

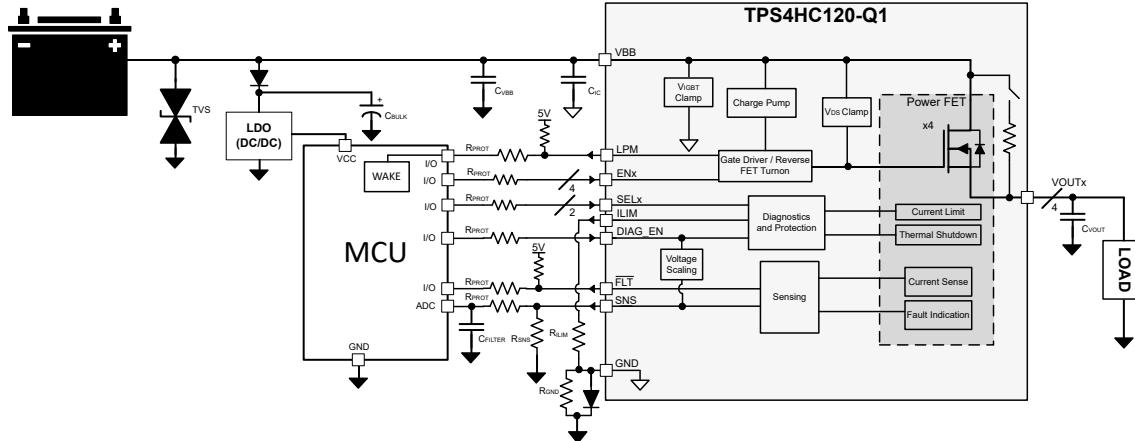
# TPS4HC120-Q1 120mΩ, 2A, Quad-Channel Automotive Smart High-Side Switch

## 1 Features

- Quad-channel 120mΩ automotive smart high-side switch with full diagnostics
  - Open-drain status output
  - Current sense analog output
- Wide operating voltage: 3V to 28V
- Low power mode (LPM) with automatic entry and exit
  - $I_{Q,LPM} < 20\mu A/ch$  with all 4 channels on and in LPM mode
- Ultra-low sleep current,  $< 1\mu A$  at 25°C
- Selectable current limit, 0.25A to 5A
- Protection
  - Overload and short-circuit protection
  - Thermal shutdown and swing with self recovery
  - Inductive load negative voltage clamp
  - Loss-of-GND, loss-of-battery, and reverse battery protection
- Diagnostics
  - Global fault report for fast interrupt
  - Overcurrent and short-to-ground detection
  - Open-load and short-to-battery detection
- Automotive qualified
  - AEC-Q100 qualified for automotive applications:
    - Temperature:  $-40^\circ C$  to  $125^\circ C$ ,  $T_A$
    - Electrical transient disturbance immunity certification of ISO7637-2 and ISO16750-2
  - Package: 28-pin thermally-enhanced HVSSOP

## 2 Applications

- ADAS modules
- Automotive display module
- Body control module



An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, intellectual property matters and other important disclaimers. PRODUCTION DATA.

## 3 Description

The TPS4HC120-Q1 is an automotive quad-channel, smart high-side switch, with integrated NMOS power FET and charge pump, designed to meet the requirements of 12V automotive battery systems. The low  $R_{ON}$  (120mΩ) minimizes the device power dissipation when driving a wide range of output load current up to 2A when all four channels are enabled or 2.5A when only one channel is enabled.

The device integrates protection features such as thermal shutdown, output clamp, and current limit. These features improve system robustness during fault events such as short circuit. The TPS4HC120-Q1 implements a selectable current limiting circuit that improves the reliability of the system by reducing inrush current when driving large capacitive loads and minimizing overload current. The device offers 10 selectable current limit settings (0.25A to 5A) based on the external resistor used on the ILIM pin. The device also provides an accurate load current sense that allows for improved load diagnostics such as overload and open-load detection, which enables better predictive maintenance.

The TPS4HC120-Q1 is available in a 28-pin, 7.1mm × 4.9mm HVSSOP leadless package with 0.5mm pin pitch minimizing the PCB footprint.

## Package Information

PART NUMBER <sup>(1)</sup>	PACKAGE <sup>(2)</sup>	PACKAGE SIZE <sup>(3)</sup>
TPS4HC120-Q1	DGQ (HVSSOP, 28)	7.1mm × 4.9mm

(1) See also [Section 4](#).

(2) For more information, see [Section 11](#).

(3) The package size (length × width) is a nominal value and includes pins, where applicable.

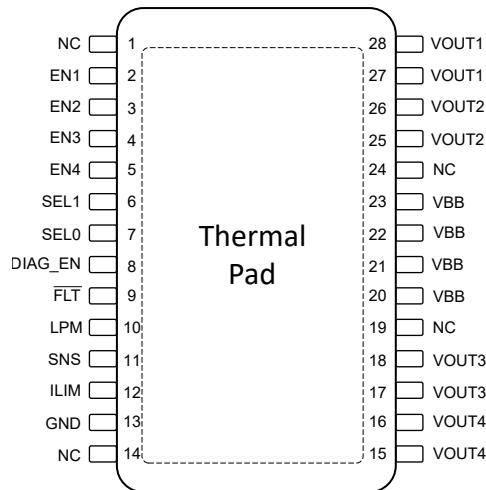
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## 4 Device Comparison Table

PART NUMBER	BEHAVIOR AFTER THERMAL FAULT
TPS4HC120A-Q1	LATCH off the faulted channel after thermal fault. Toggle EN to re-enable the specific channel.
TPS4HC120B-Q1	Auto-retry after thermal fault.

## 5 Pin Configuration and Functions



**Figure 5-1. DGQ Package, 28-Pin HVSOP (Top View)**

**Table 5-1. Pin Functions**

See Applications Section for full list of recommended components

PIN		TYPE	DESCRIPTION
NO.	NAME		
1, 14, 19, 24	NC	N/A	No internal connection.
2	EN1	Input	Input control for channel 1 activation, internal pulldown.
3	EN2	Input	Input control for channel 2 activation, internal pulldown.
4	EN3	Input	Input control for channel 3 activation, internal pulldown.
5	EN4	Input	Input control for channel 4 activation, internal pulldown.
6	SEL1	Input	SNS channel-selection high bit; internal pulldown.
7	SEL0	Input	SNS channel-selection low bit; internal pulldown.
8	DIAG_EN	Input	Enable-disable pin for diagnostics, internal pulldown.
9	FLT	Output	Open drain global fault output. Referred to $\overline{\text{FAULT}}$ , $\text{FLT}$ , or fault pin. Recommended $5\text{k}\Omega$ – $10\text{k}\Omega$ pullup resistor.
10	LPM	Output	Open drain LPM status pin. Pulled high by external supply if the device is in LPM or SLEEP state. Pulled low internally when device is in ACTIVE mode. Recommended $5\text{k}\Omega$ – $10\text{k}\Omega$ pullup resistor.
11	SNS	Output	SNS current output.
12	ILIM	Output	Adjustable current limit. Connect a resistor to chip GND, SHORT the pin to chip GND, or leave the pin OPEN to set the current limit value.
13	GND	Power	Ground of device. Connect to resistor-diode ground network to have reverse battery protection.
15, 16	VOUT4	Power	Output of channel 4 of the high side switch, connected to load.
17, 18	VOUT3	Power	Output of channel 3 of the high side switch, connected to load.
20, 21, 22, 23	VBB	Power	Power supply
25, 26	VOUT2	Power	Output of channel 2 of the high side switch, connected to load.
27, 28	VOUT1	Power	Output of channel 1 of the high side switch, connected to load.
Thermal Pad	Pad	Power	Thermal Pad, internally shorted to ground.

## 6 Specifications

### 6.1 Absolute Maximum Ratings

Over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
$V_{BB}$	Maximum continuous supply voltage		28	V
$V_{LD}$	Load dump voltage, ISO16750-2:2010(E)		35	V
$V_{REV}$	Reverse polarity voltage, maximum duration of 3 minutes and with the application circuit	-18		V
$I_{EN1}, I_{EN2}, I_{EN3}, I_{EN4}$	Enable pin current	-0.5	20	mA
$V_{EN1}, V_{EN2}, V_{EN3}, V_{EN4}$	Enable pin voltage	-1.5	5.5	V
$I_{DIA\_EN}$	Diagnostic enable pin current	-0.5	20	mA
$V_{DIA\_EN}$	Diagnostic enable pin voltage	-1.5	5.5	V
$I_{SNS}$	Sense pin current	-10	150	mA
$V_{SNS}$	Sense pin voltage	-1.5	5.5	V
$I_{SELx}$	SELx pin current	-0.5	20	mA
$V_{SELx}$	SELx pin voltage	-1.5	5.5	V
$I_{FLT}$	FLT pin current	-30	2.5	mA
$V_{FLT}$	FLT pin voltage	-0.3	5.5	V
$I_{LPM}$	LPM pin current	-30	2.5	mA
$V_{LPM}$	LPM pin voltage	-0.3	5.5	V
$I_{ILIM}$	ILIM pin current	-0.5	20	mA
$V_{ILIM}$	ILIM pin voltage	-1.5	5.5	V
$I_{GND}$	Reverse ground current, $V_{BB} < 0V$	-50		mA
$T_J$	Maximum junction temperature		150	°C
$T_{stg}$	Storage temperature	-65	150	°C

(1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

### 6.2 ESD Ratings

				VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge <sup>(1)</sup>	Human-body model (HBM), per AEC Q100-002 <sup>(2)</sup>	All pins except $V_{BB}$ and $V_{OUT}$	$\pm 2000$	V
		Human-body model (HBM), per AEC Q100-002 <sup>(2)</sup>	$V_{BB}$ and $V_{OUT}$	$\pm 4000$	
		Charged-device model (CDM), per AEC Q100-011	All pins	$\pm 750$	

(1) All ESD strikes are with reference from the pin mentioned to GND pin.

(2) AEC-Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specifications.

## 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted) (1)Digital input pins are EN1, EN2, EN3, EN4, SEH, SEL, DIAG\_EN

		MIN	MAX	UNIT
V <sub>VBB_NOM</sub>	Nominal supply voltage (1)	4	18	V
V <sub>VBB_EXT</sub>	Extended supply voltage(2)	3	28	V
V <sub>VBB_SC</sub>	Short circuit supply voltage capability		28	V
V <sub>DIN</sub>	All digital input pin voltage	-1	5.5	V
T <sub>A</sub>	Operating free-air temperature	-40	125	°C

(1) All operating voltage conditions are measured with respect to device GND pin.

(2) The device functions within the extended operating range, however some parametric values do not apply.

## 6.4 Thermal Information

THERMAL METRIC <sup>(1) (2)</sup>		TPS4HC120-Q1	UNIT
		DGQ (HVSSOP)	
		28 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	32.1	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	32.4	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	8.4	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	1.0	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	8.3	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	2.1	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application note.

(2) The thermal parameters are based on a 4-layer PCB according to the JESD51-5 and JESD51-7 standards.

## 6.5 Electrical Characteristics

V<sub>BB</sub> = 6V to 18V, T<sub>A</sub> = -40°C to +125°C (unless otherwise noted); Typical application is 13.5V, 1A, RILIM = Open (unless otherwise specified). Digital input pins are EN1, EN2, EN3, EN4, SEL0, SEL1, DIAG\_EN.

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>INPUT VOLTAGE AND CURRENT</b>					
V <sub>UVLOR</sub>	V <sub>BB</sub> undervoltage lockout rising	Measured with respect to the GND pin of the device	3.2	3.6	4.0
V <sub>UVLOF</sub>	V <sub>BB</sub> undervoltage lockout falling	Measured with respect to the GND pin of the device	2.5	2.75	3.0
V <sub>Clamp</sub>	VDS clamp voltage	T <sub>J</sub> = 25°C	35	43	V
		T <sub>J</sub> = -40°C to +150°C	34	45	
V <sub>OUT,clamp</sub>	VOUT clamp voltage	T <sub>J</sub> = -40°C to +150°C	-31	-23	V
I <sub>Q</sub>	Quiescent current all channels enabled	V <sub>BB</sub> ≤ 28V, V <sub>ENx</sub> = V <sub>DIAG_EN</sub> = 5V, I <sub>OUTx</sub> = 0A		3.8	4.5
I <sub>Q,DIAG_DIS</sub>	Quiescent current channel enabled diagnostic disabled	V <sub>BB</sub> ≤ 28V V <sub>EN</sub> = 5V V <sub>DIAG_EN</sub> = 0V, I <sub>OUTx</sub> = 0A		3.8	4.2
I <sub>SB</sub>	Current consumption in standby mode	V <sub>BB</sub> ≤ 18V, I <sub>SNS</sub> = 0mA V <sub>ENx</sub> = 0V, V <sub>DIAG_EN</sub> = 5V, V <sub>OUT</sub> = 0V		3.8	4.5
t <sub>STBY</sub>	Delay time to remain in standby mode before entering sleep mode	V <sub>ENx</sub> = V <sub>DIAG_EN</sub> = 5V to 0V		20	ms

## 6.5 Electrical Characteristics (continued)

$V_{BB}$  = 6V to 18V,  $T_A$  = –40°C to +125°C (unless otherwise noted); Typical application is 13.5V, 1A, RILIM = Open (unless otherwise specified). Digital input pins are EN1, EN2, EN3, EN4, SEL0, SEL1, DIAG\_EN.

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT	
$I_{SLEEP}$	Sleep current (total device leakage including MOSFET channels)	$V_{BB} \leq 18V$ , $V_{ENx} = V_{DIAG\_EN} = 0V$ , $V_{OUT} = 0V$	$T_A = 25^\circ C$		0.5		$\mu A$	
			$T_A = 125^\circ C$		2			
$I_{OUT(sleep)}$	Output leakage current per channel	$V_{BB} \leq 18V$ , $V_{ENx} = V_{DIAG\_EN} = 0V$ , $V_{OUT} = 0V$	$T_A = 25^\circ C$	0.01	0.2		$\mu A$	
			$T_A = 125^\circ C$		0.5			
$I_{L-NOM}$	Continuous load current, per channel	All channels enabled	$T_A = 85^\circ C$		2		A	
		One channel enabled			3			
<b><math>R_{ON}</math> CHARACTERISTICS</b>								
$R_{ON}$	On-resistance	$5V < V_{BB} \leq 28V$ , $I_{OUT} = 1A$	$T_J = 25^\circ C$	120			$m\Omega$	
			$T_J = 150^\circ C$		250			
		$3V \leq V_{BB} \leq 5V$ , $I_{OUT} = 1A$	$T_J = 25^\circ C$	175				
			$T_J = 150^\circ C$	280				
$\Delta R_{ON}$	Percentage difference in $R_{ON}$ between channels	$5V < V_{BB} \leq 28V$ , $I_{OUT} = 1A$	$T_J = -40^\circ C$ to $+150^\circ C$	5			%	
$R_{ON(REV)}$	On-resistance during reverse polarity	$-18V \leq V_{BB} \leq -6V$	$T_J = 25^\circ C$	120			$m\Omega$	
			$T_J = 150^\circ C$		250			
$V_F$	Body diode forward conduction voltage	$V_{EN} = 0V$ $I_{OUT} = -0.1A$		0.8	1		V	
<b>CURRENT SENSE CHARACTERISTICS</b>								
$K_{SNS}$	Current sense ratio $I_{OUT} / I_{SNS}$	$I_{OUT} = 1A$		1040				
$I_{SNS}$	Current sense current and accuracy	$V_{EN} = V_{DIAG\_EN} = 5V$	$I_{OUT} = 2A$	1.9			$mA$	
				–4	3		%	
			$I_{OUT} = 1.5A$	1.43			$mA$	
				–4	3		%	
			$I_{OUT} = 750mA$	0.72			$mA$	
				–4	4		%	
			$I_{OUT} = 300mA$	0.29			$mA$	
				–5	5		%	
			$I_{OUT} = 100mA$	0.1			$mA$	
				–12	12		%	
			$I_{OUT} = 75mA$	0.072			$mA$	
				–16	16		%	
			$I_{OUT} = 30mA$	0.03			$mA$	
				–35	35		%	
			$I_{OUT} = 15mA$	0.014			$mA$	
				–75	75		%	
<b>SNS CHARACTERISTICS</b>								
$V_{SNSFH}$	$V_{SNS}$ fault high-level	$V_{DIAG\_EN} = 5V$ , $R_{SNS} = 1k\Omega$		4.5	5	5.2	V	
		$V_{DIAG\_EN} = 3.3V$ , $R_{SNS} = 1k\Omega$		3.2	3.6	3.9		
		$V_{DIAG\_EN} = 1.8V$ , $R_{SNS} = 1k\Omega$		3.2	3.6	3.9		
$I_{SNSFH}$	$I_{SNS}$ fault high-level	$V_{DIAG\_EN} > V_{IH,DIAG\_EN}$		4.5		6.5	mA	
$V_{BB\_ISNS}$	V <sub>BB</sub> headroom needed for full current sense and fault functionality	$V_{DIAG\_EN} = 3.3V$	Measured with respect to GND pin of device	5			V	
		$V_{DIAG\_EN} = 5V$		6.5				

## 6.5 Electrical Characteristics (continued)

$V_{BB} = 6V$  to  $18V$ ,  $T_A = -40^{\circ}C$  to  $+125^{\circ}C$  (unless otherwise noted); Typical application is  $13.5V$ ,  $1A$ , RILIM = Open (unless otherwise specified). Digital input pins are EN1, EN2, EN3, EN4, SEL0, SEL1, DIAG\_EN.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>CURRENT LIMIT CHARACTERISTICS</b>						
$I_{CL}$	$I_{CL}$ current limit setting	$R_{ILIM} > 60k\Omega$ (ILIM = OPEN)	3.8	4.8	5.6	A
		$R_{ILIM} < 1.1k\Omega$ (ILIM = GND)	1.9	2.2	2.4	
		$R_{ILIM} = 2.49k\Omega$		1.9		
		$R_{ILIM} = 4.87k\Omega$		1.7		
		$R_{ILIM} = 9.76k\Omega$		1.5		
		$R_{ILIM} = 16.5k\Omega$	1.1	1.25	1.4	
		$R_{ILIM} = 23.2k\Omega$		1		
		$R_{ILIM} = 31.6k\Omega$		0.75		
		$R_{ILIM} = 43.2k\Omega^{(1)}$		0.5		
		$R_{ILIM} = 57.6k\Omega^{(1)}$	0.19	0.25	0.32	
$I_{CL\_LINPK}$	Linear Mode peak	$T_J = -40^{\circ}C$ to $+150^{\circ}C$ , $dI/dt < 0.01A/ms$	$I_{ILIM} = 0.25A$ to $2.2A$		$1.6 \times I_{CL}$	A
$I_{CL\_ENPS}$	Peak current enabling into permanent short	$T_J = -40^{\circ}C$ to $+150^{\circ}C$	Load = $5\mu H + 100m\Omega$		$2.25 \times I_{CL}$	A
$I_{OVCR}$	OVCR Peak current when short is applied while switch enabled	$T_J = -40^{\circ}C$ to $+150^{\circ}C$	Load = $5\mu H + 100m\Omega$		12	A
<b>FAULT CHARACTERISTICS</b>						
$R_{OL}$	Open-load (OL) detection internal resistor	$V_{EN} = 0V$ , $V_{DIAG\_EN} = 5V$	100	150	175	$k\Omega$
$t_{OL}$	Open-load (OL) detection deglitch time	$V_{EN} = 0V$ , $V_{DIAG\_EN} = 5V$ , When $V_{BB} - V_{OUT} < V_{OL}$ , duration longer than $t_{OL}$ . Openload detected.		300	500	$\mu s$
$V_{OL}$	Open-load (OL) detection voltage	$V_{EN} = 0V$ , $V_{DIAG\_EN} = 5V$		1.5		V
$t_{OL1}$	OL and STB indication-time from EN falling	$V_{EN} = 5V$ to $0V$ , $V_{DIAG\_EN} = 5V$ $I_{OUT} = 0mA$ , $V_{OUT} = V_{BB} - V_{OL}$		500		$\mu s$
$t_{OL2}$	OL and STB indication-time from DIA_EN rising	$V_{EN} = 0V$ , $V_{DIAG\_EN} = 0V$ to $5V$ $I_{OUT} = 0mA$ , $V_{OUT} = V_{BB} - V_{OL}$		600		$\mu s$
$T_{ABS}$	CHx Thermal shutdown threshold		162			$^{\circ}C$
$T_{HYS}$	CHx Thermal shutdown hysteresis			30		$^{\circ}C$
$T_{REL}$	CHx Relative thermal shutdown			80		$^{\circ}C$
$t_{FAULT\_FLT}$	Fault indication-time	$V_{DIAG\_EN} = 5V$ Time between fault and $\overline{FLT}$ asserting		60		$\mu s$
$t_{FAULT\_SNS}$	Fault indication-time	$V_{DIAG\_EN} = 5V$ Time between fault and $I_{SNS}$ settling at $V_{SNSFH}$		60		$\mu s$
$t_{RETRY}$	Retry time	Time from fault shutdown until switch re-enable (thermal shutdown).	1	2	3	ms
<b>LOW POWER MODE</b>						
$I_{LPM,enter}$	Load current level for entry to LPM	$t > t_{STBY}$	83	110	137	mA
$I_{LPM,exit}$	Load current level for exit of LPM		130	165	200	mA
$R_{DS0N,LPM}$	$R_{DS0N}$ in Low Power Mode	50mA $I_{LOAD}$		130		$m\Omega$

