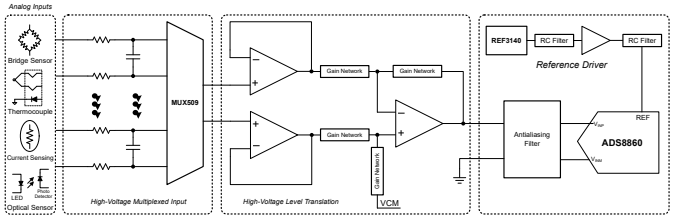
OPA4H199-SEP 40-V, Radiation Hardened, Rail-to-Rail Input/Output, Low Offset Voltage, Low Noise Op Amp in Space Enhanced Plastic

1 Features

- Radiation hardened
  - Single Event Latch-up (SEL) immune to 43 MeV-cm^2/mg at 125°C
  - ELDRS free to 30 krad(Si)
  - Total Ionizing Dose (TID) RLAT for every wafer lot up to 30 krad(Si)
- Supports defense, aerospace, and medical applications
  - Single controlled baseline
  - One fabrication, assembly and test site
  - Gold wire
  - NiPdAu lead finish
  - Available in military (–55°C to 125°C) temperature range
  - Extended product life cycle
  - Extended product-change notification
  - Product traceability
  - Enhanced mold compound for low outgassing
- Low offset voltage: ±125 µV
- Low noise: 10.8 nV/√Hz at 1 kHz
- High common-mode rejection: 130 dB
- Low bias current: ±10 pA
- Rail-to-rail input and output
- Wide bandwidth: 4.5 MHz GBW
- High slew rate: 21 V/µs
- High capacitive load drive: 1 nF
- MUX-friendly/comparator inputs
- Low quiescent current: 560 µA per amplifier
- Wide supply: ±1.35 V to ±20 V, 2.7 V to 40 V
- Robust EMIRR performance: EMI/RFI filters on input and supply pins

2 Applications

- Support low earth orbit space applications
- Space sensor and control (telemetry)
- Satellite electrical power system (EPS)
- Flight control
- Satellite command & data handling
- Satellite payloads



OPA4H199-SEP in a High-Voltage Signal Chain

3 Description

The OPA4H199-SEP is a high voltage (40 V) general purpose operational amplifiers for space application. The device offers exceptional DC precision and AC performance, including rail-to-rail input/output, low offset (±125 µV, typ), low offset drift (±0.3 µV/°C, typ), low noise (10.8 nV/√Hz and 1.8 μV_{PP}), and 4.5-MHz bandwidth.

Unique features such as differential and common-mode input-voltage range to the supply rail, high output current (±75 mA), high slew rate (21 V/µs), and high capacitive load drive (1 nF) make the OPA4H199-SEP a robust, high-performance operational amplifier for high-voltage space applications.

The OPA4H199-SEP is available in a small-sized, radiation-hardened plastic, 14-pin SOT-23 (DYY) package. The SOT-23 (DYY) package has a body size that is less than 1/5th of the size of traditional 14-pin ceramic packages. The OPA4H199-SEP is specified from –55°C to 125°C.

Device Information

PART NUMBER(1)	PACKAGE	BODY SIZE (NOM)
OPA4H199-SEP	SOT-23 (14)	4.20 mm × 1.90 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, intellectual property matters and other important disclaimers. PRODUCTION DATA.

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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

DATE	REVISION	NOTES
November 2022	*	Initial Release

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5 Pin Configuration and Functions

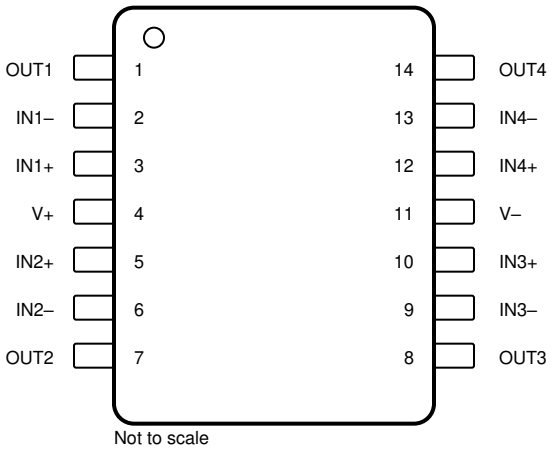


Figure 5-1. OPA4H199-SEP DYY Package
14-Pin SOT-23 (14)
Top View

Table 5-1. Pin Functions: OPA4H199-SEP

PIN		I/O	DESCRIPTION
NAME	NO.		
IN1+	3	I	Noninverting input, channel 1
IN1–	2	I	Inverting input, channel 1
IN2+	5	I	Noninverting input, channel 2
IN2–	6	I	Inverting input, channel 2
IN3+	10	I	Noninverting input, channel 3
IN3–	9	I	Inverting input, channel 3
IN4+	12	I	Noninverting input, channel 4
IN4–	13	I	Inverting input, channel 4
OUT1	1	O	Output, channel 1
OUT2	7	O	Output, channel 2
OUT3	8	O	Output, channel 3
OUT4	14	O	Output, channel 4
V+	4	—	Positive (highest) power supply
V–	11	—	Negative (lowest) power supply

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6 Specifications

6.1 Absolute Maximum Ratings

over operating ambient temperature range (unless otherwise noted) (1)

		MIN	MAX	UNIT
Supply voltage, V_S = (V+) – (V–)		0	42	V
Signal input pins	Common-mode voltage (3)	(V–) – 0.5	(V+) + 0.5	V
	Differential voltage (3)		V_S + 0.2	V
	Current (3)	–10	10	mA
Output short-circuit (2)		Continuous		
Operating ambient temperature, T_A		–55	150	°C
Junction temperature, T_J			150	°C
Storage temperature, T_{stg}		–65	150	°C

(1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings,* the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
(2) Short-circuit to ground, one amplifier per package. This device has been designed to limit *electrical* damage due to excessive output current, but extended short-circuit current, especially with higher supply voltage, can cause excessive heating and eventual *thermal* destruction. See the *Thermal Protection* section for more information.
(3) Input pins are diode-clamped to the power-supply rails. Input signals that may swing more than 0.5 V beyond the supply rails must be current limited to 10 mA or less.

6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001(1)	±2000	V
		Charged device model (CDM), per JEDEC specification JESD22-C101 (2)	±1000	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating ambient temperature range (unless otherwise noted)

		MIN	MAX	UNIT
V_S	Supply voltage, (V+) – (V–)	2.7	40	V
V_I	Input voltage range	(V–) – 0.1	(V+) + 0.1	V
T_A	Specified ambient temperature	–55	125	°C

6.4 Thermal Information for Quad Channel

THERMAL METRIC (1)		OPA4H199-SEP DYY (SOT-23) 14 PINS	UNIT
$R_{\theta JA}$	Junction-to-ambient thermal resistance	121.6	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	53.6	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	47.8	°C/W
ψ_{JT}	Junction-to-top characterization parameter	2.1	°C/W
ψ_{JB}	Junction-to-board characterization parameter	47.6	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	N/A	°C/W

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, SPRA953.

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6.5 Electrical Characteristics

For V_S = (V+) – (V–) = 2.7 V to 40 V (±1.35 V to ±20 V) at T_A = 25°C, R_L = 10 kΩ connected to V_S / 2, V_{CM} = V_S / 2, and $V_{O\ UT}$ = V_S / 2, unless otherwise noted.

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
OFFSET VOLTAGE							
V_{OS}	Input offset voltage	V_{CM} = V–			±125	±895	µV
			T_A = –-55°C to 125°C			±925	
dV_{OS}/dT	Input offset voltage drift		T_A = –-55°C to 125°C		±0.3		µV/°C
PSRR	Input offset voltage versus power supply	V_{CM} = V–, V_S = 4 V to 40 V	T_A = –-55°C to 125°C		±0.3	±1	µV/V
		V_{CM} = V–, V_S = 2.7 V to 40 V(2)			±1	±5	
	Channel separation	f = 0 Hz			5		µV/V
INPUT BIAS CURRENT							
I_B	Input bias current				±10		pA
I_{OS}	Input offset current				±10		pA
NOISE							
E_N	Input voltage noise	f = 0.1 Hz to 10 Hz			1.8		μV_{PP}
					0.3		μV_{RMS}
e_N	Input voltage noise density	f = 1 kHz			10.8		nV/√Hz
		f = 10 kHz			9.4		
i_N	Input current noise	f = 1 kHz			82		fA/√Hz
INPUT VOLTAGE RANGE							
V_{CM}	Common-mode voltage range			(V–) – 0.1		(V+) + 0.1	V
CMRR	Common-mode rejection ratio	V_S = 40 V, (V–) – 0.1 V < V_{CM} < (V+) – 2 V (Main input pair)	T_A = –-55°C to 125°C	107	130		dB
		V_S = 4 V, (V–) – 0.1 V < V_{CM} < (V+) – 2 V (Main input pair)		82	100		
		V_S = 2.7 V, (V–) – 0.1 V < V_{CM} < (V+) – 2 V (Main input pair)(2)		75	95		
		V_S = 2.7 V to 40 V, (V+) – 1 V < V_{CM} < (V+) + 0.1 V (Aux input pair)			85		
INPUT CAPACITANCE							
Z_{ID}	Differential				100 || 9		MΩ || pF
Z_{ICM}	Common-mode				6 || 1		TΩ || pF
OPEN-LOOP GAIN							
A_{OL}	Open-loop voltage gain	V_S = 40 V, V_{CM} = V– (V–) + 0.1 V < V_O < (V+) – 0.1 V		120	145		dB
			T_A = –-55°C to 125°C		142		
		V_S = 4 V, V_{CM} = V– (V–) + 0.1 V < V_O < (V+) – 0.1 V		104	130		
			T_A = –-55°C to 125°C		125		
		V_S = 2.7 V, V_{CM} = V– (V–) + 0.1 V < V_O < (V+) – 0.1 V(2)		101	120		
			T_A = –-55°C to 125°C		118		

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6.5 Electrical Characteristics (continued)

For V_S = (V+) – (V–) = 2.7 V to 40 V (±1.35 V to ±20 V) at T_A = 25°C, R_L = 10 kΩ connected to V_S / 2, V_{CM} = V_S / 2, and $V_{O\ UT}$ = V_S / 2, unless otherwise noted.

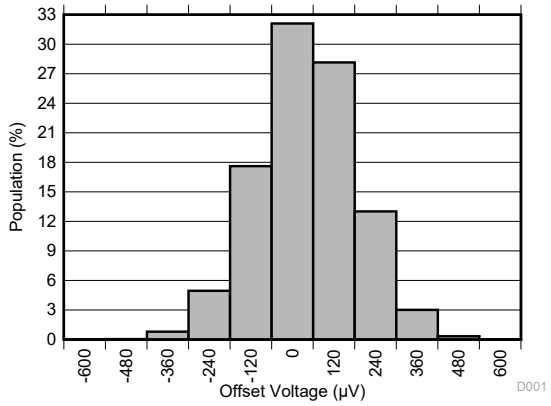
PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
FREQUENCY RESPONSE							
GBW	Gain-bandwidth product				4.5		MHz
SR	Slew rate	V_S = 40 V, G = +1, C_L = 20 pF			21		V/µs
t_S	Settling time	To 0.01%, V_S = 40 V, V_{STEP} = 10 V , G = +1, C_L = 20 pF			2.5		µs
		To 0.01%, V_S = 40 V, V_{STEP} = 2 V , G = +1, C_L = 20 pF			1.5		
		To 0.1%, V_S = 40 V, V_{STEP} = 10 V , G = +1, C_L = 20 pF			2		
		To 0.1%, V_S = 40 V, V_{STEP} = 2 V , G = +1, C_L = 20 pF			1		
	Phase margin	G = +1, R_L = 10 kΩ, C_L = 20 pF			60		°
	Overload recovery time	V_{IN} × gain > V_S			400		ns
THD+N	Total harmonic distortion + noise (1)	V_S = 40 V, V_O = 3 V_{RMS}, G = 1, f = 1 kHz			0.00021%		
OUTPUT							
	Voltage output swing from rail	Positive and negative rail headroom	V_S = 40 V, R_L = no load(2)		5	10	mV
			V_S = 40 V, R_L = 10 kΩ		50	70	
			V_S = 40 V, R_L = 2 kΩ		300	350	
			V_S = 2.7 V, R_L = no load(2)		1	6	
			V_S = 2.7 V, R_L = 10 kΩ		5	12	
			V_S = 2.7 V, R_L = 2 kΩ		25	40	
I_{SC}	Short-circuit current				±75		mA
C_{LOAD}	Capacitive load drive				1000		pF
Z_O	Open-loop output impedance	f = 1 MHz, I_O = 0 A			525		Ω
POWER SUPPLY							
I_Q	Quiescent current per amplifier	V_{CM} = V–, I_O = 0 A			560	685	µA
			T_A = –-55°C to 125°C			750	

(1) Third-order filter; bandwidth = 80 kHz at –3 dB.
(2) Specified by characterization only.

