6-32. REG0x24_Fault_Status Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
4	VBAT_OV_STAT	R	0x0		Battery over-voltage status: 0b = Normal 1b = Device in Battery over-voltage protection
3	TSHUT_STAT	R	0x0		Thermal shutdown status: 0b = Normal 1b = Device in thermal shutdown protection
2	CHG_TMR_STAT	R	0x0		Charge safety timer status: 0b = Normal 1b = Charge safety timer expired
1	DRV_OKZ_STAT	R	0x0	In battery-only mode with ADC disabled, this bit always reads '1'	DRV_SUP pin voltage status: 0b = Normal 1b = DRV_SUP pin voltage is out of valid range
0	RESERVED	R	0x0		Reserved

6.5.25 REG0x25_Charger_Flag_1 Register (Address = 0x25) [Reset = 0x00]

REG0x25_Charger_Flag_1 is shown in [Table 6-33](#).

Return to the [Summary Table](#).

Table 6-33. REG0x25_Charger_Flag_1 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	ADC_DONE_FLAG	R	0x0		ADC conversion INT flag (in one-shot mode only): Note: always reads 0 in continuous mode Access: R (ClearOnRead) 0b = Conversion not complete 1b = Conversion complete
6	IAC_DPM_FLAG	R	0x0		Input Current regulation INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Device entered Input Current regulation
5	VAC_DPM_FLAG	R	0x0		Input Voltage regulation INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Device entered Input Voltage regulation
4	RESERVED	R	0x0		Reserved
3	WD_FLAG	R	0x0		I2C Watchdog timer INT flag: Access: R (ClearOnRead) 0b = Normal 1b = WD_STAT rising edge detected
2	RESERVED	R	0x0		Reserved
1	RESERVED	R	0x0		Reserved
0	CHARGE_FLAG	R	0x0		Charge cycle INT flag: Access: R (ClearOnRead) 0b = Not charging 1b = CHARGE_STAT[2:0] bits changed (transition to any state)

6.5.26 REG0x26_Charger_Flag_2 Register (Address = 0x26) [Reset = 0x00]

REG0x26_Charger_Flag_2 is shown in [Table 6-34](#).

Return to the [Summary Table](#).

Table 6-34. REG0x26_Charger_Flag_2 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	PG_FLAG	R	0x0		Input Power Good INT flag: Access: R (ClearOnRead) 0b = Normal 1b = PG signal toggle detected
6	RESERVED	R	0x0		Reserved
5	RESERVED	R	0x0		Reserved
4	TS_FLAG	R	0x0		TS (Battery NTC) INT flag: Access: R (ClearOnRead) 0b = Normal 1b = TS_STAT[2:0] bits changed (transitioned to any state)
3	REVERSE_FLAG	R	0x0		Reverse Mode INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Reverse Mode toggle detected
2	RESERVED	R	0x0		Reserved
1	FSW_SYNC_FLAG	R	0x0		FSW_SYNC pin signal INT flag: Access: R (ClearOnRead) 0b = Normal 1b = FSW_SYNC status changed
0	MPPT_FLAG	R	0x0		Max Power Point Tracking INT flag: Access: R (ClearOnRead) 0b = Normal 1b = MPPT_STAT[1:0] bits changed (transitioned to any state)

6.5.27 REG0x27_Fault_Flag Register (Address = 0x27) [Reset = 0x00]

REG0x27_Fault_Flag is shown in [Table 6-35](#).

Return to the [Summary Table](#).

Table 6-35. REG0x27_Fault_Flag Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	VAC_UV_FLAG	R	0x0		Input under-voltage INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Entered input under-voltage fault
6	VAC_OV_FLAG	R	0x0		Input over-voltage INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Entered Input over-voltage fault
5	IBAT_OCP_FLAG	R	0x0		Battery over-current INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Entered Battery over-current fault
4	VBAT_OV_FLAG	R	0x0		Battery over-voltage INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Entered battery over-voltage fault

Table 6-35. REG0x27_Fault_Flag Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
3	TSHUT_FLAG	R	0x0		Thermal shutdown INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Entered TSHUT fault
2	CHG_TMR_FLAG	R	0x0		Charge safety timer INT flag: Access: R (ClearOnRead) 0b = Normal 1b = Charge Safety timer expired rising edge detected
1	DRV_OKZ_FLAG	R	0x0		DRV_SUP pin voltage INT flag: Access: R (ClearOnRead) 0b = Normal 1b = DRV_SUP pin fault detected
0	RESERVED	R	0x0		Reserved

6.5.28 REG0x28_Charger_Mask_1 Register (Address = 0x28) [Reset = 0x00]

REG0x28_Charger_Mask_1 is shown in [Table 6-36](#).

Return to the [Summary Table](#).

Table 6-36. REG0x28_Charger_Mask_1 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	ADC_DONE_MASK	R/W	0x0	Reset by: REG_RESET	ADC conversion INT mask (in one-shot mode only): 0b = ADC_DONE produces INT pulse 1b = ADC_DONE does not produce INT pulse
6	IAC_DPM_MASK	R/W	0x0	Reset by: REG_RESET	Input Current regulation INT mask: 0b = IAC_DPM_FLAG produces INT pulse 1b = IAC_DPM_FLAG does not produce INT pulse
5	VAC_DPM_MASK	R/W	0x0	Reset by: REG_RESET	Input Voltage regulation INT mask: 0b = VAC_DPM_FLAG produces INT pulse 1b = VAC_DPM_FLAG does not produce INT pulse
4	RESERVED	R	0x0		Reserved
3	WD_MASK	R/W	0x0	Reset by: REG_RESET	I2C Watchdog timer INT mask: 0b = WD expiration produces INT pulse 1b = WD expiration does not produce INT pulse
2	RESERVED	R	0x0		Reserved
1	RESERVED	R	0x0	Reset by: REG_RESET	Reserved
0	CHARGE_MASK	R/W	0x0	Reset by: REG_RESET	Charge cycle INT mask: 0b = CHARGE_STAT change produces INT pulse 1b = CHARGE_STAT change does not produces INT pulse

6.5.29 REG0x29_Charger_Mask_2 Register (Address = 0x29) [Reset = 0x00]

REG0x29_Charger_Mask_2 is shown in [Table 6-37](#).

Return to the [Summary Table](#).

Table 6-37. REG0x29_Charger_Mask_2 Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	PG_MASK	R/W	0x0	Reset by: REG_RESET	Input Power Good INT mask: 0b = PG toggle produces INT pulse 1b = PG toggle does not produce INT pulse
6	RESERVED	R	0x0		Reserved
5	RESERVED	R	0x0		Reserved
4	TS_MASK	R/W	0x0	Reset by: REG_RESET	TS (Battery NTC) INT mask: 0b = TS_STAT change produces INT pulse 1b = TS_STAT change does not produce INT pulse
3	REVERSE_MASK	R/W	0x0	Reset by: REG_RESET	Reverse Mode INT mask: 0b = REVERSE_STAT toggle produces INT pulse 1b = REVERSE_STAT toggle does no produce INT pulse
2	RESERVED	R	0x0		Reserved
1	FSW_SYNC_MASK	R/W	0x0	Reset by: REG_RESET	FSW_SYNC pin signal INT mask: 0b = FSW_SYNC status change produces INT pulse 1b = FSW_SYNC status change does not produce INT pulse
0	MPPT_MASK	R/W	0x0	Reset by: REG_RESET	Max Power Point Tracking INT mask: 0b = MPPT_STAT rising edge produces INT pulse 1b = MPPT_STAT rising edge does no produce INT pulse

6.5.30 REG0x2A_Fault_Mask Register (Address = 0x2A) [Reset = 0x00]

REG0x2A_Fault_Mask is shown in [Table 6-38](#).

Return to the [Summary Table](#).

Table 6-38. REG0x2A_Fault_Mask Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	VAC_UV_MASK	R/W	0x0	Reset by: REG_RESET	Input under-voltage INT mask: 0b = Input under-voltage event produces INT pulse 1b = Input under-voltage event does not produce INT pulse
6	VAC_OV_MASK	R/W	0x0	Reset by: REG_RESET	Input over-voltage INT mask: 0b = Input over-voltage event produces INT pulse 1b = Input over-voltage event does not produce INT pulse
5	IBAT_OCP_MASK	R/W	0x0	Reset by: REG_RESET	Battery over-current INT mask: 0b = Battery over-current event produces INT pulse 1b = Battery over-current event does not produce INT pulse
4	VBAT_OV_MASK	R/W	0x0	Reset by: REG_RESET	Battery over-voltage INT mask: 0b = Battery over-voltage event produces INT pulse 1b = Battery over-voltage event does not produce INT pulse
3	TSHUT_MASK	R/W	0x0	Reset by: REG_RESET	Thermal shutdown INT mask: 0b = TSHUT event produces INT pulse 1b = TSHUT event does not produce INT pulse

Table 6-38. REG0x2A_Fault_Mask Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
2	CHG_TMR_MASK	R/W	0x0	Reset by: REG_RESET	Charge safety timer INT mask: 0b = Timer expired rising edge produces INT pulse 1b = Timer expired rising edge does not produce INT pulse
1	DRV_OKZ_MASK	R/W	0x0	Reset by: REG_RESET	DRV_SUP pin voltage INT mask: 0b = DRV_SUP pin fault produces INT pulse 1b = DRV_SUP pin fault does not produce INT pulse
0	RESERVED	R	0x0		Reserved

6.5.31 REG0x2B_ADC_Control Register (Address = 0x2B) [Reset = 0x60]

REG0x2B_ADC_Control is shown in [Table 6-39](#).

Return to the [Summary Table](#).

Table 6-39. REG0x2B_ADC_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	ADC_EN	R/W	0x0	Reset by: REG_RESET WATCHDOG	ADC control: 0b = Disable ADC 1b = Enable ADC
6	ADC_RATE	R/W	0x1	Reset by: REG_RESET	ADC conversion rate control: 0b = Continuous conversion 1b = One-shot conversion
5:4	ADC_SAMPLE	R/W	0x2	Reset by: REG_RESET	ADC sample speed: 00b = 15 bit effective resolution 01b = 14 bit effective resolution 10b = 13 bit effective resolution 11b = Reserved
3	ADC_AVG	R/W	0x0	Reset by: REG_RESET	ADC average control: 0b = Single value 1b = Running average
2	ADC_AVG_INIT	R/W	0x0	Reset by: REG_RESET	ADC average initial value control: 0b = Start average using existing register value 1b = Start average using new ADC conversion
1:0	RESERVED	R	0x0		Reserved

6.5.32 REG0x2C_ADC_Channel_Control Register (Address = 0x2C) [Reset = 0x0A]

REG0x2C_ADC_Channel_Control is shown in [Table 6-40](#).

Return to the [Summary Table](#).

