

TPS562207 4.3-V to 17-V Input, 2-A Synchronous Buck Converter in SOT563

1 Features

- 2-A converter integrated 140-mΩ and 84-mΩ FETs
- D-CAP2™ mode control with fast transient response
- Input voltage range: 4.3 V to 17 V
- Output voltage range: 0.804 V to 7 V
- Forced continuous conduction mode
- 580-kHz switching frequency
- Low shutdown current less than 3 μA
- 2% feedback voltage accuracy (25 °C)
- Support pre-bias function
- Cycle-by-cycle over current limit
- Hiccup-mode over current protection
- Non-latch UVP and TSD protections
- Fixed soft start: 1.2 ms

2 Applications

- [Digital TV power supply](#)
- [Smart speaker](#)
- [Wired networking](#)
- [Digital set top box \(STB\)](#)
- [Surveillance](#)

3 Description

TPS562207 is a simple, easy-to-use, 2-A synchronous buck converter in a SOT563 package.

The device is optimized to operate with minimum external component counts and also optimized to achieve low standby current.

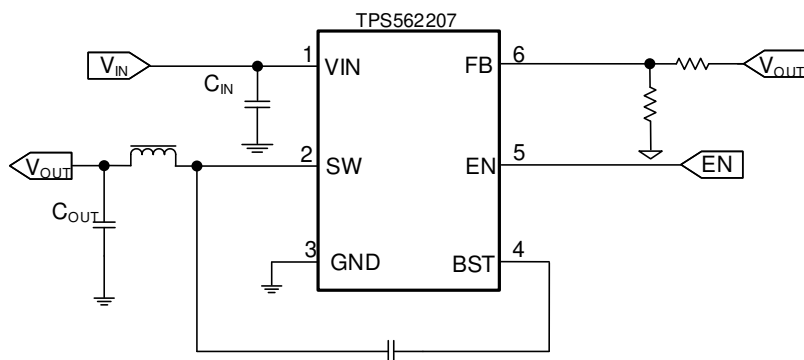
This switch mode power supply (SMPS) device employs D-CAP2 mode control providing a fast transient response and supporting both low-equivalent series resistance (ESR) output capacitors such as specialty polymer and ultra-low ESR ceramic capacitors with no external compensation components.

TPS562207 operates in Forced Continuous Conduction Mode (FCCM), which maintains fixed switching frequency and output voltage ripple is very small. TPS562207 is available in a 6-pin 1.6-mm × 1.6-mm SOT563 (DRL) package, and specified from a –40°C to 125°C junction temperature.

Device Information

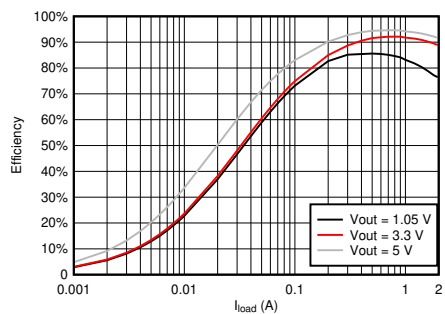
PART NUMBER	PACKAGE ⁽¹⁾	BODY SIZE (NOM)
TPS562207	DRL (6)	1.60 mm × 1.60 mm

- (1) For all available packages, see the orderable addendum at the end of the data sheet.



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Simplified Schematic



TPS562207 Efficiency



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4 Revision History

Changes from Revision A (June 2020) to Revision B (April 2021)	Page
• Updated the numbering format for tables, figures, and cross-references throughout the document.	1

Changes from Revision * (January 2020) to Revision A (June 2020)	Page
• Changed marketing status from Advance Information to initial release.	1

5 Pin Configuration and Functions

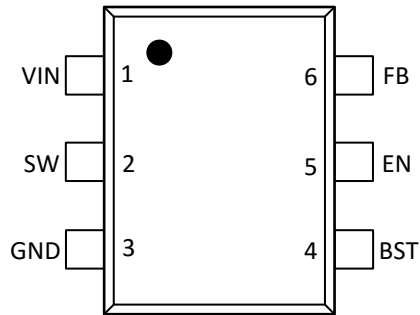


Figure 5-1. DRL Package 6-Pin SOT563 Top View

Table 5-1. Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
VIN	1	I	Input voltage supply pin.
SW	2	O	Switch node connection between high-side NFET and low-side NFET.
GND	3	—	Ground pin Source terminal of low-side power NFET as well as the ground terminal for controller circuit. Connect sensitive FB to this GND at a single point.
BST	4	O	Supply input for the high-side NFET gate drive circuit. Connect 0.1 uF capacitor between BST and SW pin.
EN	5	I	Enable input control. Active high and must be pulled up to enable the device.
FB	6	I	Converter feedback input. Connect to output voltage with feedback resistor divider.

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
Input voltage	VIN, EN	-0.3	19	V
	BST	-0.3	25	V
	BST (10 ns transient)	-0.3	27	V
	BST (vs SW)	-0.3	6.5	V
	FB	-0.3	6.5	V
	SW	-2	19	V
	SW (10 ns transient)	-3.5	21	V
Operating junction temperature, T _J		-40	150	°C
Storage temperature, T _{stg}		-55	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

6.2 ESD Ratings

		VALUE	UNIT
V _(ESD) Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V
	Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V _{IN}	Supply input voltage range	4.3		17	V
V _I	Input voltage range	BST		23	V
		BST (10 ns transient)	-0.1	26	
		BST (vs SW)	-0.1	6	
		EN	-0.1	17	
		FB	-0.1	5.5	
		SW	-1.8	17	
		SW (10 ns transient)	-3.5	20	
T _J	Operating junction temperature	-40		125	°C

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TPS562207	UNIT
		DRL	
		6 PINS	
R _{θJA}	Junction-to-ambient thermal resistance	141.0	°C/W
R _{θJA} _effective	Junction-to-ambient thermal resistance with TI EVM board ⁽²⁾	75	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	42.0	°C/W
R _{θJB}	Junction-to-board thermal resistance	25.5	°C/W

THERMAL METRIC ⁽¹⁾		TPS562207	
		DRL	
		6 PINS	
			UNIT
Ψ_{JT}	Junction-to-top characterization parameter	1.0	°C/W
Ψ_{JB}	Junction-to-board characterization parameter	25.3	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.
- (2) This $R_{\theta JA_effective}$ is tested on TPS562207EVM board(2 layer, copper thickness is 2 OZ) at $V_{IN} = 12V$, $V_{OUT} = 5V$, $I_{OUT} = 2A$, $T_A = 25^{\circ}C$.

6.5 Electrical Characteristics

$T_J = -40^{\circ}\text{C}$ to 125°C , $V_{IN} = 12\text{ V}$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY CURRENT						
I_{VIN}	Operating – non-switching supply current	V_{IN} current, EN = 5 V, $V_{FB} = 1\text{ V}$		590	750	μA
I_{VINSN}	Shutdown supply current	V_{IN} current, EN = 0 V		1	3	μA
LOGIC THRESHOLD						
V_{ENH}	EN high-level input voltage	EN		1.35	1.6	V
V_{ENL}	EN low-level input voltage	EN	0.8	1.05		V
R_{EN}	EN pin resistance to GND	$V_{EN} = 12\text{ V}$	225	400	900	k Ω
V_{FB} VOLTAGE AND DISCHARGE RESISTANCE						
V_{FBTH}	V_{FB} threshold voltage	$T_A = 25^{\circ}\text{C}$	788	804	820	mV
I_{FB}	V_{FB} input current	$V_{FB} = 1\text{ V}$		0	± 0.1	μA
MOSFET						
$R_{DS(on)h}$	High-side switch resistance	$T_A = 25^{\circ}\text{C}$, $V_{BST} - SW = 5.5\text{ V}$		140		m Ω
$R_{DS(on)l}$	Low-side switch resistance	$T_A = 25^{\circ}\text{C}$		84		m Ω
CURRENT LIMIT						
$I_{ocl_l_source}$	Low side FET source current limit		2.24	3.1	4	A
$I_{Nocl_l_sink}$	Low side FET sink current limit			1.1		A
THERMAL SHUTDOWN						
T_{SDN}	Thermal shutdown threshold ⁽¹⁾	Shutdown temperature		160		$^{\circ}\text{C}$
		Hysteresis		25		
ON-TIME TIMER CONTROL						
$t_{OFF(MIN)}$	Minimum off time	$V_{FB} = 0.5\text{ V}$		220	310	ns
SOFT START						
T_{SS}	Soft-start time	Internal soft-start time, Test Vout from 10% to 90%		1.2		ms
FREQUENCY						
F_{sw}	Switching frequency	$V_O = 1.05\text{ V}$		580		kHz
OUTPUT UNDERVOLTAGE						
V_{UVP}	Output UVP threshold	Hiccup detect ($H > L$)		65%		
T_{HICCUP_WAIT}	Hiccup on time			2.2		ms
T_{HICCUP_RE}	Hiccup time before restart			18		ms
UVLO						
UVLO	UVLO threshold	Wake up VIN voltage		4.0	4.3	V
		Shutdown VIN voltage	3.3	3.6		
		Hysteresis VIN voltage		0.4		