## 6.5 Electrical Characteristics (continued)

$V_{BB} = 6V$  to  $18V$ ,  $T_A = -40^\circ C$  to  $+125^\circ C$  (unless otherwise noted); Typical application is  $13.5V$ ,  $1A$ , RILIM = Open (unless otherwise specified). Digital input pins are EN1, EN2, EN3, EN4, SEL0, SEL1, DIAG\_EN.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$I_{Q,LPM}$	Quiescent current per channel in LPM with all channels enabled	$I_{LOAD} = 0mA$ , $T_A = -40^\circ C$ to $+125^\circ C$			20	$\mu A$
$t_{LPM}$	LPM transition indication-time	Device in LPM transition out time between current increase and LPM asserting			50	$\mu s$
$t_{WAKE}$	Recovery/exit time from LPM	Device in LPM transition out time between wake interrupt (EN, DIAG_EN pin) and LPM asserting			50	$\mu s$
$I_{PKLPM,exit}$	Current peak coming out of LPM, current setting $\leq 2.25A$	Peak current for immediate shutoff in LPM, $T_A = -40^\circ C$ to $+125^\circ C$			$1.6 \times I_{LIM}$	

### DIGITAL INPUT PIN CHARACTERISTICS

$V_{IL, DIN}$	Input voltage low-level	No GND network		0.8	V	
$V_{IH, DIN}$	Input voltage high-level	No GND network	1.5		V	
$V_{IHYS, DIN}$	Input voltage hysteresis		100		mV	
$R_{PD, DIN}$	Internal pulldown resistor for ENx, DIAG_EN		0.7	1	1.3	
	Internal pulldown resistor for SEL0, SEL1		0.7	1	1.3	
$I_{IH, DIN}$	Input current high-level for SEL0, SEL1	$V_{DINx} = 5.5V$			10	
	Input current high-level for DIAG_EN	$V_{DIAG\_EN} = 5.5V$			30	
$I_{IH, DIN}$	Input current high-level for ENx	$V_{ENx} = 5.5V$		30	$\mu A$	
<b>DIGITAL OUTPUT PIN CHARACTERISTICS</b>						
$V_{LPM}$	LPM low output voltage	$I_{LPM} = 2mA$			0.4	V
$V_{FLT}$	FLT low output voltage	$I_{FLT} = 2mA$			0.4	V

(1) If using GND network, accuracy for this current limit setting is shifted from the table value.

## 6.6 Timing Characteristics, SNS

$V_{BB} = 6V$  to  $18V$ ,  $T_A = -40^\circ C$  to  $125^\circ C$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>SNS TIMING - CURRENT SENSE</b>						
$t_{SNSION1}$	Settling time from rising edge of DIAG_EN 50% of $V_{DIAG\_EN}$ to 90% of settled ISNS	$V_{EN} = 5V$ , $V_{DIAG\_EN} = 0V$ to $5V$ $R_{SNS} = 1k\Omega$ , $I_L = 30mA$		60		$\mu s$
		$V_{ENx} = 5V$ , $V_{DIAG\_EN} = 0V$ to $5V$ $R_{SNS} = 1k\Omega$ , $I_L = 1A$		30		
$t_{SNSION2}$	Settling time from rising edge of EN and DIAG_EN 50% of $V_{DIAG\_EN}$ $V_{EN}$ to 90% of settled ISNS	$V_{EN} = V_{DIAG\_EN} = 0V$ to $5V$ $V_{BB} = 13.5V$ $R_{SNS} = 1k\Omega$ , $R_{LOAD} = 20\Omega$		150		$\mu s$
$t_{SNSION3}$	Settling time from rising edge of EN with DIAG_EN HI; 50% of $V_{DIAG\_EN}$ $V_{EN}$ to 90% of settled ISNS	$V_{EN} = 0V$ to $5V$ , $V_{DIAG\_EN} = 5V$ , $V_{BB} = 13.5V$ , $R_{SNS} = 1k\Omega$ , $R_{LOAD} = 20\Omega$		150		$\mu s$
$t_{SNSIOFF}$	Settling time from falling edge of DIAG_EN	$V_{EN} = 5V$ , $V_{DIAG\_EN} = 5V$ to $0V$ , $V_{BB} = 13.5V$ , $R_{SNS} = 1k\Omega$ , $R_L = 20\Omega$		20		$\mu s$

## 6.6 Timing Characteristics, SNS (continued)

$V_{BB} = 6V$  to  $18V$ ,  $T_A = -40^\circ C$  to  $125^\circ C$  (unless otherwise noted)

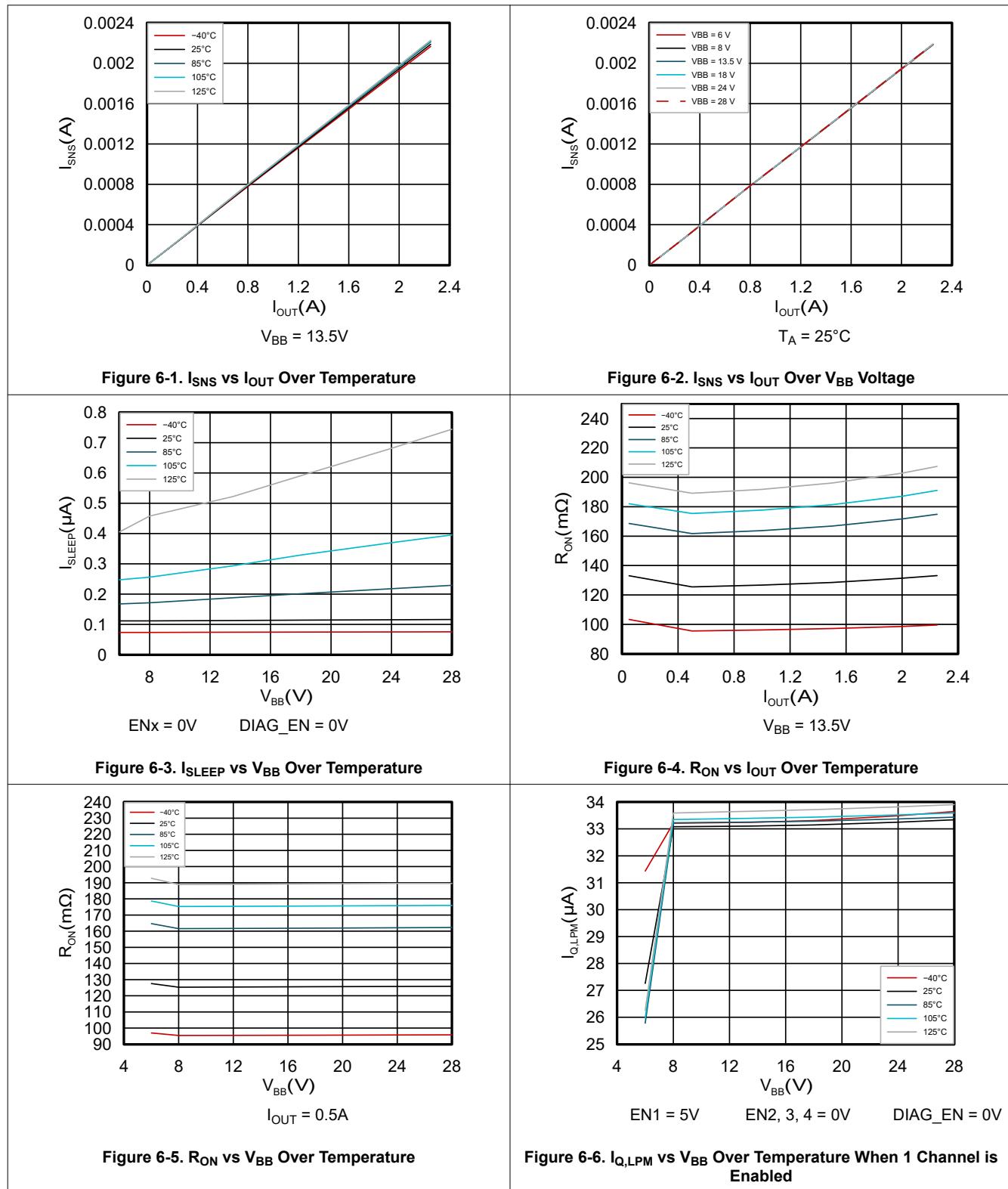
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{SETTLEH}$	Settling time from rising edge of load step	$V_{EN} = 5V$ , $V_{DIAG\_EN} = 5V$ $R_{SNS} = 1k\Omega$ , $I_{OUT} = 10mA$ to $1A$			20	$\mu s$
$t_{SETTLEL}$	Settling time from falling edge of load step	$V_{EN} = 5V$ , $V_{DIAG\_EN} = 5V$ $R_{SNS} = 1k\Omega$ , $I_{OUT} = 1A$ to $10mA$			20	$\mu s$
$t_{SELx}$	Multi-sense transition delay from channel to channel	$V_{EN} = 5V$ , $V_{DIAG\_EN} = 5V$ $R_{SNS} = 1k\Omega$ , $I_{OUT1} = 1A$ to $I_{OUT2} = 0.5A$			50	$\mu s$

## 6.7 Switching Characteristics

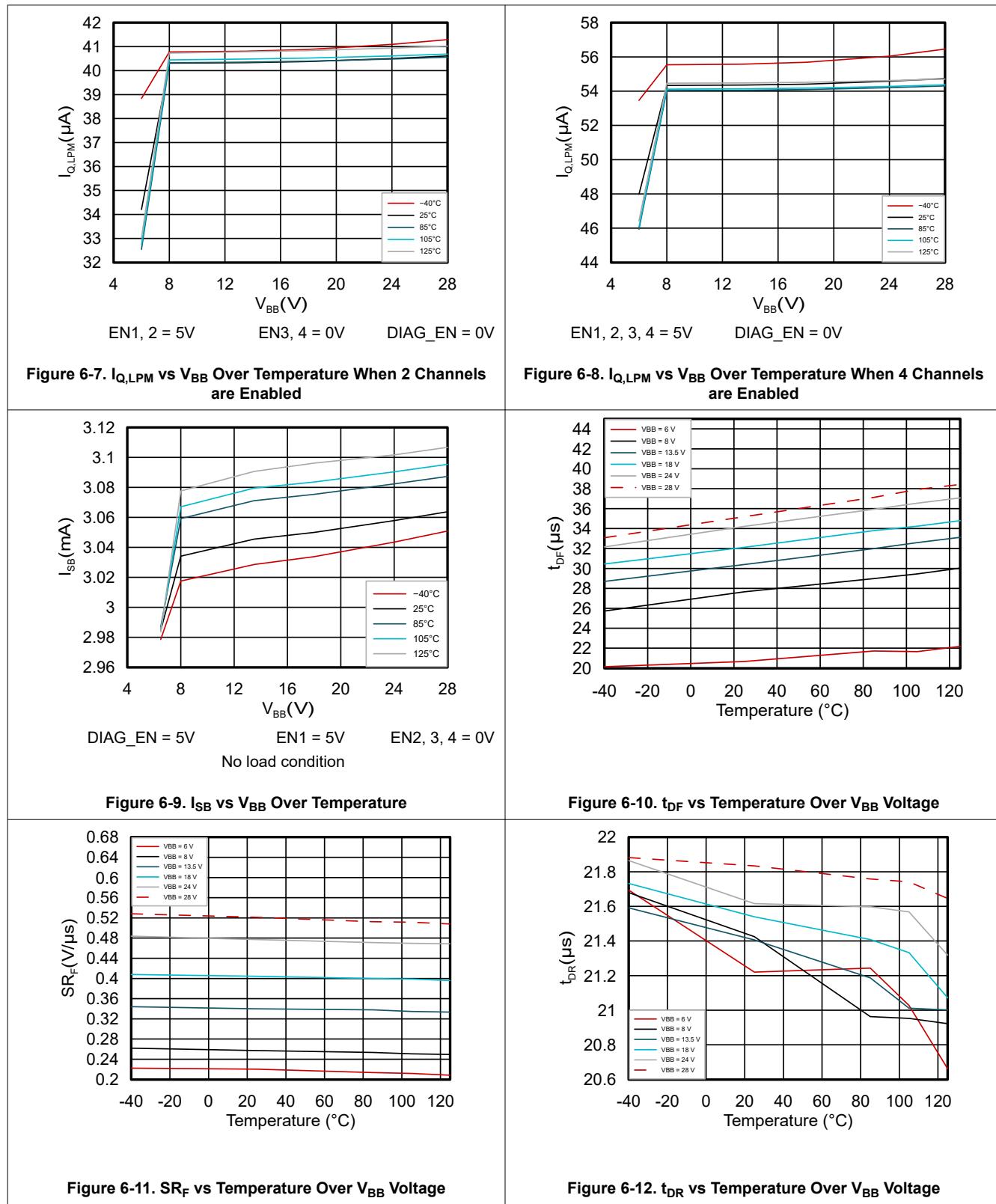
$V_{BB} = 13.5V$ ,  $T_A = -40^\circ C$  to  $125^\circ C$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{DR}$	Channel turn-on delay time (from Active)	$V_{BB} = 13.5V$ , $R_L = 1k\Omega$ 50% of EN to 10% of VOUT		30	55	$\mu s$
	Channel turn-on delay time (from Sleep or LPM)			40	60	
$t_{DF}$	Channel turn-off delay time (from Active)	$V_{BB} = 13.5V$ , $R_L = 10\Omega$ 50% of EN to 90% of VOUT		30	55	$\mu s$
	Channel turn-off delay time (from LPM)			30	85	
$SR_R$	VOUT rising slew rate	$V_{BB} = 13.5V$ , 20% to 80% of VOUT, $R_L = 10\Omega$	0.1	0.3	0.55	V/ $\mu s$
$SR_F$	VOUT falling slew rate	$V_{BB} = 13.5V$ , 80% to 20% of VOUT, $R_L = 10\Omega$	0.1	0.3	0.5	V/ $\mu s$
$t_{ON}$	Channel turn-on time (Standby delay to Active)	$V_{BB} = 13.5V$ , $R_L = 10\Omega$ 50% of EN to 80% of VOUT	30	50	100	$\mu s$
$t_{OFF}$	Channel turn-off time (Active to Standby delay)	$V_{BB} = 13.5V$ , $R_L = 10\Omega$ 50% of EN to 20% of VOUT	30	70	145	$\mu s$
$t_{ON} - t_{OFF}$	Turn-on and off matching	1ms enable pulse $V_{BB} = 13.5V$ , $R_L = 10\Omega$		-40	40	$\mu s$
		200- $\mu s$ enable pulse, $V_{BB} = 13.5V$ , $R_L = 10\Omega$		-40	40	
$\Delta_{PWM}$	PWM accuracy - average load current	200- $\mu s$ enable pulse (1ms period), $V_{BB} = 13.5V$ , $R_L = 10\Omega$		-25	25	%
		PWM $\leq 500Hz$ , 50% duty cycle, $V_{BB} = 13.5V$ , $R_L = 10\Omega$		-12	12	
$E_{ON}$	Switching energy losses during turn-on	$V_{BB} = 13.5V$ , $R_L = 10\Omega$		0.5		mJ
$E_{OFF}$	Switching energy losses during turn-off	$V_{BB} = 13.5V$ , $R_L = 10\Omega$		0.5		mJ

## 6.8 Typical Characteristics



## 6.8 Typical Characteristics (continued)



## 6.8 Typical Characteristics (continued)

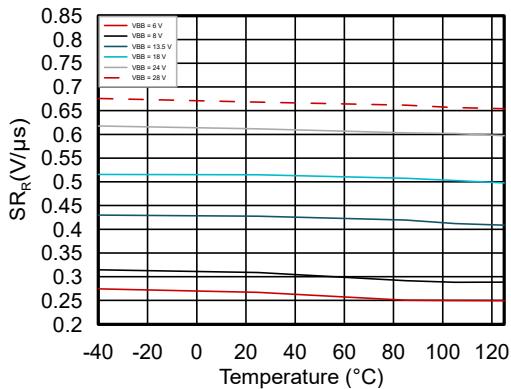
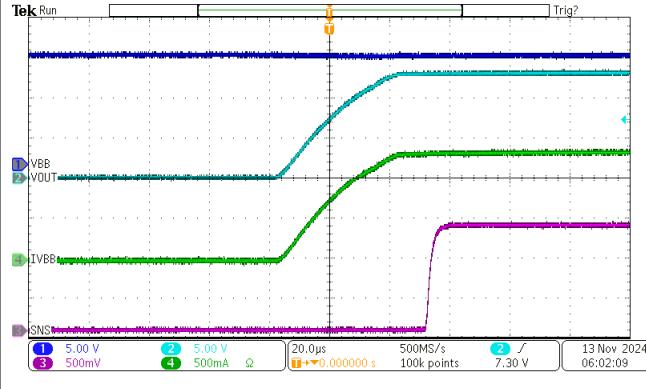
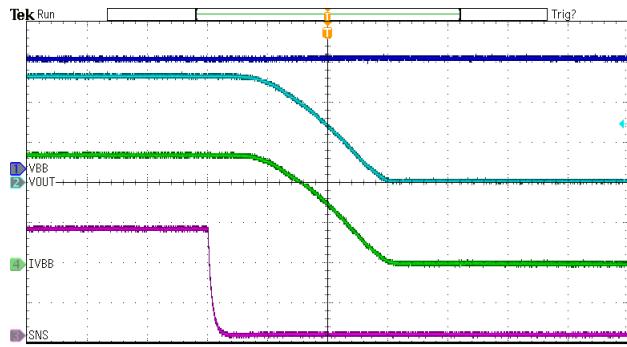