Table 6-40. REG0x2C_ADC_Channel_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	IAC_ADC_DIS	R/W	0x0	Reset by: REG_RESET	IAC ADC control 0b = Enable 1b = Disable
6	IBAT_ADC_DIS	R/W	0x0	Recommend to disable IBAT ADC channel when EN_IBAT_LOAD bit is 1 Reset by: REG_RESET	IBAT ADC control 0b = Enable 1b = Disable

Table 6-40. REG0x2C_ADC_Channel_Control Register Field Descriptions (continued)

Bit	Field	Type	Reset	Notes	Description
5	VAC_ADC_DIS	R/W	0x0	Reset by: REG_RESET	VAC ADC control 0b = Enable 1b = Disable
4	VBAT_ADC_DIS	R/W	0x0	Reset by: REG_RESET	VBAT ADC control 0b = Enable 1b = Disable
3	RESERVED	R	0x1		Reserved
2	TS_ADC_DIS	R/W	0x0	Reset by: REG_RESET	TS ADC control 0b = Enable 1b = Disable
1	VFB_ADC_DIS	R/W	0x1	Reset by: REG_RESET	VFB ADC control Recommend to disable this channel when charging is enabled 0b = Enable 1b = Disable
0	RESERVED	R	0x0		Reserved

6.5.33 REG0x2D_IAC_ADC Register (Address = 0x2D) [Reset = 0x0000]

REG0x2D_IAC_ADC is shown in [Table 6-41](#).

Return to the [Summary Table](#).

I2C REG0x2E=[15:8], I2C REG0x2D=[7:0]

Table 6-41. REG0x2D_IAC_ADC Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:0	IAC_ADC	R	0x0		IAC ADC reading with 5mΩ RAC_SNS: Reported as 2s complement POR: 0mA(0h) Format: 2s Complement Range: -20000mA - 20000mA (9E58h-61A8h) Clamped Low Clamped High Bit Step: 0.8mA

6.5.34 REG0x2F_IBAT_ADC Register (Address = 0x2F) [Reset = 0x0000]

REG0x2F_IBAT_ADC is shown in [Table 6-42](#).

Return to the [Summary Table](#).

I2C REG0x30=[15:8], I2C REG0x2F=[7:0]

Table 6-42. REG0x2F_IBAT_ADC Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:0	IBAT_ADC	R	0x0		IBAT ADC reading with 5mΩ RBAT_SNS: Reported as 2s complement POR: 0mA (0h) Format: 2s Complement Range: -20000mA-20000mA (D8F0h-2710h) Clamped Low Clamped High Bit Step: 2mA

6.5.35 REG0x31_VAC_ADC Register (Address = 0x31) [Reset = 0x0000]

REG0x31_VAC_ADC is shown in [Table 6-43](#).

Return to the [Summary Table](#).

I2C REG0x32=[15:8], I2C REG0x31=[7:0]

Table 6-43. REG0x31_VAC_ADC Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:0	VAC_ADC	R	0x0		VAC ADC reading: Reported as unsigned integer POR: 0mV (0h) Format: 2s Complement Range: 0mV-65534mV (0h-7FFFh) Clamped Low Bit Step: 2mV

6.5.36 REG0x33_VBAT_ADC Register (Address = 0x33) [Reset = 0x0000]

REG0x33_VBAT_ADC is shown in [Table 6-44](#).

Return to the [Summary Table](#).

I2C REG0x34=[15:8], I2C REG0x33=[7:0]

Table 6-44. REG0x33_VBAT_ADC Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:0	VBAT_ADC	R	0x0		VBAT ADC reading: Reported as unsigned integer POR: 0mV (0h) Format: 2s Complement Range: 0mV-65534mV (0h-7FFFh) Clamped Low Bit Step: 2mV

6.5.37 REG0x37_TS_ADC Register (Address = 0x37) [Reset = 0x0000]

REG0x37_TS_ADC is shown in [Table 6-45](#).

Return to the [Summary Table](#).

I2C REG0x38=[15:8], I2C REG0x37=[7:0]

Table 6-45. REG0x37_TS_ADC Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:0	TS_ADC	R	0x0		TS ADC reading as percentage of REGN: Reported as unsigned integer POR: 0%(0h) Range: 0% - 99.90234375% (0h-3FFh) Clamped High Bit Step: 0.09765625%

6.5.38 REG0x39_VFB_ADC Register (Address = 0x39) [Reset = 0x0000]

REG0x39_VFB_ADC is shown in [Table 6-46](#).

Return to the [Summary Table](#).

I2C REG0x3A=[15:8], I2C REG0x39=[7:0]

Table 6-46. REG0x39_VFB_ADC Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
15:0	VFB_ADC	R	0x0		VFB ADC reading: POR: 0mV (0h) Range: 0mV-2047mV (0h-7FFh) Clamped High Bit Step: 1mV

6.5.39 REG0x3B_Gate_Driver_Strength_Control Register (Address = 0x3B) [Reset = 0x00]

REG0x3B_Gate_Driver_Strength_Control is shown in [Table 6-47](#).

Return to the [Summary Table](#).

Table 6-47. REG0x3B_Gate_Driver_Strength_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	BOOST_HS_DRV	R/W	0x0	Reset by: REG_RESET	Boost High Side FET Gate Driver Strength: 00b = Fastest 01b = Faster 10b = Slower 11b = Slowest
5:4	BUCK_HS_DRV	R/W	0x0	Reset by: REG_RESET	Buck High Side FET Gate Driver Strength: 00b = Fastest 01b = Faster 10b = Slower 11b = Slowest
3:2	BOOST_LS_DRV	R/W	0x0	Reset by: REG_RESET	Boost Low Side FET Gate Driver Strength: 00b = Fastest 01b = Faster 10b = Slower 11b = Slowest
1:0	BUCK_LS_DRV	R/W	0x0	Reset by: REG_RESET	Buck Low Side FET Gate Driver Strength: 00b = Fastest 01b = Faster 10b = Slower 11b = Slowest

6.5.40 REG0x3C_Gate_Driver_Dead_Time_Control Register (Address = 0x3C) [Reset = 0x00]

REG0x3C_Gate_Driver_Dead_Time_Control is shown in [Table 6-48](#).

Return to the [Summary Table](#).

Table 6-48. REG0x3C_Gate_Driver_Dead_Time_Control Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:4	RESERVED	R	0x0		Reserved
3:2	BOOST_DEAD_TIME	R/W	0x0	Reset by: REG_RESET	Boost Side FETs Dead Time Control: 00b = 45ns 01b = 75ns 10b = 105ns 11b = 135ns
1:0	BUCK_DEAD_TIME	R/W	0x0	Reset by: REG_RESET	Buck Side FETs Dead Time Control: 00b = 45ns 01b = 75ns 10b = 105ns 11b = 135ns

6.5.41 REG0x3D_Part_Information Register (Address = 0x3D) [Reset = 0x12]

REG0x3D_Part_Information is shown in [Table 6-49](#).

Return to the [Summary Table](#).

Table 6-49. REG0x3D_Part_Information Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7	RESERVED	R	0x0		Reserved
6:3	PART_NUM	R	0x2		Part Number: 010 - BQ25756
2:0	DEV_REV	R	0x2		Device Revision:

6.5.42 REG0x62_Reverse_Mode_Battery_Discharge_Current Register (Address = 0x62) [Reset = 0x02]

REG0x62_Reverse_Mode_Battery_Discharge_Current is shown in [Table 6-50](#).

Return to the [Summary Table](#).

Table 6-50. REG0x62_Reverse_Mode_Battery_Discharge_Current Register Field Descriptions

Bit	Field	Type	Reset	Notes	Description
7:6	IBAT_REV	R/W	0x0	Reset by: REG_RESET	Reverse mode battery discharge current limit: 00b = 20A 01b = 15A 10b = 10A 11b = 5A
5:2	RESERVED	R	0x0		Reserved
1	EN_CONV_FAST_TRANSIENT	R/W	0x1	Reset by: REG_RESET	Enable converter fast transient response in reverse mode only - 0b = Disable 1b = Enable
0	RESERVED	R	0x0		Reserved

7 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

7.1 Application Information

7.2 Typical Applications

7.2.1 Typical Application

The device can be configured as a solar charger using the MPPT Control Register (REG1A). When the input source falls outside the VAC operating window programmed through ACUV and ACOV, the device automatically stops switching. Figure 7-1 shows a typical schematic when using the device as a solar charging from either single 18V panel or two panels in series up-to 36Vin. The charging parameters and MPPT search window are programmed via the I²C registers.

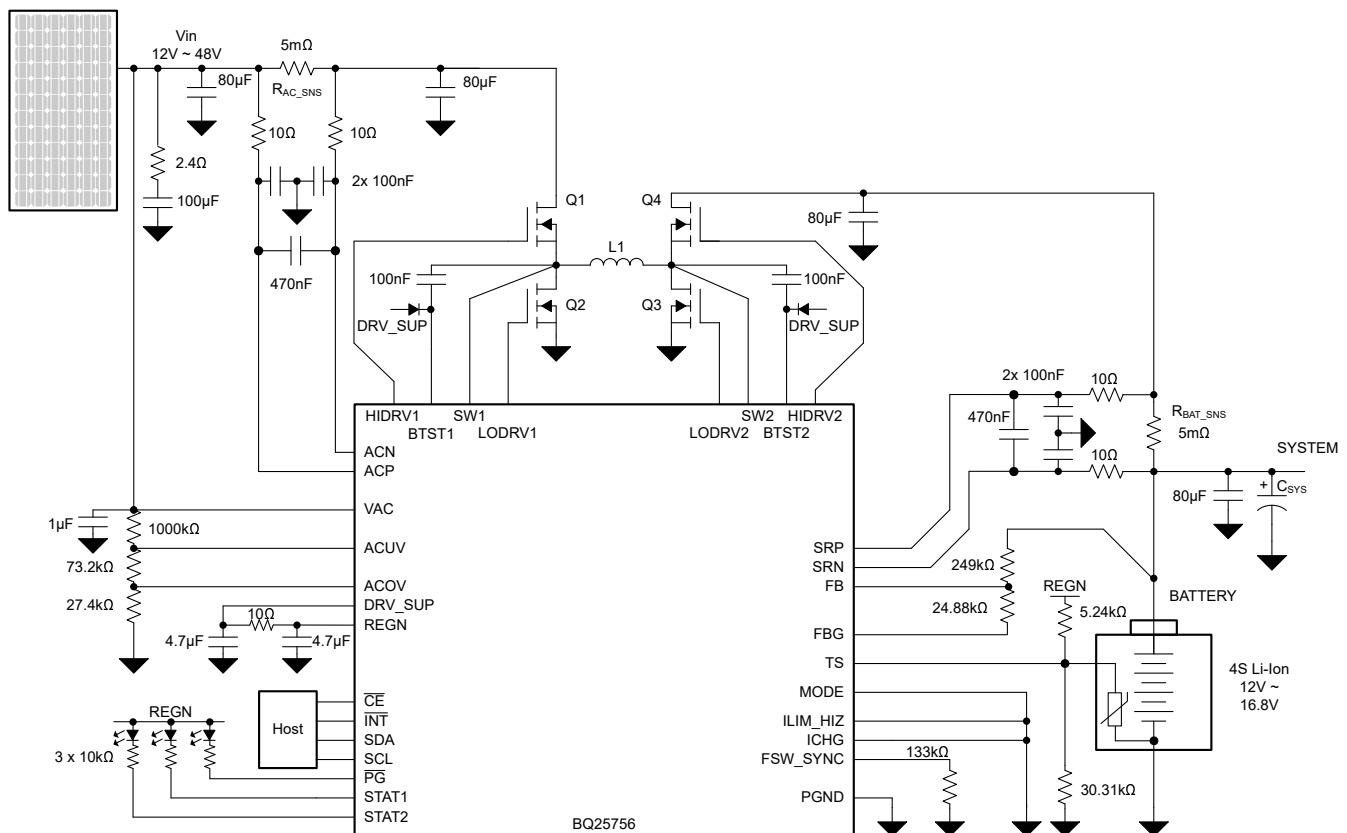


Figure 7-1. BQ25756: Solar Charging with Autonomous MPPT Algorithm to Charge 4s Battery with Maximum 15A Charge Current

Table 7-1. Recommended Part Numbers:

COMPONENT	VALUE	RECOMMENDED PART NUMBER
Q1, Q2, Q3, Q4	60V, 3.1mΩ	AONS66614
L1	10μH, 12mΩ	IHLP6767GZ-01

7.2.1.1 Design Requirements

For this design example, use the parameters shown in the table below.