(1) Not production tested.

6.6 Typical Characteristics

$V_{IN} = 12\text{ V}$ (unless otherwise noted)

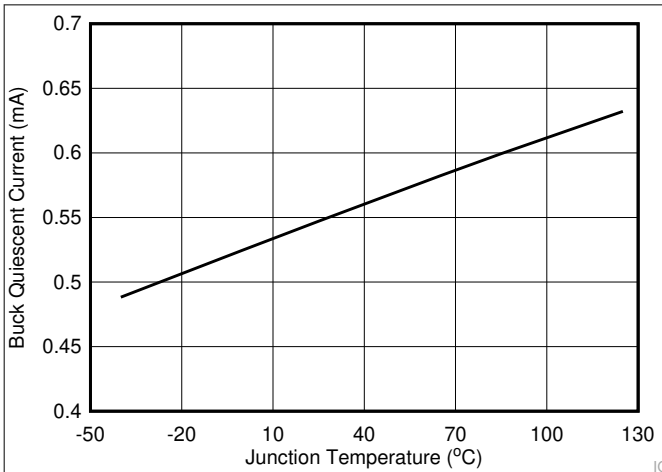


Figure 6-1. Supply Current vs Junction Temperature

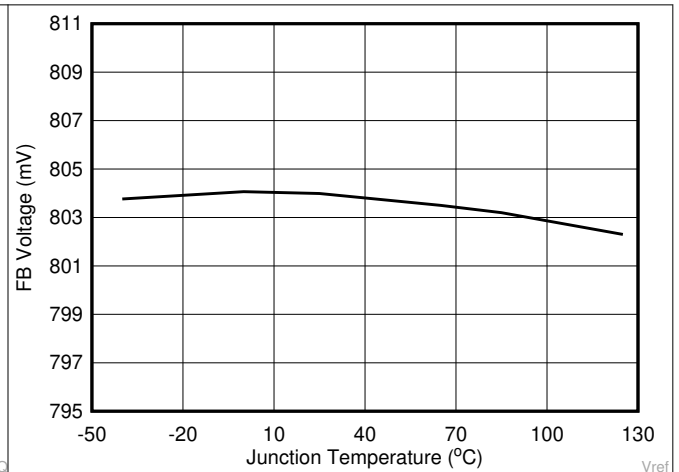


Figure 6-2. FB Voltage vs Junction Temperature

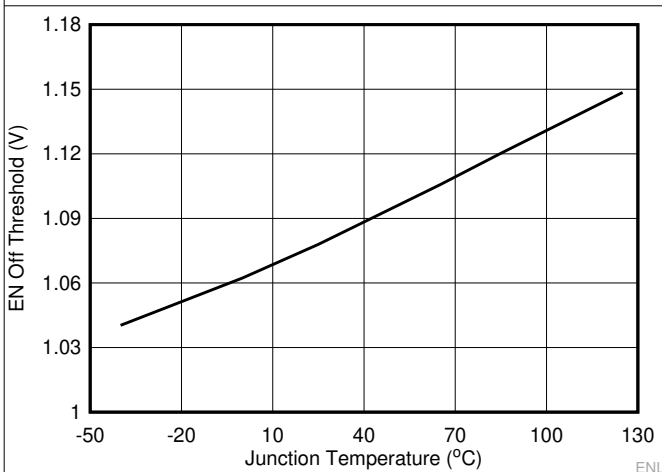


Figure 6-3. EN Off threshold Voltage vs Junction Temperature

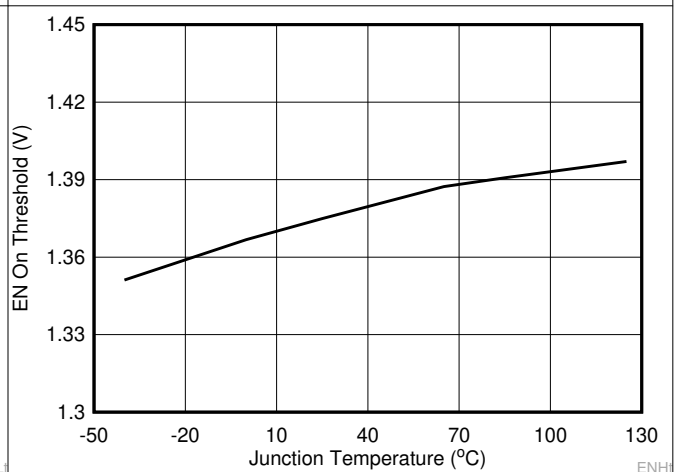


Figure 6-4. EN On threshold Voltage vs Junction Temperature

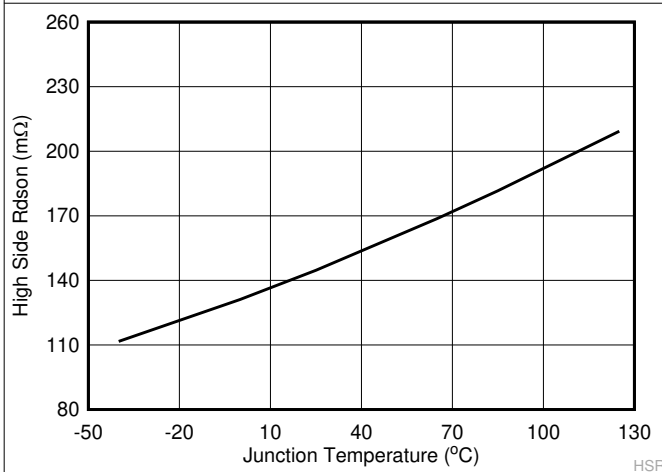


Figure 6-5. High-Side R_{ds-On} vs Junction Temperature

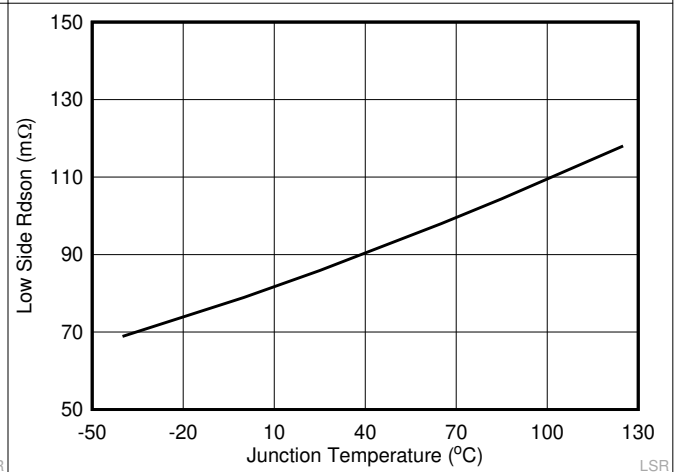


Figure 6-6. Low-Side R_{ds-On} vs Junction Temperature

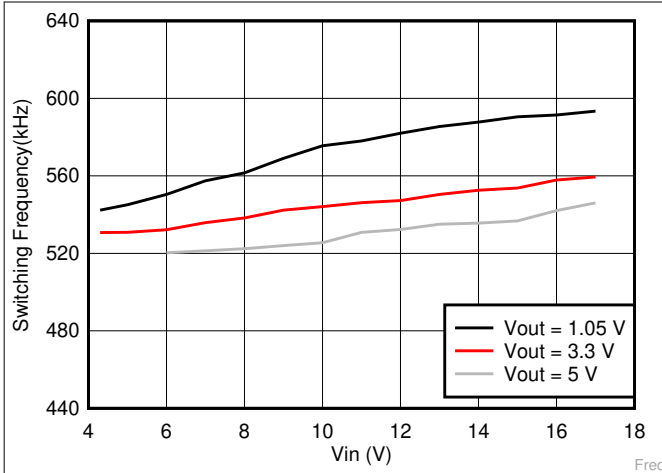


Figure 6-7. Switching Frequency vs Input Voltage

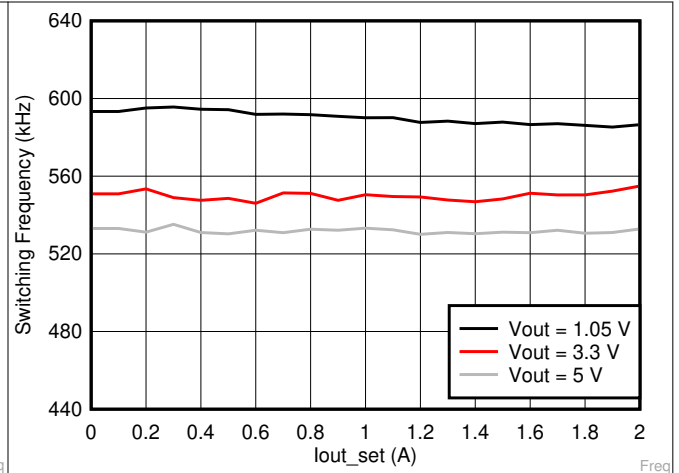


Figure 6-8. Switching Frequency vs Output Current

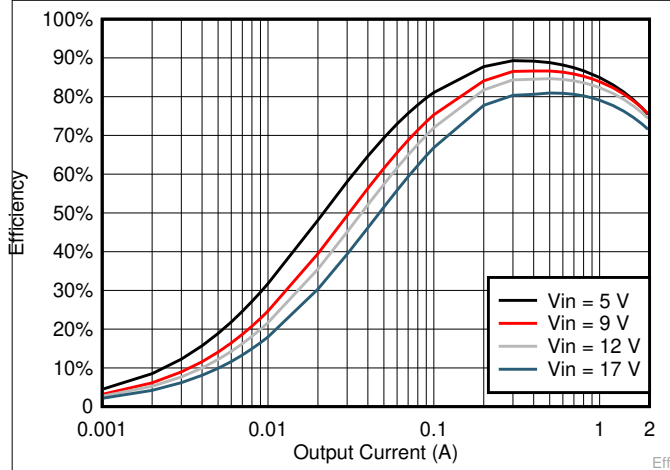


Figure 6-9. $V_{OUT} = 0.95\text{ V}$ Efficiency, $L = 2.2\mu\text{H}$

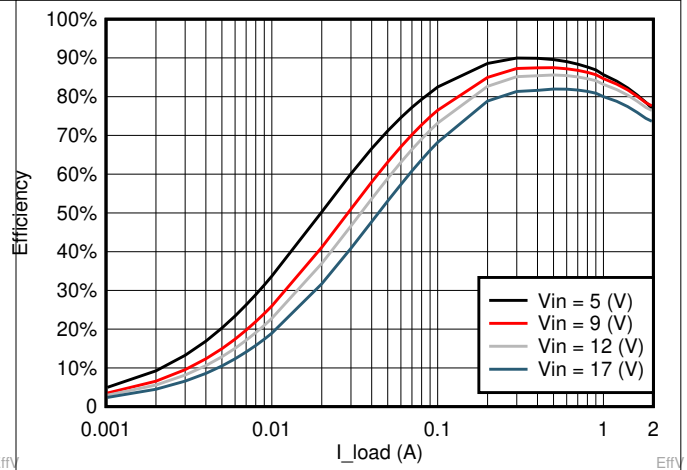


Figure 6-10. $V_{OUT} = 1.05\text{ V}$ Efficiency, $L = 2.2\mu\text{H}$

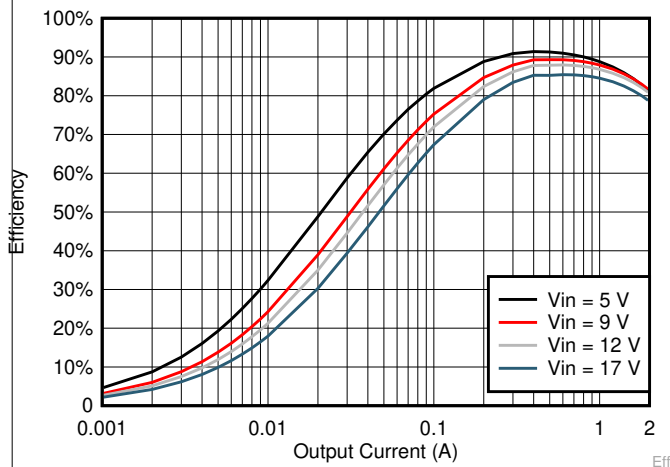


Figure 6-11. $V_{OUT} = 1.5\text{ V}$ Efficiency, $L = 2.2\mu\text{H}$

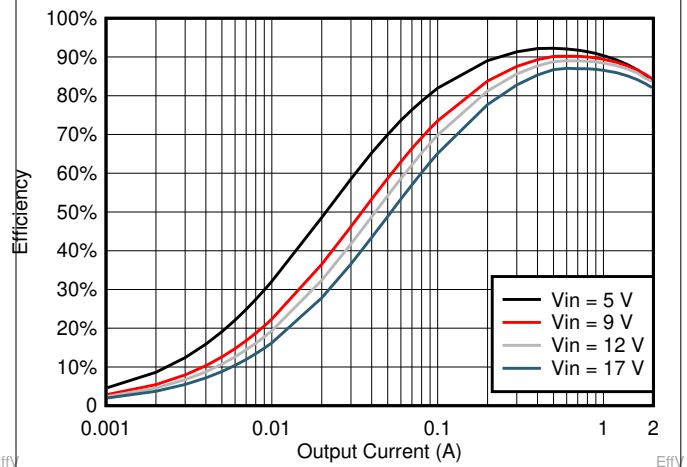


Figure 6-12. $V_{OUT} = 1.8\text{ V}$ Efficiency, $L = 2.2\mu\text{H}$

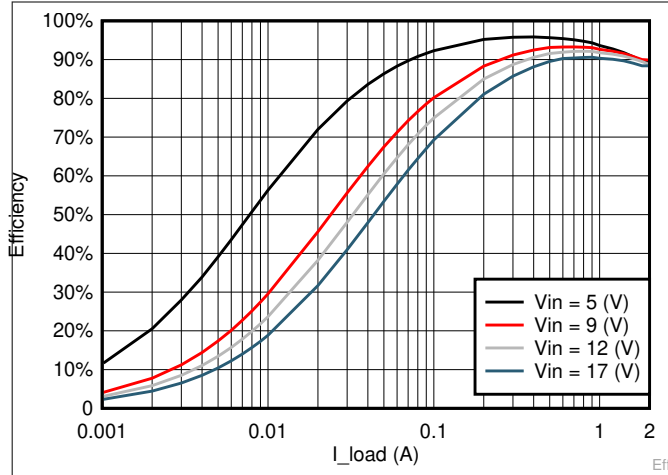


Figure 6-13. $V_{OUT} = 3.3\text{ V}$ Efficiency, $L = 3.3\ \mu\text{H}$

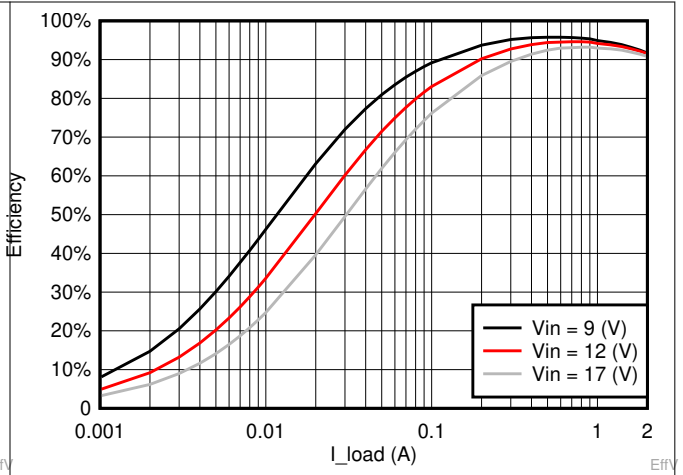


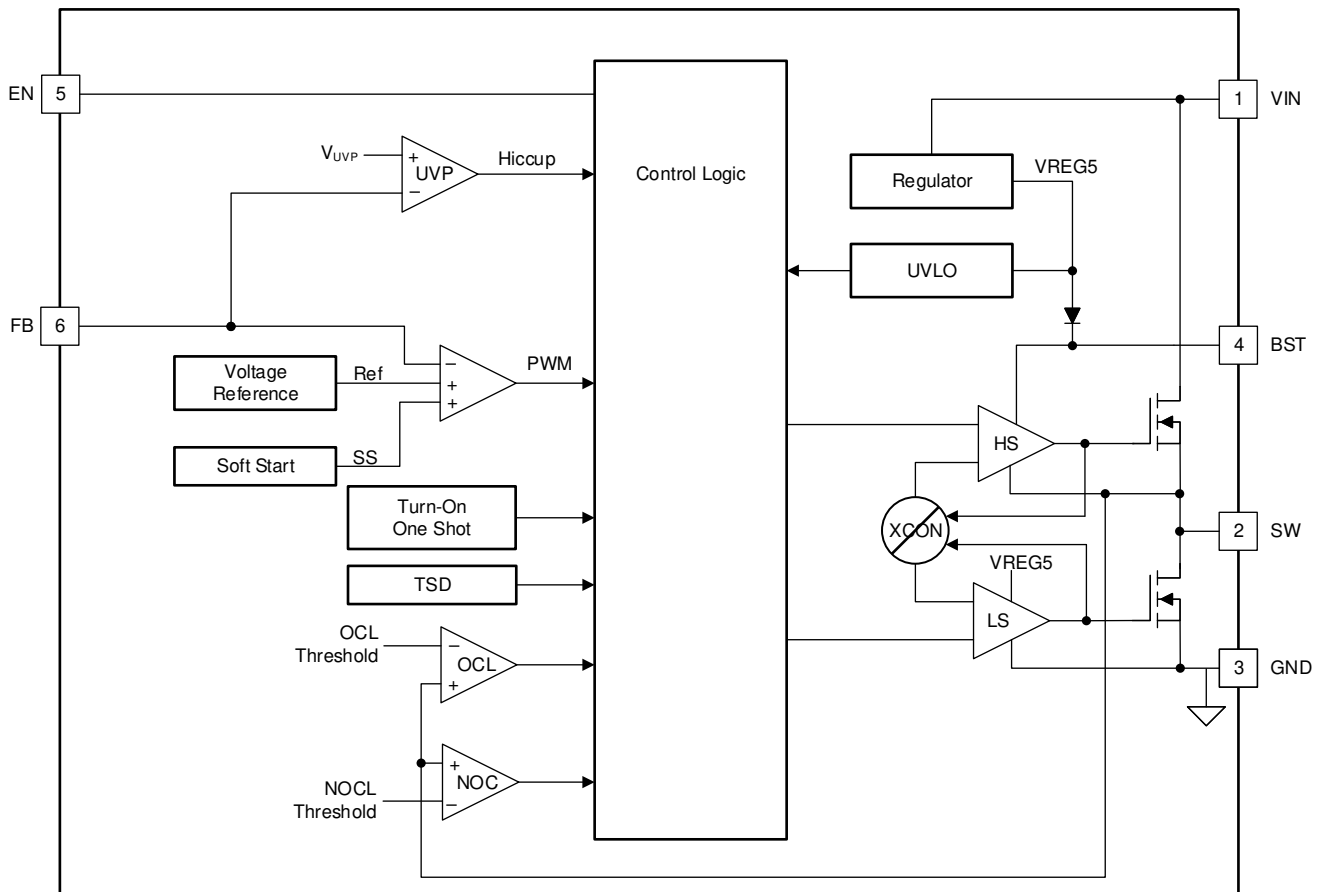