Figure 6-13.  $SR_R$  vs Temperature Over  $V_{BB}$  Voltage



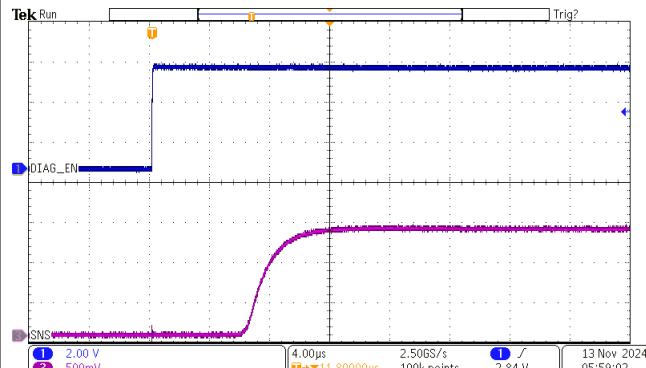
$V_{BB} = 13.5V$     $R_{SNS} = 1k\Omega$     $ILIM = OPEN$   
 $R_{OUT} = 10\Omega$     $T_A = 25^\circ C$

Figure 6-14. Switch Turn-On



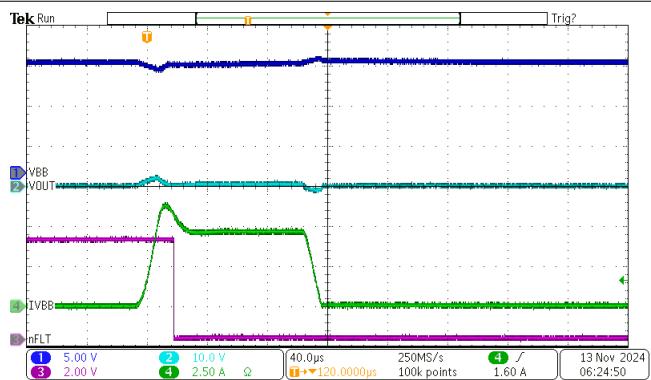
$V_{BB} = 13.5V$     $R_{SNS} = 1k\Omega$     $ILIM = OPEN$   
 $R_{OUT} = 10\Omega$     $T_A = 25^\circ C$

Figure 6-15. Switch Turn-Off



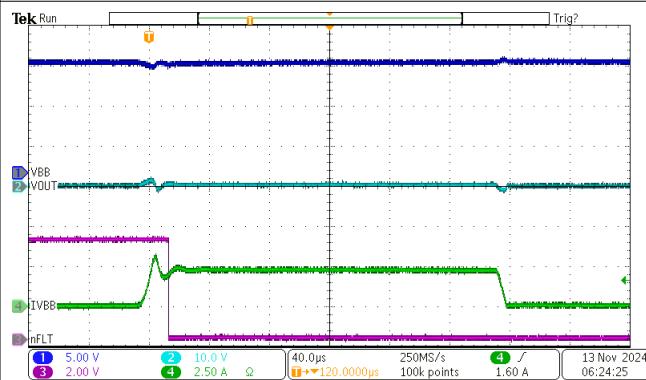
$V_{BB} = 13.5V$     $R_{SNS} = 1k\Omega$     $ILIM = OPEN$   
 $R_{OUT} = 10\Omega$     $T_A = 25^\circ C$

Figure 6-16. SNS Pin Voltage With DIAG\_EN Turning ON



$V_{BB} = 13.5V$     $R_{SNS} = 1k\Omega$     $ILIM = OPEN$   
 $Z_{OUT} = 100m\Omega + 5\mu H$     $T_{AMB} = 25^\circ C$

Figure 6-17. Permanent Short Behavior With ILIM Open



$V_{BB} = 13.5V$     $R_{SNS} = 1k\Omega$     $ILIM = Short-to-GND$   
 $Z_{OUT} = 100m\Omega + 5\mu H$     $T_A = 25^\circ C$

Figure 6-18. Permanent Short Behavior With ILIM Short-to-GND

## 7 Detailed Description

## 7.1 Overview

The TPS4HC120-Q1 device is a smart high-side switch, with internal charge pump and quad-channel integrated NMOS power FETs. Full diagnostics and high-accuracy current-sense features enable intelligent control of the load. The adjustable current-limit function greatly improves the reliability of the whole system.

The device has logic pins to enable each of the four channels and a separate pin to enable the diagnostic output with two pins to select the channel to be output on the analog current SNS pin. The device also implements a global FLT pin for use as an interrupt to the MCU.

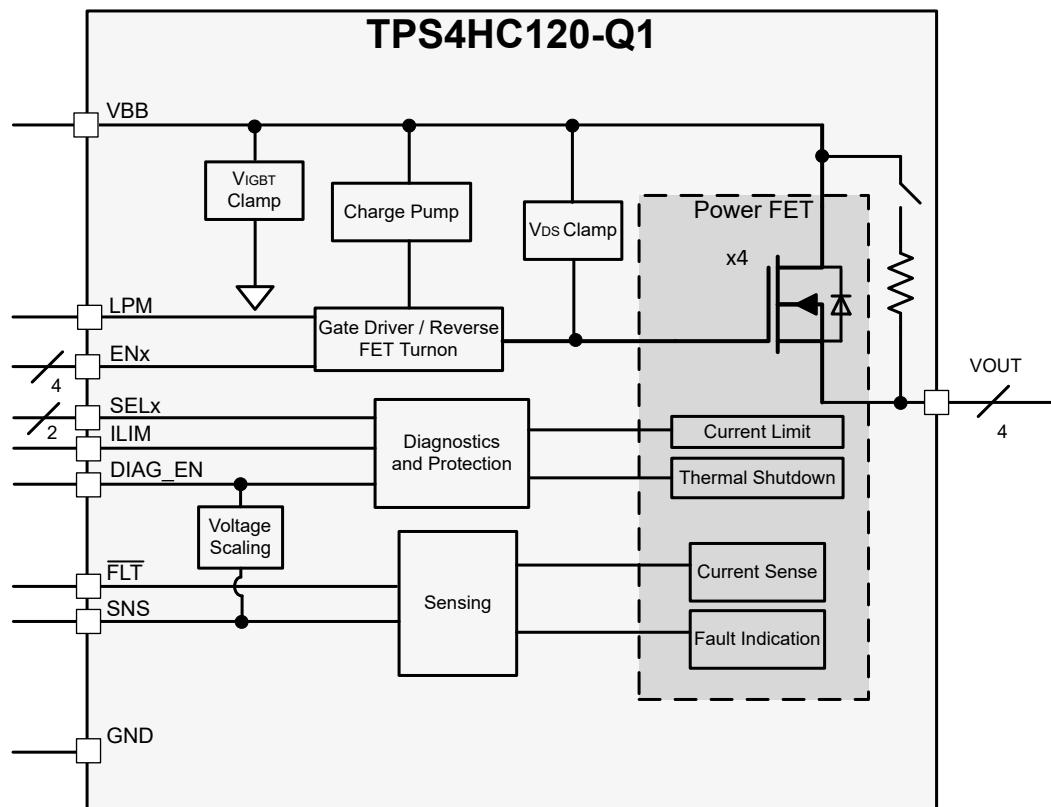
The external high-accuracy current limit allows setting the current-limit value by applications. When overcurrent occurs, the device improves system reliability by clamping the inrush current effectively. The device also helps save system cost by reducing the size of PCB traces and connectors, and the capacity of the preceding power stage.

For inductive loads (relays, solenoids, valves), the device implements an active clamp between drain and source for protection. During the inductive switching-off cycle, both the energy of the power supply and the load are dissipated on the high-side switch. The device also optimizes the switching-off slew rate when the clamp is active, which helps the system design by keeping the effects of transient power and EMI to a minimum.

When the current consumptions on all channels are small, along with other requirements described in [Section 7.3.2.1](#), the device automatically enters low power mode. This mode has ultra-low quiescent current consumption, and is applicable for loads that are active when the vehicle is off to preserve the battery. There is a dedicated LPM pin that indicates the mode of the device, and is useful as an interrupt signal to wake up the MCU.

The TPS4HC120-Q1 device is able to drive a wide variety of resistive, inductive, and capacitive loads, including low-wattage bulbs, LEDs, relays, solenoids, heaters, and sub-modules.

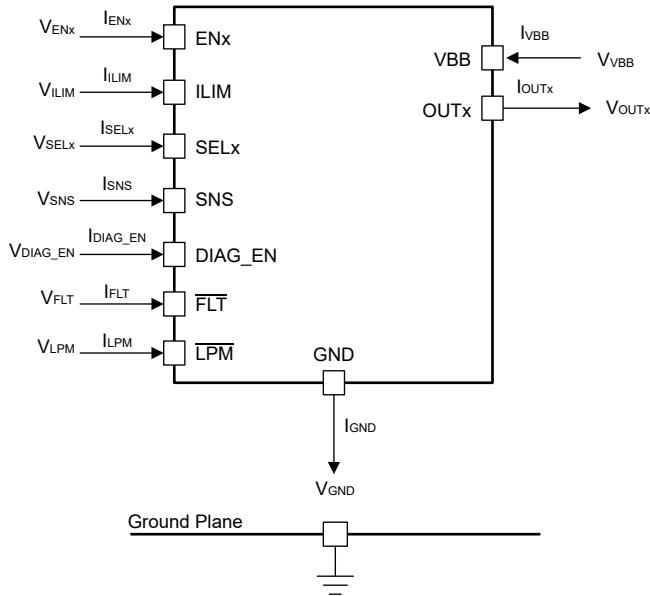
## 7.2 Functional Block Diagram



## 7.3 Feature Description

### 7.3.1 Pin Current and Voltage Conventions

For reference purposes throughout the data sheet, current directions on each pin are as shown by the arrows in Figure 7-1. All voltages are measured relative to the ground plane.



**Figure 7-1. Voltage and Current Conventions**

### 7.3.2 Low Power Mode

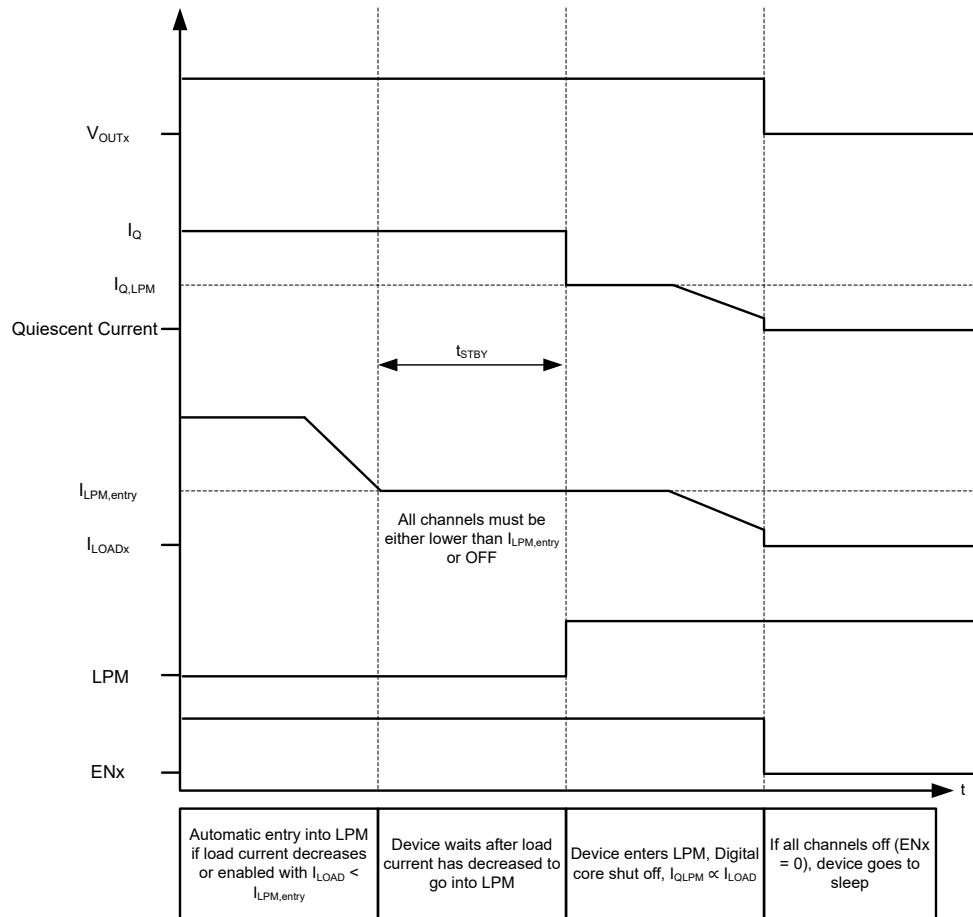
Low power mode (LPM) is designed to be able to still provide small amounts of current to loads without consuming much quiescent current. This type of feature is useful in power-at-all-time loads or to just generally reduce the amount of power dissipation from the supply. The quiescent current draw during this mode is defined in [Section 6.5](#) under  $I_{Q,LPM}$ . The TPS4HC120-Q1 can automatically enter and exit this mode by detecting that the load current is below  $I_{LPM,enter}$  on all active channels, and then exits this mode when load current increases above  $I_{LPM,exit}$ . This section describes the entry, exit and protections mechanisms in this mode.

#### 7.3.2.1 Entry into LPM

When the load current going through the channel is below the  $I_{LPM,enter}$  threshold on all active channels and diagnostics are turned off (DIAG\_EN is low) for longer than  $t_{STBY}$ , the device automatically enters into LPM. This means that the digital core is turned off and the charge pump strength is reduced to reduce the quiescent current to  $I_{Q,LPM}$ .

All the requirements below need to be met for the device to enter the LPM automatically:

- $T_J < 125^\circ\text{C}$
- $V_{BB} \geq 6\text{V}$
- DIAG\_EN is LOW
- At least one channel is ON
- All the ON channels have load currents  $< I_{LPM,enter}$  per channel
- No EN pin toggling
- All the above conditions are true for time longer than  $t_{STBY}$



**Figure 7-2. Entering LPM**

### 7.3.2.2 During LPM

The quiescent current of the device during LPM,  $I_{Q,LPM}$ , is a function of how many channels are active.  $I_{Q,LPM}$  is proportional to the load current, meaning that the lower the load current is during this time, then the lower the quiescent current is. Additionally, because the digital core is disabled, diagnostics such as current sensing or open load detection are not available during this mode. If diagnostics are desired, enable the **DIAG\_EN** pin to exit LPM and return the device back to normal operation. After **DIAG\_EN** is disabled, the device goes back into LPM after  $t_{STBY}$ . Similarly, the current limit mechanism is not active in the same manner. By definition, the minimum current limit is higher than the entry point of LPM. However, the short-circuit protection is still in place to protect the device.

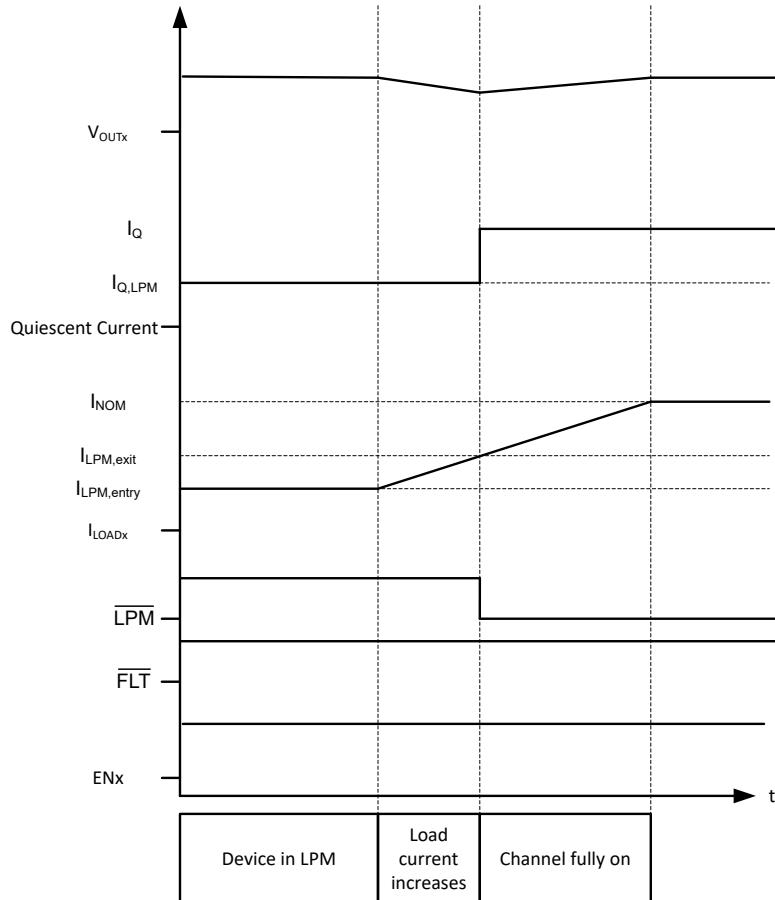
The following summary lists the behavior of the device during LPM:

- $I_Q$  reduces to  $I_{Q,LPM}$  per channel
- $R_{DS,ON}$  per channel increases to  $R_{DS,ON,LPM}$
- No clamped current limit for overload conditions as the device exits the LPM first
- Short-circuit protection is in place to shut off the device if load current increases to  $I_{PKLPM,exit}$  during LPM
- No thermal shutdown protection

### 7.3.2.3 Exiting LPM

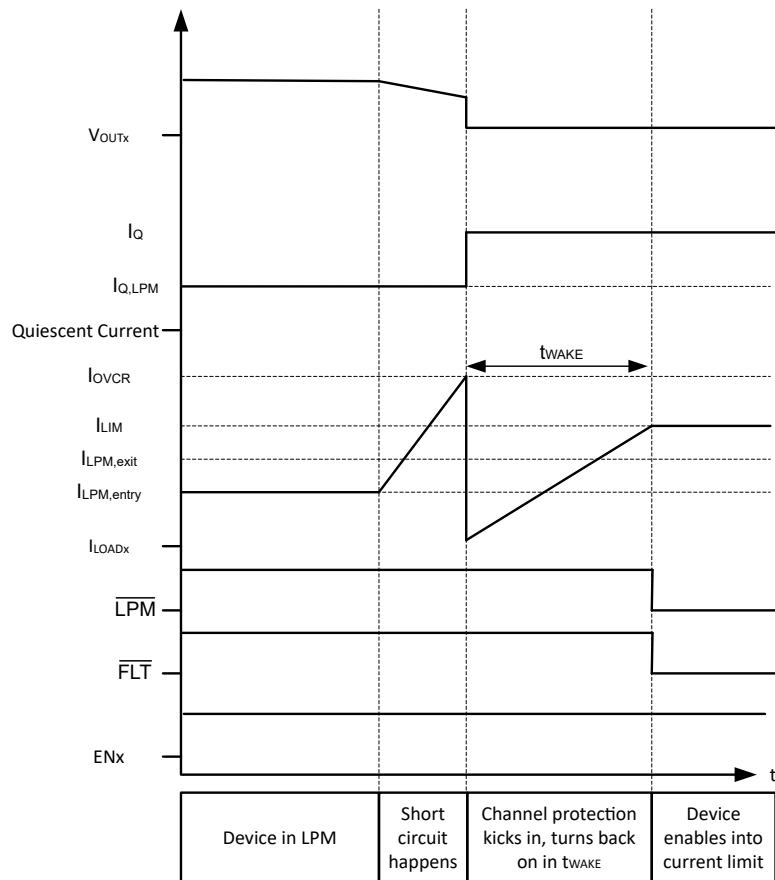
The device exits LPM if any one of four conditions is met:

- Load current increases slowly: If the load current increases beyond  $I_{LPM,exit}$  slowly, the device wakes up and pulls the LPM pin low to signal the device is no longer in low power mode. The output voltage droop is minimal.