Table 7-2. Design Parameters

PARAMETER	VALUE
Input voltage operating range (V_{AC})	12V to 48V
Input current limit (I_{AC})	Optimal current determined by MPPT
Output current limit (I_{OUT})	15A
Battery charge voltage (V_{BAT_REG})	17.4V
Switching frequency	250kHz

7.2.1.2 Detailed Design Procedure

7.2.1.2.1 ACUV / ACOV Input Voltage Operating Window Programming

The input voltage operating window is programmed by an ACUV / ACOV window with a resistor divider from V_{AC} to GND. The top resistor, R_{AC1} , is typically selected as 1,000k Ω to minimize the input voltage leakage current. Assuming the desired trip-points for under-voltage and over-voltage protection are labeled V_{VACUV} and V_{VACOV} , the resistor divider required can be calculated as follows. The internal reference for the over-voltage threshold (V_{REF_ACOV}) is 1.2V. The internal reference for the under-voltage threshold (V_{REF_ACUV}) is 1.1V.

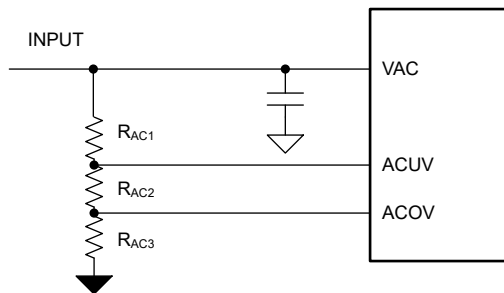


Figure 7-2. ACUV and ACOV Resistor Divider

$$V_{VACOV} = \frac{1.2V(1,000k\Omega + R_{AC2} + R_{AC3})}{R_{AC3}} \quad (8)$$

$$V_{VACUV} = \frac{1.1V(1,000k\Omega + R_{AC2} + R_{AC3})}{R_{AC2} + R_{AC3}} \quad (9)$$

For the default device operating window of 4.4V to 60V, the ACUV can be pulled up directly to V_{AC} , while the ACOV can be pulled directly to GND.

7.2.1.2.2 Charge Voltage Selection

The battery regulation voltage is programmed using a resistor divider to the FB pin. The default internal voltage reference is 1.536V, and can be changed via the V_{FB_REG} register bits. The top of the resistor divider is selected to be 249 k Ω .

$$R_{TOP} = 249 \text{ k}\Omega$$

The bottom resistor can be calculated as:

$$R_{BOT} = R_{TOP} \times \frac{V_{FB}}{V_{BATREG} - V_{FB}} - R_{FBG} \quad (10)$$

where

- V_{FB} is the target feedback voltage programmed through I²C (default 1.536 V),

- V_{BATREG} is the desired battery regulation target (16.8 V in this example)
- R_{FBG} is the internal FBG pull-down resistor (33 Ω)

$$R_{FB_BOT} = 25.09 \text{ k}\Omega.$$

Choosing the nearest 0.1% resistor value, gives $R_{FB_BOT} = 24.88 \text{ k}\Omega$, for a nominal charge voltage of 16.89 V. Further fine-tuning of the regulation voltage can be achieved by changing the internal feedback reference. For example, to get the regulation voltage to exactly 16.8 V with the selected resistor divider, the internal voltage reference could be changed to 1.528 V via V_{FB_REG} .

It is recommended to use 0.1% accurate resistors to maximize the charge voltage accuracy.

7.2.1.2.3 Switching Frequency Selection

The switching frequency is set by a resistor connected from the FSW_SYNC pin to PGND. The RFSW resistor required to set the desired frequency is calculated using [Equation 3](#) or [Table 6-2](#). A 1% standard resistor of 133k Ω is selected to set $f_{SW} = 250\text{kHz}$.

7.2.1.2.4 Inductor Selection

Higher switching frequency allows the use of smaller inductor and capacitor values. Inductor saturation current must be higher than the inductor current (I_L) plus half the ripple current (I_{RIPPLE}):

$$I_{SAT} \geq I_L + \frac{1}{2}I_{RIPPLE} \quad (11)$$

The inductor ripple current in buck operation depends on input voltage (V_{AC}), duty cycle ($D_{BUCK} = V_{BAT}/V_{AC}$), switching frequency (f_{SW}) and inductance (L):

$$I_{RIPPLE_BUCK} = \frac{V_{AC} \times D_{BUCK} \times (1 - D_{BUCK})}{f_{SW} \times L} \quad (12)$$

The maximum inductor ripple current happens with $D = 0.5$ or close to 0.5. Ripple calculations must be analyzed for both forward and reverse operating modes if applicable.

Usually inductor ripple is designed in the range of (20 – 40%) maximum inductor current (in either forward or reverse mode) as a trade-off between inductor size and efficiency for a practical design. For system stability, the inductor's time constant must be between 0.05 $\mu\text{H}/\text{m}\Omega$ and 1.26 $\mu\text{H}/\text{m}\Omega$.

7.2.1.2.5 Input (VAC) Capacitor

Input capacitor should have enough ripple current rating to absorb input switching ripple current. The worst case RMS ripple current is half of the output when duty cycle is 0.5 in forward buck mode, or reverse boost mode. If the converter does not operate at 50% duty cycle, then the worst case capacitor RMS current occurs where the duty cycle is closest to 50% and can be estimated by [Equation 13](#):

$$I_{CIN} = I_{CHG} \times \sqrt{D \times (1 - D)} \quad (13)$$

A combination of ceramic and bulk capacitors must be used to provide a short path for high di/dt current and to reduce the voltage ripple. Ceramic capacitors must be placed close to the switching half-bridge. Given total bulk input capacitance, it is recommended to distribute equally on either side of R_{AC_SNS} . The complete schematic is a good starting point for input capacitor for typical applications.

7.2.1.2.6 Output (VBAT) Capacitor

The output capacitor conducts high ripple current. The output capacitor RMS ripple current is given by where the minimum VAC corresponds to the maximum capacitor current.

$$I_{CBAT} = I_{BAT} \sqrt{\frac{V_{BAT}}{V_{AC}} - 1} \quad (14)$$

A 5mΩ output capacitor ESR causes an output voltage ripple of 74mV as given by:

$$\Delta V_{RIPPLE(ESR)} = I_{BAT} \times \frac{V_{BAT}}{V_{AC,min}} \times ESR \quad (15)$$

A 140μF output capacitor causes a capacitive ripple voltage of 66mV as given by:

$$\Delta V_{RIPPLE(CBAT)} = I_{BAT} \times \frac{\left(1 - \frac{V_{AC,min}}{V_{BAT}}\right)}{C_{BAT} \times f_{SW}} \quad (16)$$

A combination of ceramic and bulk capacitors must be used to provide low ESR and high ripple current capacity. Ceramic capacitors must be placed close to the switching half-bridge. Given total bulk output capacitance, it is recommended to distribute equally on either side of R_{BAT_SNS}. The complete schematic is a good starting point for C_{BAT} for typical applications.

7.2.1.2.7 Sense Resistor (R_{AC_SNS} and R_{BAT_SNS}) and Current Programming

The battery current sense resistor between SRP and SRN is fixed at 5mΩ; using a different value is not recommended. The input current sense resistor between ACP and ACN is typically 2mΩ, but can be changed to 5mΩ. In USB-PD applications, a 5mΩ sense resistor is recommended to achieve programmability in 50mA/step whereas for power-path applications, a 2mΩ sense resistor is preferred. In addition, if input current limit function is not desired, ACP and ACN can be shorted together. For both of these sense resistors, a filter network is recommended as shown in the Typical Application.

For both the input current and the output current, the limits may be programmed using the I²C interface or an external programming resistor on ILIM_HIZ and ICHG pins, respectively.

Table 7-3. Sense Resistor and Current Programming

PARAMETER	FORMULA	VALUE
Input Current Hardware Limit	Unused	Pull ILIM_HIZ pin to GND
Input Current Software Limit	Unused, set by MPPT	REG06 = 0x0640 (20A with 5mΩ R _{AC_SNS})
Output Current Hardware Limit	Unused	Pull ICHG pin to GND
Output Current Software Limit	ICHG = 15A	REG02 = 0x04B0(15A)

The default input sense resistor (R_{AC_SNS}) is 2mΩ, and the register allows for a range of up-to 50A input current limit. If a 5mΩ R_{AC_SNS} is used, and the register is programmed to a value of 0x60, the true maximum current across the R_{AC_SNS} will be: 50A * 2/5 = 20A. With a 5mΩ R_{AC_SNS} resistor, a 6A current limit would be achieved as: R_{ILIM} = K_{ILIM} * (2/5) / 6A = 3.3kΩ.

7.2.1.2.8 Power MOSFETs Selection

External N-channel MOSFETs are used for a synchronous switching buck battery charger. The gate drivers are integrated into the IC with 5V of gate drive voltage. An external gate drive voltage can be provided directly into the DRV_SUP pin for increased efficiency.

Figure-of-merit (FOM) is usually used for selecting proper MOSFET based on a tradeoff between the conduction loss and switching loss. For the top side MOSFET, FOM is defined as the product of a MOSFET's on-resistance, R_{DS(ON)}, and the gate-to-drain charge, Q_{GD}. For the bottom side MOSFET, FOM is defined as the product of the MOSFET's on-resistance, R_{DS(ON)}, and the total gate charge, Q_G.

$$FOM_{top} = R_{DS(on)} \cdot Q_{GD}; FOM_{bottom} = R_{DS(on)} \cdot Q_G \quad (17)$$

The lower the FOM value, the lower the total power loss. Usually lower R_{DS(ON)} has higher cost with the same package size.