Figure 6-14. $V_{OUT} = 5\text{ V}$ Efficiency, $L = 4.7\ \mu\text{H}$

7 Detailed Description

7.1 Overview

TPS562207 is a 2-A synchronous buck converter. The proprietary D-CAP2 mode control supports low ESR output capacitors such as specialty polymer capacitors and multi-layer ceramic capacitors without complex external compensation circuits. The fast transient response of D-CAP2 mode control can reduce the output capacitance required to meet a specific level of performance.

7.2 Functional Block Diagram



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7.3 Feature Description

7.3.1 Adaptive On-Time Control and PWM Operation

The main control loop of the TPS562207 is adaptive on-time pulse width modulation (PWM) controller that supports a proprietary D-CAP2 mode control. The D-CAP2 mode control combines adaptive on-time control with an internal compensation circuit for pseudo-fixed frequency and low external component count configuration with both low-ESR and ceramic output capacitors. It is stable even with virtually no ripple at the output.

At the beginning of each cycle, the high-side MOSFET is turned on. This MOSFET is turned off after internal one shot timer expires. This one shot duration is set proportional to the converter input voltage, V_{IN} , and inversely proportional to the output voltage, V_O , to maintain a pseudo-fixed frequency over the input voltage range, hence it is called adaptive on-time control. The one-shot timer is reset and the high-side MOSFET is turned on again when the feedback voltage falls below the reference voltage. An internal ramp is added to reference voltage to simulate output ripple, eliminating the need for ESR induced output ripple from D-CAP2 mode control.

7.3.2 Soft Start and Pre-Biased Soft Start

TPS562207 have an internal 1.2-ms soft-start. When the EN pin becomes high, the internal soft-start function begins ramping up the reference voltage to the PWM comparator.

If the output capacitor is pre-biased at startup, the devices initiate switching and start ramping up only after the internal reference voltage becomes greater than the feedback voltage V_{FB} . This scheme ensures that the converters ramp up smoothly into regulation point.

7.3.3 Current Protection

The output over-current limit (OCL) is implemented using a cycle-by-cycle valley detect control circuit. The switch current is monitored during the OFF state by measuring the low-side FET drain to source voltage. This voltage is proportional to the switch current. To improve accuracy, the voltage sensing is temperature compensated.

During the on time of the high-side FET switch, the switch current increases at a linear rate determined by V_{in} , V_{out} , the on-time and the output inductor value. During the on time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current I_{out} . If the monitored current is above the OCL level, the converter maintains low-side FET on and delays the creation of a new set pulse, even the voltage feedback loop requires one, until the current level becomes OCL level or lower. In subsequent switching cycles, the on-time is set to a fixed value and the current is monitored in the same manner.