**Figure 7-3. Exiting LPM With Load Current Slow Increase**

- Load current increases rapidly (short-circuit): If the load current increases rapidly beyond  $I_{LPM,exit}$ , the device shuts down for protection and comes back on within the  $t_{WAKE}$  time in normal operation with full functionality. As the device comes back on, the LPM pin is pulled LOW to represent that the device has come out of LPM. The  $\overline{FLT}$  pin also pulls low if the fault is still present.



**Figure 7-4. Exiting LPM With Rapid Load Current Increase (Short-Circuit)**

- Any  $ENx$  is toggled (from ON to OFF or OFF to ON): If any channel is turned ON or turned OFF during LPM, the device wakes up and performs the desired action. After the device wakes up, if the LPM entry conditions are still met, the device enters LPM again after  $t_{STBY}$ .
- DIAG\_EN is turned ON: if DIAG\_EN goes high, the device goes into the DIAGNOSTIC mode, which fully turns on the device so that all of the functionality works as intended in the DIAGNOSTIC state. If DIAG\_EN goes back low, with all LPM entry conditions are met, the device goes back into LPM after  $t_{STBY}$ .

Any time the device comes out of LPM to ACTIVE state, the LPM pin pulls LOW. If the system must wake up when the device comes out of LPM, then the LPM pin is able to be used to send a wake up signal to the MCU. Otherwise, ignore the LPM pin.

### 7.3.3 Accurate Current Sense

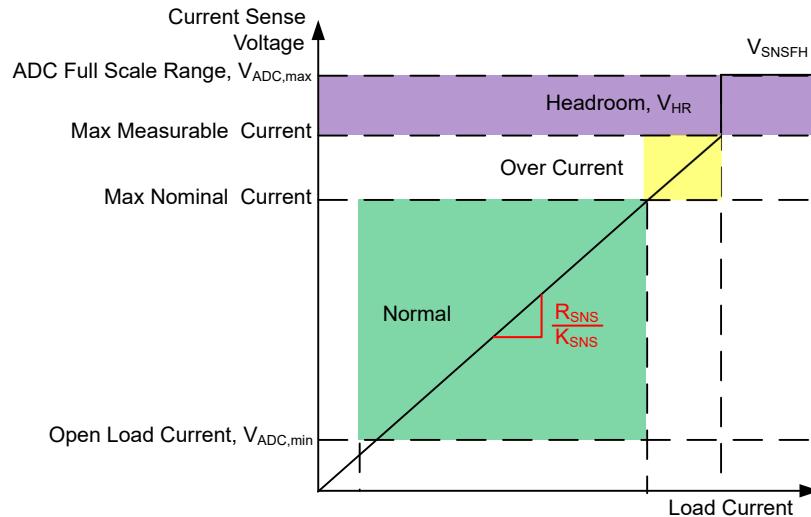
The high-accuracy current-sense function is internally implemented, which allows a better real-time monitoring effect and more-accurate diagnostics without further calibration. A current mirror is used to source  $1 / K_{SNS}$  of the load current, flowing out to the external resistor between the SNS pin and GND, and reflected as voltage on the SNS pin.

$K_{SNS}$  is the ratio of the output current and the sense current. The accuracy values of  $K_{SNS}$  quoted in the *Electrical Characteristics* take into consideration temperature and supply voltage. Each device is internally calibrated while in production, so post-calibration by users is not required in most cases.

The maximum voltage out on the SNS pin is clamped to  $V_{SNSFH}$ , which is the fault voltage level. To ensure that this voltage is not higher than the system can tolerate, limit the max voltage at the DIAG\_EN pin to the voltage at the SNS pin. If DIAG\_EN is between  $V_{IH}$  and 3.3V, the maximum output on the SNS pin is approximately 3.3V. However, if the voltage at DIAG\_EN is above 3.3V, then the fault SNS voltage,  $V_{SNSFH}$ , tracks that voltage up to 5V. Tracking is done because the GPIO voltage output that is powering the diagnostics through DIAG\_EN is

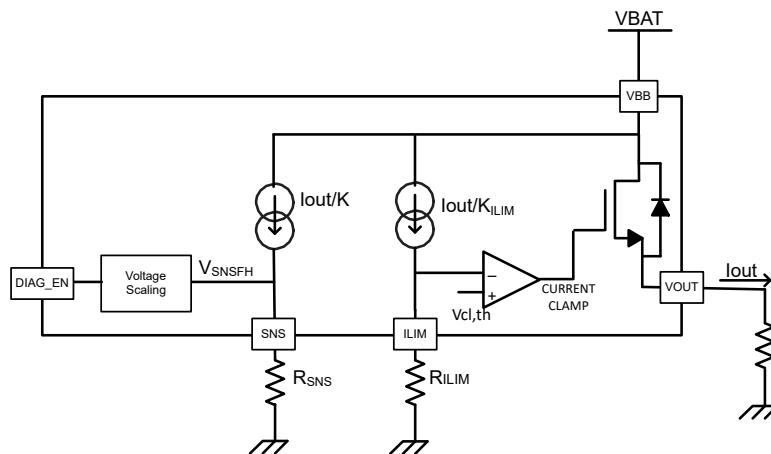
close to the maximum acceptable ADC voltage within the same microcontroller. Therefore, choose the sense resistor value,  $R_{SNS}$ , to maximize the range of currents needed to be measured by the system. Choose the  $R_{SNS}$  value based on application need. The maximum usable  $R_{SNS}$  value is bounded by the ADC minimum acceptable voltage,  $V_{ADC,min}$ , for the smallest load current needed to be measured by the system,  $I_{LOAD,min}$ . Choose the minimum acceptable  $R_{SNS}$  value so that the  $V_{SNS}$  voltage is less than the  $V_{SNSFH}$  value, allowing for the system to correctly determine faults. This difference between the maximum readable current through the SNS pin,  $I_{LOAD,max} \times R_{SNS}$ , and the  $V_{SNSFH}$  is called the headroom voltage,  $V_{HR}$ . The headroom voltage is determined by the system but is important so that there is a difference between the maximum readable current and a fault condition. Therefore, the minimum  $R_{SNS}$  value has to be the  $V_{SNSFH}$  minus the  $V_{HR}$  times the sense current ratio,  $K_{SNS}$  divided by the maximum load current the system must measure,  $I_{LOAD,max}$ . Use the following equation to set the boundary equation.

$$V_{ADC,min} \times K_{SNS} / I_{LOAD,min} \leq R_{SNS} \leq (V_{SNSFH} - V_{HR}) \times K_{SNS} / I_{LOAD,max} \quad (1)$$



**Figure 7-5. Voltage Indication on the Current-Sense Pin**

The maximum current the system wants to read,  $I_{LOAD,max}$ , must be less than the current-limit threshold because after the current-limit threshold is tripped, the  $V_{SNS}$  value goes to  $V_{SNSFH}$ .



**Figure 7-6. Current-Sense and Current-Limit Block Diagram**

Because this scheme adapts based on the voltage coming in from the MCU, there is no need to have a Zener diode on the SNS pin to protect from high voltages.

### 7.3.4 Adjustable Current Limit

A high-accuracy adjustable current limit allows higher reliability, which protects the power supply and wires during short circuit or power up by being programmed to an acceptable level. Also, current limiting help save system costs by reducing PCB traces, connector size, capacity of the preceding power stage and possibly reducing wire gauge.

Current limit offers protection from over-stressing to the load and integrated power FET. the current limit regulates the output current to the set value, asserts the  $\overline{\text{FLT}}$  pin, and pulls up the SNS pin to  $V_{\text{SNSFH}}$  if the device is set up to output that channel on the SNS pin.

The device can be programmed to different current limit values through an external resistor on the ILIM pin. There are 10 current limit settings which are set based on resistors values in [Table 7-1](#). Tolerance resistors  $\leq 1\%$  are recommended for the  $R_{\text{ILIM}}$  resistor.

**Table 7-1. Current Limit Setting Through  
External Resistor**

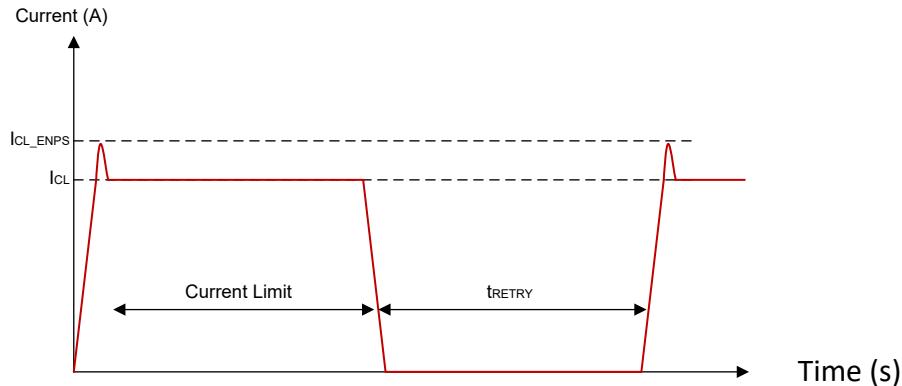
ALLOWED RESISTOR VALUE <sup>(1)</sup>	ILIM THRESHOLD
57.6k $\Omega$	250mA
43.2k $\Omega$	500mA
31.6k $\Omega$	750mA
23.2k $\Omega$	1A
16.5k $\Omega$	1.25A
9.76k $\Omega$	1.5A
4.87k $\Omega$	1.75A
2.49k $\Omega$	2A
Short to GND (< 1.1k $\Omega$ )	2.25A
Open (> 60k $\Omega$ )	5A

(1) Interpret any resistor settings that are not listed in this table as one of the adjacent levels, which are not recommended configurations.

To set a different inrush current limit and steady state current limit, the current limit resistor is able to change dynamically when the device is on. Adopt the MOSFET-based control scheme to change the current limit on the fly. However, carefully consider the components and the layout at ILIM pin to minimize the capacitance at the pin. Any capacitance  $\geq 100\text{pF}$  at ILIM pin possibly affects the current limit functionality. Select a MOSFET with low input capacitance for the dynamic current limit.

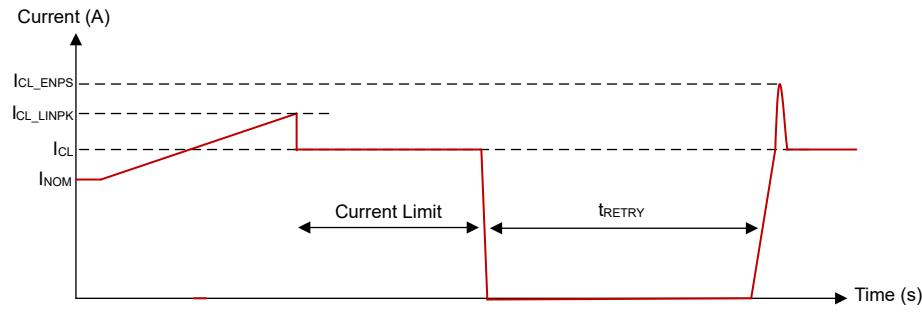
A current limit event occurs when  $I_{\text{OUT}_X}$  reaches the regulation threshold level,  $I_{\text{CL}}$ . When  $I_{\text{OUT}}$  reaches the current limit threshold,  $I_{\text{CL}}$ , the device is able to remain enabled and limit  $I_{\text{OUT}_X}$  to  $I_{\text{CL}}$ . When the device remains enabled (and limits  $I_{\text{OUT}}$ ), thermal shutdown potentially triggers due to the high amount of power dissipation in the FET. [Figure 7-7](#) shows the regulation loop response when the device is enabled into a short circuit. The figure shows the scenario with the auto-retry version listed in [Section 4](#). The LATCH version latches off after the first thermal shutdown. Be aware that the current peak is able to be at a higher value ( $I_{\text{CL\_ENPS}}$ ) than the regulation threshold ( $I_{\text{CL}}$ ).

When an overcurrent event occurs, the current limit must respond quickly to limit the peak current seen on short circuits (both hot and enabling into a short). Limit the peak so that the supply does not droop for a given amount of supply capacitance. This peak limiting is especially important in applications where the device is powered from a DC/DC instead of car battery.



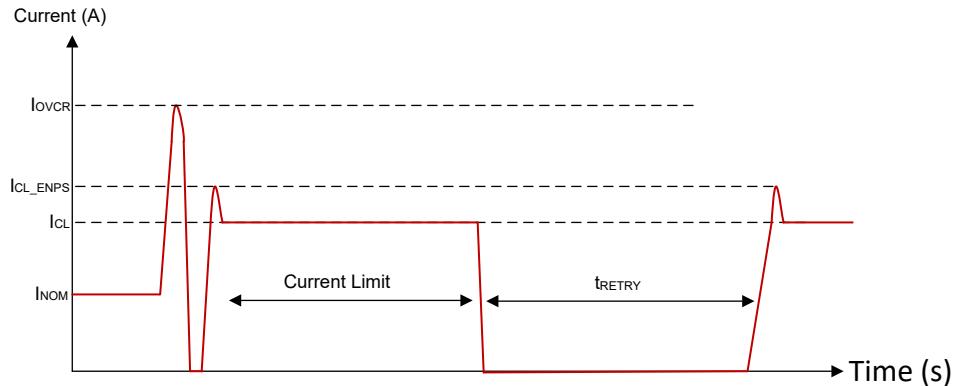
**Figure 7-7. Enable Into Short Current Limit (Auto-Retry Version)**

However, a higher output current ( $I_{CL\_LINPK}$ ) than the current limit regulation loop threshold ( $I_{CL}$ ) is potentially available from the switch during an overload condition before the current limitation is applied.



**Figure 7-8. Linear Peak From Soft Short (Auto-Retry Version)**

The device applies a strong pulldown to limit the current during the short circuit event while the switch is enabled. The current then drops down to zero before the current limit regulation loop engages the switch turn-on, and the behavior is similar to the enable into a short circuit case.



**Figure 7-9. Hot Short Event (Auto-Retry Version)**

### 7.3.5 Inductive-Load Switching-Off Clamp

When switching an inductive load off, the inductive reactance tends to pull the output voltage negative. Excessive negative voltage can cause the power FET to break down. To protect the power FET, an internal clamp between drain and source is implemented, namely  $V_{DS(\text{clamp})}$ .

$$V_{DS(\text{clamp})} = V_{VS} - V_{OUT} \quad (2)$$

During the period of demagnetization ( $t_{\text{decay}}$ ), the power FET is turned on for inductance-energy dissipation. The total energy is dissipated in the high-side switch. Total energy includes the energy of the power supply ( $E_{(VS)}$ ) and the energy of the load ( $E_{(\text{load})}$ ). If resistance is in series with inductance, some of the load energy is dissipated on the resistance.

$$E_{(\text{HSS})} = E_{(VS)} + E_{(\text{load})} = E_{(VS)} + E_{(L)} - E_{(R)} \quad (3)$$

When an inductive load switches off,  $E_{(\text{HSS})}$  causes high thermal stressing on the device. The upper limit of the power dissipation depends on the device intrinsic capacity, ambient temperature, and board dissipation.

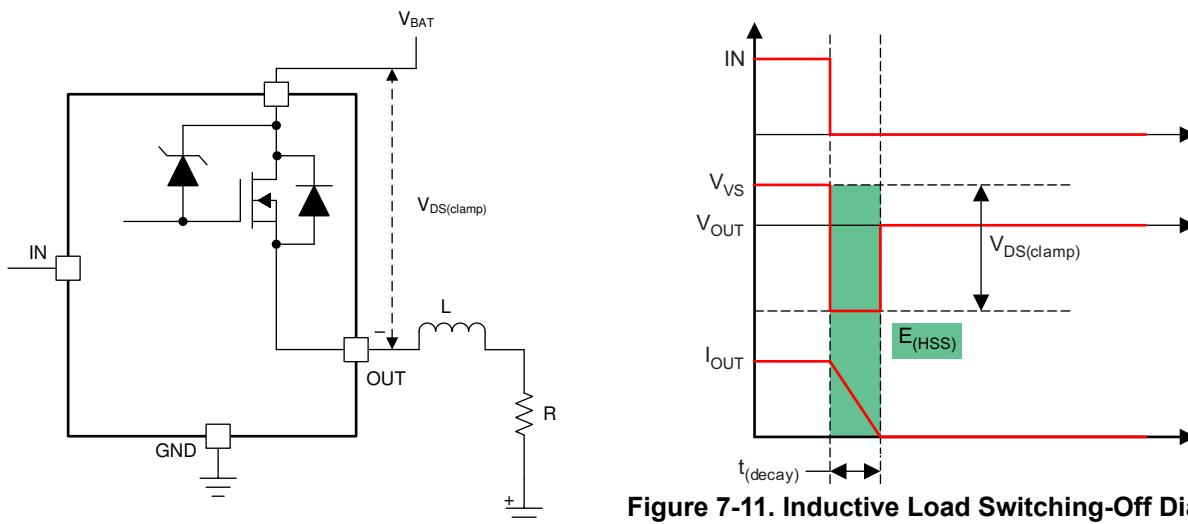


Figure 7-10. Drain-to-Source Clamping Structure

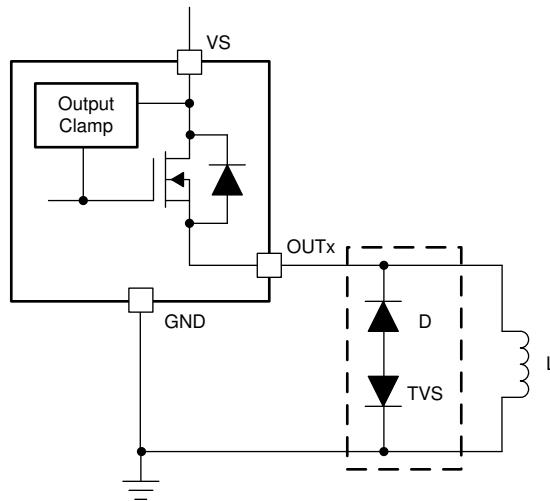
From the high-side switch perspective,  $E_{(\text{HSS})}$  equals the integration value during the demagnetization period.

$$\begin{aligned} E_{(\text{HSS})} &= \int_0^{t_{\text{decay}}} V_{DS(\text{clamp})} \times I_{OUT}(t) dt \\ t_{\text{decay}} &= \frac{L}{R} \times \ln \left( \frac{R \times I_{OUT(\text{max})} + |V_{OUT}|}{|V_{OUT}|} \right) \\ E_{(\text{HSS})} &= L \times \frac{V_{VS} + |V_{OUT}|}{R^2} \times \left[ R \times I_{OUT(\text{max})} - |V_{OUT}| \ln \left( \frac{R \times I_{OUT(\text{max})} + |V_{OUT}|}{|V_{OUT}|} \right) \right] \end{aligned} \quad (4)$$

When  $R$  approximately equals 0,  $E_{(\text{HSS})}$  is given simply as:

$$E_{(\text{HSS})} = \frac{1}{2} \times L \times I_{OUT(\text{max})}^2 \frac{V_{VS} + |V_{OUT}|}{|V_{OUT}|} \quad (5)$$

The recommendation for PWM-controlled inductive loads is to add the external freewheeling circuitry shown in [Figure 7-12](#) to protect the device from repetitive power stressing. The TVS is used to achieve the fast decay. See also [Figure 7-12](#).