The top-side MOSFET loss includes conduction loss and switching loss. Taking buck mode operation as an example the power loss is a function of duty cycle ($D=V_{OUT}/V_{IN}$), charging current (I_{CHG}), MOSFET's on-resistance ($R_{DS(on)_{top}}$), input voltage (V_{IN}), switching frequency (f_S), turn-on time (t_{on}) and turn-off time (t_{off}):

$$P_{top} = P_{con_top} + P_{sw_top} \quad (18)$$

$$P_{con_top} = D \cdot I_{L_RMS}^2 \cdot R_{DS(on)_{top}} \quad (19)$$

$$I_{L_RMS}^2 = I_{L_DC}^2 + I_{ripple}^2 / 12 \quad (20)$$

- I_{L_DC} is the average inductor DC current;
- I_{ripple} is the inductor current ripple peak-to-peak value;

$$P_{sw_top} = P_{IV_top} + P_{Qoss_top} + P_{Gate_top} \quad (21)$$

The first item P_{con_top} represents the conduction loss which is straight forward. The second term P_{sw_top} represents the multiple switching loss items in top MOSFET including voltage and current overlap losses (P_{IV_top}), MOSFET parasitic output capacitance loss (P_{Qoss_top}) and gate drive loss (P_{Gate_top}). To calculate voltage and current overlap losses (P_{IV_top}):

$$P_{IV_top} = 0.5 \times V_{IN} \cdot I_{valley} \cdot t_{on} \cdot f_S + 0.5 \times V_{IN} \cdot I_{peak} \cdot t_{off} \cdot f_S \quad (22)$$

$$I_{valley} = I_{L_DC} - 0.5 \cdot I_{ripple} \text{ (inductor current valley value);} \quad (23)$$

$$I_{peak} = I_{L_DC} + 0.5 \cdot I_{ripple} \text{ (inductor current peak value);} \quad (24)$$

- t_{on} is the MOSFET turn-on time that V_{DS} falling time from V_{IN} to almost zero (MOSFET turn on conduction voltage);
- t_{off} is the MOSFET turn-off time that I_{DS} falling time from I_{peak} to zero;

The MOSFET turn-on and turn-off times are given by:

$$t_{on} = \frac{Q_{SW}}{I_{on}}, \quad t_{off} = \frac{Q_{SW}}{I_{off}} \quad (25)$$

where Q_{SW} is the switching charge, I_{on} is the turn-on gate driving current, and I_{off} is the turn-off gate driving current. If the switching charge is not given in MOSFET datasheet, it can be estimated by gate-to-drain charge (Q_{GD}) and gate-to-source charge (Q_{GS}):

$$Q_{sw} = Q_{GD} + Q_{GS} \quad (26)$$

Gate driving current can be estimated by REGN voltage (V_{REGN}), MOSFET plateau voltage (V_{plt}), total turn-on gate resistance (R_{on}), and turn-off gate resistance (R_{off}) of the gate driver:

$$I_{on} = \frac{V_{REGN} - V_{plt}}{R_{on}}, \quad I_{off} = \frac{V_{plt}}{R_{off}} \quad (27)$$

To calculate top MOSFET parasitic output capacitance loss (P_{Qoss_top}):

$$P_{Qoss_top} = 0.5 \cdot V_{IN} \cdot Q_{oss} \cdot f_S \quad (28)$$

- Q_{oss} is the MOSFET parasitic output charge which can be found in MOSFET datasheet. It is recommended to limit the total switch node capacitance C_{SW} (nF) $< 160/V_{IN}$; for example, for a 60V application, it is recommended to keep the total $C_{SW} < 2.67$ nF

To calculate top MOSFET gate drive loss (P_{Gate_top}):

$$P_{\text{Gate_top}} = V_{\text{IN}} \cdot Q_{\text{Gate_top}} \cdot f_s \quad (29)$$

- $Q_{\text{Gate_top}}$ is the top MOSFET gate charge which can be found in MOSFET datasheet;
- Note here V_{IN} is used instead of real gate drive voltage because the gate drive is generated based on LDO from V_{IN} , the total gate drive related loss are all considered when V_{IN} is used for gate drive loss calculation.
- Alternatively, gate drive voltage can be supplied directly by external high efficiency supply into the DRV_SUP pin. In this case, the power loss to drive the gates becomes: $P_{\text{Gate_top}} = V_{\text{DRV_SUP}} \cdot Q_{\text{Gate_top}} \cdot f_s$

The bottom-side MOSFET loss also includes conduction loss and switching loss:

$$P_{\text{bottom}} = P_{\text{con_bottom}} + P_{\text{sw_bottom}} \quad (30)$$

$$P_{\text{con_bottom}} = (1 - D) \cdot I_{\text{L_RMS}}^2 \cdot R_{\text{DS(on)_bottom}} \quad (31)$$

$$P_{\text{sw_bottom}} = P_{\text{RR_bottom}} + P_{\text{Dead_bottom}} + P_{\text{Gate_bottom}} \quad (32)$$

The first item $P_{\text{con_bottom}}$ represents the conduction loss which is straight forward. The second term $P_{\text{sw_bottom}}$ represents the multiple switching loss items in bottom MOSFET including reverse recovery losses ($P_{\text{RR_bottom}}$), Dead time body diode conduction loss ($P_{\text{Dead_bottom}}$) and gate drive loss ($P_{\text{Gate_bottom}}$). The detail calculation can be found below:

$$P_{\text{RR_bottom}} = V_{\text{IN}} \cdot Q_{\text{rr}} \cdot f_s \quad (33)$$

- Q_{rr} is the bottom MOSFET reverse recovery charge which can be found in MOSFET data sheet;

$$P_{\text{Dead_bottom}} = V_F \cdot I_{\text{valley}} \cdot f_s \cdot t_{\text{dead_rise}} + V_F \cdot I_{\text{peak}} \cdot f_s \cdot t_{\text{dead_fall}} \quad (34)$$

- V_F is the body diode forward conduction voltage drop;
- $t_{\text{dead_rise}}$ is the SW rising edge deadtime between top and bottom MOSFETs which is around 45ns;
- $t_{\text{dead_fall}}$ is the SW falling edge deadtime between top and bottom MOSFETs which is around 45ns;

$P_{\text{Gate_bottom}}$ can follow the same method as top MOSFET gate drive loss calculation approach.

7.2.1.2.9 Converter Fast Transient Response

The device integrates all the loop compensation, thereby providing a high density solution with ease of use. For faster a transient response, the EN_CONV_FAST_TRANSIENT bit can be set to 1. If device is not used in boost mode operation, this section can be disregarded.

When the converter is operating in boost mode, the non-continuous inductor current flow to the load results in a right-half plane (RHP) zero. The RHP zero location is:

$$RHPz = \frac{V_{\text{IN,boost}}}{I_{\text{IN,boost}}} \frac{1}{2\pi L} \quad (35)$$

For good phase margin, the unity gain bandwidth (UGBW) of the converter must be about 1/3 of the RHPz. The boost output capacitor (C_{load}), and the converter transient parameters (R_1 , gm_1) need to be scaled to move the location of the UGBW of the converter.

$$1 \approx \frac{A_{\text{div}} \times gm_1 (sR_1 C_1 + 1)}{sC_1} \left[\frac{V_i}{I_o \times 50m} \right] \left[\frac{1}{1 + s \frac{C_{\text{load}} R_{\text{load}}}{2}} \right] \quad (36)$$

The device adjusts A_{div} , gm_1 and R_1 based on the output voltage and the EN_CONV_FAST_TRANSIENT bit setting per the table below. During some boost case scenarios, the C_{load} needs to be adjusted to limit the converter bandwidth.

Table 7-4. Converter Fast Transient Response

BOOST OUTPUT VOLTAGE	<i>A_{div}</i>	<i>C₁</i>	EN_CONV_FAST_TRANSIENT = 0		EN_CONV_FAST_TRANSIENT = 1	
			<i>gm₁</i>	<i>R₁</i>	<i>gm₁</i>	<i>R₁</i>
≤8V	1/5	75pF	0.4μ	600kΩ	2μ	1.3MΩ
8V to 16V	1/10	75pF	0.47μ	1MΩ	2μ	1.8MΩ
16V to 32V	1/20	75pF	0.67μ	2.8MΩ	2μ	2.8MΩ
>32V	1/40	75pF	2μ	2.8MΩ	2μ	2.8MΩ

As an example, assume the device operates in reverse boost mode from a 5V supply to provide a 7V boost output voltage with load up-to 5A and 10μH inductor. The RHPz is approximately located at:

$$RHPz = \frac{V_{IN,boost}}{I_{IN,boost}} \frac{1}{2\pi L} = 11.4kHz \quad (37)$$

For best stability, the UGBW of the converter must be limited to 1/3 of the RHP zero, or 3.8kHz. If EN_CONV_FAST_TRANSIENT = 1, the equation becomes:

$$1 \approx \frac{0.2 \times 2\mu (j\omega \times 1.3M\Omega \times 75pF + 1)}{j\omega \times 75pF} \left[\frac{5V}{5A \times 50m} \right] \left[\frac{1}{1 + j\omega \frac{C_{load} \times 1.4}{2}} \right] \quad (38)$$

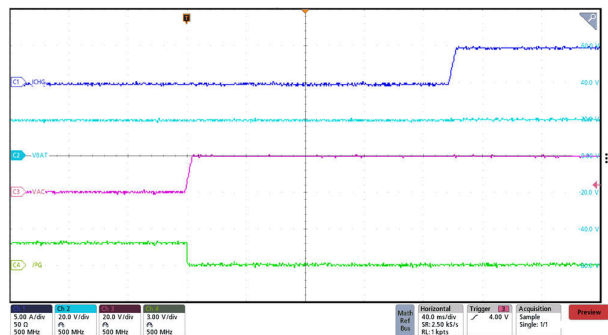
Solving the above for *C_{load}* gives ≥674μF capacitor requirement.

Conversely, if EN_CONV_FAST_TRANSIENT = 0, the UGBW equation becomes:

$$1 \approx \frac{0.2 \times 0.4\mu (j\omega \times 0.6M\Omega \times 75pF + 1)}{j\omega \times 75pF} \left[\frac{5V}{5A \times 50m} \right] \left[\frac{1}{1 + j\omega \frac{C_{load} \times 1.4}{2}} \right] \quad (39)$$

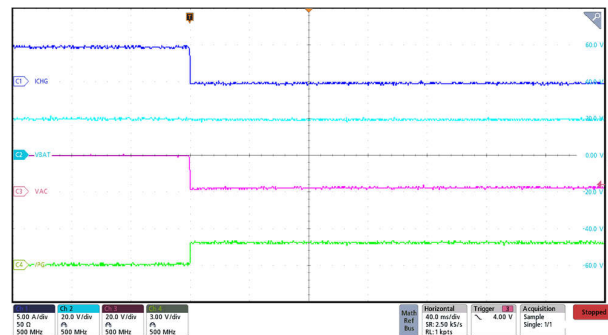
Solving the above for *C_{load}* gives ≥51μF capacitor requirement. However, the minimum recommended capacitor for converter stability is 80μF, so this minimum value must be used.