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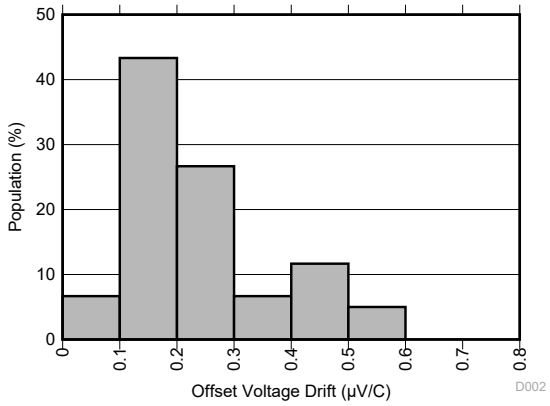
6.6 Typical Characteristics

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)



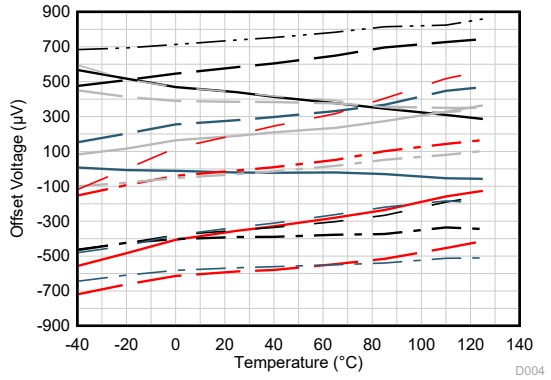
Distribution from 15462 amplifiers, T_A = 25°C

Figure 6-1. Offset Voltage Production Distribution



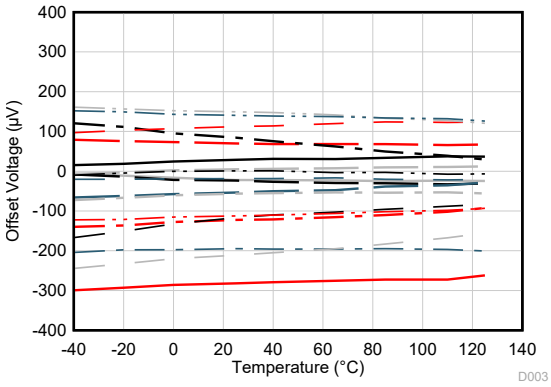
Distribution from 60 amplifiers

Figure 6-2. Offset Voltage Drift Distribution



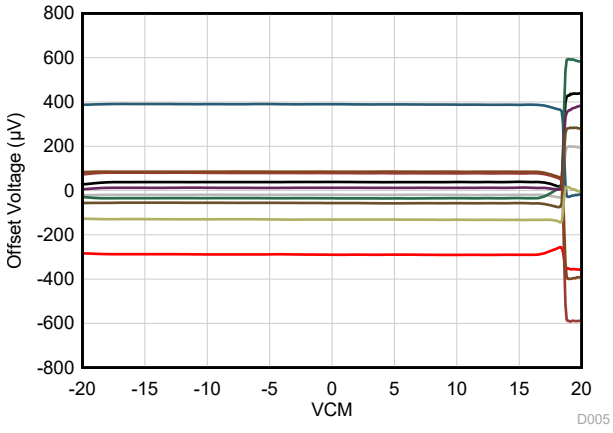
V_{CM} = V+

Figure 6-3. Offset Voltage vs Temperature



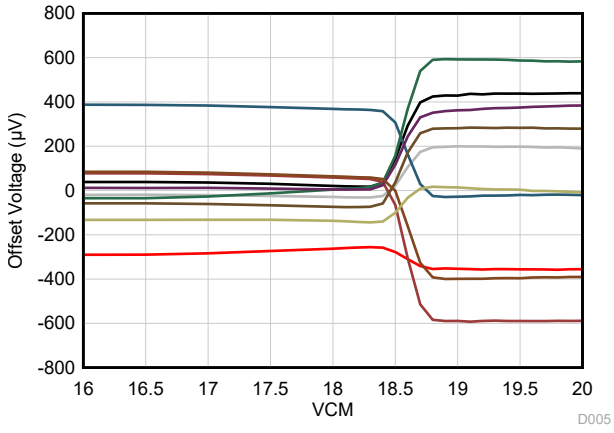
V_{CM} = V–

Figure 6-4. Offset Voltage vs Temperature



T_A = 25°C

Figure 6-5. Offset Voltage vs Common-Mode Voltage



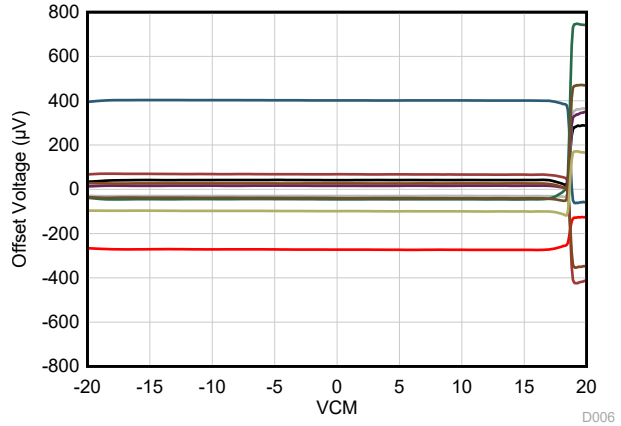
T_A = 25°C

Figure 6-6. Offset Voltage vs Common-Mode Voltage (Transition Region)

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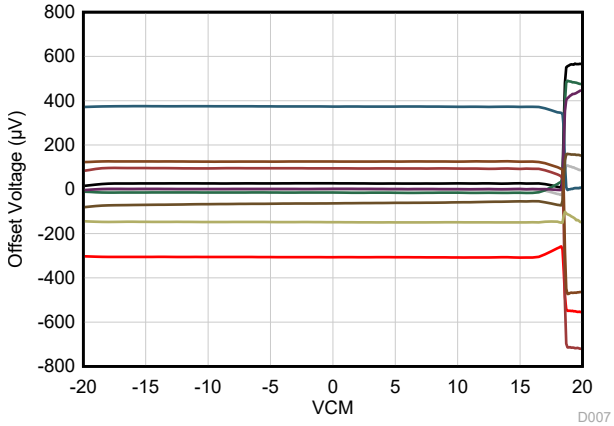
6.6 Typical Characteristics (continued)

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)



T_A = 125°C

Figure 6-7. Offset Voltage vs Common-Mode Voltage



T_A = –40°C

Figure 6-8. Offset Voltage vs Common-Mode Voltage

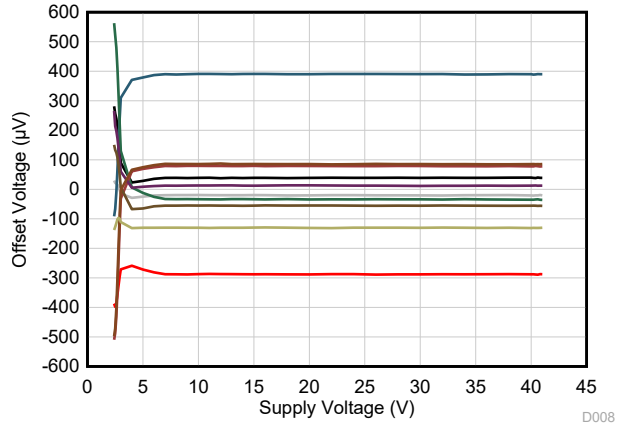
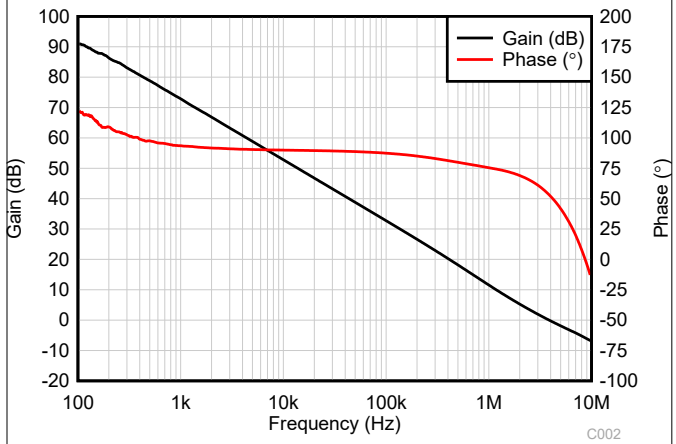


Figure 6-9. Offset Voltage vs Power Supply



C_L = 20 pF

Figure 6-10. Open-Loop Gain and Phase vs Frequency

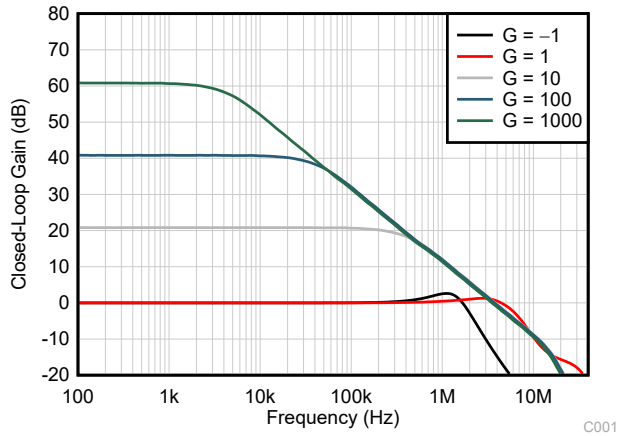


Figure 6-11. Closed-Loop Gain vs Frequency

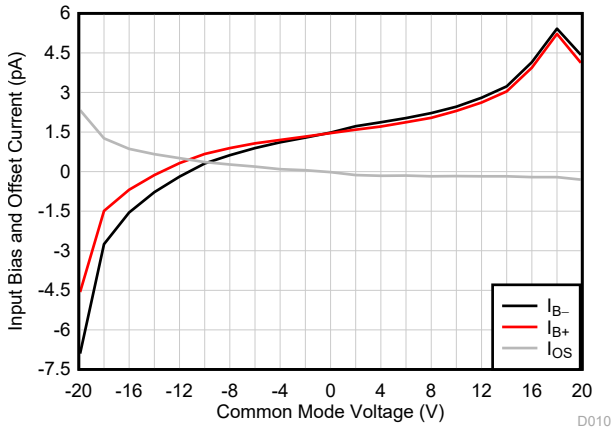


Figure 6-12. Input Bias Current vs Common-Mode Voltage

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6.6 Typical Characteristics (continued)

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)

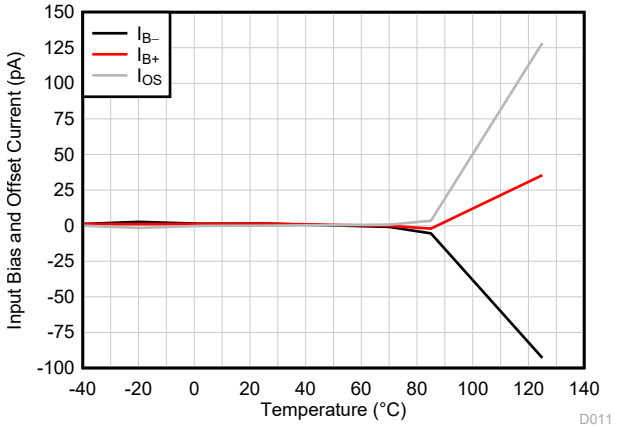


Figure 6-13. Input Bias Current vs Temperature

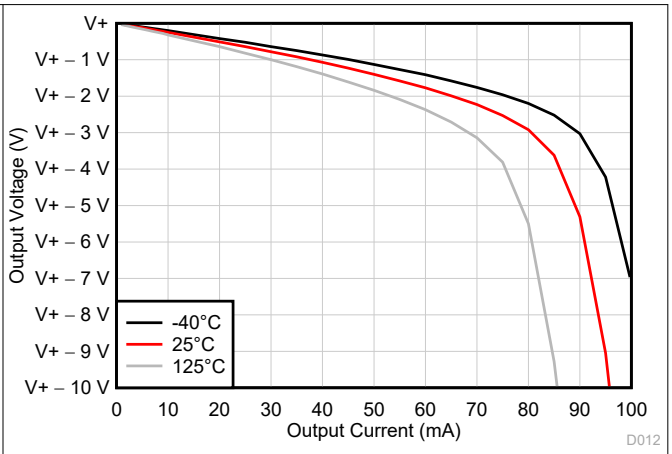


Figure 6-14. Output Voltage Swing vs Output Current (Sourcing)

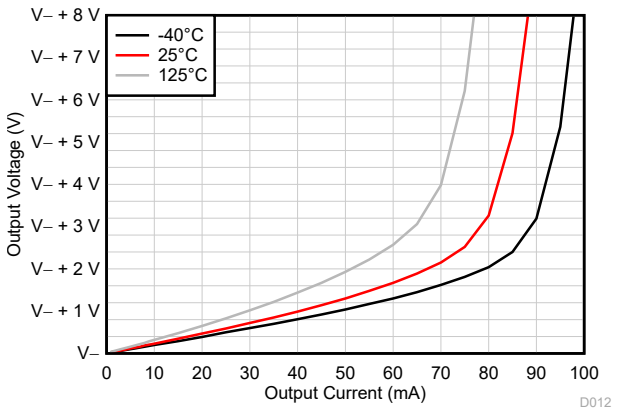


Figure 6-15. Output Voltage Swing vs Output Current (Sinking)