**Figure 7-12. Protection With External Circuitry**

### 7.3.6 Fault Detection and Reporting

#### 7.3.6.1 Diagnostic Enable Function

The DIAG\_EN pin enables or disables the diagnostic functions. If multiple devices are used, but the ADC resource is limited in the microcontroller, the MCU can use GPIOs to set DIAG\_EN high to enable the diagnostics of one device while disabling the diagnostics of the other devices by setting DIAG\_EN low. In addition, the device can keep the power consumption to a minimum by setting DIAG\_EN and ENx low.

#### 7.3.6.2 Multiplexing of Current Sense

SELx pins are used to multiplex the shared current-sense function among the four channels within the same device. Pulling each pin high or low sets the corresponding channel to be output on the SNS pin if DIAG\_EN is high. FLT still represents a global interrupt that goes low if a fault occurs on any channel.

If current sense information is multiplexed across different devices, do not directly tie the SNS pins together across multiple devices. When the DIAG\_EN is LOW, there is an internal clamp at SNS pin that clamps the voltage to approximately 2V. One device SNS pin is able to affect the SNS readback of other devices if tied directly.

To use the SNS pin across multiple devices, connect individual SNS pin to different analog input pins of MCU; see [Figure 7-13](#). Alternatively, use an external analog MUX to connect to a single MCU pin; see [Figure 7-14](#).

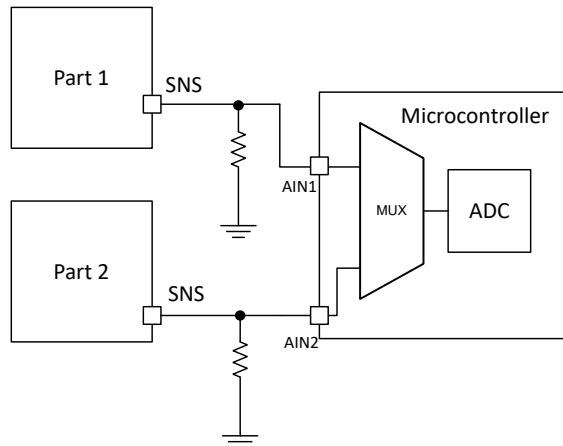


Figure 7-13. SNS Sharing Across Multiple Devices  
Method 1

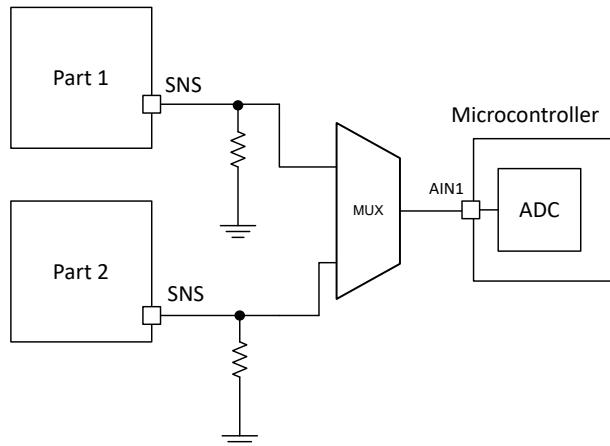


Figure 7-14. SNS Sharing Across Multiple Devices  
Method 2

Table 7-2. Diagnosis Configuration Table

DIAG_EN	ENx	SEL0	SEL1	SNS ACTIVATED CHANNEL	SNS	FLT	PROTECTIONS AND DIAGNOSTICS
L	H	—	—	—	0V. Clamp to 2V internally if external voltage is applied to the pin.	See Table 7-3	SNS disabled, FLT reporting, full protection
	L					High-Z	Diagnostics disabled, no protection
H	—	0	0	Channel 1	See Table 7-3	See Table 7-3	See Table 7-3
		0	1	Channel 2			
		1	0	Channel 3			
		1	1	Channel 4			

### 7.3.6.3 FAULT Reporting

The global  $\overline{\text{FLT}}$  pin is used to monitor the global fault condition among all the channels. When a fault condition occurs on any channel, the  $\overline{\text{FLT}}$  pin is pulled down to GND. A 3.3V or 5V external pullup is required to match the supply level of the microcontroller. The  $\overline{\text{FLT}}$  pin reports faults on any channel as long as the device is not in the SLEEP or LOW POWER MODE.

After the  $\overline{\text{FAULT}}$  report, the microcontroller can check and identify the channel in fault status by multiplexed current sensing. The SNS pin also works as a fault report with an internal pullup voltage,  $V_{\text{SNSFH}}$  if  $\text{DIAG\_EN}$  is high.

### 7.3.6.4 Fault Table

**Table 7-3. Fault Table**

CONDITIONS	ENx	OUTx	SNS (If $\text{DIAG\_EN}$ is high)	$\overline{\text{FLT}}$ (with external pullup)	BEHAVIOR	FAULT RECOVERY
Normal	L	L	0	H	Normal	—
	H	$V_{\text{BB}} - I_{\text{LOAD}} \times R_{\text{ON}}$	$I_{\text{LOAD}} / K_{\text{SNS}}$	H	Normal	—
Overcurrent	H	$V_{\text{BB}} - I_{\text{LIM}} \times R_{\text{ON}}$	$V_{\text{SNSFH}}$	L	Holds the current at the current limit until thermal shutdown or when the overcurrent event is removed.	Auto
Open load, short to battery, reverse polarity	L	H	$V_{\text{SNSFH}}$	L	Internal pull-up resistor is active. Fault is asserted when $V_{\text{VS}} - V_{\text{OUTx}} < V_{(\text{ol},\text{off})}$	Auto
	H	H	$I_{\text{LOAD}} / K_{\text{SNS}} \approx 0$	H	Normal behavior. User can make judgment based on SNS pin output.	—
Hot short	H	L	$V_{\text{SNSFH}}$	L	Device immediately shuts down, and re-enables into current limit.	Auto-retry into current limit until thermal shutdown. Auto-retry version repeats until the fault goes away. Latch version must toggle EN after first thermal shutdown.
Enable into permanent short	$L \rightarrow H$	L	$V_{\text{SNSFH}}$	L	Device enables into current limit until thermal shutdown.	Enable into current limit until thermal shutdown. Auto-retry version repeats until the fault goes away. Latch version requires EN to be toggled after the first thermal shutdown.
Absolute thermal shutdown, Relative thermal shutdown	H	L	$V_{\text{SNSFH}}$	L	Shuts down when devices hits relative or absolute thermal shutdown.	For auto-retry version, output auto-retry after $t_{\text{RETRY}}$ . Fault recovers when $T_J < T_{\text{HYS}}$ or when EN toggles. Latch version recovers only when EN toggles.
Reverse polarity	X	X	X		X	Channel turns on to lower power dissipation. Limit current into ground pin by external ground network.

### 7.3.7 Full Diagnostics

#### 7.3.7.1 Short-to-GND and Overload Detection

When a channel is on, a short to GND or overload condition causes overcurrent. If the overcurrent triggers either the internal or external current-limit threshold, the fault condition is reported out. The microcontroller can handle the overcurrent by turning off the switch. The device clamps the current to  $I_{CL}$  until thermal shutdown. TPS4HC120A automatically recovers when the fault condition is removed.

In a hot short condition, when the short-circuit is applied when the EN is HIGH, the device shuts down immediately and auto-retries the same as enable into permanent short condition, as shown in [Figure 7-9](#).

#### 7.3.7.2 Open-Load Detection

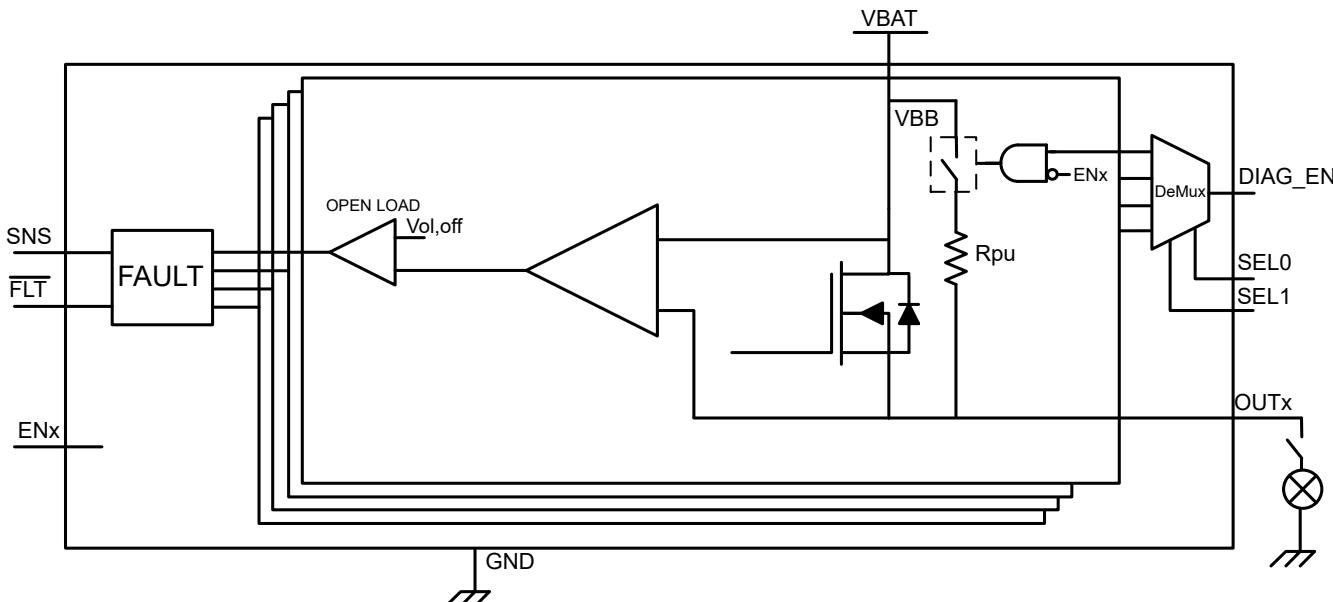
##### 7.3.7.2.1 Channel On

When a channel is ON, benefiting from the high-accuracy current sense in the small current range, an open-load event can be detected as an ultra low  $V_{SNS}$  and handled by the microcontroller. Note that the detection is not reported on the  $\overline{FAULT}$  pin or the fault registers. The microcontroller must multiplex the SEL and SEH pins to output the correct channel out on the SNS pin.

##### 7.3.7.2.2 Channel Off

In the OFF state, when  $DIAG\_EN$  is high, there is an internal pull-up resistor  $R_{OL}$  that pulls up a channel to  $V_{BB}$ . The specific channel that gets pulled up is based on the selection of SEL0 and SEL1, and the other channels do not have the pull-up resistor engaged.

If there is load present at the selected channel, then the output voltage is pulled to around 0V, as the load is much stronger than the  $R_{OL}$ . In the case of an open load, the output voltage is pulled close to the supply voltage by the  $R_{OL}$ . If  $V_{BB} - V_{OUT} < V_{OL,off}$  for the selected channel, the  $\overline{FLT}$  pin goes low to indicate the fault to the MCU, and the SNS pin is pulled up to  $I_{SNSFH}$ .



**Figure 7-15. Open-Load Detection in Off-State**

#### 7.3.7.3 Short-to-Battery Detection

Short-to-battery has the same detection mechanism and behavior as open-load detection, in both the on-state and off-state. See [Table 7-3](#) for more details.

#### 7.3.7.4 Reverse-Polarity and Battery Protection

Reverse-polarity, commonly referred to as reverse battery, occurs when the ground of the device goes to the battery potential,  $V_{GND} = V_{BAT}$ , and the supply pin goes to ground,  $V_{BB} = 0V$ . In this case, if the EN2 pin has a path to the *ground* plane, then the FET turns on to lower the power dissipation through the main channel and prevent current flow through the body diode. The resistor-diode ground network (if there is no central blocking diode on the supply) is required for device protection during a reverse-battery event.

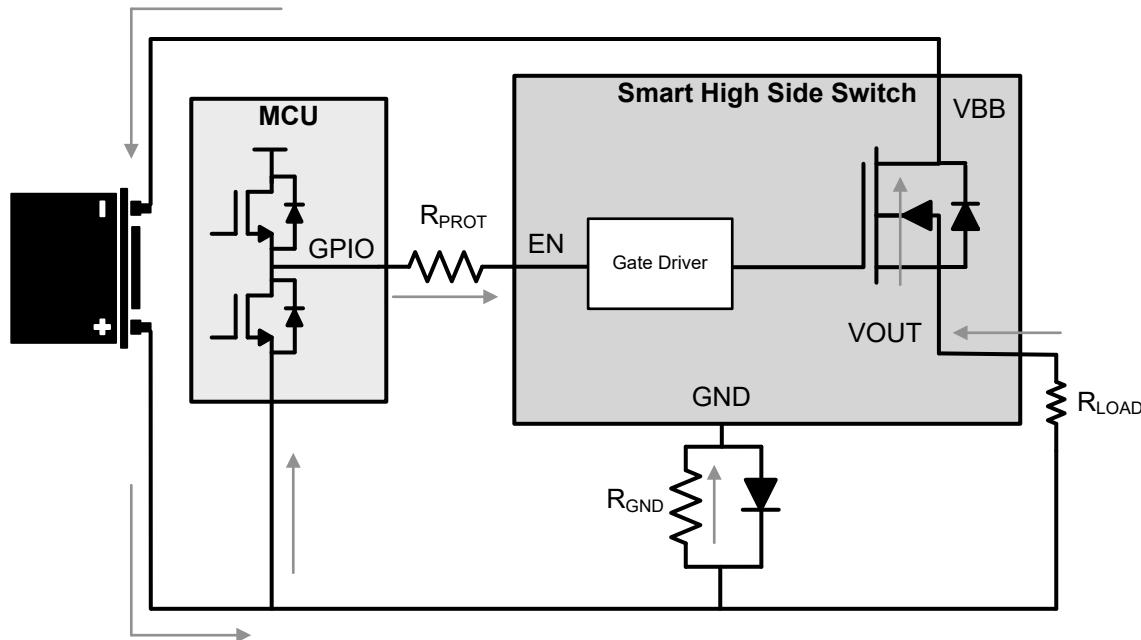


Figure 7-16. Reverse Battery Circuit

See also [Section 7.3.8.4](#) and [Table 7-3](#).

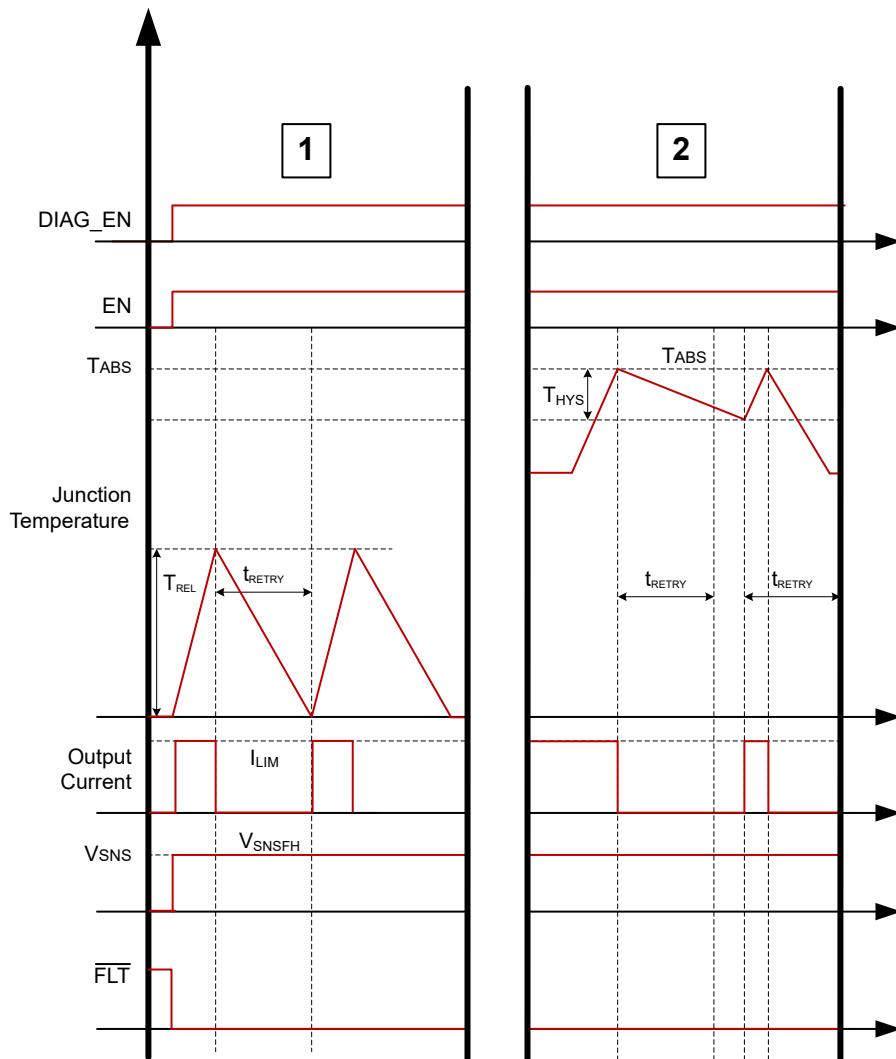
#### 7.3.7.5 Thermal Fault Detection

To protect the device in severe power stressing cases, the device implements two types of thermal fault detection, absolute temperature protection (absolute thermal shutdown) and dynamic temperature protection (relative thermal shutdown). Respective temperature sensors are integrated close to each power FET, so the thermal fault is reported by each channel. This arrangement can help the device keep the cross-channel effect to a minimum when some channels are in a thermal fault condition.

##### 7.3.7.5.1 Thermal Protection Behavior

The thermal protection behavior can be split up into three categories of events that can happen. [Figure 7-17](#) shows each of these categories.

- Relative thermal shutdown:** The device is enabled into an overcurrent event. The output current rises up to the  $I_{ILIM}$  level and the  $\overline{FLT}$  goes low. With this large amount of current going through the junction temperature of the FET increases rapidly with respect to the controller temperature. When the power FET temperature rises  $T_{REL}$  amount above the controller junction temperature  $\Delta T = T_{FET} - T_{CON} > T_{REL}$ , the device shuts down. For auto-retry version, after  $t_{RETRY}$ , the part tries to restart. The latch version requires EN to be toggled to re-enable the channel. The  $\overline{FLT}$  pin is asserted until the fault condition is cleared.
- Absolute thermal shutdown:** The device is still enabled in an overcurrent event. However, in this case the junction temperature rises up and hits an absolute reference temperature,  $T_{ABS}$ , and then shuts down. For auto-retry version, the device does not recover until both  $T_J < T_{ABS} - T_{hys}$  and the  $t_{RETRY}$  timer has expired. For latch version, toggling EN is required to re-enable the channel.



**Figure 7-17. Thermal Behavior for Auto-Retry Version**

### 7.3.8 Full Protections

#### 7.3.8.1 UVLO Protection

The device monitors the supply voltage  $V_{VBB}$ , to prevent unpredicted behaviors when  $V_{VBB}$  is too low. When  $V_{VBB}$  falls down to  $V_{UVLOF}$ , the device shuts down. When  $V_{VBB}$  rises up to  $V_{UVLOR}$ , the device turns on.

#### 7.3.8.2 Loss of GND Protection

When loss of GND occurs, output is turned off regardless of whether the input signal is high or low.