7.2.1.3 Application Curves

$$C_{VAC} = 160\mu F, C_{OUT} = 160\mu F$$


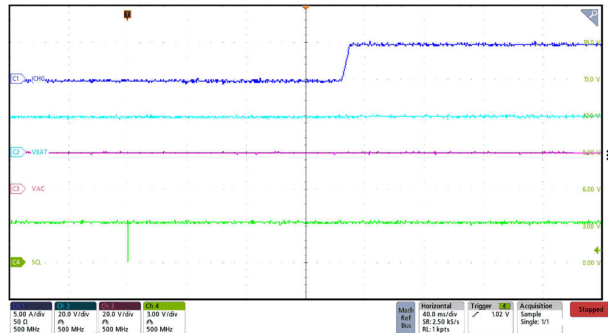
VAC = 20V VBAT = 20V ICHG = 5A

Figure 7-3. VAC Plug-In Power Up with 5A ICHG



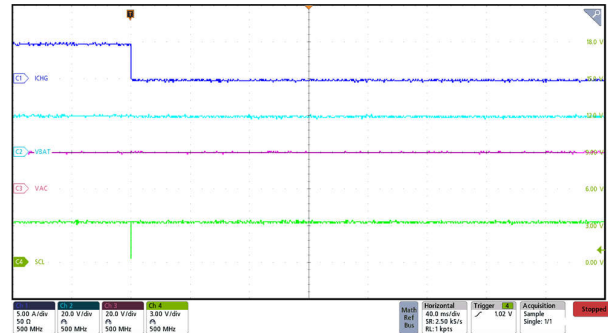
VAC = 20V → 0V VBAT = 20V ICHG = 5A

Figure 7-4. VAC Un-plug Power Down with 5A ICHG



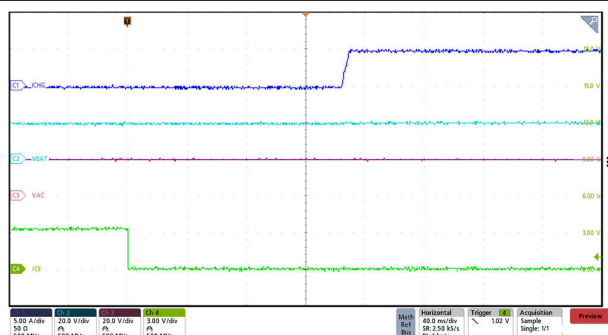
VAC = 20V VBAT = 24V ICHG = 5A

Figure 7-5. Charge Enable via I²C with 5A ICHG



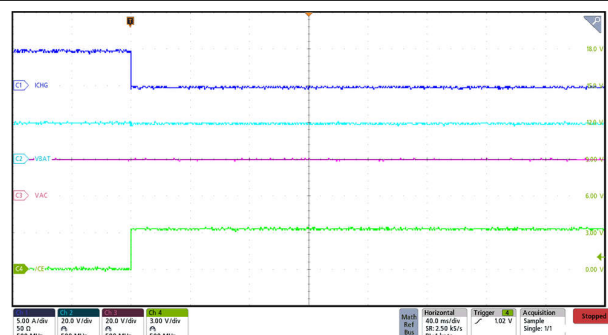
VAC = 20V VBAT = 24V ICHG = 5A

Figure 7-6. Charge Disable via I²C with 5A ICHG



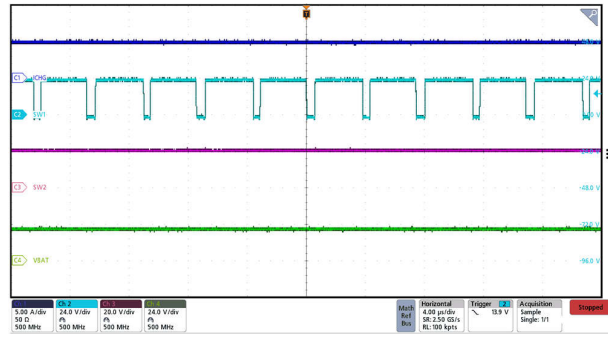
VAC = 20V VBAT = 24V ICHG = 5A

Figure 7-7. Charge Enable via $\overline{\text{CE}}$ Pin with 5A ICHG



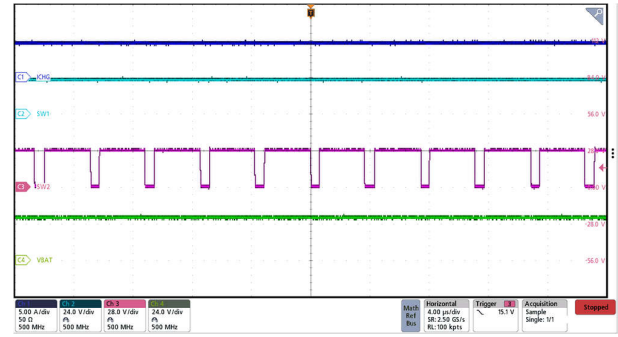
VAC = 20V VBAT = 24V ICHG = 5A

Figure 7-8. Charge Disable via $\overline{\text{CE}}$ Pin with 5A ICHG



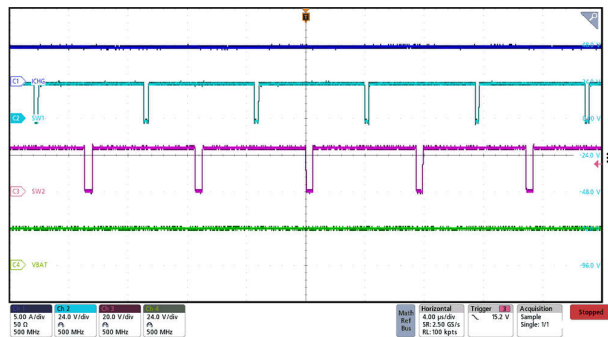
VAC = 24V VBAT = 20V ICHG = 5A

Figure 7-9. Buck Switching Waveform



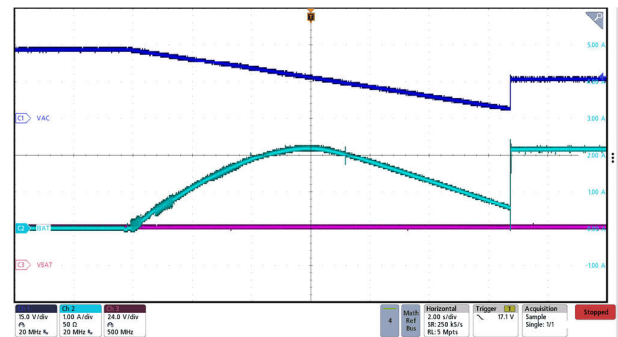
VAC = 24V VOUT = 28V ICHG = 5A

Figure 7-10. Boost Switching Waveform



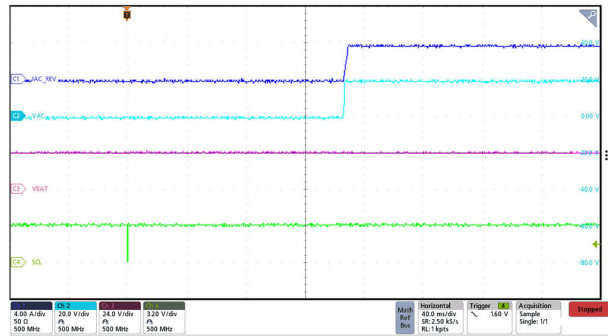
VAC = 24V VBAT = 24V ICHG = 5A

Figure 7-11. Buck-Boost Switching Waveform



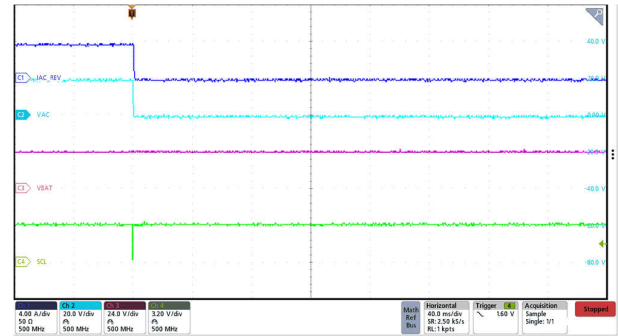
V_{OC} = 30V VBAT = 24V EN_CHG = 0 → 1
I_{SC} = 3.5A

Figure 7-12. Max Power Point Tracking (MPPT) Full Panel Sweep



VBAT = 24V VAC_REV = 20V ILOAD = 4A

Figure 7-13. Reverse Mode Power Up with 4A Load



VBAT = 24V VAC_REV = 20V ILOAD = 4A

Figure 7-14. Reverse Mode Power Down with 4A Load

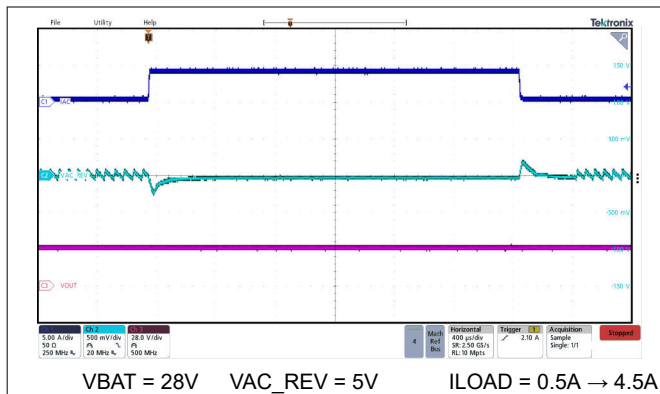


Figure 7-15. Reverse Mode Buck Transient Response

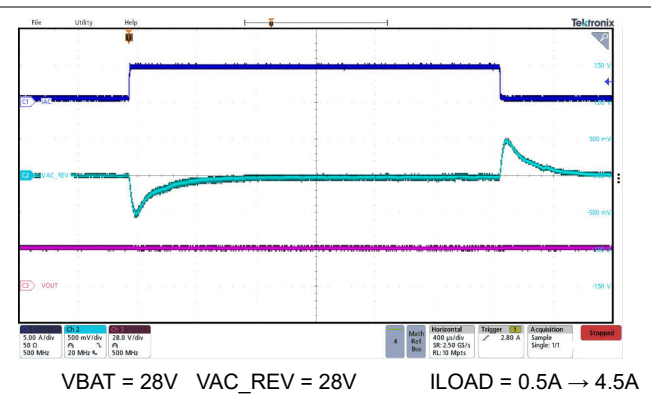


Figure 7-16. Reverse Mode Buck-Boost Transient Response

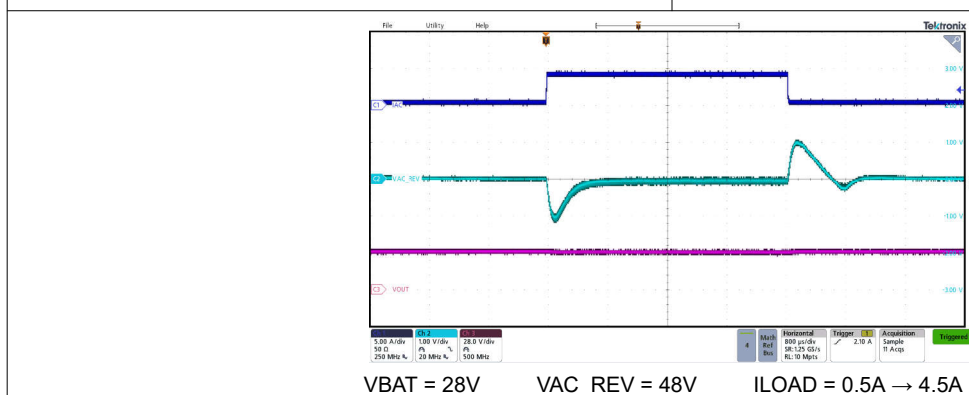


Figure 7-17. Reverse Mode Boost Transient Response

7.2.2 Typical Application (USB-PD EPR Configuration)

The device can be configured as a bidirectional buck-boost charger for USB-PD EPR charging applications. In this mode, the device can charge the battery from USB power and provide power back to the port when not charging. An optional gate drive voltage can be provided using the DRV_SUP pin to reduce switching losses. [Figure 7-18](#) shows a typical schematic when using the device as a buck-boost charger for 10-cell Li-ion battery with USB-PD EPR input and bidirectional output for 240W applications. The TPS26750 device communicates with the USB port, and controls the BQ25756 via I²C to charge with only the available power. In reverse mode, the TPS26750 negotiates with downstream device for the power profile, and controls the BQ25756 via I²C to provide the correct voltage and current to the USB port. The TPS2663x eFUSE can isolate the VBUS port from the BQ25756 input port when a fault is detected or the power source is removed.