There are some important considerations for this type of over-current protection. The load current is higher than the over-current threshold by one half of the peak-to-peak inductor ripple current. Also, when the current is being limited, the output voltage tends to fall as the demanded load current may be higher than the current available from the converter. This may cause the output voltage to fall. When the FB voltage falls below the UVP threshold voltage, the UVP comparator detects it. And then, the device will shut down after the UVP delay time (typically 24 μ s) and re-start after the hiccup time (typically 18 ms).

When the over current condition is removed, the output voltage returns to the regulated value.

TPS562207 works in Forced Continuous Conduction Mode (FCCM). To support light load operation, the current flowing through low-side FET is allowed to be negative, which means the current flow from drain to source of low-side FET. This negative current is compared with low-side FET sink current limit to prevent device from being over-current damaged. Once the sink current cross limit, the low-side FET will turn off and the high-side FET will turn on to limit the negative current from overcurrent.

7.3.4 Undervoltage Lockout (UVLO) Protection

UVLO protection monitors the internal regulator voltage. When the voltage is lower than UVLO threshold voltage, the device is shut off. This protection is non-latching.

7.3.5 Thermal Shutdown

The device monitors the temperature of itself. If the temperature exceeds the threshold value (typically 160°C), the device is shut off. This is a non-latch protection. The device will resume normal working once the temperature return below the recovery threshold value (typically 135°C).

7.4 Device Functional Modes

7.4.1 Normal Operation

When the input voltage is above the UVLO threshold and the EN voltage is above the enable threshold, TPS562207 can operate in their normal switching modes. In continuous conduction mode (CCM), TPS562207 operates at a quasi-fixed frequency of 580 kHz.

7.4.2 Standby Operation

TPS562207 can be placed in standby mode by asserting the EN pin low.

8 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

The devices are typical buck DC-DC converters. It typically uses to convert a higher dc voltage to a lower dc voltage with a maximum available output current of 2 A. The following design procedure can be used to select component values for TPS562207. Alternately, the WEBENCH® software may be used to generate a complete design. The WEBENCH software uses an iterative design procedure and accesses a comprehensive database of components when generating a design. This section presents a simplified discussion of the design process.

8.2 Typical Application

The application schematic in Figure 8-1 was developed to meet the previous requirements. This circuit is available as the evaluation module (EVM). The sections provide the design procedure.

Figure 8-1 shows the TPS562207 4.3-V to 17-V input, 1.05-V output converter schematics.

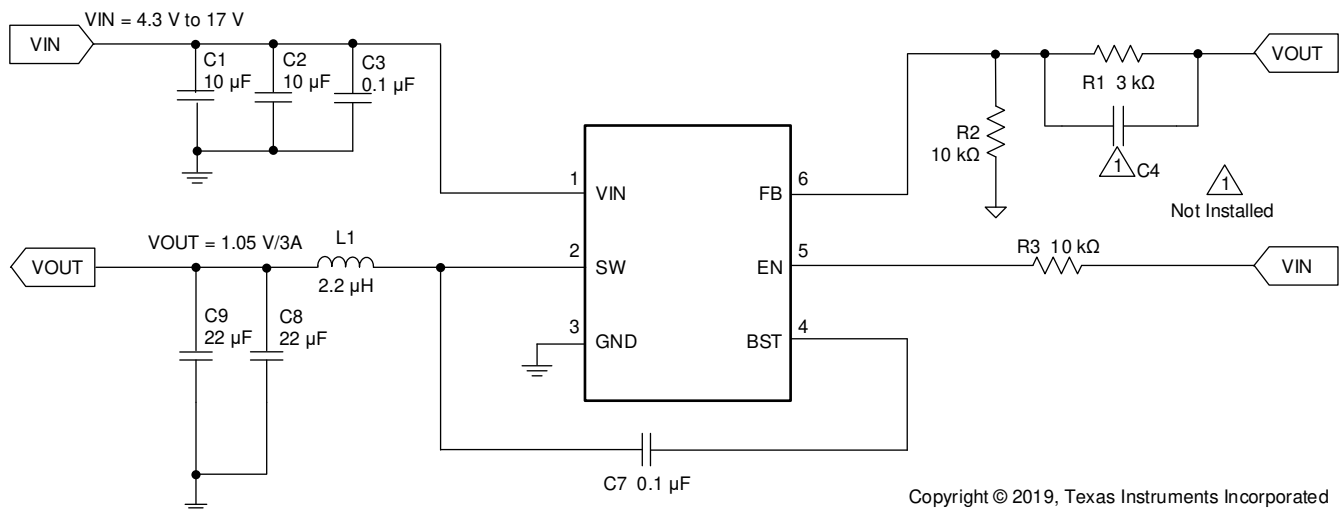


Figure 8-1. 1.05-V/2-A Reference Design

8.2.1 Design Requirements

Table 8-1 shows the design parameters for this application.

Table 8-1. Design Parameters

PARAMETER	EXAMPLE VALUE
Input voltage range	4.3 to 17 V
Output voltage	1.05 V
Transient response, load step: 10% ~ 90% of full loading	$\Delta V_{out} = \pm 5\%$
Input ripple voltage	200 mV
Output ripple voltage	20 mV
Output current rating	2 A
Operating frequency	580 kHz

8.2.2 Detailed Design Procedure

8.2.2.1 Output Voltage Resistors Selection

The output voltage is set with a resistor divider from the output node to the FB pin. TI recommends to use 1% tolerance or better divider resistors. Start by using Equation 1 to calculate V_{OUT} .

To improve efficiency at very light loads consider using larger value resistors, too high of resistance will be more susceptible to noise and voltage errors from the FB input current will be more noticeable.

$$V_{out} = 0.804 \times (1 + R_{FBT}/R_{FBB}) \quad (1)$$

8.2.2.2 Output Filter Selection

The LC filter used as the output filter has double pole at:

$$f_p = \frac{1}{2\pi\sqrt{L_{OUT} \times C_{OUT}}} \quad (2)$$

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the device. The low frequency phase is 180°. At the output filter pole frequency, the gain rolls off at a –40 dB per decade rate and the phase drops rapidly. D-CAP2 introduces a high frequency zero that reduces the gain roll off to –20 dB per decade and increases the phase to 90° one decade above the zero frequency. The inductor and capacitor for the output filter must be selected so that the double pole of Equation 2 is located below the high frequency zero but close enough that the phase boost provided by the high frequency zero provides adequate phase margin for a stable circuit. To meet this requirement use the values recommended in Table 8-2.

Table 8-2. Recommended Component Values

OUTPUT VOLTAGE (V)	R1 (k Ω)	R2 (k Ω)	TYP L1 (μ H)	C8 + C9 (μ F)			CFF (pF)
				Min	Typ	Max	
0.85	0.55	10.0	2.2	20	44	110	-
0.9	1.2	10.0	2.2	20	44	110	-
1	2.4	10.0	2.2	20	44	110	-
1.05	3	10.0	2.2	20	44	110	-
1.2	4.9	10.0	2.2	20	44	110	-
1.5	8.6	10.0	2.2	20	44	110	-
1.8	12.3	10.0	2.2	20	44	110	-
2.5	21	10.0	3.3	20	44	110	-
3.3	31	10.0	3.3	20	44	110	10-220

Table 8-2. Recommended Component Values (continued)

OUTPUT VOLTAGE (V)	R1 (kΩ)	R2 (kΩ)	TYP L1 (μH)	C8 + C9 (μF)			CFF (pF)
				Min	Typ	Max	
5	52	10.0	4.7	20	44	110	10-220
6.5	70.5	10.0	4.7	20	44	110	10-220

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 3](#), [Equation 4](#), and [Equation 5](#). The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current.

$$I_{P-P} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}} \quad (3)$$

$$I_{PEAK} = I_O + \frac{I_{P-P}}{2} \quad (4)$$

$$I_{LO(RMS)} = \sqrt{I_O^2 + \frac{1}{12} I_{P-P}^2} \quad (5)$$

For this design example, the calculated peak current is 2.35 A and the calculated RMS current is 2.01 A. The inductor used is a WE 74437349022 with an RMS current rating of 7.5 A.