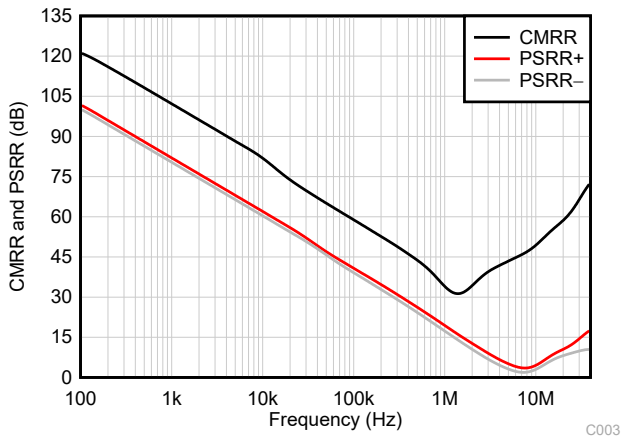
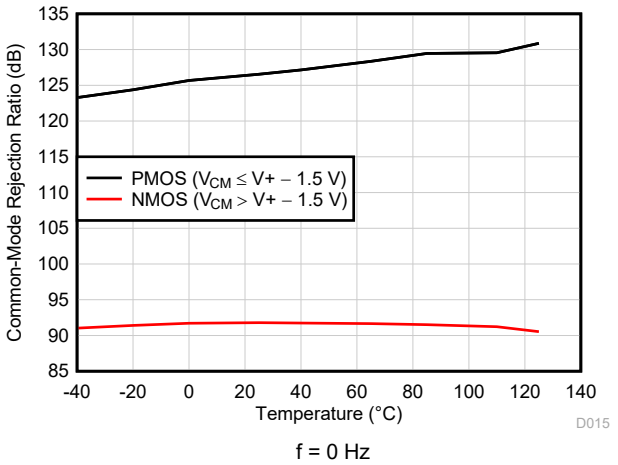
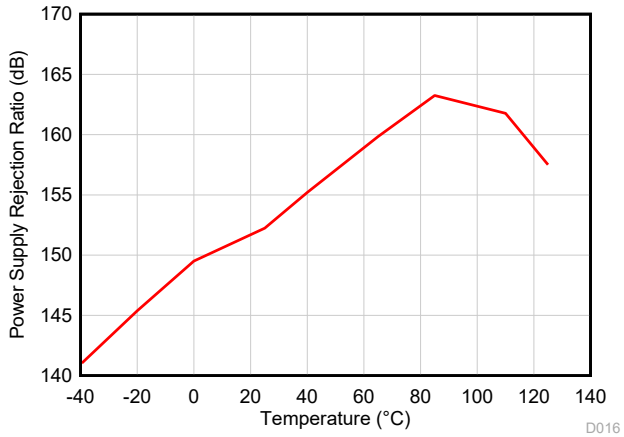


Figure 6-16. CMRR and PSRR vs Frequency



f = 0 Hz

Figure 6-17. CMRR vs Temperature (dB)



f = 0 Hz

Figure 6-18. PSRR vs Temperature (dB)

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6.6 Typical Characteristics (continued)

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)

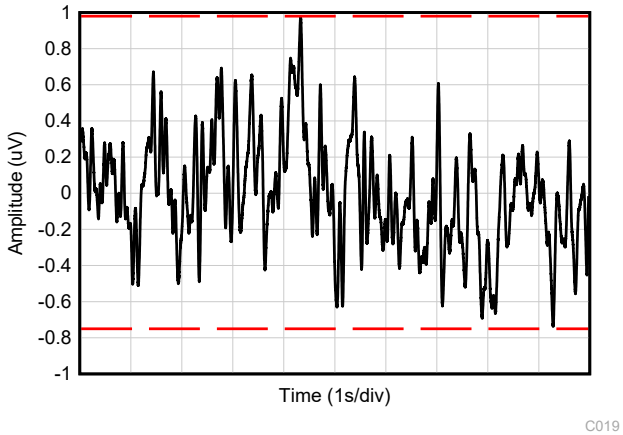


Figure 6-19. 0.1-Hz to 10-Hz Noise

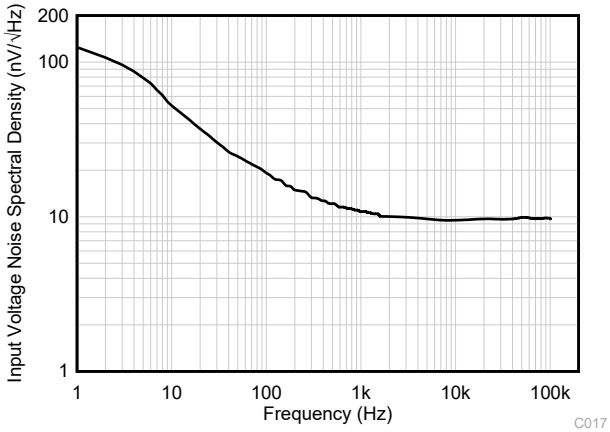
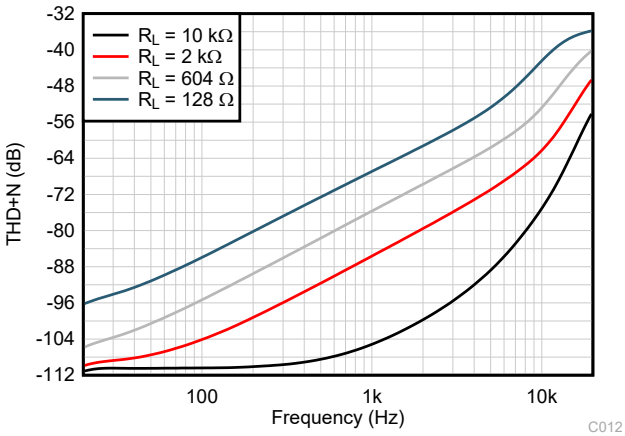
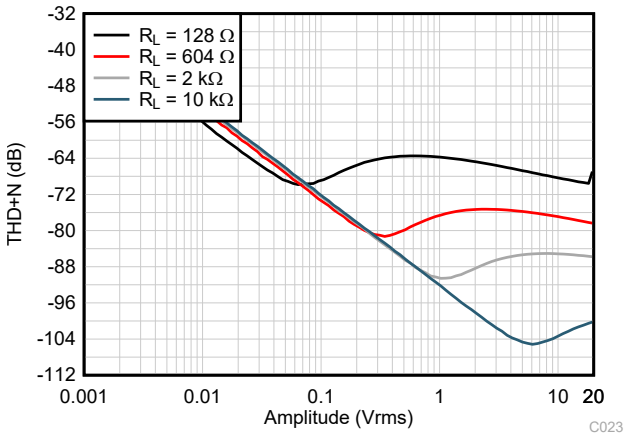


Figure 6-20. Input Voltage Noise Spectral Density vs Frequency



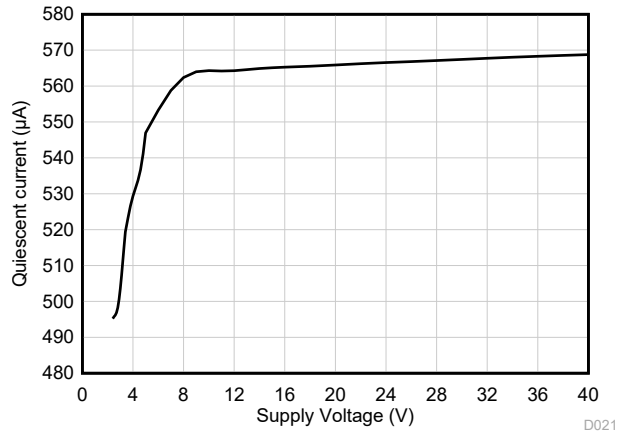
BW = 80 kHz, V_{OUT} = 1 V_{RMS}

Figure 6-21. THD+N Ratio vs Frequency



BW = 80 kHz, f = 1 kHz

Figure 6-22. THD+N vs Output Amplitude



V_{CM} = V–

Figure 6-23. Quiescent Current vs Supply Voltage

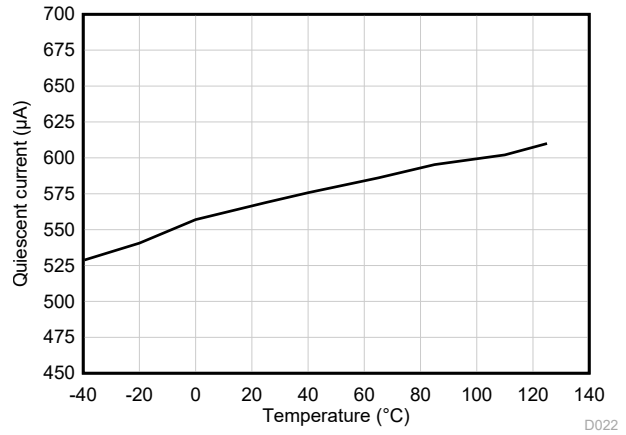


Figure 6-24. Quiescent Current vs Temperature

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6.6 Typical Characteristics (continued)

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)

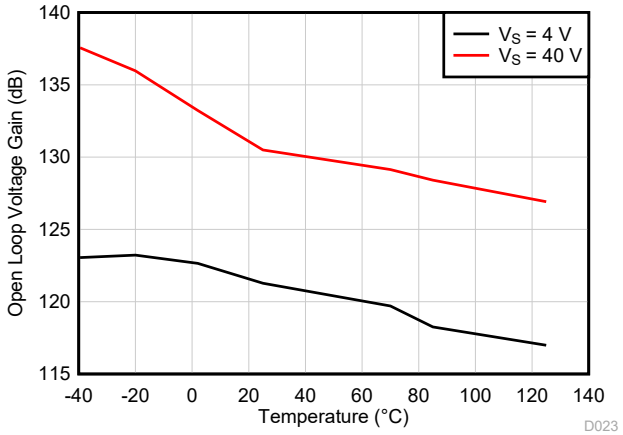


Figure 6-25. Open-Loop Voltage Gain vs Temperature (dB)

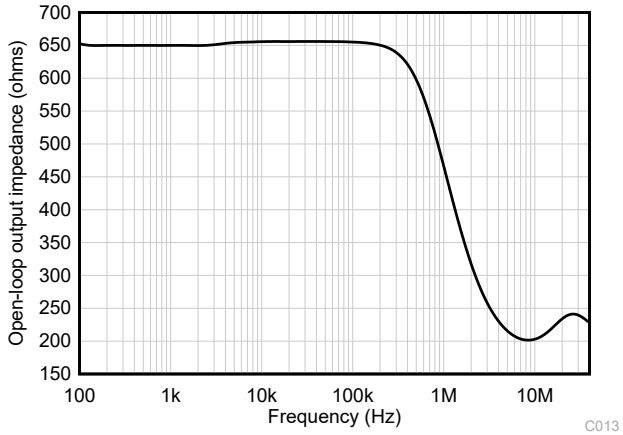
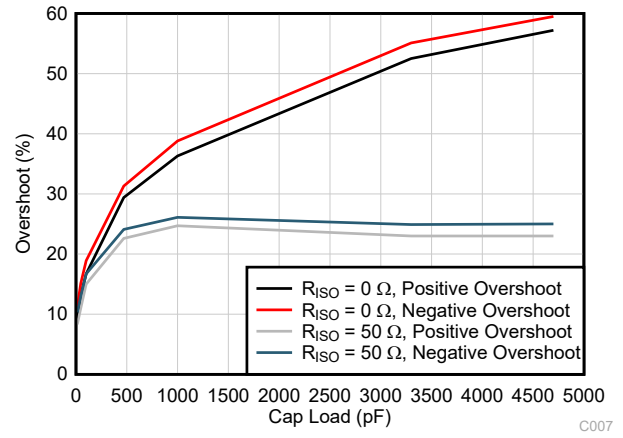
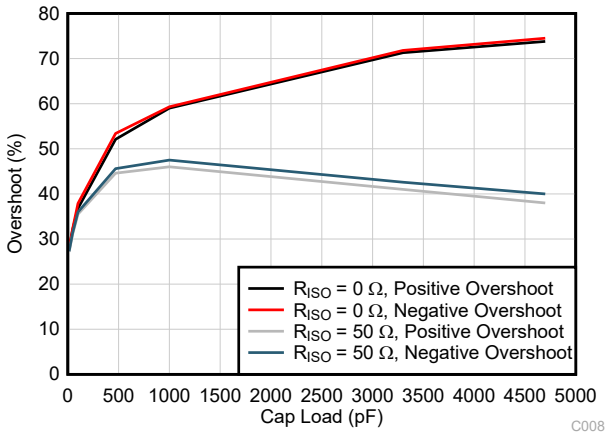