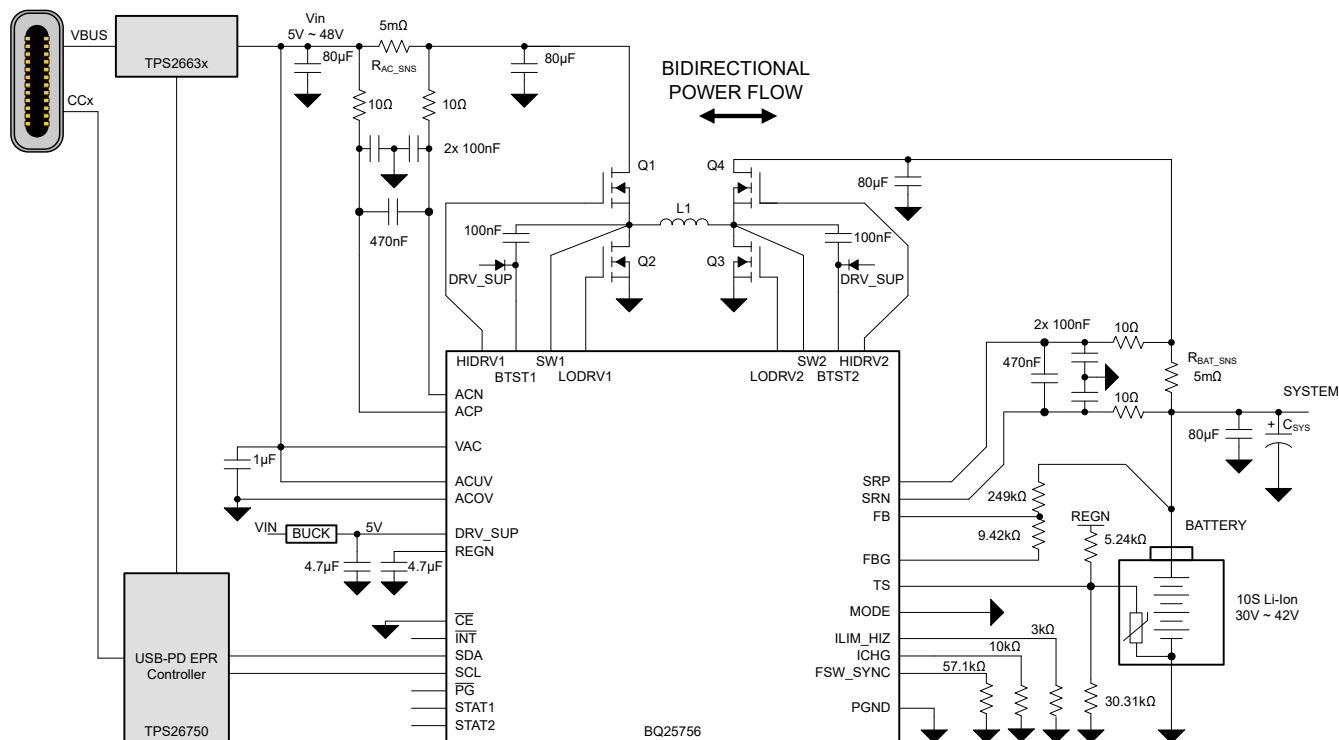


Figure 7-18. BQ25756: USB-PD EPR Input to Charge 10s Battery with up-to 240 W. Bidirectional Power Flow to Provide USB-PD EPR Power to the Input Port.

Table 7-5. Recommended Part Numbers

COMPONENT	VALUE	RECOMMENDED PART NUMBER
Q1, Q2, Q3, Q4	80V, 6.2mΩ	SiR880BDP
L1	10μH, 19mΩ	CMLB135T-100MS

7.2.2.1 Design Requirements

For this design example, use the parameters shown in the table below.

Table 7-6. Design Parameters

PARAMETER	VALUE
Input voltage operating range (V_{AC})	5V to 48V
Input current limit (I_{AC})	HW limit: 6.7A SW limit: set by TPS26750 PD controller
Charge current limit (I_{CHG})	5A
Battery charge voltage (V_{BAT_REG})	42V
Switching frequency	450kHz
Reverse Mode voltage regulation (V_{AC_REV})	Set by TPS26750: 5V to 48V
Reverse Mode current regulation (I_{AC_REV})	HW limit: 6.7A SW limit: set by TPS26750 PD controller

8 Power Supply Recommendations

The power supply for the device is any DC voltage source within the specified input range. The supply must also be capable of supplying sufficient current based on the programmed input current limit. The input supply must be bypassed with a combination of electrolytic and ceramic capacitors to avoid ringing due to the parasitic impedance of the connecting cables.

When device is operating in the reverse direction, the supply at the OUTPUT should follow the same recommendations as the input supply mentioned above.

9 Layout

9.1 Layout Guidelines

Proper layout of the components to minimize high frequency current path loops is important to prevent electrical and magnetic field radiation and high frequency resonant problems. Here is a PCB layout priority list for proper layout.

Table 9-1. PCB Layout Guidelines

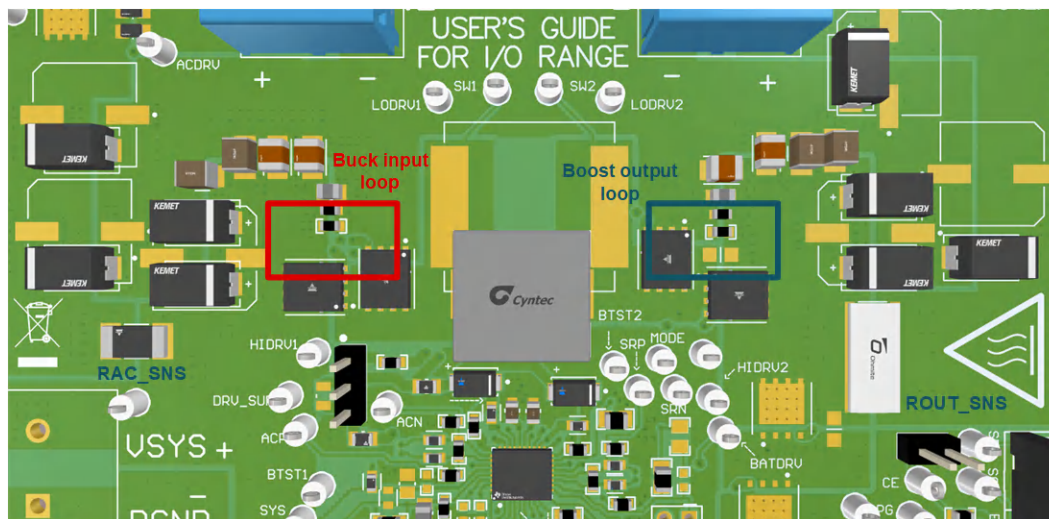
COMPONENTS	FUNCTION	IMPACT	GUIDELINES
Buck high side FET, Buck low side FET, input capacitors	Buck input loop	High frequency noise, ripple, efficiency	This path forms a high frequency switching loop due to the pulsating current at the input of the buck. Place components on the same side of the board. Minimize loop area to reduce parasitic inductance. Maximize trace width to reduce parasitic resistance. Place input ceramic capacitors close to the switching FETs.
Boost low side FET, boost high side FET, output capacitors	Boost output loop	High frequency noise, ripple, efficiency	This path forms a high frequency switching loop due to the pulsating current at the output of the boost. Place components on the same side of the board. Minimize loop area to reduce parasitic inductance. Maximize trace width to reduce parasitic resistance. Place output ceramic capacitors close to the switching FETs.
Sense resistors, switching FETs, inductor	Current path	Efficiency	The current path from input to output through the power stage and sense resistors needs to have low impedance. Pay attention to via resistance if the components are not on the same side. The number of vias can be estimated as 1 to 2A per via for a 10-mil via with 1 oz. copper thickness.
Switching FETs, inductor	Power stage	Thermal, efficiency	The switching FETs and inductor are the components with highest power loss. Allow enough copper area for heat dissipation. Multiple thermal vias can be used to connect more copper layers together and dissipate more heat.
DRV_SUP, BTST1, BTST2 capacitors	Switching FET gate drive	High frequency noise, parasitic ringing, gate drive integrity	The DRV_SUP capacitor is used to supply the power to drive the low side FETs. The BTST capacitors are used to drive the high side FETs. It is recommended to place the capacitors as close as possible to the IC.
LODRV1, LODRV2	Low side gate drive	High frequency noise, parasitic ringing, gate drive integrity	LODRV1 and LODRV2 supplies the gate drive current to turn on the low side FETs. The return of LODRV1 and LODRV2 is PGND. As current takes the path of least impedance, a ground plane close to the low side gate drive traces is recommended. Minimize gate drive length and aim for at least 20-mil gate drive trace width.
HIDRV1, HIDRV2, SW1 (pin trace), SW2 (pin trace)	High side gate drive	High frequency noise, parasitic ringing, gate drive integrity	HIDRV1 and HIDRV2 supplies the gate drive current to turn on the high side FETs. The return of HIDRV1 and HIDRV2 are SW1 and SW2, respectively. Route the HIDRV1/SW1 and the HIDRV2/SW2 pair next to each other to reduce gate drive parasitic inductance. Minimize gate drive length and aim for at least 20-mil gate drive trace width. Do not route the HIDRV1/HIDRV2 trace next to the LODRV1/LODRV2 trace.

Table 9-1. PCB Layout Guidelines (continued)

COMPONENTS	FUNCTION	IMPACT	GUIDELINES
Current limit resistors, FSW_SYNC resistor	IC programmable settings	Regulation accuracy, switching integrity	Pin voltage determines the settings for input current limit, output current limit and switching frequency. Ground noise on these could lead to inaccuracy. Minimize ground return from these resistors to the IC ground pin.
Input (ACP, ACN) and output (SRP, SRN) current sense	Current regulation	Regulation accuracy	Use Kelvin-sensing technique for input and output current sense resistors. Connect the current sense traces to the center of the pads, and run current sense traces as differential pairs, away from switching nodes.
Input (ACUV), and output (FB, VO_SNS) voltage sensing	Voltage sense and regulation	Regulation accuracy	ACUV divider sets internal input voltage regulation in forward mode (V_{ACUV_DPM}). FB divider sets battery voltage regulation in forward mode (V_{FB_ACC}). Route the top of the divider point to the target regulation location. Avoid routing close to high power switching nodes.
Bypass capacitors	Noise filter	Noise immunity	Place lowest value capacitors closest to the IC.