The capacitor value and ESR determines the amount of output voltage ripple. TPS562207 is intended for use with ceramic or other low ESR capacitors. Recommended values range from 20 μF to 110 μF. Use [Equation 6](#) to determine the required RMS current rating for the output capacitor.

$$I_{CO(RMS)} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{\sqrt{12} \times V_{IN} \times L_O \times f_{SW}} \quad (6)$$

For this design two MuRata GRM21BR61A226ME44L 22-μF output capacitors are used. The typical ESR is 2 mΩ each. The calculated RMS current is 0.286 A and each output capacitor is rated for 4 A.

8.2.2.3 Input Capacitor Selection

The TPS562207 require an input decoupling capacitor and a bulk capacitor is needed depending on the application. TI recommends a ceramic capacitor over 10 μF for the decoupling capacitor. An additional 0.1-μF capacitor (C3) from pin 1 to ground is necessary to provide additional high frequency filtering. The capacitor voltage rating needs to be greater than the maximum input voltage.

8.2.2.4 Bootstrap Capacitor Selection

A typical 0.1-μF ceramic capacitor must be connected between the BST to SW pin for proper operation. TI recommends to use a ceramic capacitor.

8.2.3 Application Curves

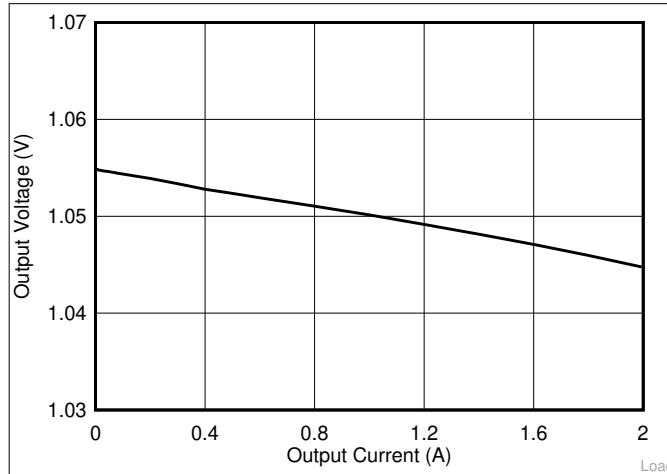


Figure 8-2. Load Regulation with different loading

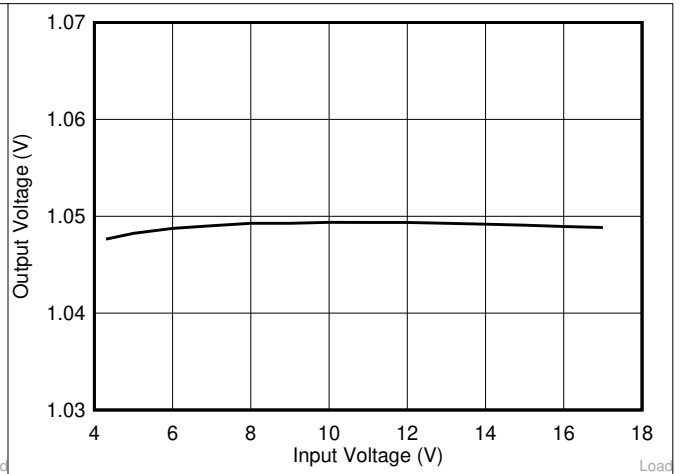


Figure 8-3. Load Regulation with different input voltage

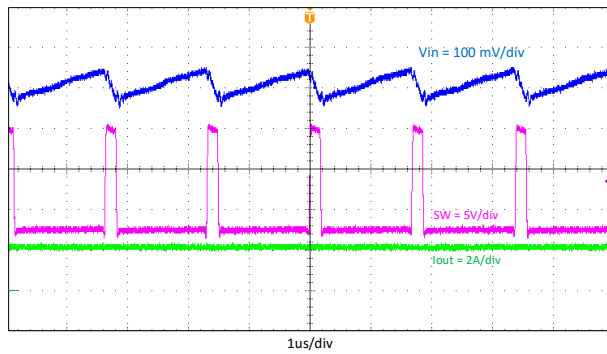


Figure 8-4. Input Voltage Ripple

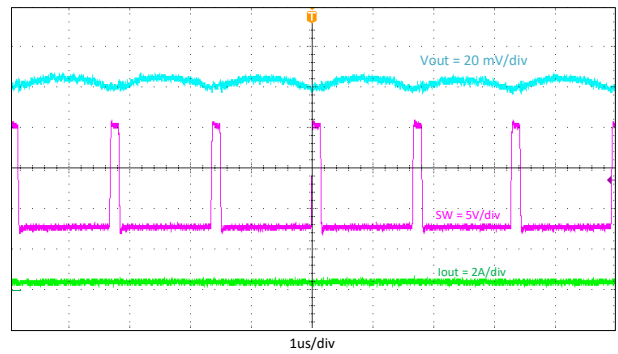


Figure 8-5. Output Voltage Ripple, $I_{out} = 0.2 \text{ A}$

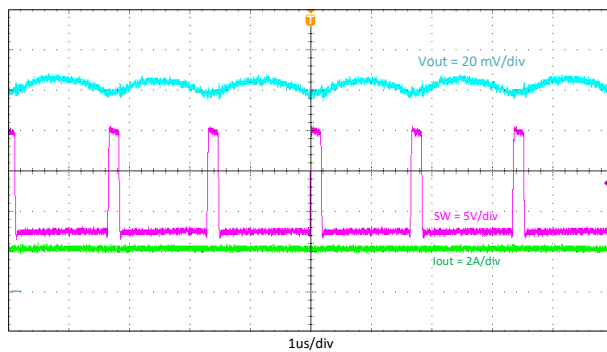


Figure 8-6. Output Voltage Ripple, $I_{out} = 2 \text{ A}$

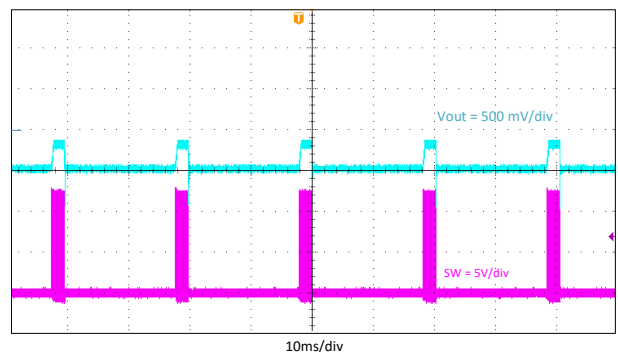


Figure 8-7. Hiccup, $I_{out} = 5 \text{ A}$

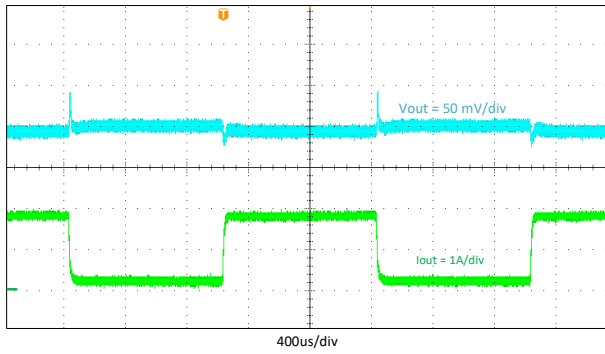


Figure 8-8. Transient Response, 0.2 to 1.8 A

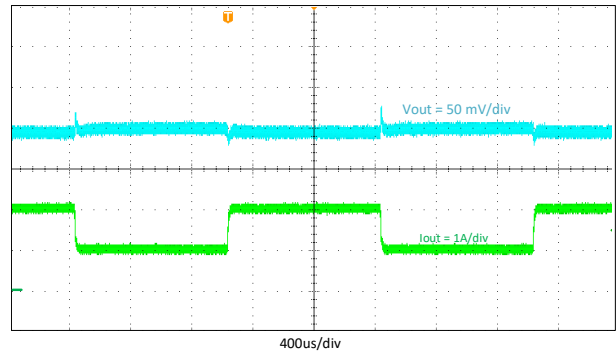


Figure 8-9. Transient Response, 1 to 2 A

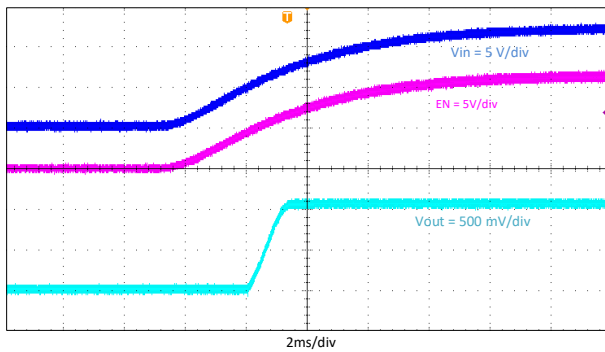


Figure 8-10. Start Up Relative to V_{IN}

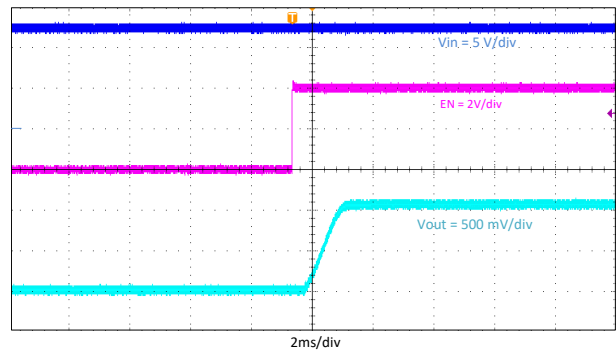


Figure 8-11. Start Up Relative to EN

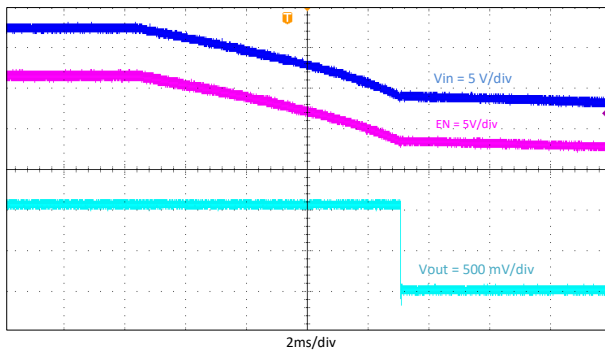


Figure 8-12. Shutdown Relative to V_{IN}