Figure 6-26. Open-Loop Output Impedance vs Frequency



G = –1, 10-mV output step

Figure 6-27. Small-Signal Overshoot vs Capacitive Load



G = 1, 10-mV output step

Figure 6-28. Small-Signal Overshoot vs Capacitive Load

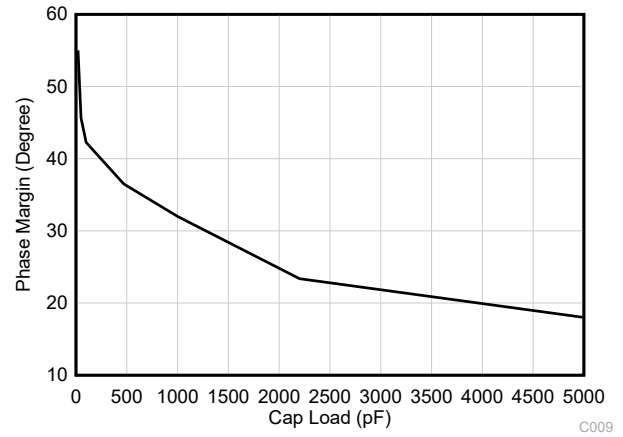
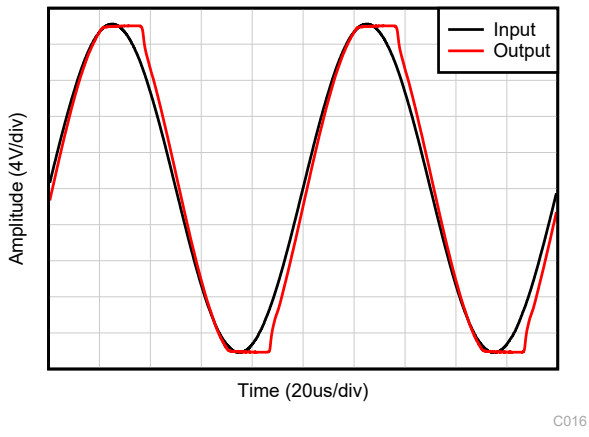


Figure 6-29. Phase Margin vs Capacitive Load



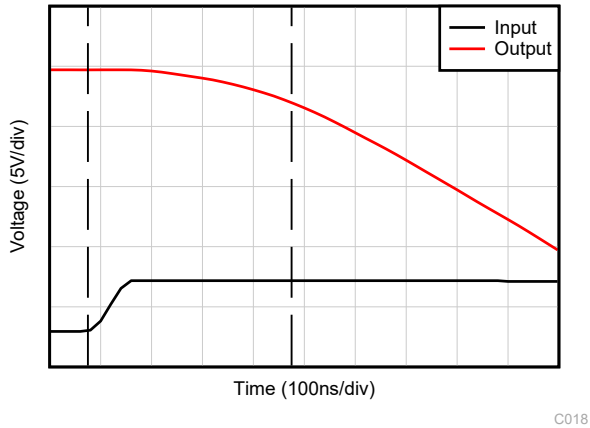
V_{IN} = ±20 V; V_S = V_{OUT} = ±17 V

Figure 6-30. No Phase Reversal

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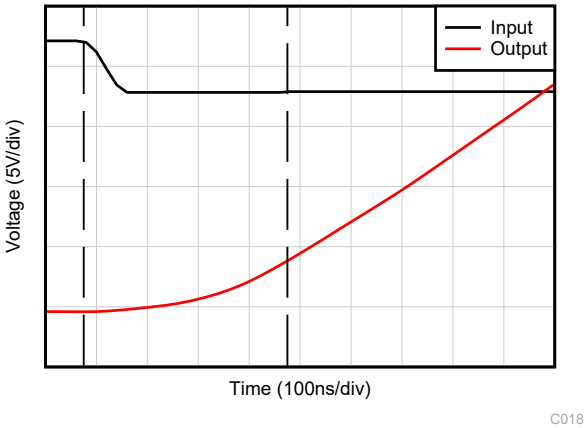
6.6 Typical Characteristics (continued)

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)



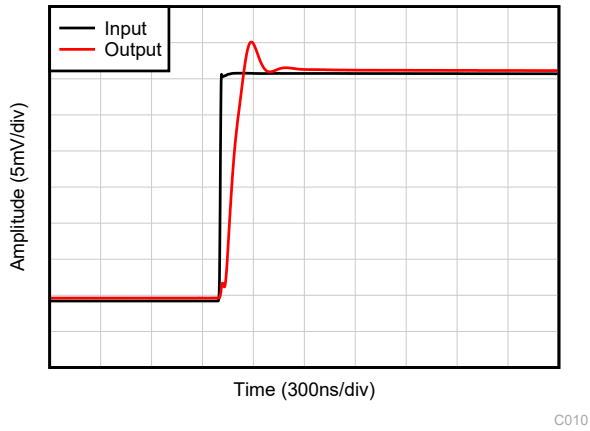
G = –10

Figure 6-31. Positive Overload Recovery



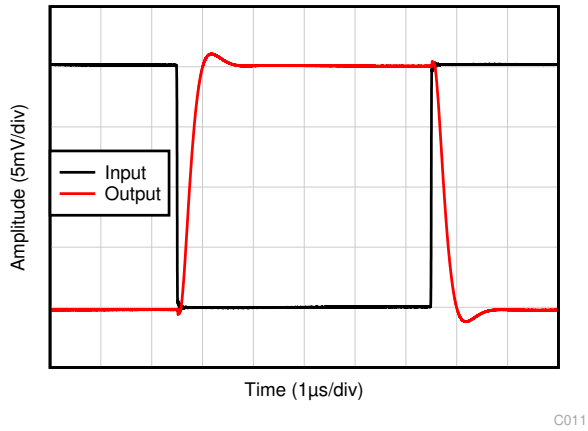
G = –10

Figure 6-32. Negative Overload Recovery



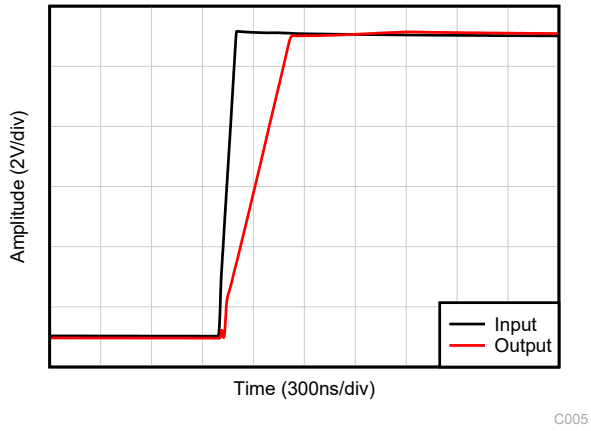
C_L = 20 pF, G = 1, 20-mV step response

Figure 6-33. Small-Signal Step Response, Rising



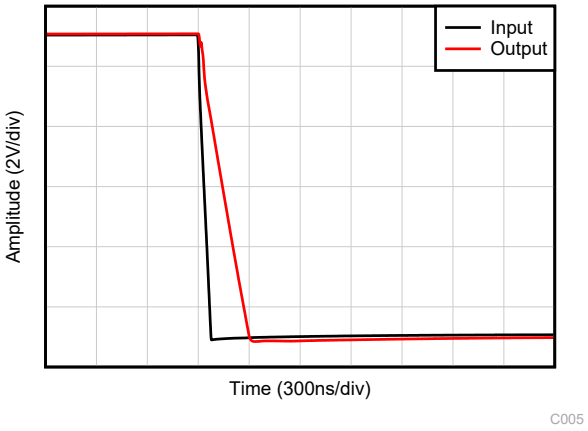
C_L = 20 pF, G = -1, 20-mV step response

Figure 6-34. Small-Signal Step Response



C_L = 20 pF, G = 1

Figure 6-35. Large-Signal Step Response (Rising)



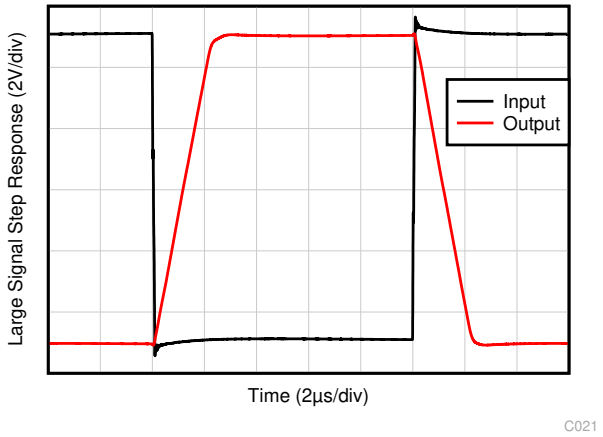
C_L = 20 pF, G = 1

Figure 6-36. Large-Signal Step Response (Falling)

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6.6 Typical Characteristics (continued)

at T_A = 25°C, V_S = ±20 V, V_{CM} = V_S / 2, R_{LOAD} = 10 kΩ connected to V_S / 2, and C_L = 10 pF (unless otherwise noted)



C_L = 20 pF, G = –1

Figure 6-37. Large-Signal Step Response

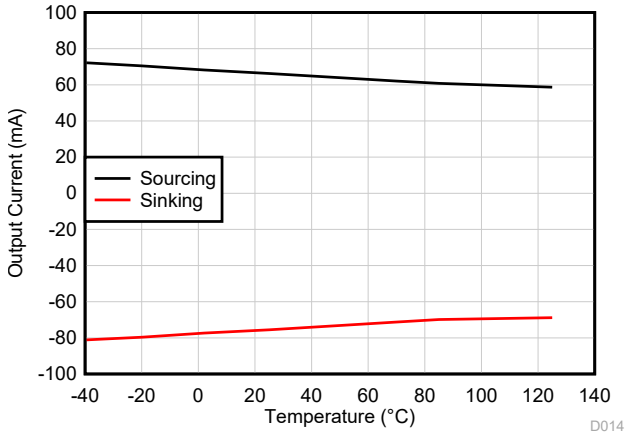


Figure 6-38. Short-Circuit Current vs Temperature

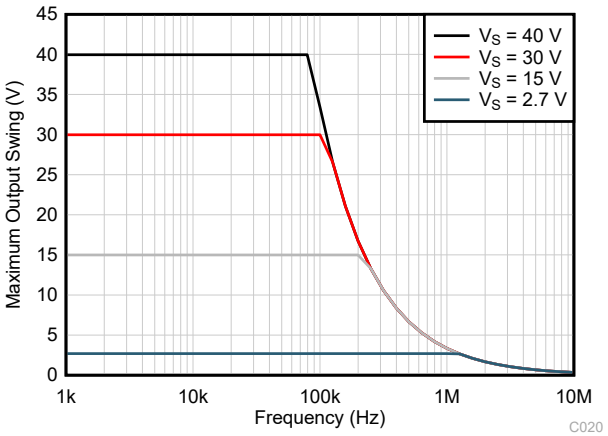


Figure 6-39. Maximum Output Voltage vs Frequency

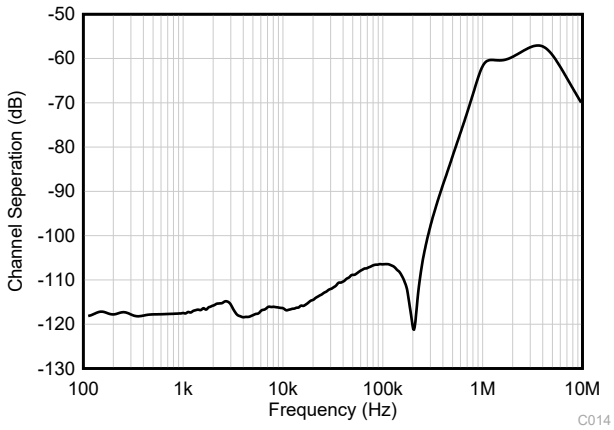


Figure 6-40. Channel Separation vs Frequency

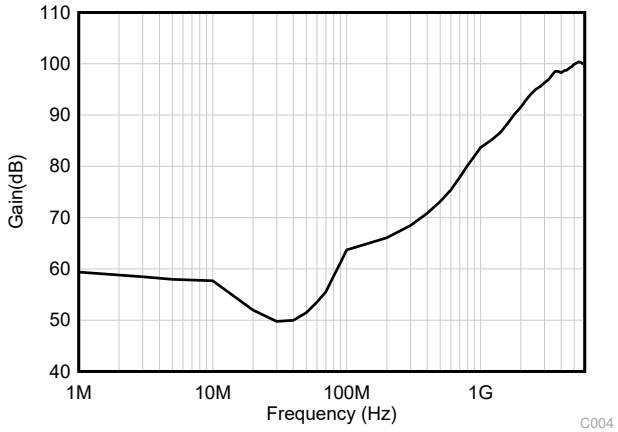


Figure 6-41. EMIRR (Electromagnetic Interference Rejection Ratio) at Inputs vs Frequency

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7 Detailed Description

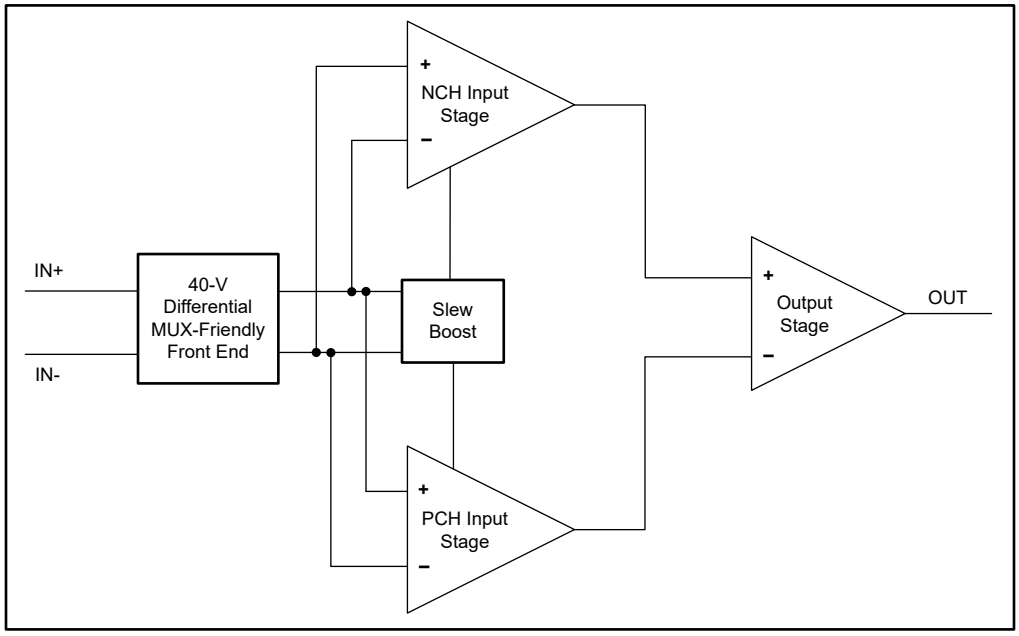
7.1 Overview

The OPA4H199-SEP is a new 40-V general purpose operational amplifier.