**Case 1 (loss of device/IC GND):** loss of GND protection is active when the thermal pad (Tab), IC GND, and current limit ground are one trace connected to the system ground, as shown in [Figure 7-18](#).

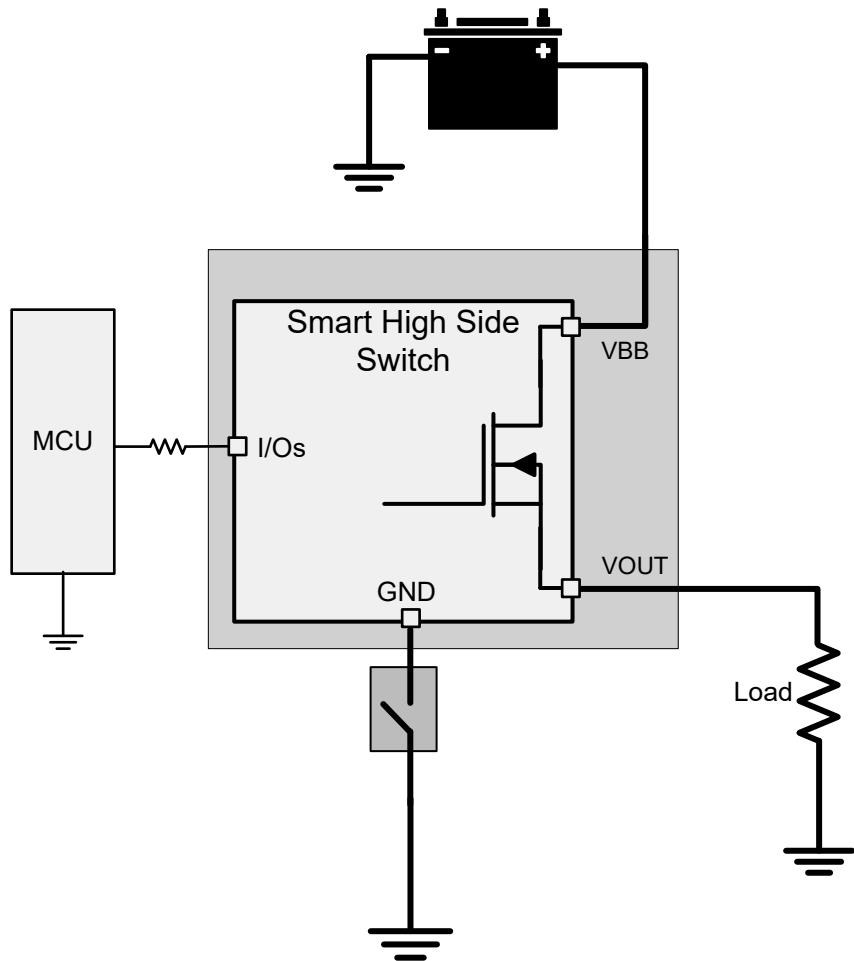


Figure 7-18. Loss of Device GND

**Case 2 (loss of module GND):** when the whole ECU module GND is lost, protections are also active. At this condition, the load GND remains connected.

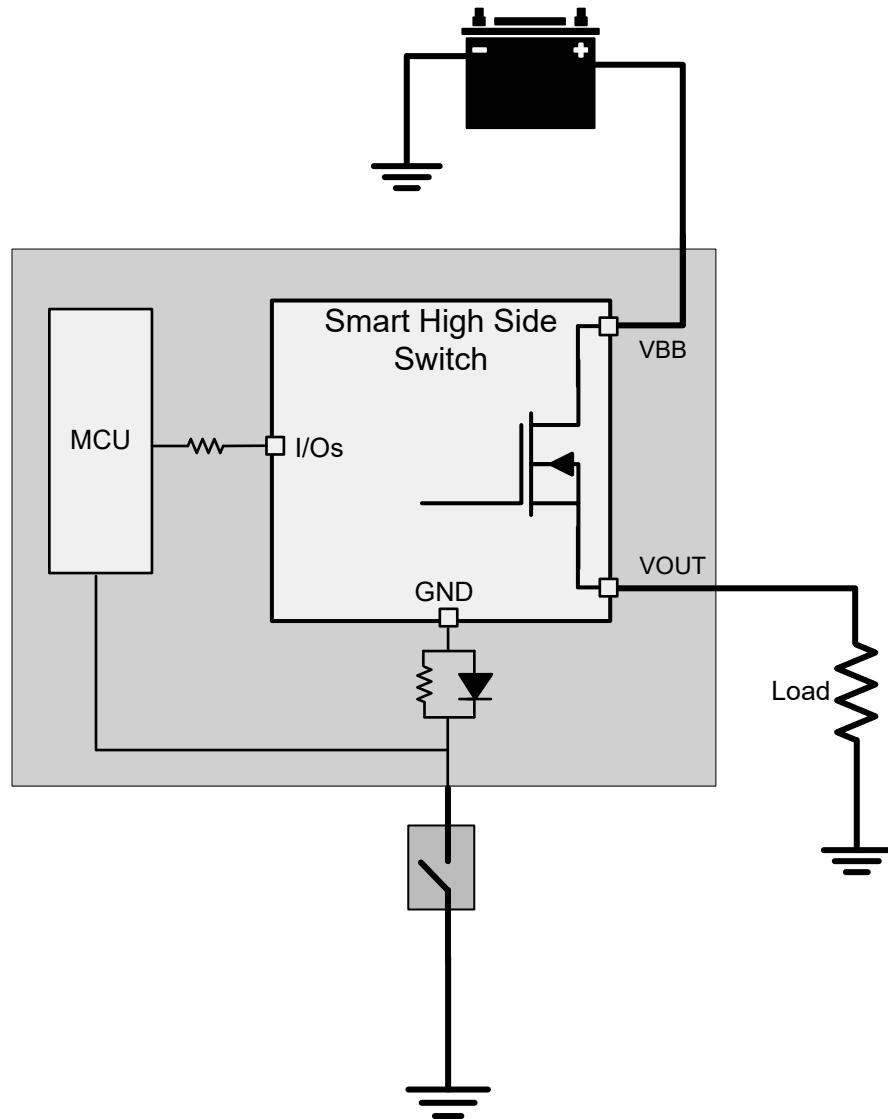


Figure 7-19. Loss of Module GND

### 7.3.8.3 Loss of Power Supply Protection

When loss of supply occurs, output is turned off regardless of whether the input is high or low. For a resistive or capacitive load, loss of supply protection is easy to achieve due to no more power. The worst case is a charged inductive load. In this case, the current is driven from all of the IOs to maintain the inductance output loop. TI recommends either the MCU serial resistor plus the GND network (diode and resistor in parallel) or external free-wheeling circuitry.

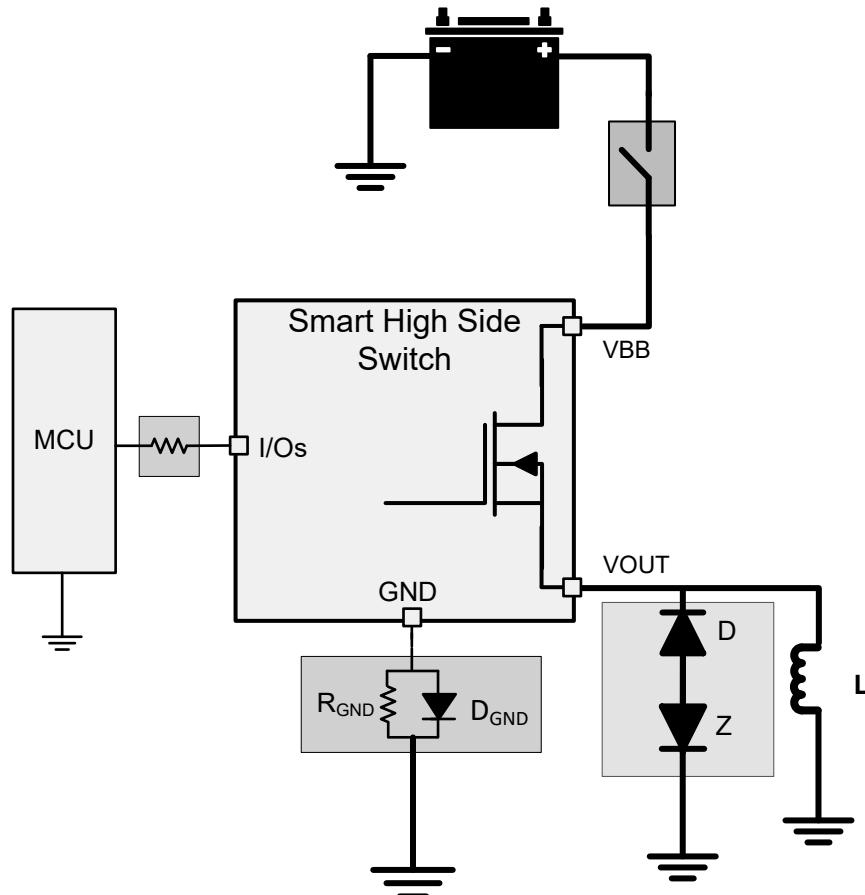


Figure 7-20. Loss of Battery

#### 7.3.8.4 Reverse Polarity Protection

**Method 1:** Block diode connected with  $V_{BB}$ . Both the device and load are protected when in reverse polarity. The blocking diode does not allow any of the current to flow during reverse battery condition.

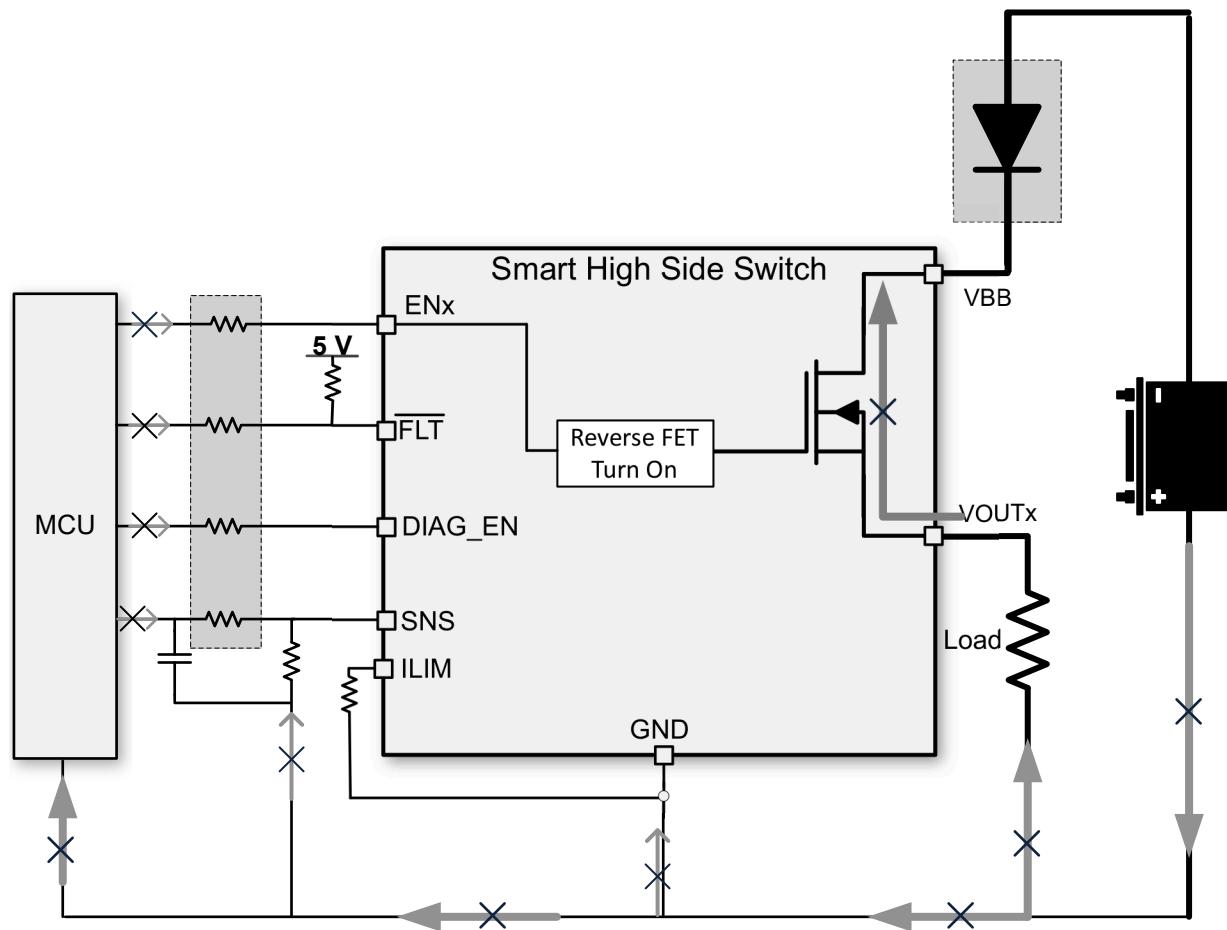


Figure 7-21. Reverse Protection With Block Diode

**Method 2 (GND network protection):** Only the high-side device is protected under this connection. The load reverse current is limited by the impedance of the load. When reverse polarity happens, the continuous reverse current through the power FET must not make the heat build up be greater than the absolute maximum junction temperature. Device temperature is calculated using the  $R_{ON(REV)}$  value and the  $R_{\theta JA}$  specification. In the reverse-battery condition, ensure that the FET comes on to lower the power dissipation. This action is achieved through the path from EN to system ground where the positive voltage is being applied. No matter what types of connection are between the device GND and the board GND, if a GND voltage shift happens, ensure the following proper connections for the normal operation:

- Connect the current limit programmable resistor to the device GND.

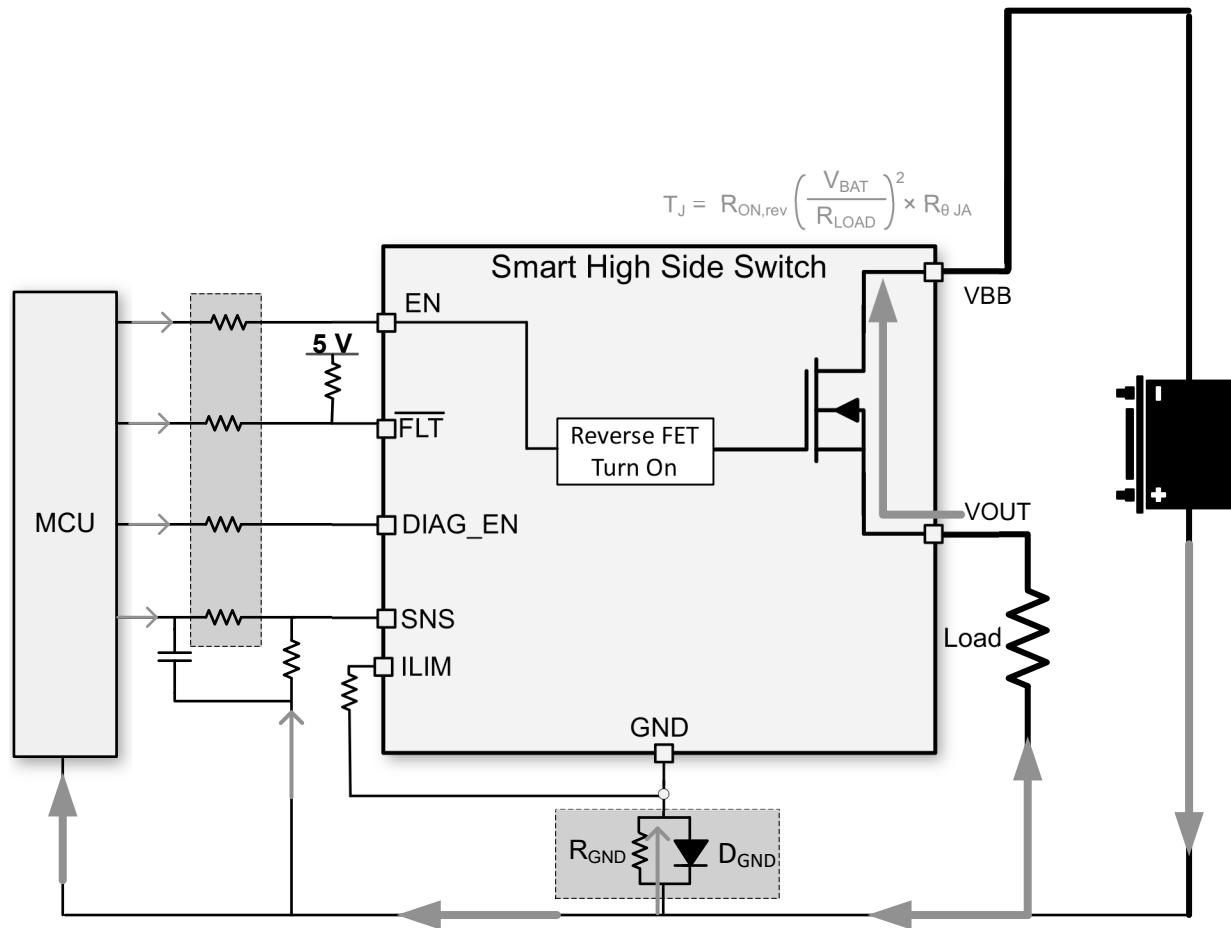


Figure 7-22. Reverse Protection With GND Network

- Recommendation – resistor and diode in parallel:** A peak negative spike sometimes occurs when the inductive load is switching off, which can damage the HSD or the diode. Therefore, TI recommends a resistor in parallel with the diode when driving an inductive load. The recommended selection are a 1kΩ resistor in parallel with an  $I_F > 100\text{mA}$  diode. If multiple high-side switches are used, share the resistor and diode among devices.

If multiple high-side power switches are used, share the resistor among devices.

- Ground Resistor:** The higher resistor value contributes to a better current limit effect when the reverse battery or negative ISO pulses.

$$R_{GND} \geq \frac{(-V_{CC})}{(-I_{GND})} \quad (6)$$

where

- $-V_{CC}$  is the maximum reverse battery voltage (typically  $-16\text{V}$ ).
- $-I_{GND}$  is the maximum reverse current the ground pin can withstand, which is available in the *Absolute Maximum Ratings*.
- Ground Diode:** A diode is needed to block the reverse voltage, which also brings a ground shift ( $\approx 600\text{mV}$ ). Additionally, the diode must be  $\approx 200\text{V}$  reverse voltage for the ISO 7637 pulse 1 testing so that the diode is not biased.

#### 7.3.8.5 Protection for MCU I/Os

In many conditions, such as the negative ISO pulse, or the loss of battery with an inductive load, a negative potential on the device GND pin is able to potentially damage the MCU I/O pins (more likely, the internal circuitry connected to the pins). Therefore, serial resistors between MCU and HSS are required.

Also, for proper protection against loss of GND, TI recommends 10k $\Omega$  resistance for the  $R_{PROT}$  resistors.