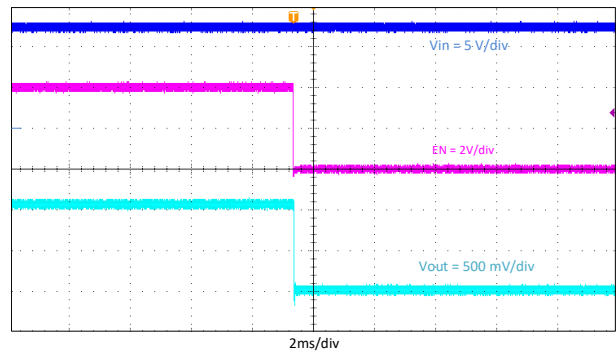


Figure 8-13. Shutdown Relative to EN

9 Layout

9.1 Layout Guidelines

1. VIN and GND traces should be as wide as possible to reduce trace impedance. The wide areas are also of advantage from the view point of heat dissipation.
2. The input capacitor and output capacitor should be placed as close to the device as possible to minimize trace impedance.
3. Provide sufficient vias for the input capacitor and output capacitor.
4. Keep the SW trace as physically short and wide as practical to minimize radiated emissions.
5. Do not allow switching current to flow under the device.
6. A separate VOUT path should be connected to the upper feedback resistor.
7. Make a Kelvin connection to the GND pin for the feedback path.
8. Voltage feedback loop should be placed away from the high-voltage switching trace, and preferably has ground shield.
9. The trace of the FB node should be as small as possible to avoid noise coupling.
10. The GND trace between the output capacitor and the GND pin should be as wide as possible to minimize its trace impedance.

9.2 Layout Example

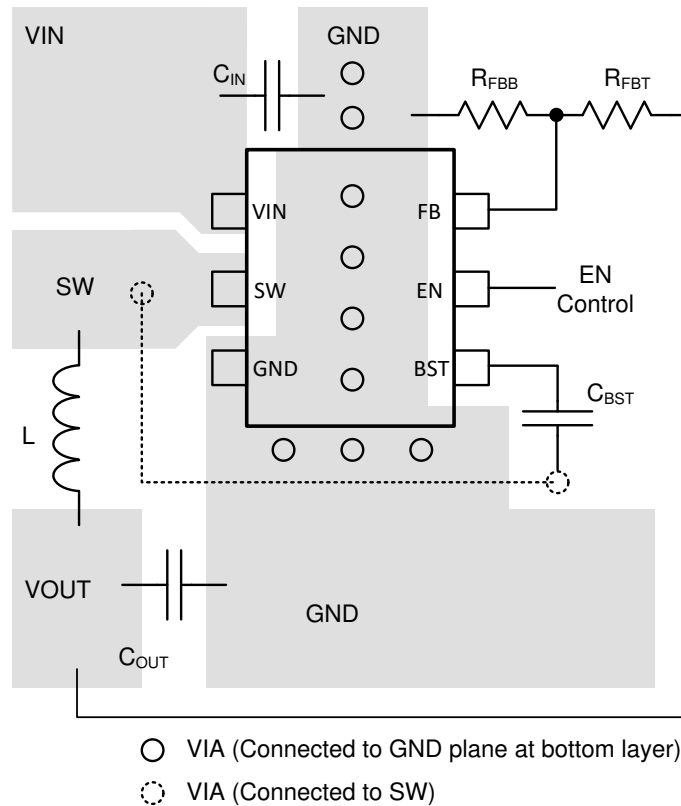


Figure 9-1. TPS562207 Layout

10 Device and Documentation Support

10.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

10.2 Support Resources

TI E2E™ [support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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10.3 Trademarks

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10.4 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

10.5 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS562207DRLR	Active	Production	SOT-5X3 (DRL) 6	4000 LARGE T&R	Yes	Call TI Sn	Level-1-260C-UNLIM	-40 to 125	2207
TPS562207DRLR.A	Active	Production	SOT-5X3 (DRL) 6	4000 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	2207

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS562207DRLR	SOT-5X3	DRL	6	4000	180.0	8.4	1.8	1.8	0.75	4.0	8.0	Q3
TPS562207DRLR	SOT-5X3	DRL	6	4000	180.0	8.4	1.8	1.8	0.75	4.0	8.0	Q3

TAPE AND REEL BOX DIMENSIONS


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS562207DRLR	SOT-5X3	DRL	6	4000	210.0	185.0	35.0
TPS562207DRLR	SOT-5X3	DRL	6	4000	210.0	185.0	35.0