This device offers excellent DC precision and AC performance, including rail-to-rail input/output, low offset (±125 µV, typ), low offset drift (±0.3 µV/°C, typ), and 4.5-MHz bandwidth.

Unique features, such as differential and common-mode input-voltage range to the supply rail, high output current (±75 mA) and high slew rate (21 V/µs), make the OPA4H199-SEP a robust, high-performance operational amplifier for high-voltage space applications.

7.2 Functional Block Diagram



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7.3 Feature Description

7.3.1 Input Protection Circuitry

The OPA4H199-SEP uses a unique input architecture to eliminate the requirement for input protection diodes but still provides robust input protection under transient conditions. Figure 7-1 shows conventional input diode protection schemes that are activated by fast transient step responses and introduce signal distortion and settling time delays because of alternate current paths, as shown in Figure 7-2. For low-gain circuits, these fast-ramping input signals forward-bias back-to-back diodes, causing an increase in input current and resulting in extended settling time.

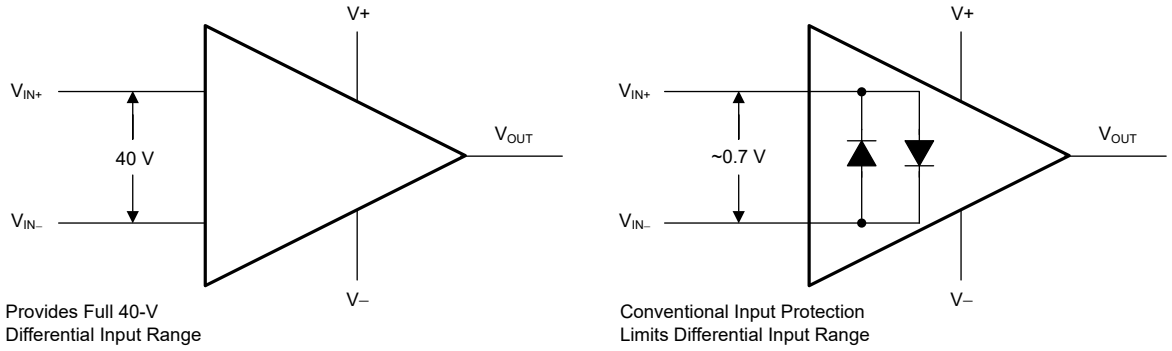


Figure 7-1. OPA4H199-SEP Input Protection Does Not Limit Differential Input Capability

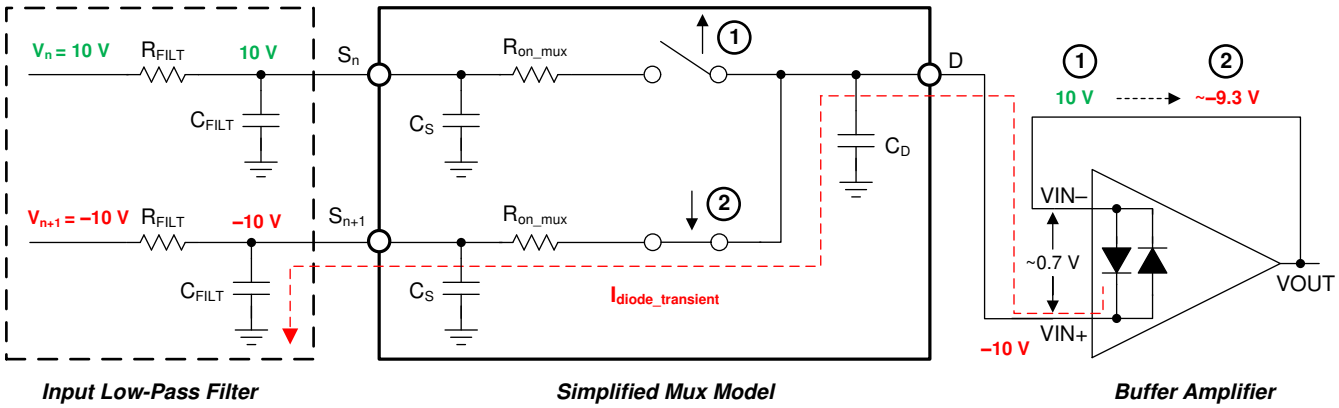


Figure 7-2. Back-to-Back Diodes Create Settling Issues

The OPA4H199-SEP provides a true high-impedance differential input capability for high-voltage applications using a patented input protection architecture that does not introduce additional signal distortion or delayed settling time, making the device an excellent choice as op amp for multichannel, high-switched, input applications. The OPA4H199-SEP tolerates a maximum differential swing (voltage between inverting and non-inverting pins of the op amp) of up to 40 V, making the device good for use as a comparator or in applications with fast-ramping input signals such as data-acquisition systems; see the TI TechNote *MUX-Friendly Precision Operational Amplifiers* for more information.

7.3.2 EMI Rejection

The OPA4H199-SEP uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the OPA4H199-SEP benefits from these design improvements. Texas Instruments has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. Figure 7-3 shows the results of this testing on the OPA4H199-SEP. Table 7-1 shows the EMIRR IN+ values for the OPA4H199-SEP at particular frequencies commonly encountered in real-world applications. The

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EMI Rejection Ratio of Operational Amplifiers application report contains detailed information on the topic of EMIRR performance as it relates to op amps and is available for download from www.ti.com.

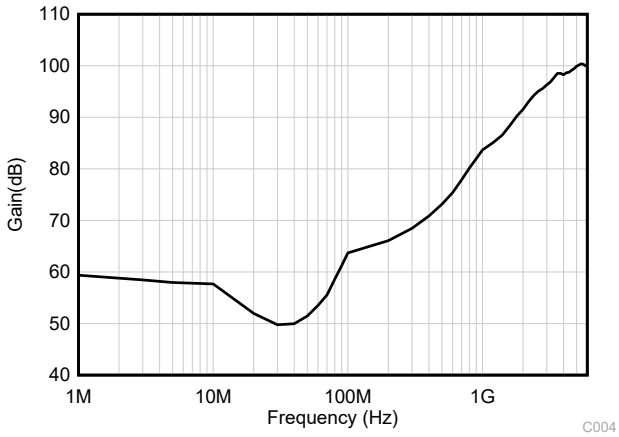


Figure 7-3. EMIRR Testing

Table 7-1. OPA4H199-SEP EMIRR IN+ for Frequencies of Interest

FREQUENCY	APPLICATION OR ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite, space operation, weather, radar, ultra-high frequency (UHF) applications	73.2 dB
900 MHz	Global system for mobile communications (GSM) applications, radio communication, navigation, GPS (to 1.6 GHz), GSM, aeronautical mobile, UHF applications	82.5 dB
1.8 GHz	GSM applications, mobile personal communications, broadband, satellite, L-band (1 GHz to 2 GHz)	89.7 dB
2.4 GHz	802.11b, 802.11g, 802.11n, Bluetooth®, mobile personal communications, industrial, scientific and medical (ISM) radio band, amateur radio and satellite, S-band (2 GHz to 4 GHz)	93.9 dB
3.6 GHz	Radiolocation, aero communication and navigation, satellite, mobile, S-band	95.7 dB
5 GHz	802.11a, 802.11n, aero communication and navigation, mobile communication, space and satellite operation, C-band (4 GHz to 8 GHz)	98.0 dB

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7.3.3 Thermal Protection

The internal power dissipation of any amplifier causes the internal (junction) temperature to rise. This phenomenon is called *self heating*. The absolute maximum junction temperature of the OPA4H199-SEP is 150°C. Exceeding this temperature causes damage to the device. The OPA4H199-SEP has a thermal protection feature that reduces damage from self heating. The protection works by monitoring the temperature of the device and turning off the op amp output drive for temperatures above 170°C. Figure 7-4 shows an application example for the OPA4H199-SEP that has significant self heating because of the power dissipation (0.81 W). Thermal calculations indicate that for an ambient temperature of 65°C, the device junction temperature can reach 177°C. The actual device, however, turns off the output drive to recover towards a safe junction temperature. Figure 7-4 shows how the circuit behaves during thermal protection. During normal operation, the device acts as a buffer so the output is 3 V. When self heating causes the device junction temperature to increase above the internal limit, the thermal protection forces the output to a high-impedance state and the output is pulled to ground through resistor R_L. If the condition that caused excessive power dissipation is not removed, then the amplifier can oscillate between a shutdown and enabled state until the output fault is corrected.

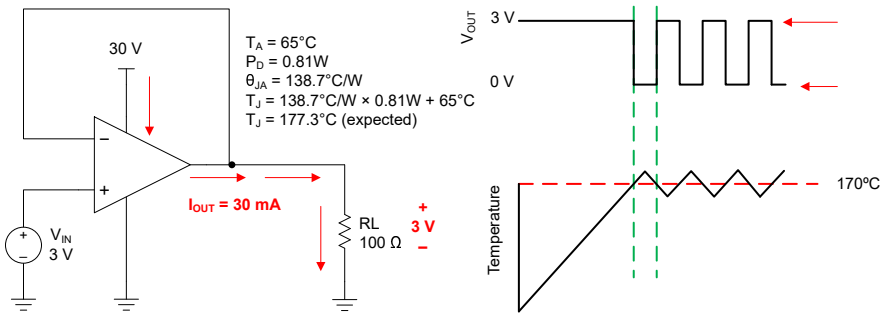


Figure 7-4. Thermal Protection

If the device continues to operate at high junction temperatures with high output power over a long period of time, regardless if the device is or is not entering thermal shutdown, the thermal dissipation of the device can slowly degrade performance of the device and eventually cause catastrophic destruction. Designers must be careful to limit output power of the device at high temperatures, or control ambient and junction temperatures under high output power conditions.

7.3.4 Capacitive Load and Stability

The OPA4H199-SEP features a resistive output stage capable of driving moderate capacitive loads, and by leveraging an isolation resistor, the device can easily be configured to drive large capacitive loads. Increasing the gain enhances the ability of the amplifier to drive greater capacitive loads; see Figure 7-5 and Figure 7-6. The particular op amp circuit configuration, layout, gain, and output loading are some of the factors to consider when establishing whether an amplifier can be stable in operation.

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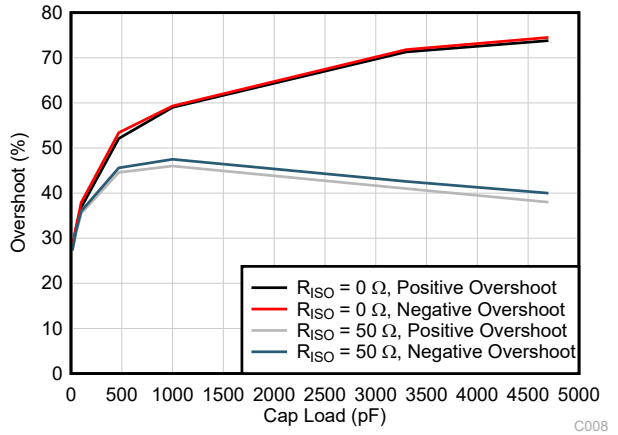


Figure 7-5. Small-Signal Overshoot vs Capacitive Load (10-mV Output Step, G = 1)

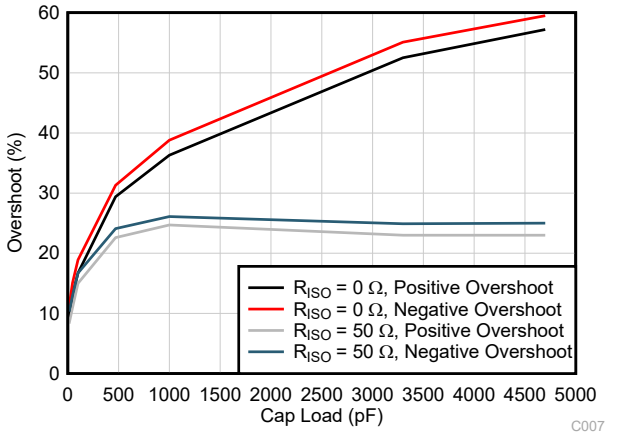


Figure 7-6. Small-Signal Overshoot vs Capacitive Load (10-mV Output Step, G = –1)

For additional drive capability in unity-gain configurations, improve capacitive load drive by inserting a small resistor, R_{ISO}, in series with the output, as shown in Figure 7-7. This resistor significantly reduces ringing and maintains DC performance for purely capacitive loads. However, if a resistive load is in parallel with the capacitive load, then a voltage divider is created, thus introducing a gain error at the output and slightly reducing the output swing. The error introduced is proportional to the ratio R_{ISO} / R_L, and is generally negligible at low output levels. A high capacitive load drive makes the OPA4H199-SEP an excellent choice for applications such as reference buffers, MOSFET gate drives, and cable-shield drives. The circuit shown in Figure 7-7 uses an isolation resistor, R_{ISO}, to stabilize the output of an op amp. R_{ISO} modifies the open-loop gain of the system for increased phase margin.