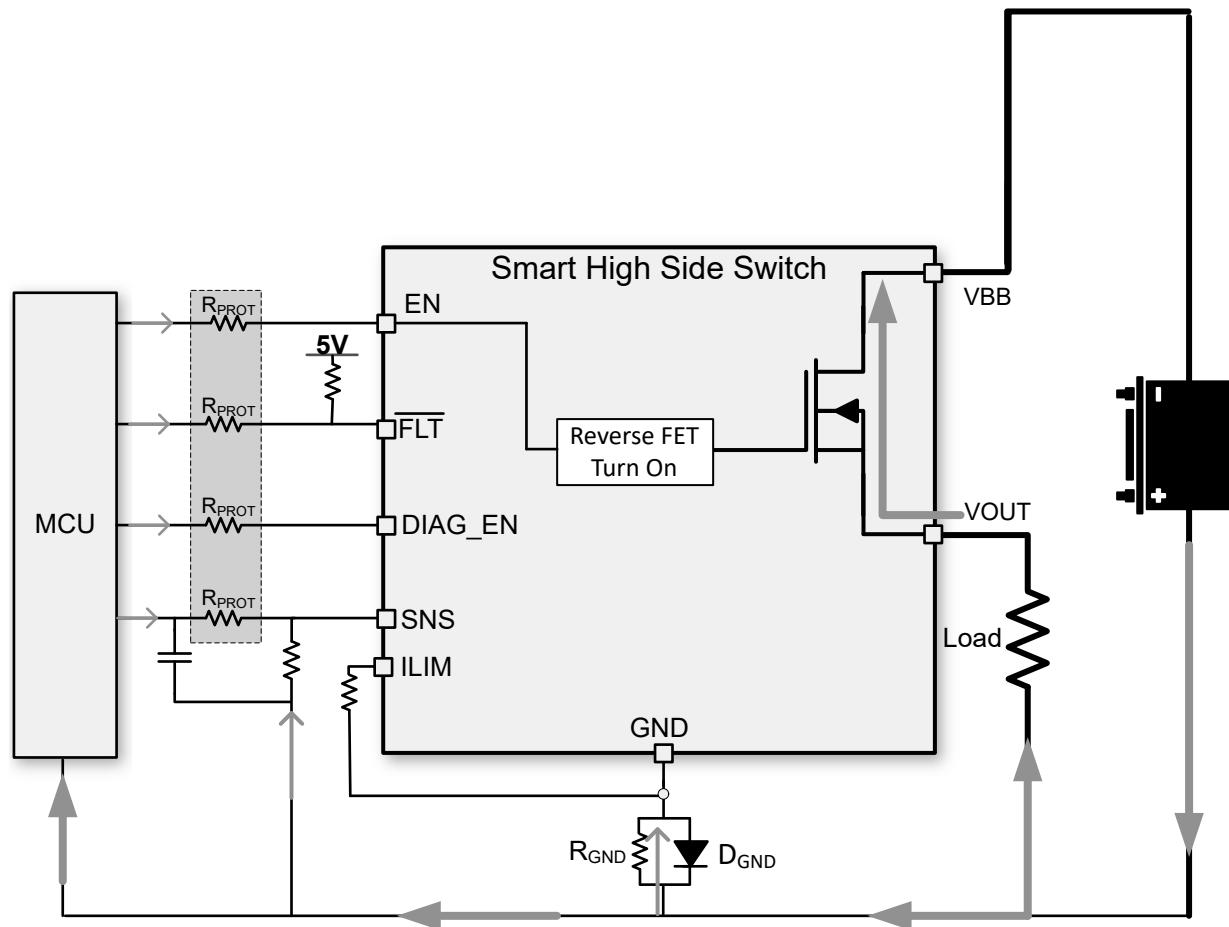


Figure 7-23. MCU I/O Protections

## 7.4 Device Functional Modes

### 7.4.1 Working Modes

This device has several states to transition into based on the ENx pins, DIAG\_EN pin, and load conditions.

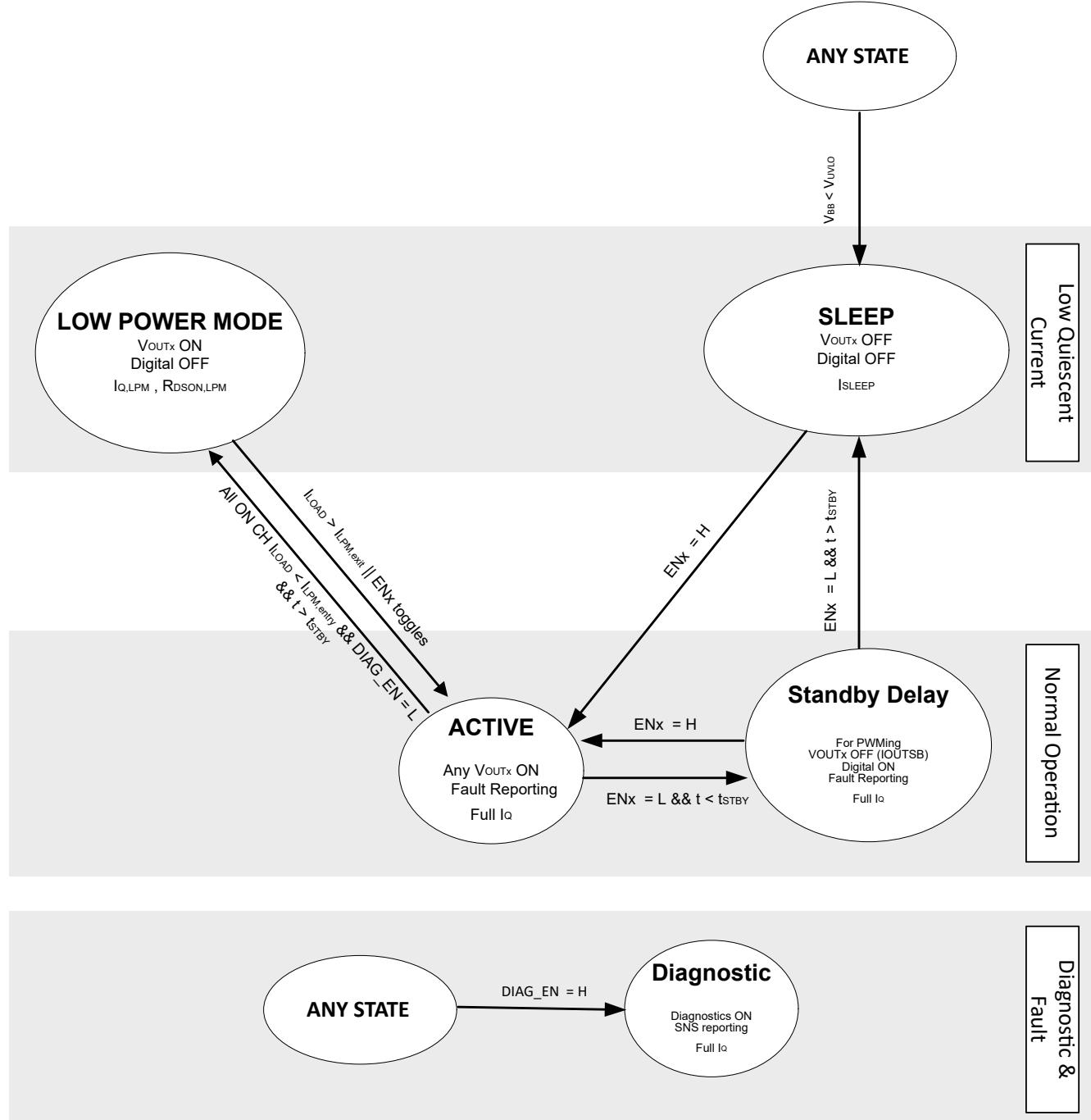


Figure 7-24. State Diagram

#### 7.4.1.1 SLEEP

In the SLEEP state, everything inside the device is turned off and the quiescent current is the  $I_{SLEEP}$ . The device only transitions out of the SLEEP state if the ENx pins or DIAG\_EN pin is pulled high. From the SLEEP state, the device is able to transfer into the ACTIVE state if any of the ENx pins are pulled high, or into the DIAGNOSTIC state if the DIAG\_EN pin, without any of the ENx pins, goes high. Additionally, if the device is in any of the states and VBB drops to less than  $V_{UVLOF}$ , the device transitions into SLEEP state.

#### 7.4.1.2 DIAGNOSTIC

The DIAGNOSTIC state is when the device is outputting diagnostics on the SNS and  $\bar{FLT}$  pins. This state occurs when the device is in any previous state and the DIAG\_EN pin goes high. The off-state diagnostics are comprised of open load detection in off-state and short-to-battery detection. The  $\bar{FLT}$  pin asserts if there is a fault on any of the channels, but the SNS pin only outputs a fault for the channel associated to the SELx pin values. From the DIAGNOSTIC state, the device transfers into the ACTIVE state if the DIAG\_EN pin goes back low and any channel is on, or into the STANDBY DELAY state if all channels are off.

#### 7.4.1.3 ACTIVE

The ACTIVE state is when any of the channel outputs are on by the ENx pin associated. In the ACTIVE state, the current limit value is set by the external resistor on the ILIM pin. If the DIAG\_EN pin is pulled high while in the ACTIVE state, the SNS pin outputs a proportional current to the load current of the channel associated to the SELx pins configuration until a fault occurs on that channel. Additionally the  $\bar{FLT}$  pin reports if there is a fault occurring on any channel. The device can transition out of the ACTIVE state by turning off all of the channels while DIAG\_EN is high or low, or a fault occurring. If all of the channels turn off and DIAG\_EN is high, the device transitions into the DIAGNOSTIC state. If all of the channels turn off and the DIAG\_EN pin is low, then the device transfers into the STANDBY DELAY state.

#### 7.4.1.4 STANDBY DELAY

The STANDBY DELAY state is when the ENx pins are all low, the outputs are all turned off, and the DIAG\_EN pin is also low, but there has not yet been  $t_{STBY}$  amount of time. This state is included so that the channel outputs are able to support PWM without all of the internal rails being cut off and put into SLEEP mode. After the device has waited  $t_{STBY}$ , the device completely shuts down and transitions into SLEEP. However, if during  $t_{STBY}$ , ENx goes high, the device transitions into ACTIVE without shutting completely down. Similarly if the DIAG\_EN goes high, the device transitions into DIAGNOSTIC.

#### 7.4.1.5 LOW POWER MODE

The LOW POWER MODE state is when the channels that are active are less than the  $I_{LPM,entry}$  level for longer than  $t_{STBY}$  and the DIAG\_EN is low. The device turns off all unnecessary internal blocks and reduces the quiescent current from  $I_Q$  to  $I_{Q,LPM}$ . The device is still protected but no diagnostics or fault reporting is possible until device comes out of this mode. See also [Section 7.3.2](#).

## 8 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 8.1 Application Information

The TPS4HC120-Q1 device is capable of driving a wide variety of resistive, inductive, and capacitive loads, including the low-wattage bulbs, LEDs, relays, solenoids, heaters, and sub-modules. Full diagnostics and high-accuracy current-sense features enable intelligent control of the load. An external adjustable current limit improves the reliability of the whole system by clamping the inrush or overload current.

#### 8.1.1 EMC Transient Disturbances Test

As a result of the severe electrical conditions in the automotive environment, immunity capacity against electrical transient disturbances is required, especially for a high-side power switch, which is connected directly to the battery. Detailed test requirements are in accordance with the ISO 7637-2:2011 and ISO 16750-2:2010 standards.

**Table 8-1. ISO 7637-2:2011(E) in 12V System**

TEST ITEM (1) (2)	TEST PULSE SEVERITY LEVEL AND V <sub>S</sub> ACCORDINGLY		PULSE DURATION (t <sub>d</sub> )	MINIMUM NUMBER OF PULSES OR TEST TIME	BURST-CYCLE PULSE- REPETITION TIME		INPUT RESISTANCE (Ω)	FUNCTION PERFORMANCE STATUS CLASSIFICATION <sup>(3)</sup>
	LEVEL	V <sub>S</sub> /V			MIN	MAX		
1	III	-112	2ms	500 pulses	0.5s	—	10	Status II
2a	III	55	50μs	500 pulses	0.2s	5s	2	Status II
2b	IV	10	0.2s to 2s	10 pulses	0.5s	5s	0 to 0.05	Status II
3a	IV	-220	0.1μs	1h	90ms	100ms	50	Status II
3b	IV	150	0.1μs	1h	90ms	100ms	50	Status II

(1) Tested both under input low condition and high condition.

(2) GND pin network is a 1kΩ resistor in parallel with a diode BAS21-7-F.

(3) Status II: The function does not perform as designed during the test, but returns automatically to normal operation after the test.

**Table 8-2. ISO 16750-2:2010(E) Load Dump Test B in 12V System**

TEST ITEM (1) (2) (3)	TEST PULSE SEVERITY LEVEL AND V <sub>S</sub> ACCORDINGLY		PULSE DURATION (t <sub>d</sub> )	MINIMUM NUMBER OF PULSES OR TEST TIME	BURST-CYCLE PULSE- REPETITION TIME		INPUT RESISTANCE (Ω)	FUNCTION PERFORMANCE STATUS CLASSIFICATION <sup>(4)</sup>
	LEVEL	V <sub>S</sub> /V			MIN	MAX		
Test B	N/A	35	40ms to 400ms	5 pulses	60s		0.5 to 4	Status II

(1) Tested both under input low condition and high condition (DIAG\_EN, ENx, and VBB are all classified as inputs).

(2) Considering the worst test condition, the device is tested without any filter capacitors on VBB and VOUTx.

(3) The GND pin network is a 1kΩ resistor in parallel with a diode BAS21-7-F.

(4) Status II: The function does not perform as designed during the test, but returns automatically to normal operation after the test.

## 8.2 Typical Application

Figure 8-1 shows an example of the external circuitry connections for TPS4HC120.

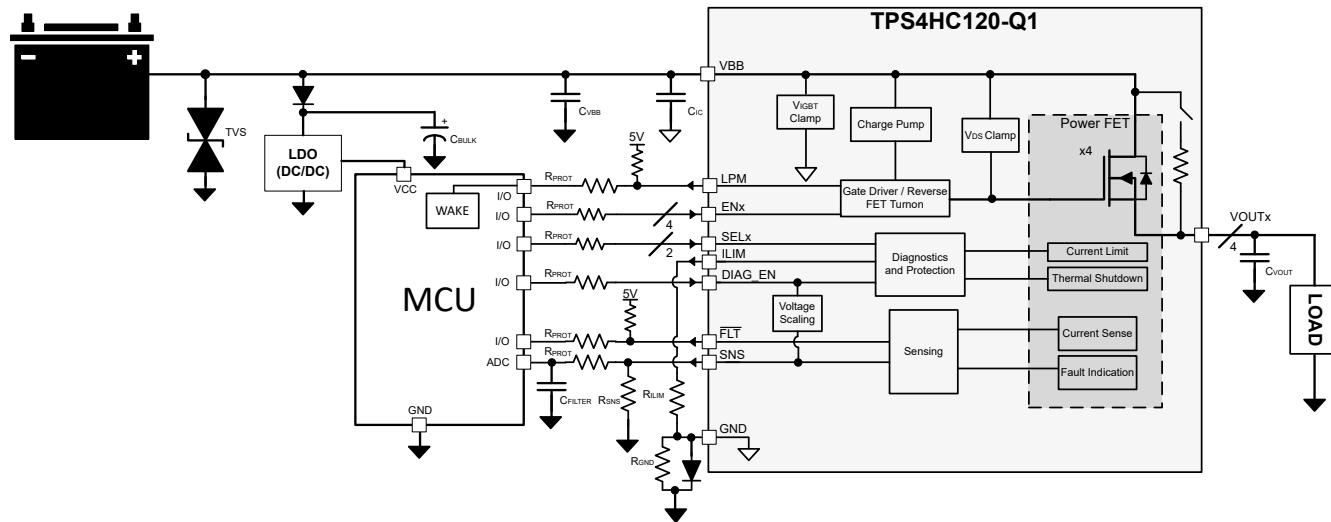


Figure 8-1. Typical Application Diagram

Table 8-3. Recommended Component Values

COMPONENT	DESCRIPTION	PURPOSE
TVS	SMBJ39CA	Filter voltage transients coming from battery (ISO7637-2)
C <sub>VBB</sub>	220nF	Better EMI performance
C <sub>IC</sub>	100nF	Minimal amount of capacitance on input for EMI mitigation
C <sub>BULK</sub>	10µF	Help filter voltage transients on the supply rail
R <sub>PROT</sub>	10kΩ	Protection resistor for microcontroller and device I/O pins
R <sub>LIM</sub>	Discrete values as listed in Table 7-1	Set current limit threshold
R <sub>SNS</sub>	1kΩ	Translate the sense current into sense voltage
C <sub>FILTER</sub>	100nF	Coupled with R <sub>PROT</sub> on the SNS line creates a low pass filter to filter out noise going into the ADC of the MCU
C <sub>VOUT</sub>	22nF	Improves EMI performance, filtering of voltage transients
R <sub>PULLUP</sub>	5kΩ	Pull up resistor for open-drain pins (FLT and LPM)
R <sub>GND</sub>	1kΩ	Stabilize GND potential during turn-off of inductive load
D <sub>GND</sub>	BAS21 Diode	Keeps GND close to system ground during normal operation

### 8.2.1 Design Requirements

Table 8-4. Example Design Requirements

PARAMETER	VALUE
V <sub>DIAG_EN</sub>	5V
I <sub>LOAD,max</sub>	1A
I <sub>LOAD,min</sub>	10mA
V <sub>ADC,min</sub>	5mV
V <sub>HR</sub>	1V

### 8.2.2 Detailed Design Procedure

To keep the 1A nominal current in the 0V to 4V current-sense range, calculate the R<sub>(SNS)</sub> resistor using Equation 7. To achieve better current-sense accuracy, a 1% tolerance or better resistor is preferred.

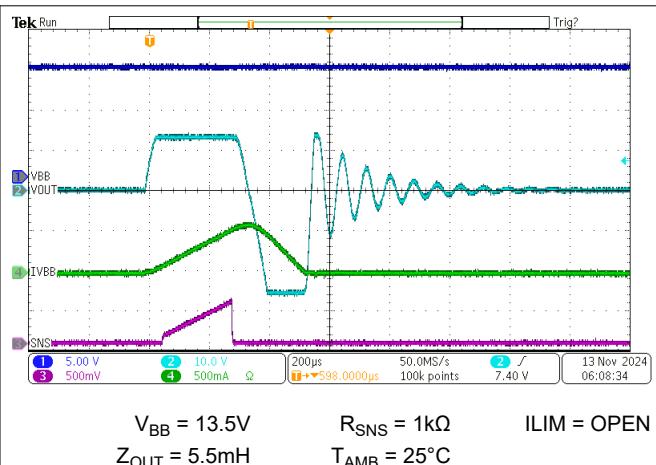
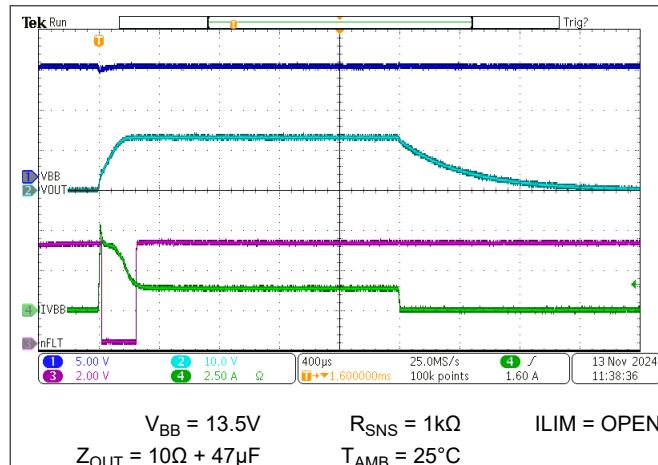
$$V_{ADC,min} \times K_{SNS} / I_{LOAD,min} \leq R_{SNS} \leq (V_{SNSFH} - V_{HR}) \times K_{SNS} / I_{LOAD,max} \quad (7)$$

The design requirement listed in [Table 8-4](#) yields  $520\Omega \leq R_{SNS} \leq 4160\Omega$ , and  $1k\Omega R_{SNS}$  satisfies the requirements.