9.2 Layout Example

Based on the above layout guidelines, the PCB layout example top view is shown below including all the key power components.

**Figure 9-1. PCB Layout Reference Example Top View**

For both input and output current sensing resistors, differential sensing and routing method are suggested and highlighted in figure below. Use wide trace for gate drive traces, minimum 20-mil trace width. Connect all analog grounds to a dedicated low-impedance copper plane, which is tied to the power ground underneath the IC exposed pad.

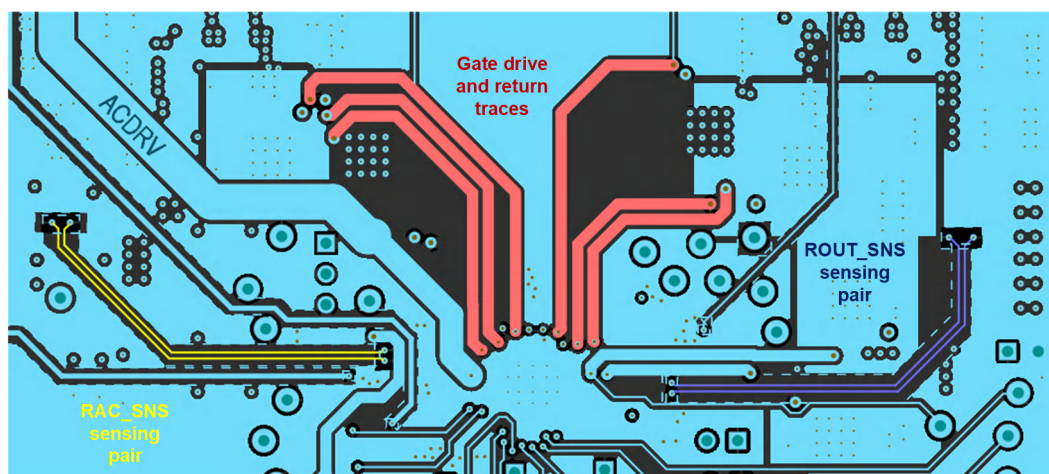


Figure 9-2. PCB Layout Gate Drive and Current Sensing Signal Layer Routing

10 Device and Documentation Support

10.1 Device Support

10.1.1 Third-Party Products Disclaimer

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To receive notification of documentation updates, navigate to the device product folder on [ti.com](https://www.ti.com). Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

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[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

10.6 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

11 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision * (August 2023) to Revision A (August 2026)	Page
• Removed mentions of buck-only mode.....	1
• Added "When the converter is disabled, the DRV_SUP supply needs to be disabled such that BTST1/BTST2 and DRV_SUP pins are not biased.".....	21
• Added Section 6.3.3.4	22
• Removed the CV Timer from the datasheet.....	23
• Removed Perturb and Observe Mode.....	29
• Updated Reverse Mode Power Direction section.....	30
• Renamed instances of VSYS_REV to VAC_REV. Clarified MPPT registers.	37
• Clarified layout guidelines.....	71

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
BQ25756RRVR	Active	Production	VQFN (RRV) 36	3000 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	BQ25756
BQ25756RRVR.A	Active	Production	VQFN (RRV) 36	3000 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	BQ25756

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

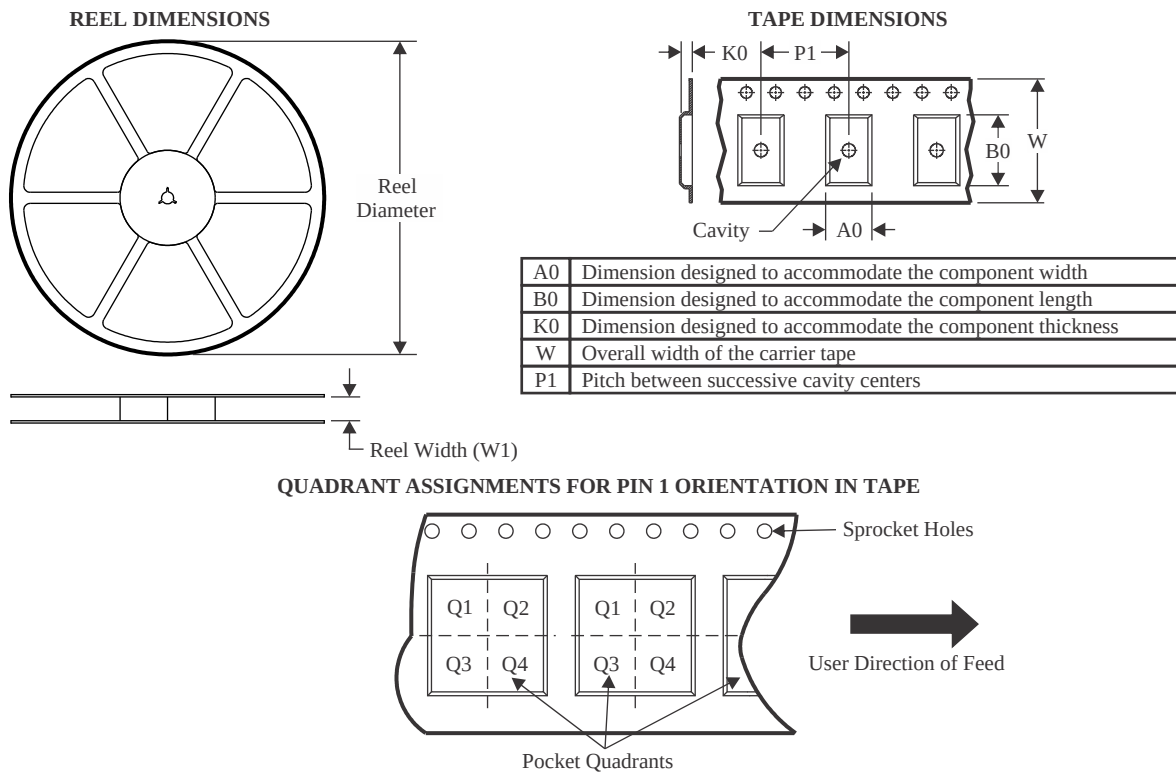
⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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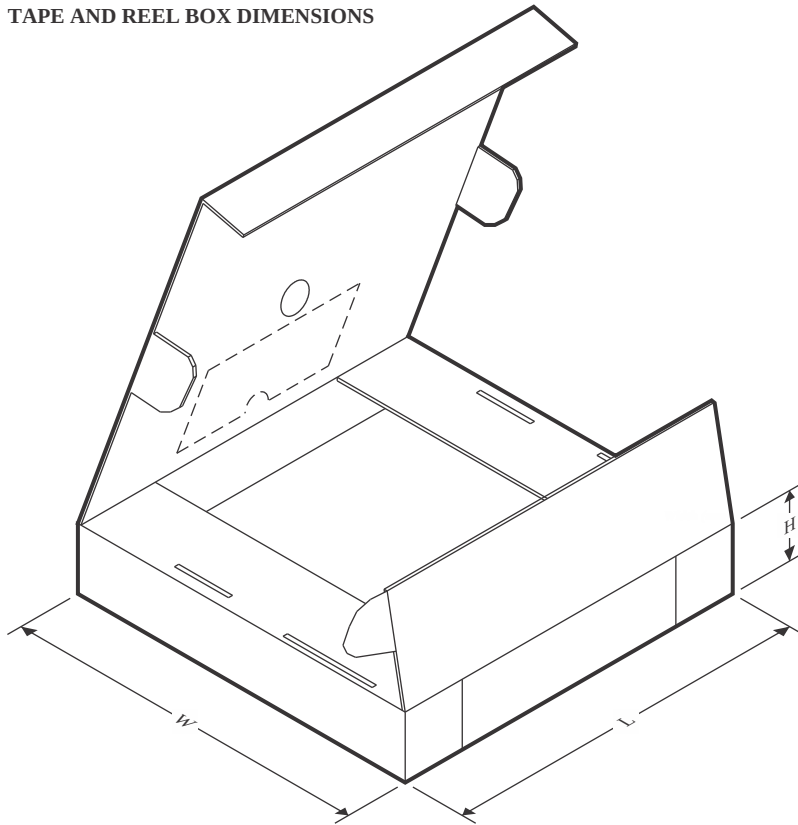
TAPE AND REEL INFORMATION



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
BQ25756RRVR	VQFN	RRV	36	3000	330.0	12.4	5.3	6.3	1.15	8.0	12.0	Q1

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
BQ25756RRVR	VQFN	RRV	36	3000	367.0	367.0	35.0