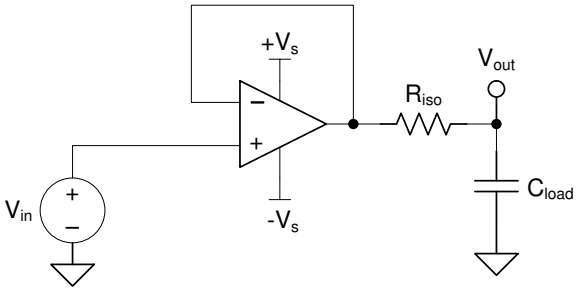


Figure 7-7. Extending Capacitive Load Drive With the OPA4H199-SEP

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7.3.5 Common-Mode Voltage Range

The OPA4H199-SEP is a 40-V, true rail-to-rail input operational amplifier with an input common-mode range that extends 100 mV beyond either supply rail. This wide range is achieved with paralleled complementary N-channel and P-channel differential input pairs, as shown in Figure 7-8. The N-channel pair is active for input voltages close to the positive rail, typically (V+) – 1 V to 100 mV above the positive supply. The P-channel pair is active for inputs from 100 mV below the negative supply to approximately (V+) – 2 V. There is a small transition region, typically (V+) – 2 V to (V+) – 1 V in which both input pairs are on. This transition region can vary modestly with process variation, and within this region PSRR, CMRR, offset voltage, offset drift, noise, and THD performance can be degraded compared to operation outside this region.

Figure 6-5 shows this transition region for a typical device in terms of input voltage offset in more detail.

For more information on common-mode voltage range and PMOS/NMOS pair interaction, see *Op Amps With Complementary-Pair Input Stages* application note.

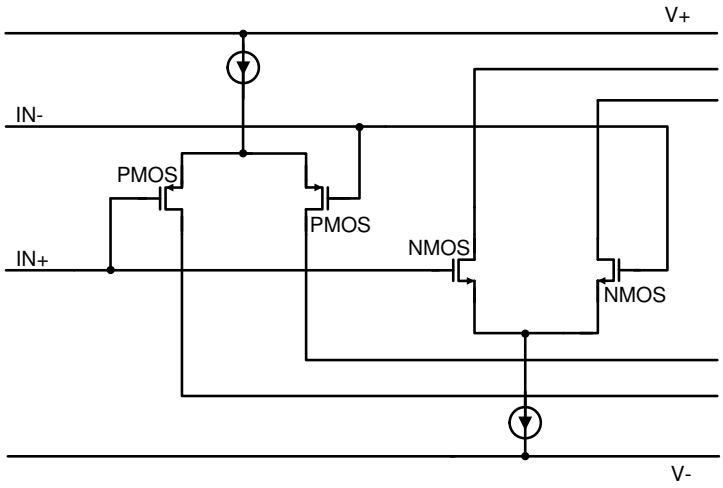


Figure 7-8. Rail-to-Rail Input Stage

7.3.6 Phase Reversal Protection

The OPA4H199-SEP family has internal phase-reversal protection. Many op amps exhibit phase reversal when the input is driven beyond the linear common-mode range. This condition is most often encountered in non-inverting circuits when the input is driven beyond the specified common-mode voltage range, causing the output to reverse into the opposite rail. The OPA4H199-SEP is a rail-to-rail input op amp; therefore, the common-mode range can extend beyond the rails. Input signals beyond the rails do not cause phase reversal; instead, the output limits into the appropriate rail. This performance is shown in Figure 7-9. For more information on phase reversal, see *Op Amps With Complementary-Pair Input Stages* application note.

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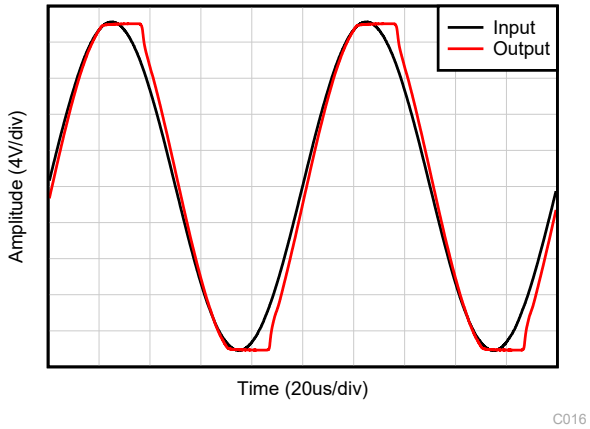


Figure 7-9. No Phase Reversal

7.3.7 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress (EOS). These questions tend to focus on the device inputs, but can involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

Having a good understanding of this basic ESD circuitry and the relevance to an electrical overstress event is helpful. Figure 7-10 shows an illustration of the ESD circuits contained in the OPA4H199-SEP (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where the diodes meet at an absorption device or the power-supply ESD cell, internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.

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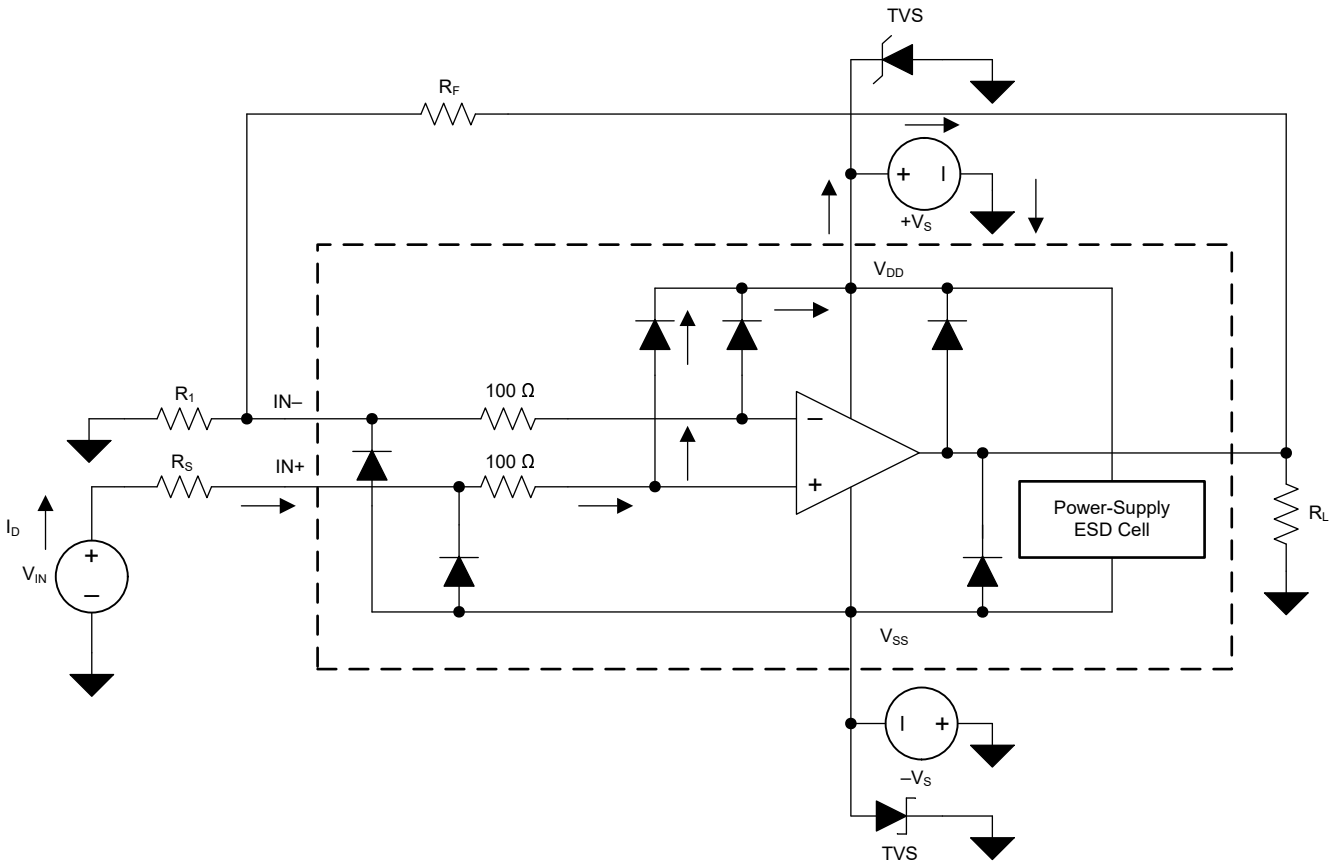


Figure 7-10. Equivalent Internal ESD Circuitry Relative to a Typical Circuit Application

An ESD event is very short in duration and very high voltage (for example; 1 kV, 100 ns), whereas an EOS event is long duration and lower voltage (for example; 50 V, 100 ms). The ESD diodes are designed for out-of-circuit ESD protection (that is, during assembly, test, and storage of the device before being soldered to the PCB). During an ESD event, the ESD signal is passed through the ESD steering diodes to an absorption circuit (labeled ESD power-supply circuit). The ESD absorption circuit clamps the supplies to a safe level.

Although this behavior is necessary for out-of-circuit protection, excessive current and damage is caused if activated in-circuit. A transient voltage suppressors (TVS) can be used to prevent against damage caused by turning on the ESD absorption circuit during an in-circuit ESD event. Using the appropriate current limiting resistors and TVS diodes allows for the use of device ESD diodes to protect against EOS events.

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7.3.8 Overload Recovery

Overload recovery is defined as the time required for the op amp output to recover from a saturated state to a linear state. The output devices of the op amp enter a saturation region when the output voltage exceeds the rated operating voltage, either due to the high input voltage or the high gain. After the device enters the saturation region, the charge carriers in the output devices require time to return back to the linear state. After the charge carriers return back to the linear state, the device begins to slew at the specified slew rate. Thus, the propagation delay in case of an overload condition is the sum of the overload recovery time and the slew time. The overload recovery time for the OPA4H199-SEP is approximately 400 ns.

7.3.9 Typical Specifications and Distributions

Designers often have questions about a typical specification of an amplifier to design a more robust circuit. Due to natural variation in process technology and manufacturing procedures, every specification of an amplifier exhibits some amount of deviation from the proper value, like an input offset voltage of the amplifier. These deviations often follow *Gaussian* (bell curve), or *normal* distributions, and circuit designers can leverage this information to guardband their system, even when there is not a minimum or maximum specification in *Section 6.5*.

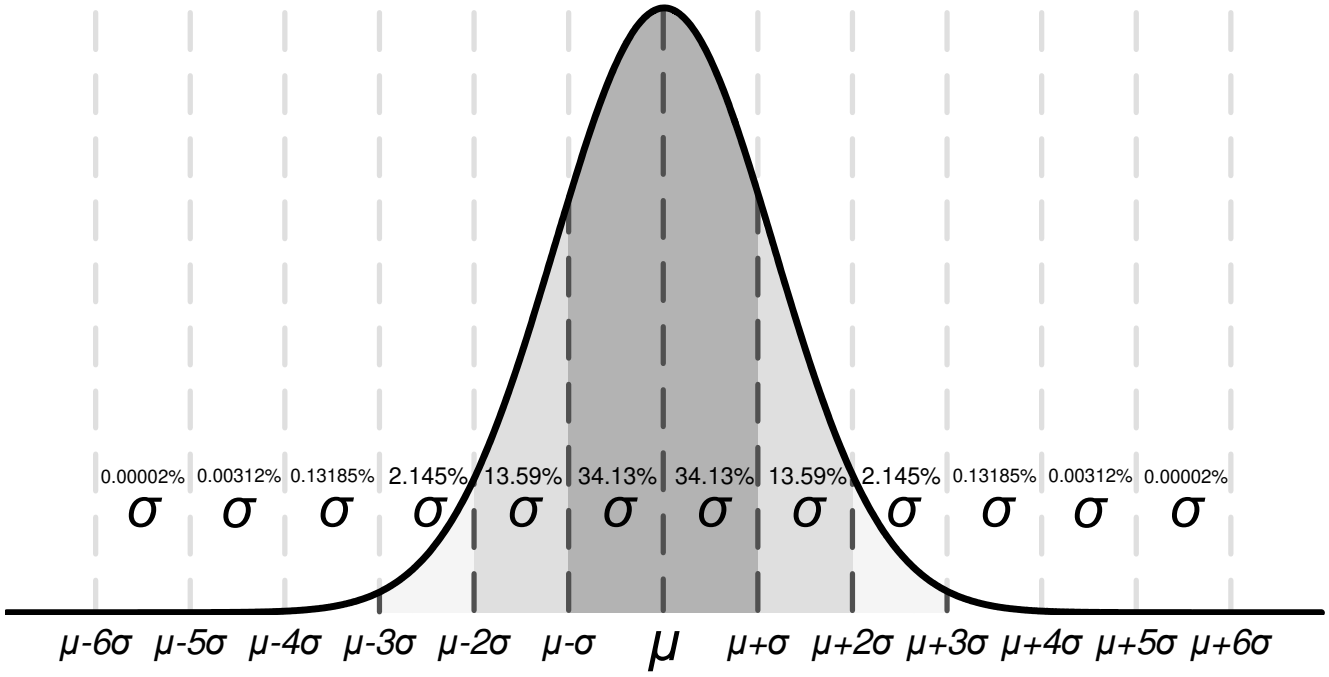


Figure 7-11. Ideal Gaussian Distribution

Figure 7-11 shows an example distribution, where μ, or *mu*, is the mean of the distribution, and where σ, or *sigma*, is the standard deviation of a system. For a specification that exhibits this kind of distribution, approximately two-thirds (68.26%) of all units can be expected to have a value within one standard deviation, or one sigma, of the mean (from $\mu - \sigma$ to $\mu + \sigma$).