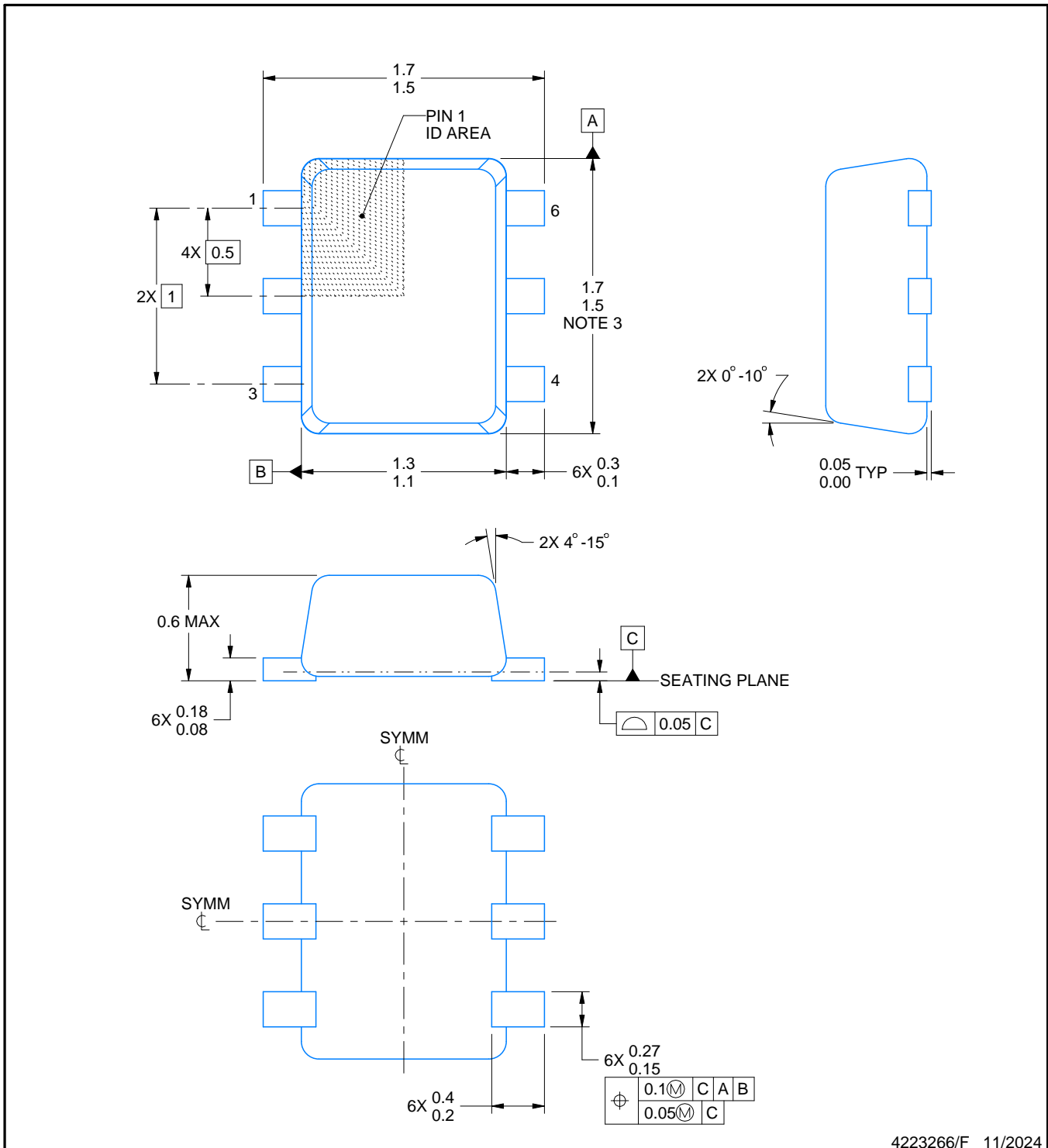
DRL0006A



PACKAGE OUTLINE

SOT - 0.6 mm max height

PLASTIC SMALL OUTLINE



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NOTES:

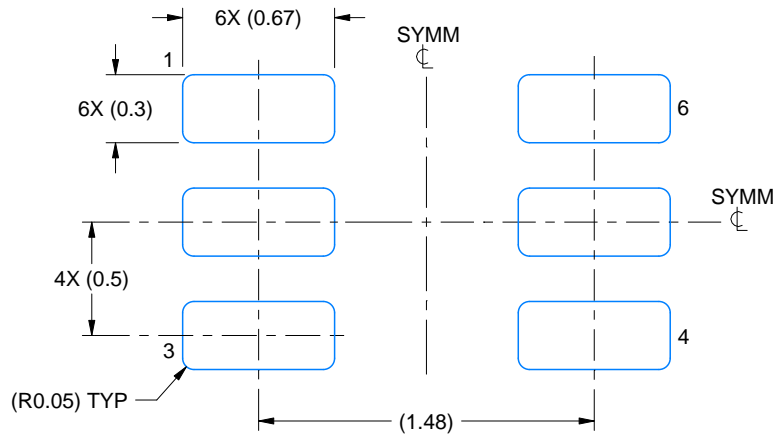
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. Reference JEDEC registration MO-293 Variation UAAD

EXAMPLE BOARD LAYOUT

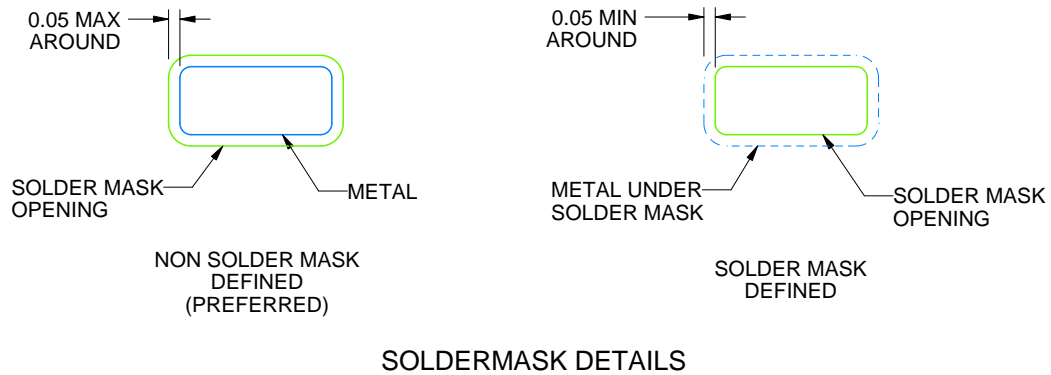
DRL0006A

SOT - 0.6 mm max height

PLASTIC SMALL OUTLINE



LAND PATTERN EXAMPLE
SCALE:30X



SOLDERMASK DETAILS

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NOTES: (continued)

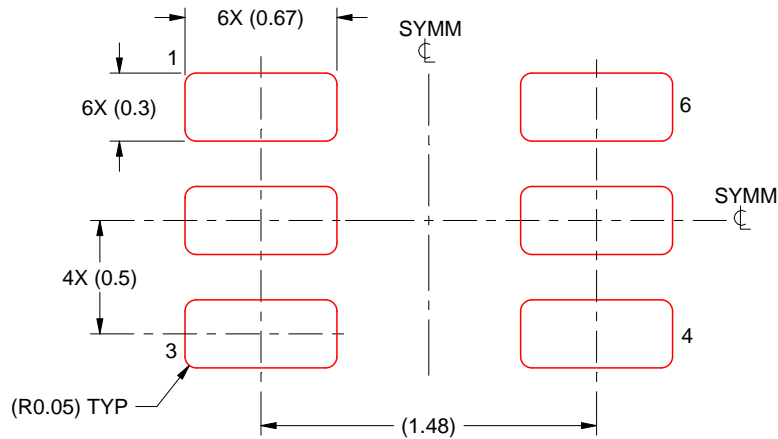
5. Publication IPC-7351 may have alternate designs.
6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
7. Land pattern design aligns to IPC-610, Bottom Termination Component (BTC) solder joint inspection criteria.

EXAMPLE STENCIL DESIGN

DRL0006A

SOT - 0.6 mm max height

PLASTIC SMALL OUTLINE



SOLDER PASTE EXAMPLE
BASED ON 0.1 mm THICK STENCIL
SCALE:30X

4223266/F 11/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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