GENERIC PACKAGE VIEW

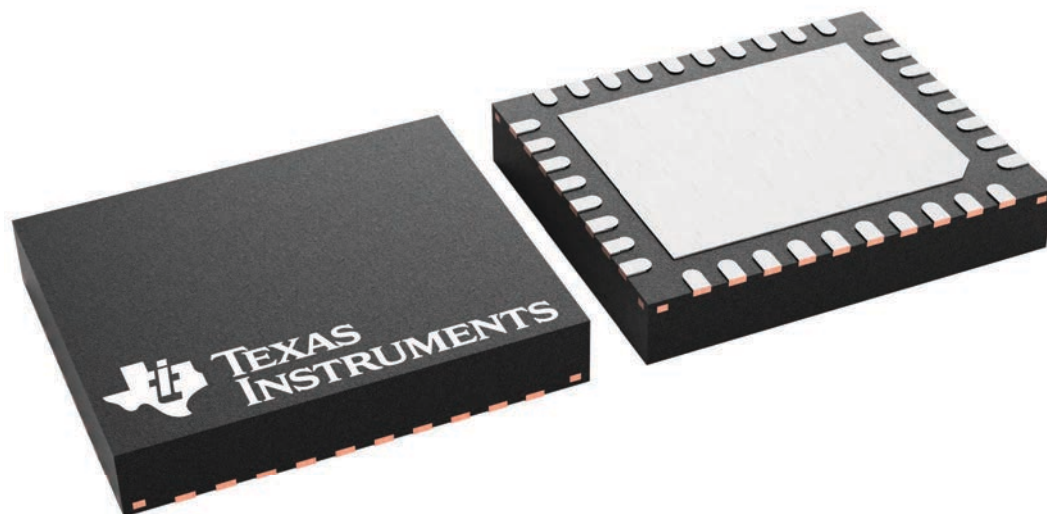
RRV 36

VQFN - 1 mm max height

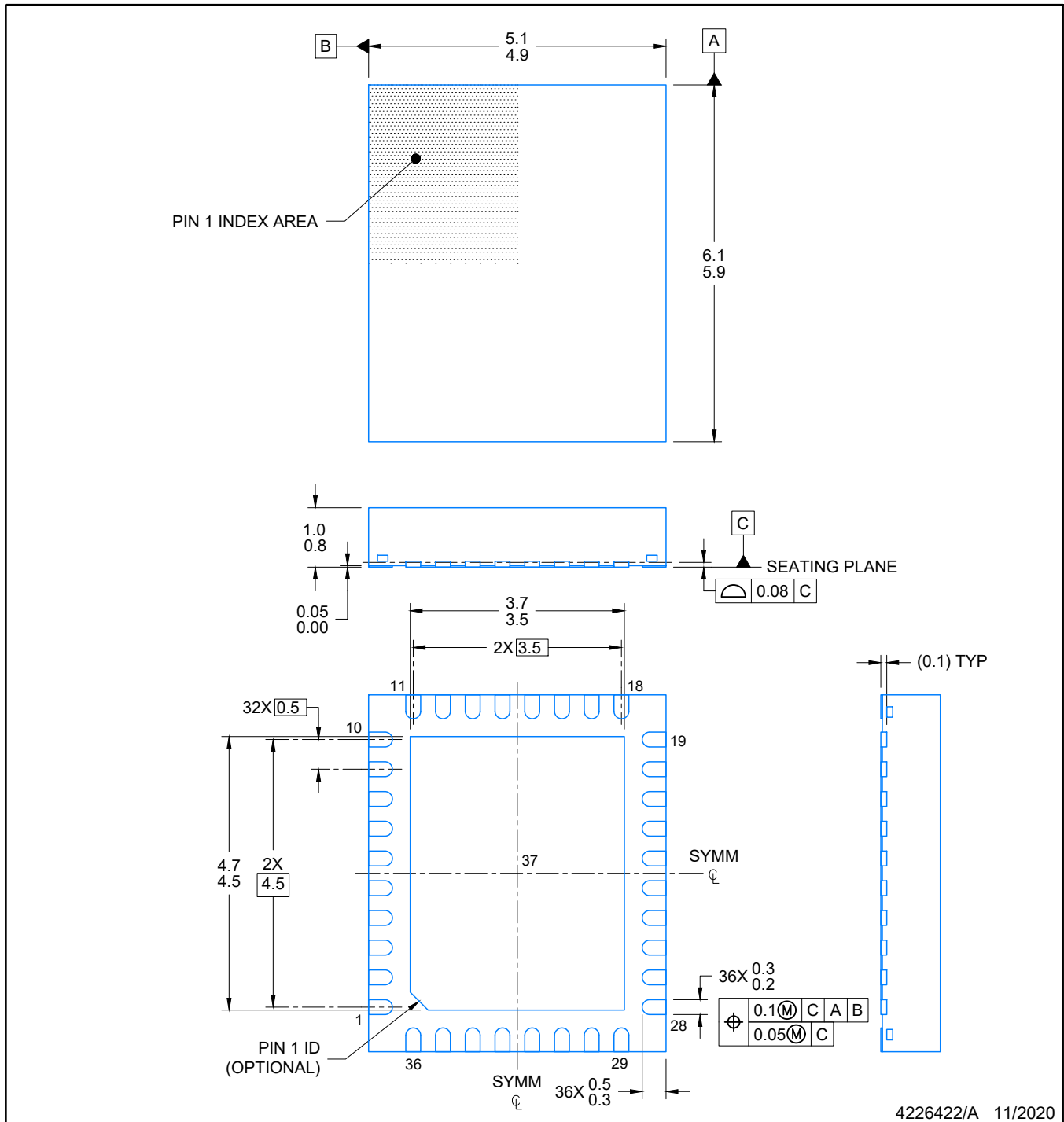
5 x 6, 0.5 mm pitch

PLASTIC QUAD FLATPACK - NO LEAD

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.



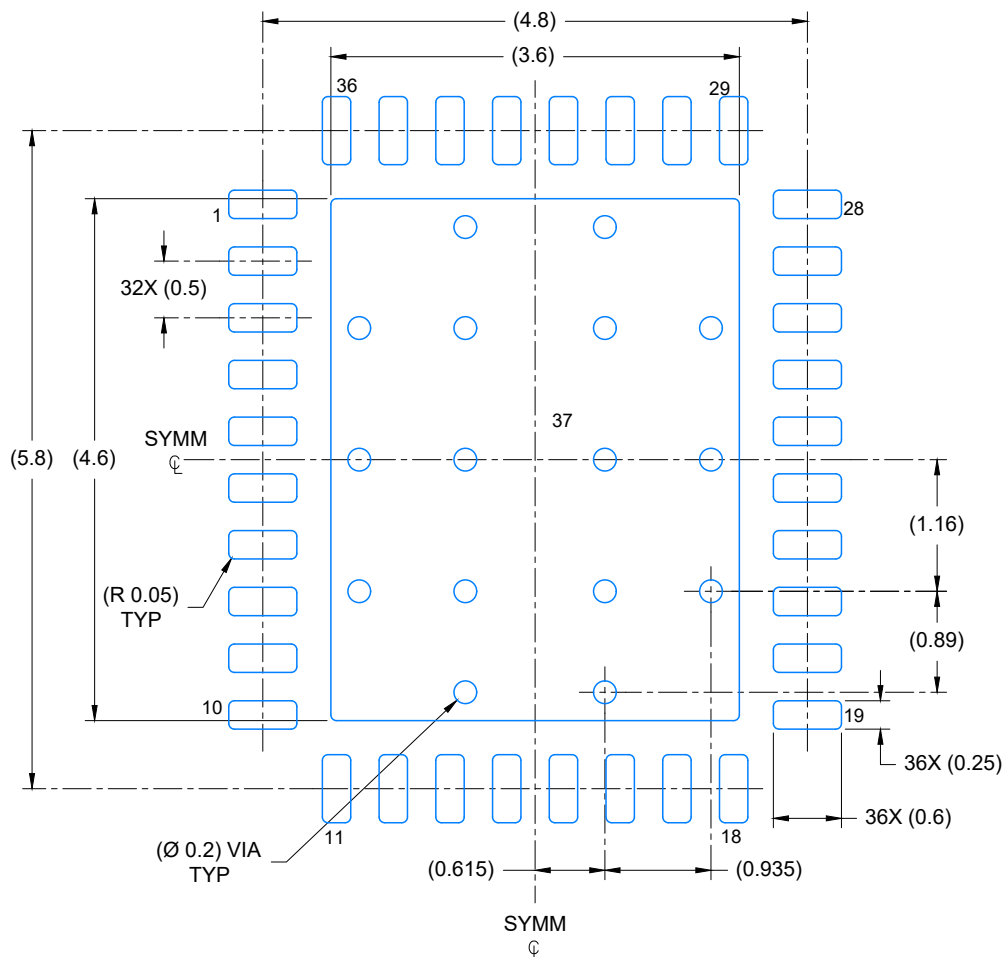
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4226422/A 11/2020

NOTES:

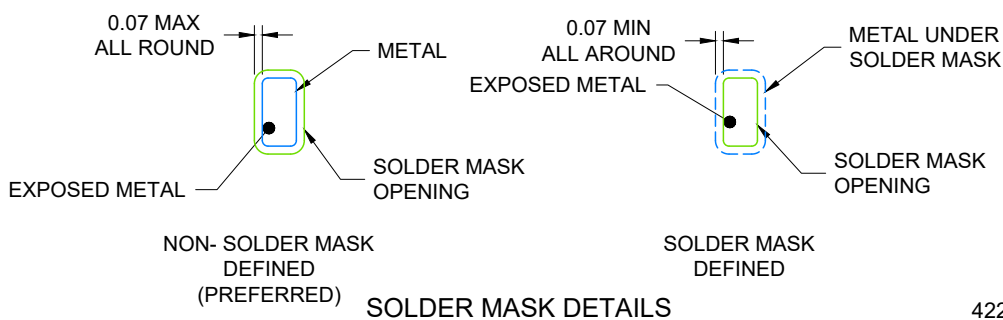
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for optimal thermal and mechanical performance.



LAND PATTERN EXAMPLE

EXPOSED METAL SHOWN

SCALE: 15X

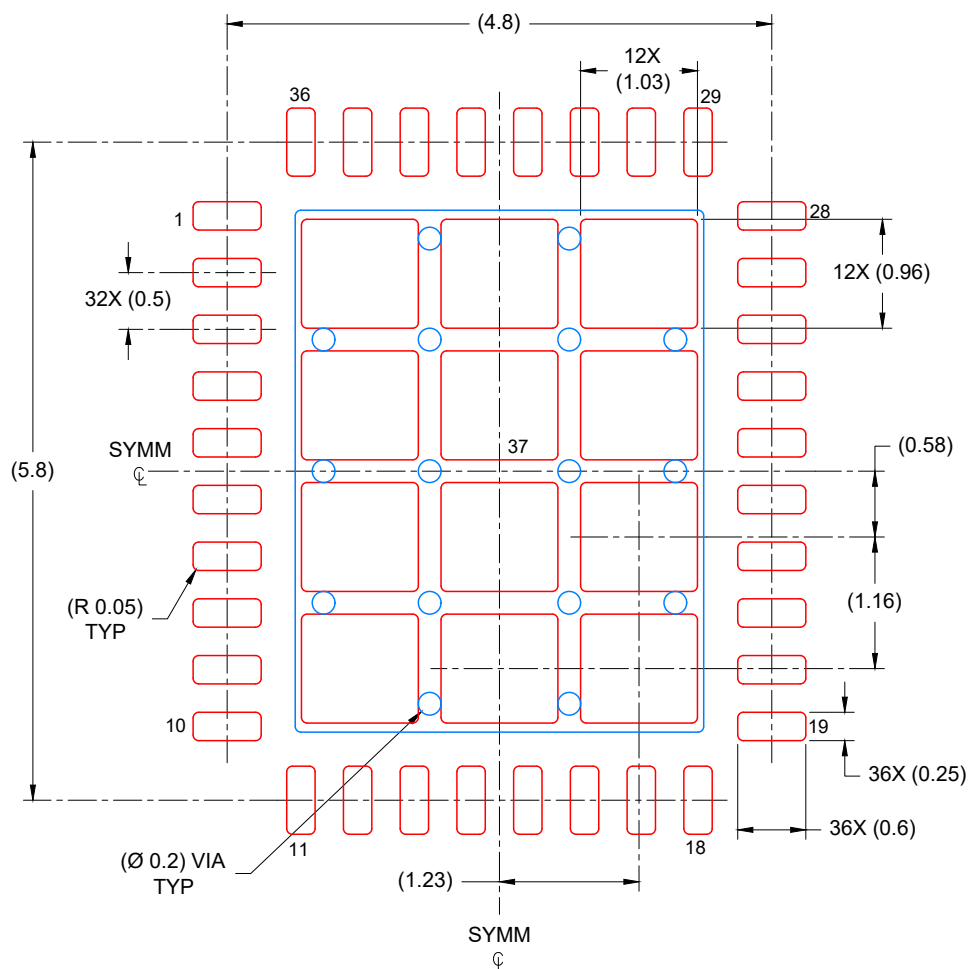


SOLDER MASK DETAILS

4226422/A 11/2020

NOTES: (continued)

- This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/sluea271).
- Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



SOLDER PASTE EXAMPLE
 BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD
 72% PRINTED COVERAGE BY AREA
 SCALE: 15X

4226422/A 11/2020

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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Last updated 10/2025