Depending on the specification, values listed in the *typical* column of the *Section 6.5* are represented in different ways. As a general rule of thumb, if a specification naturally has a nonzero mean (for example, like gain bandwidth), then the typical value is equal to the mean (μ). However, if a specification naturally has a mean near zero (like input offset voltage), then the typical value is equal to the mean plus one standard deviation (μ + σ) to most accurately represent the typical value.

You can use this chart to calculate approximate probability of a specification in a unit; for example, for OPA4H199-SEP, the typical input voltage offset is 125 μV, so 68.2% of all OPA4H199-SEP devices are expected to have an offset from –125 μV to 125 μV. At 4 σ (±500 μV), 99.9937% of the distribution has an offset voltage

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less than ±500 µV, which means 0.0063% of the population is outside of these limits, which corresponds to about 1 in 15,873 units.

TI verifes specifications with a value in the minimum or maximum column, and units outside these limits are removed from production material. For example, the OPA4H199-SEP family has a maximum offset voltage of 895 µV at 25°C, and even though this corresponds to more than 5 σ (≈1 in 1.7 million units), which is extremely unlikely, TI specifies that any unit with larger offset than 895 µV is removed from production material.

For specifications with no value in the minimum or maximum column, consider selecting a sigma value of sufficient guardband for your application, and design worst-case conditions using this value. For example, the 6-σ value corresponds to about 1 in 500 million units, which is an extremely unlikely chance, and can be an option as a wide guardband to design a system around. In this case, the OPA4H199-SEP family does not have a maximum or minimum for offset voltage drift, but based on Figure 6-2 and the typical value of 0.3 µV/°C in the *Section 6.5*, the calcuation results in a 6-σ value for offset voltage drift is about 1.8 µV/°C. When designing for worst-case system conditions, this value can be used to estimate the worst possible offset across temperature without having an actual minimum or maximum value.

However, process variation and adjustments over time can shift typical means and standard deviations, and unless there is a value in the minimum or maximum specification column, the performance of a device is not verified. This information must be used only to estimate the performance of a device.

7.4 Device Functional Modes

The OPA4H199-SEP has a single functional mode and is operational when the power-supply voltage is greater than 2.7 V (±1.35 V). The maximum power supply voltage for the OPA4H199-SEP is 40 V (±20 V).

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8 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

The OPA4H199-SEP family offers excellent DC precision and AC performance. These devices operate up to 40-V supply rails and offer true rail-to-rail input/output, low offset voltage and offset voltage drift, as well as 4.5-MHz bandwidth and high output drive. These features make the OPA4H199-SEP a robust, high-performance operational amplifier for high-voltage industrial applications.

8.2 Typical Applications

8.2.1 Low-Side Current Measurement

Figure 8-1 shows the OPA4H199-SEP configured in a low-side current sensing application. For a full analysis of the circuit shown in Figure 8-1 including theory, calculations, simulations, and measured data, see TI Precision Design TIPD129, *0-A to 1-A Single-Supply Low-Side Current-Sensing Solution*.

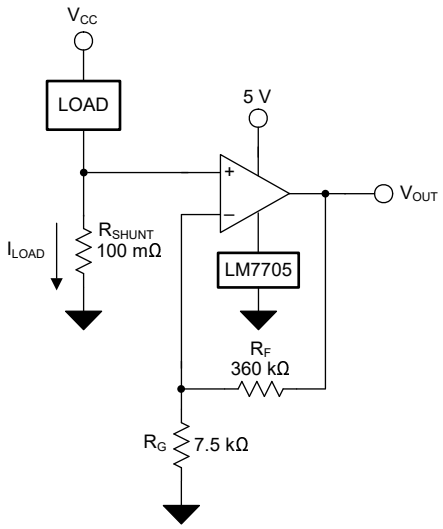


Figure 8-1. OPA4H199-SEP in a Low-Side, Current-Sensing Application

8.2.1.1 Design Requirements

The design requirements for this design are:

- Load current: 0 A to 1 A
- Output voltage: 4.9 V
- Maximum shunt voltage: 100 mV

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8.2.1.2 Detailed Design Procedure

The transfer function of the circuit in Figure 8-1 is given in Equation 1.

$$V_{OUT} = I_{LOAD} \times R_{SHUNT} \times Gain \quad (1)$$

The load current (I_{LOAD}) produces a voltage drop across the shunt resistor (R_{SHUNT}). The load current is set from 0 A to 1 A. To keep the shunt voltage below 100 mV at maximum load current, the largest shunt resistor is defined using Equation 2.

$$R_{SHUNT} = \frac{V_{SHUNT_MAX}}{I_{LOAD_MAX}} = \frac{100\ mV}{1\ A} = 100\ m\Omega \quad (2)$$

Using Equation 2, R_{SHUNT} is calculated to be 100 mΩ. The voltage drop produced by I_{LOAD} and R_{SHUNT} is amplified by the OPA4H199-SEP to produce an output voltage of 0 V to 4.9 V. The gain needed by the OPA4H199-SEP to produce the necessary output voltage is calculated using Equation 3.

$$Gain = \frac{\left(V_{OUT_MAX} - V_{OUT_{MIN}}\right)}{\left(V_{IN_MAX} - V_{IN_MIN}\right)} \quad (3)$$

Using Equation 3, the required gain is calculated to be 49 V/V, which is set with resistors R_F and R_G. Equation 4 is used to size the resistors, R_F and R_G, to set the gain of the OPA4H199-SEP to 49 V/V.

$$Gain = 1 + \frac{(R_F)}{(R_G)} \quad (4)$$

Choosing R_F as 360 kΩ, R_G is calculated to be 7.5 kΩ. R_F and R_G were chosen as 360 kΩ and 7.5 kΩ because they are standard value resistors that create a 49:1 ratio. Other resistors that create a 49:1 ratio can also be used. Figure 8-2 shows the measured transfer function of the circuit shown in Figure 8-1.

8.2.1.3 Application Curve

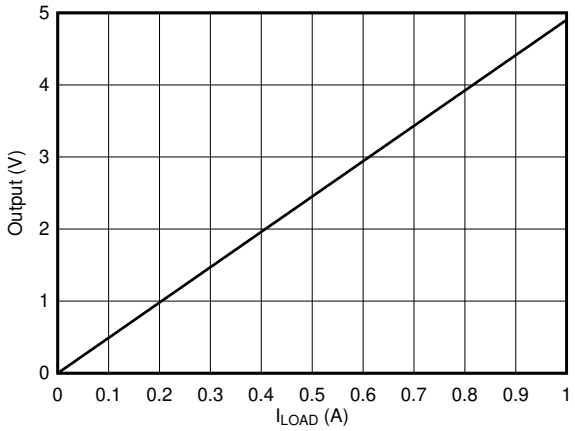


Figure 8-2. Low-Side, Current-Sense, Transfer Function

8.3 Power Supply Recommendations

The OPA4H199-SEP is specified for operation from 2.7 V to 40 V (±1.35 V to ±40 V); many specifications apply from –55°C to 125°C. Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in *Typical Characteristics*.

CAUTION

Supply voltages larger than 40 V can permanently damage the device; see *Section 6.1*.

Place 0.1-µF bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or high-impedance power supplies. For more detailed information on bypass capacitor placement, refer to *Layout*.

8.4 Layout

8.4.1 Layout Guidelines

For best operational performance of the device, use good PCB layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and op amp itself. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1-µF ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds paying attention to the flow of the ground current.
- To reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better as opposed to in parallel with the noisy trace.
- Place the external components as close to the device as possible. As illustrated in Figure 8-4, keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.
- Cleaning the PCB following board assembly is recommended for best performance.
- Any precision integrated circuit can experience performance shifts due to moisture ingress into the plastic package. Following any aqueous PCB cleaning process, baking the PCB assembly is recommended to remove moisture introduced into the device packaging during the cleaning process. A low temperature, post cleaning bake at 85°C for 30 minutes is sufficient for most circumstances.

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8.4.2 Layout Example

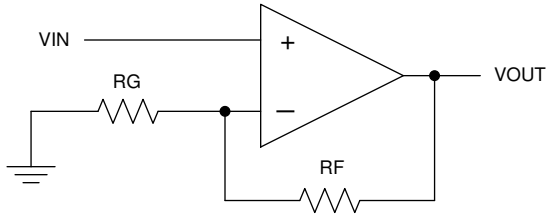


Figure 8-3. Schematic Representation

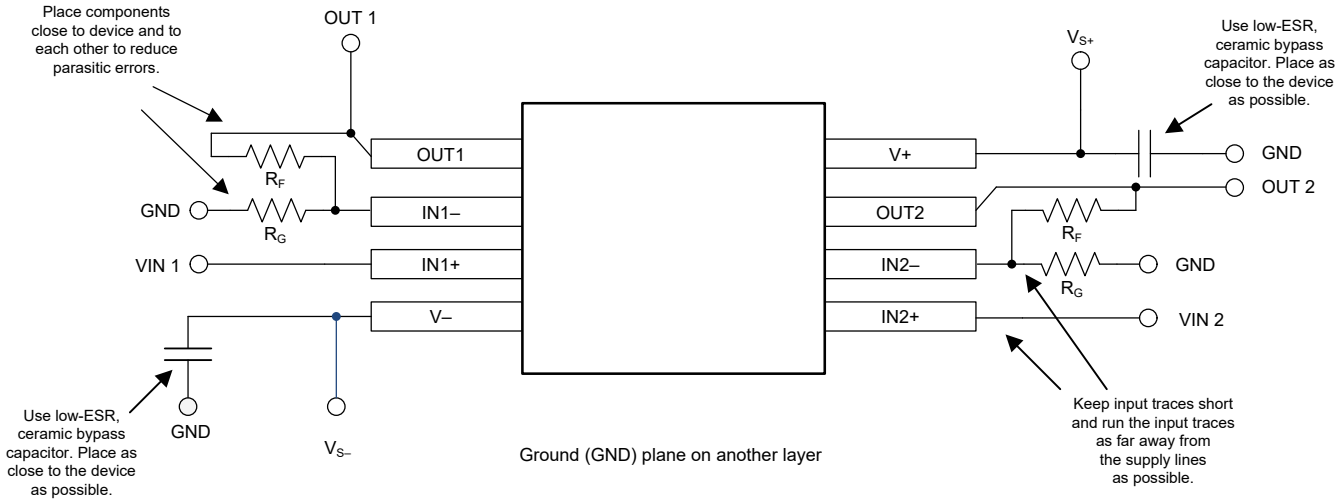


Figure 8-4. Operational Amplifier Board Layout for Noninverting Configuration

9 Device and Documentation Support

9.1 Device Support

9.1.1 Development Support

9.1.1.1 TINA-TI™ (Free Software Download)

TINA™ is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI is a free, fully-functional version of the TINA software, preloaded with a library of macro models in addition to a range of both passive and active models. TINA-TI provides all the conventional dc, transient, and frequency domain analysis of SPICE, as well as additional design capabilities.

Available as a free download from the Analog eLab Design Center, TINA-TI offers extensive post-processing capability that allows users to format results in a variety of ways. Virtual instruments offer the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

Note

These files require that either the TINA software (from DesignSoft™) or TINA-TI software be installed. Download the free TINA-TI software from the TINA-TI folder.

9.2 Documentation Support

9.2.1 Related Documentation

For related documentation, see the following:

Texas Instruments, *Analog Engineer's Circuit Cookbook: Amplifiers* solution guide.

Texas Instruments, *AN31 Amplifier Circuit Collection* application note.

Texas Instruments, *MUX-Friendly Precision Operational Amplifiers* application brief.

Texas Instruments, *EMI Rejection Ratio of Operational Amplifiers* application report.

Texas Instruments, *Op Amps With Complementary-Pair Input Stages* application note.

9.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

9.4 Support Resources

TI E2E™ support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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9.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

9.7 Glossary

TI Glossary — This glossary lists and explains terms, acronyms, and definitions.

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10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package | Pins	Package qty | Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
OPA4H199MDYYTSEP	Active	Production	SOT-23-THIN (DYY) | 14	250 | SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-55 to 125	4H199SEP
OPA4H199MDYYTSEP.A	Active	Production	SOT-23-THIN (DYY) | 14	250 | SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-55 to 125	4H199SEP
V62/21615-02XE	Active	Production	SOT-23-THIN (DYY) | 14	250 | SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	See OPA4H199MDYYTSEP	4H199SEP

(1) **Status:** For more details on status, see our product life cycle.

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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OTHER QUALIFIED VERSIONS OF OPA4H199-SEP :

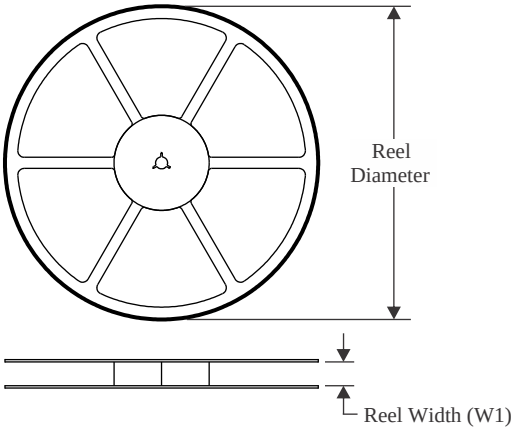
- Space : OPA4H199-SP

NOTE: Qualified Version Definitions:

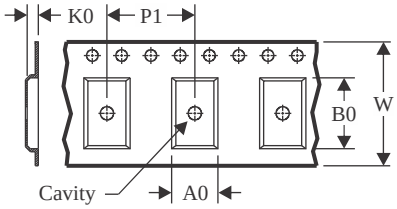
- Space - Radiation tolerant, ceramic packaging and qualified for use in Space-based application

TAPE AND REEL INFORMATION

REEL DIMENSIONS

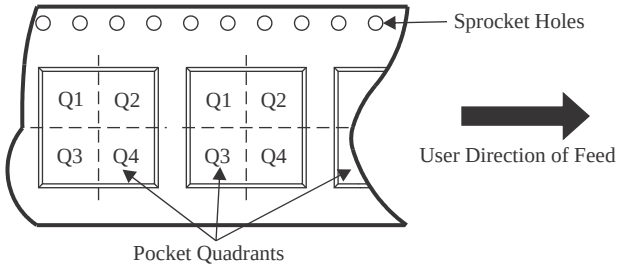


TAPE DIMENSIONS



A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

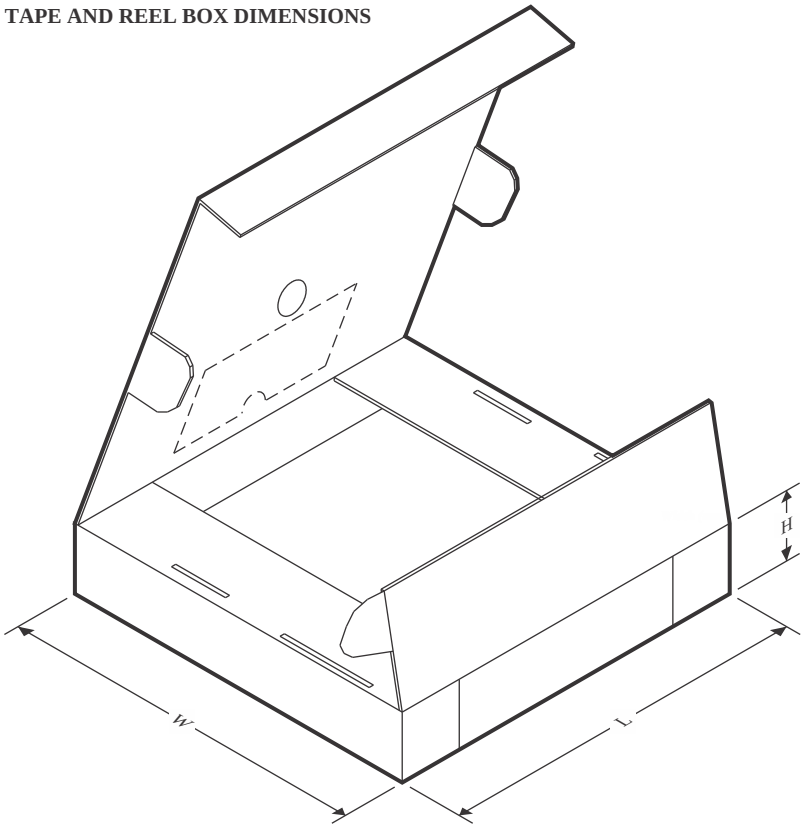
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA4H199MDYYTSEP	SOT-23-THIN	DYY	14	250	330.0	12.4	4.8	3.6	1.6	8.0	12.0	Q3

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

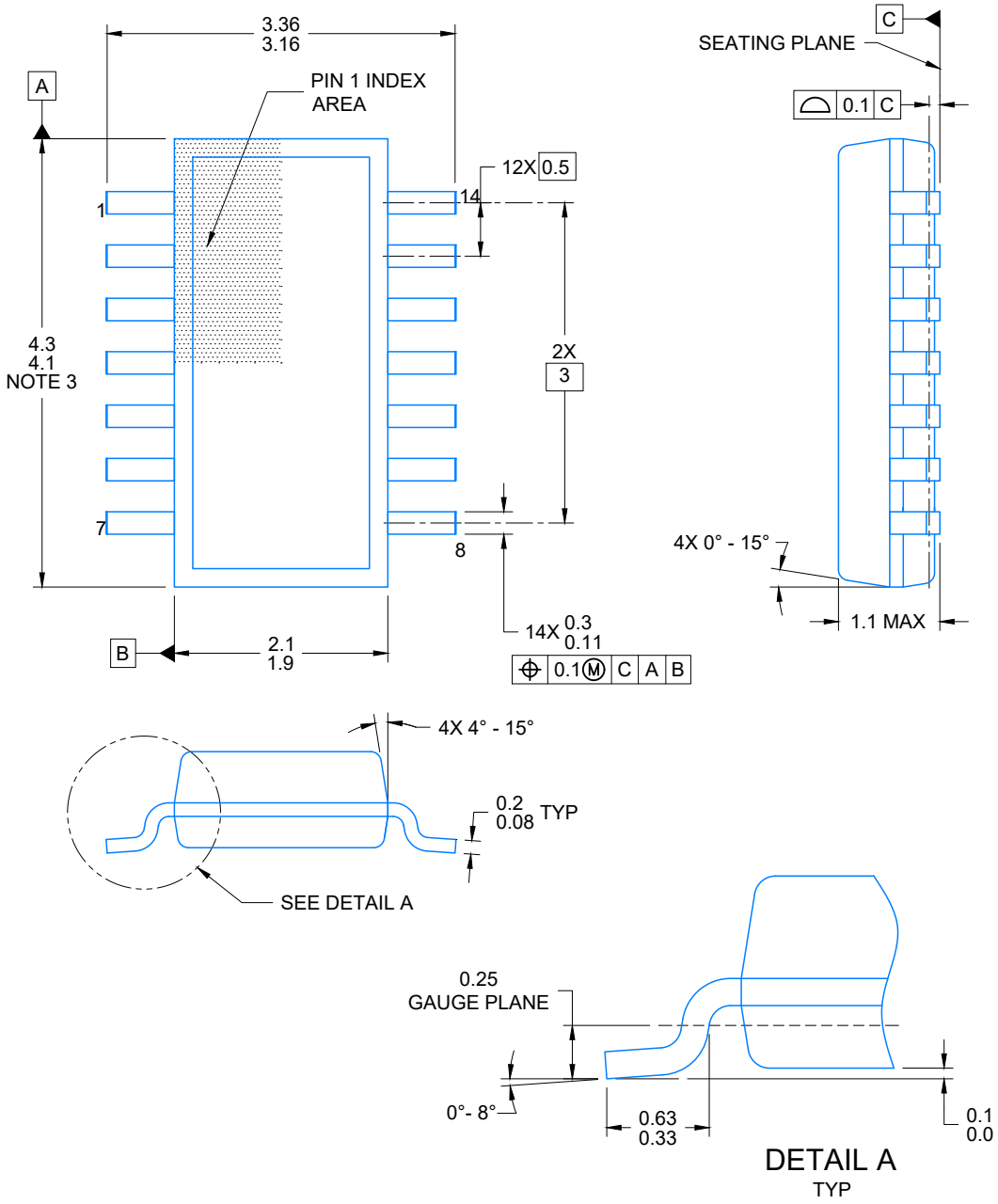
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA4H199MDYYTSEP	SOT-23-THIN	DYY	14	250	336.6	336.6	31.8

PACKAGE OUTLINE

DYY0014A

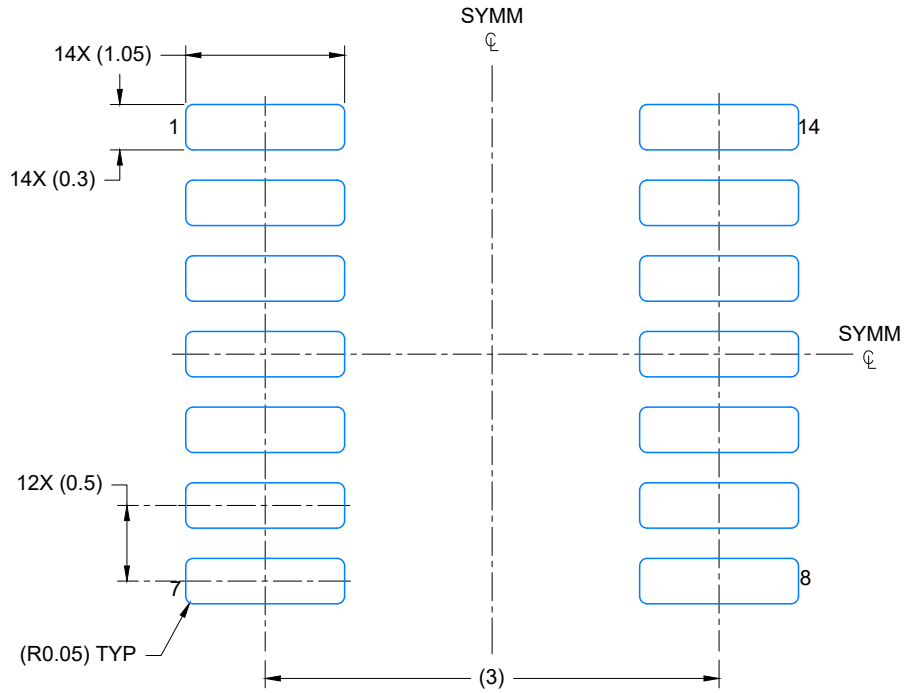
SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE

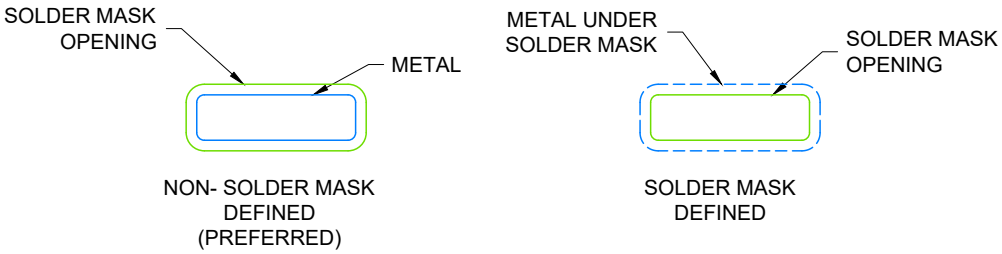


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
5. Reference JEDEC Registration MO-345, Variation AB



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 20X

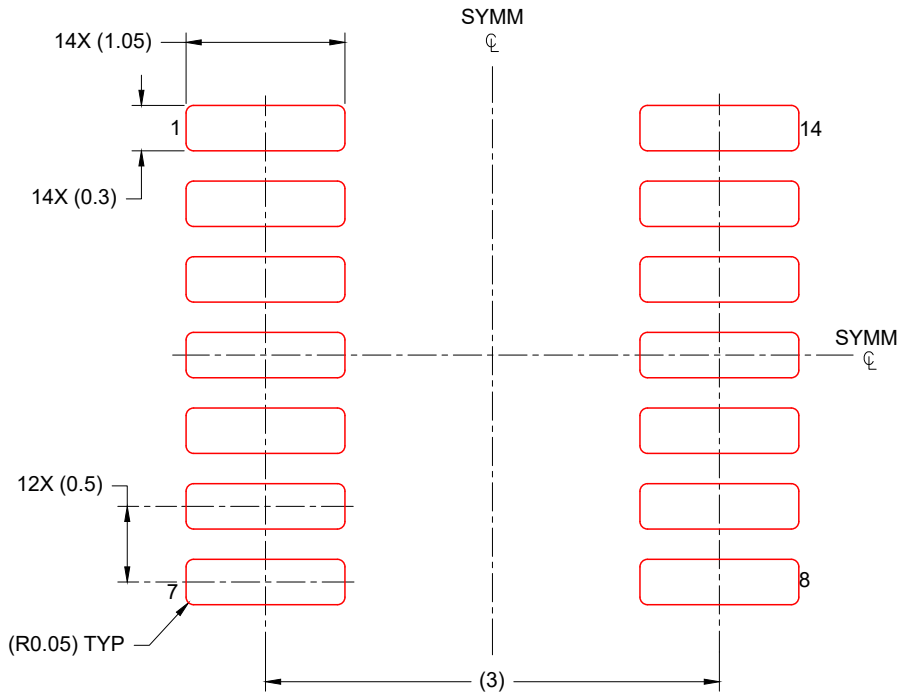


SOLDER MASK DETAILS

4224643/D 07/2024

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL
SCALE: 20X

4224643/D 07/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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