To set the adjustable current limit value, use the  $R_{ILIM}$  recommended in the [Current Limit Table](#). In this application, to leave enough margin for the current transient and ripple, a  $9.76k\Omega R_{ILIM}$  resistor satisfies the requirements.

### 8.2.3 Application Curves

[Figure 8-2](#) shows a test example of soft-start when driving a big capacitive load. [Figure 8-3](#) shows the VDS clamp engaging during inductive load discharge.



### 8.3 Power Supply Recommendations

The device is qualified for both automotive and industrial applications. The normal power supply connection is a 12V automotive system. The supply voltage must be within the range specified in the [Recommended Operating Conditions](#).

**Table 8-5. Voltage Operating Ranges**

VBB VOLTAGE RANGE	NOTE
3V to 6V	Extended lower 12V automotive battery operation such as cold crank and start-stop. Device is fully functional and protected but some parametrics such as $R_{ON}$ , current sense accuracy, current limit accuracy and timing parameters can deviate from specifications. Check the individual specifications in <a href="#">Section 6.5</a> to confirm the applicable voltage range.
6V to 18V	Nominal 12V automotive battery voltage range. All parametric specifications apply and the device is fully functional and protected.
18V to 24V	Extended upper 12V automotive battery operation such as double battery. Device is fully functional and protected but some parametrics such as $R_{ON}$ , current sense accuracy, current limit accuracy, and timing parameters can deviate from specifications. Check the individual specifications in <a href="#">Section 6.5</a> to confirm the applicable voltage range.
35V	Load dump voltage. Device is operational and lets the pulse pass through without being damaged but does not protect against short circuits.

## 8.4 Layout

### 8.4.1 Layout Guidelines

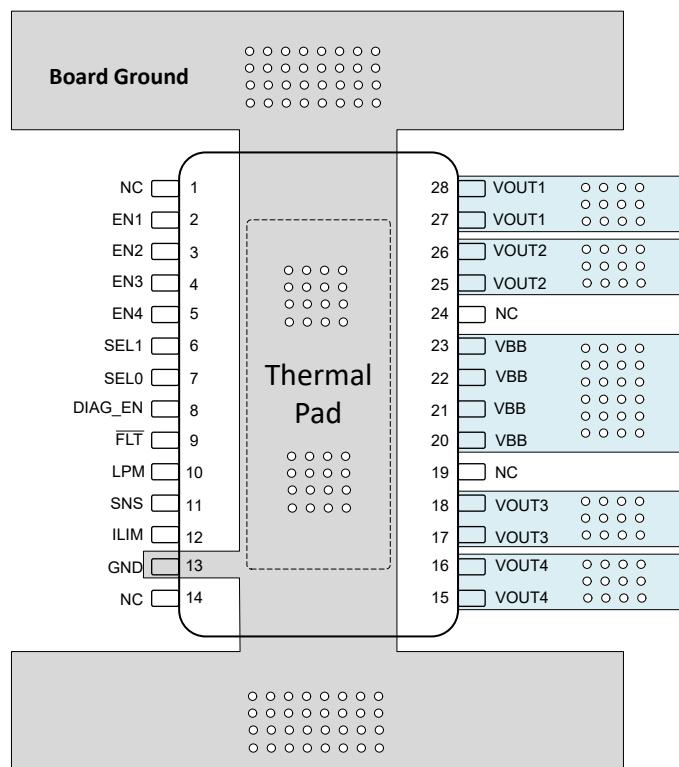
To prevent thermal shutdown,  $T_J$  must be less than 150°C. The HTSSOP package has good thermal impedance. However, the PCB layout is very important. Good PCB design helps optimize heat transfer, which is absolutely essential for the long-term reliability of the device.

- Maximize the copper coverage on the PCB to increase the thermal conductivity of the board. The major heat flow path from the package to the ambient is through the copper on the PCB. Maximum copper is extremely important when no heat sinks are attached to the PCB on the other side of the package.
- Add as many thermal vias as possible directly under the package ground pad to optimize the thermal conductivity of the board.
- To prevent solder voids, ensure that all thermal vias are either plated shut or plugged and capped on both sides of the board. To maintain reliability and performance, the maintain at least 85% solder coverage.

### 8.4.2 Layout Examples

#### 8.4.2.1 Without a GND Network

Without a GND network, tie the thermal pad directly to the board GND copper for better thermal performance.



**Figure 8-4. Layout Example Without a GND Network**

#### 8.4.2.2 With a GND Network

With a GND network, tie the thermal pad with a single trace through the GND network to the board GND copper. Have more IC GND coverage to get better thermal performance of the part.

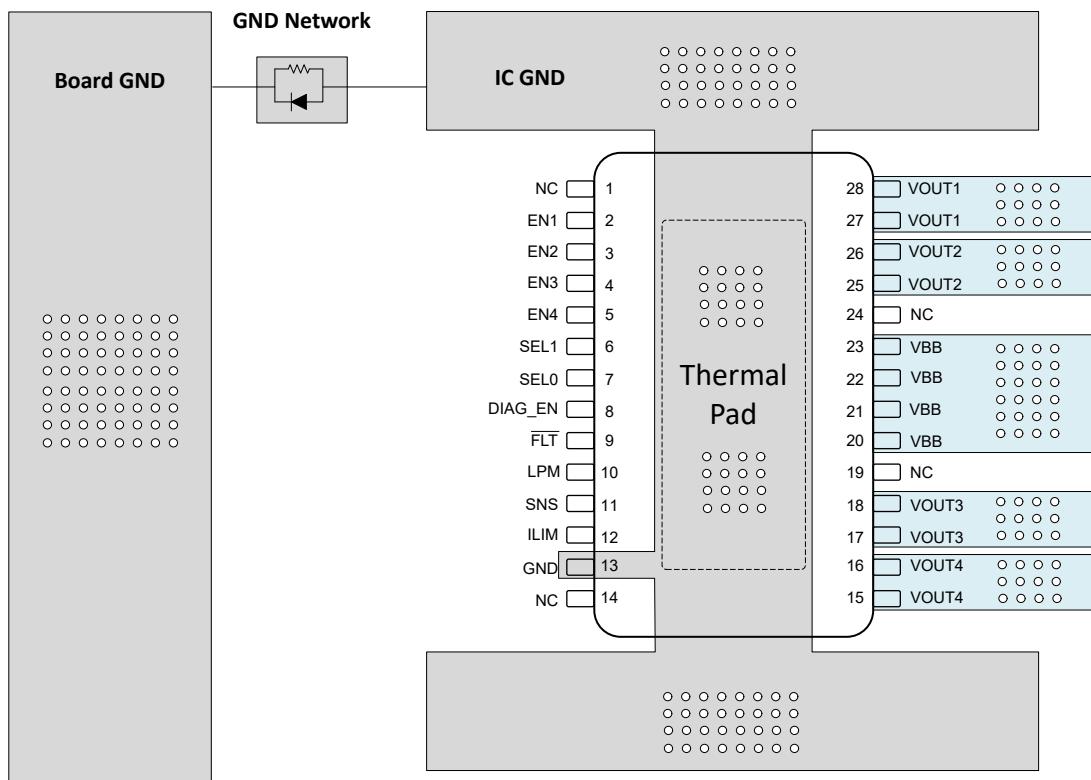


Figure 8-5. Layout Example With a GND Network

## 9 Device and Documentation Support

### 9.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](#). Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 9.2 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

### 9.3 Trademarks

TI E2E™ is a trademark of Texas Instruments.

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### 9.4 Electrostatic Discharge Caution

 This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 9.5 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

## 10 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision A (January 2025) to Revision B (July 2025)</b>	<b>Page</b>
• Changed TPS4HC120B-Q1 status from preview to production data (active).....	1
• Updated formatting and page flow for clarity.....	1

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<b>Changes from Revision * (December 2024) to Revision A (January 2025)</b>	<b>Page</b>
• Added <i>Device Comparison Table</i> .....	2
• Updated to show LPM pin added.....	14
• Added description for both auto-retry and latch versions.....	19
• FLT now reports regardless of DIAG_EN.....	22
• FLT now reports regardless of DIAG_EN.....	24
• Updated the table to add description for auto-retry and latch versions.....	24

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## 11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most-current data available for the designated device. This data is subject to change without notice and without revision of this document. For browser-based versions of this data sheet, see the left-hand navigation pane.

**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS4HC120AQDGQRQ1	Active	Production	HVSSOP (DGQ)   28	2500   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	4HC120A
TPS4HC120AQDGQRQ1.A	Active	Production	HVSSOP (DGQ)   28	2500   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	4HC120A
TPS4HC120BQDGQRQ1	Active	Production	HVSSOP (DGQ)   28	2500   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	4HC120B

<sup>(1)</sup> **Status:** For more details on status, see our [product life cycle](#).

<sup>(2)</sup> **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

<sup>(4)</sup> **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

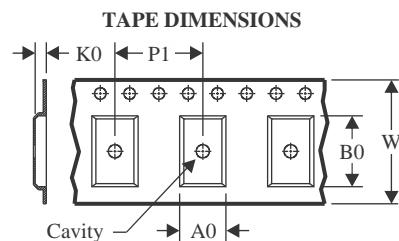
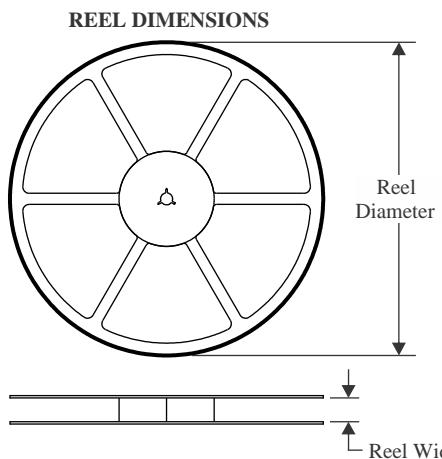
<sup>(5)</sup> **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

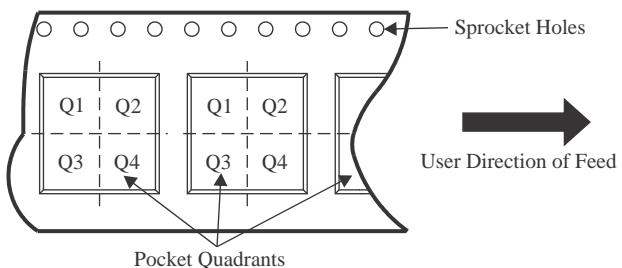
Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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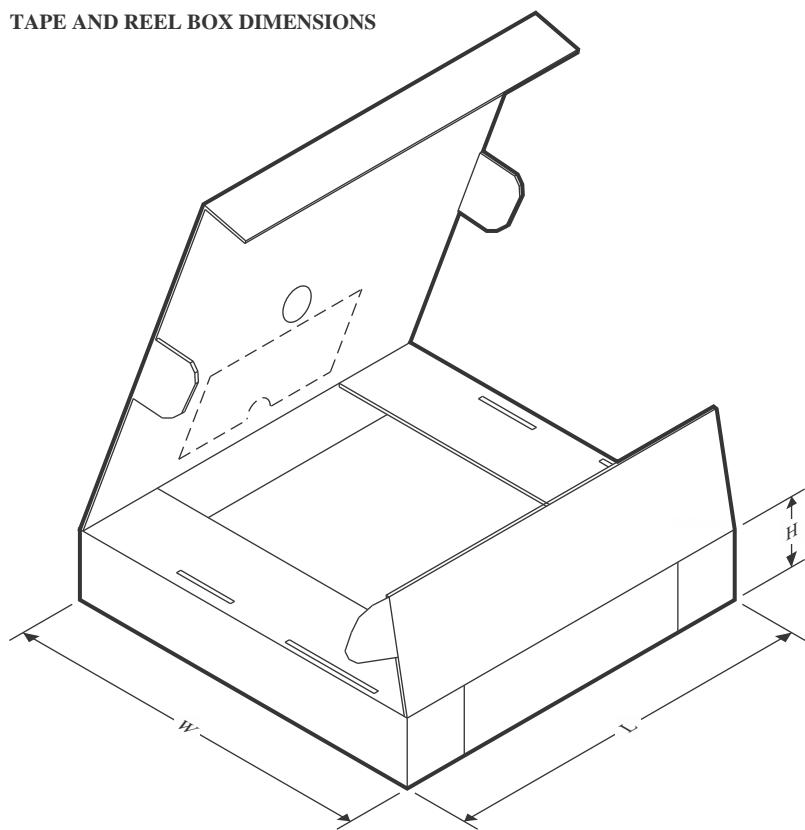
**TAPE AND REEL INFORMATION**


A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS4HC120AQDGQRQ1	HVSSOP	DGQ	28	2500	330.0	16.4	5.5	7.4	1.45	8.0	16.0	Q1
TPS4HC120BQDGQRQ1	HVSSOP	DGQ	28	2500	330.0	16.4	5.5	7.4	1.45	8.0	16.0	Q1

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS4HC120AQDGQRQ1	HVSSOP	DGQ	28	2500	353.0	353.0	32.0
TPS4HC120BQDGQRQ1	HVSSOP	DGQ	28	2500	353.0	353.0	32.0

## GENERIC PACKAGE VIEW

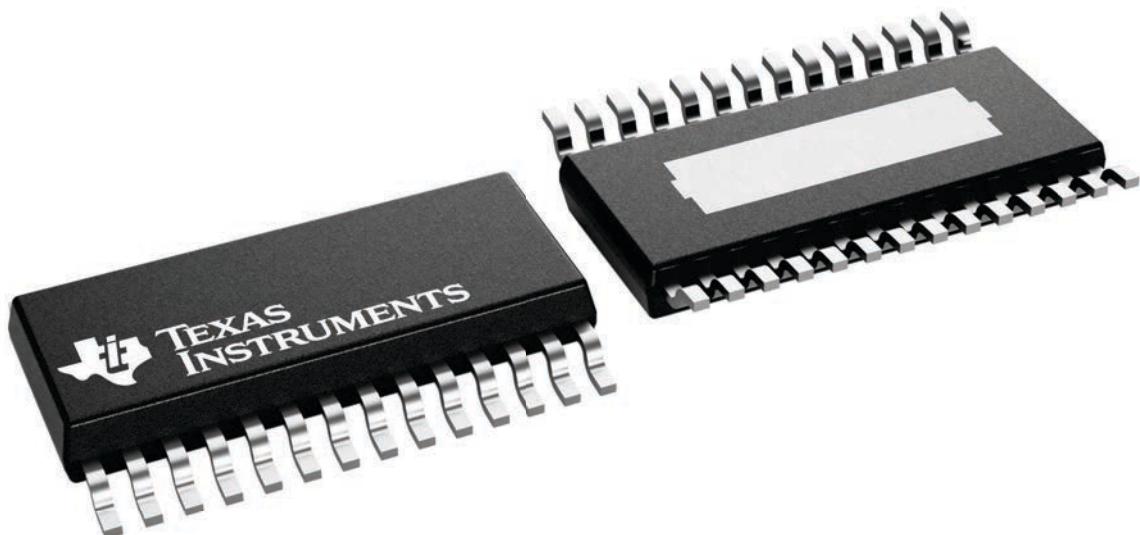
**DGQ 28**

3 x 7.1, 0.5 mm pitch

**HVSSOP - 1.1 mm max height**

SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.



4226530/A

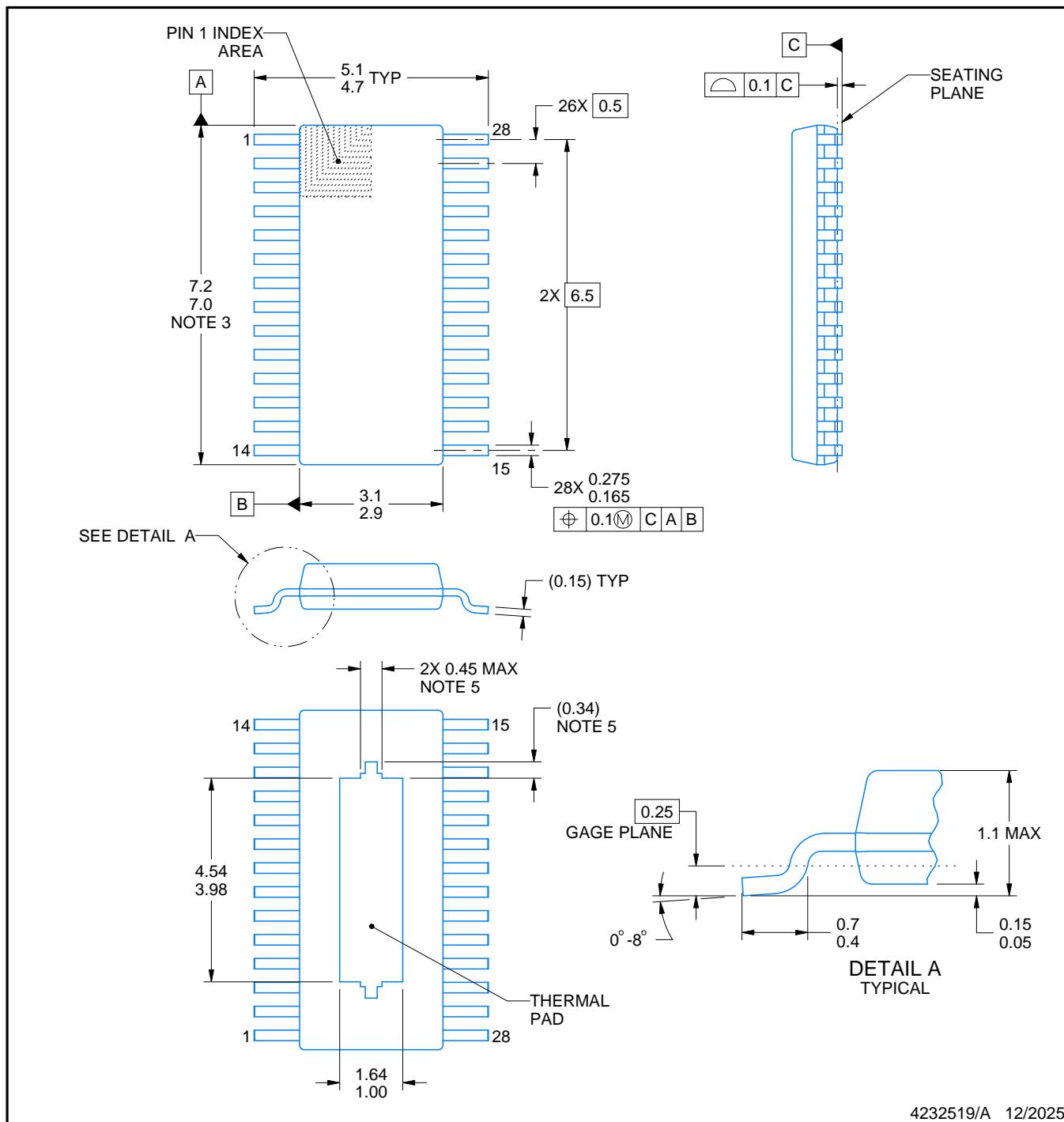
## PACKAGE OUTLINE

DGQ0028C



## PowerPAD™ VSSOP - 1.1 mm max height

## SMALL OUTLINE PACKAGE



## NOTES:

PowerPAD is a trademark of Texas Instruments.

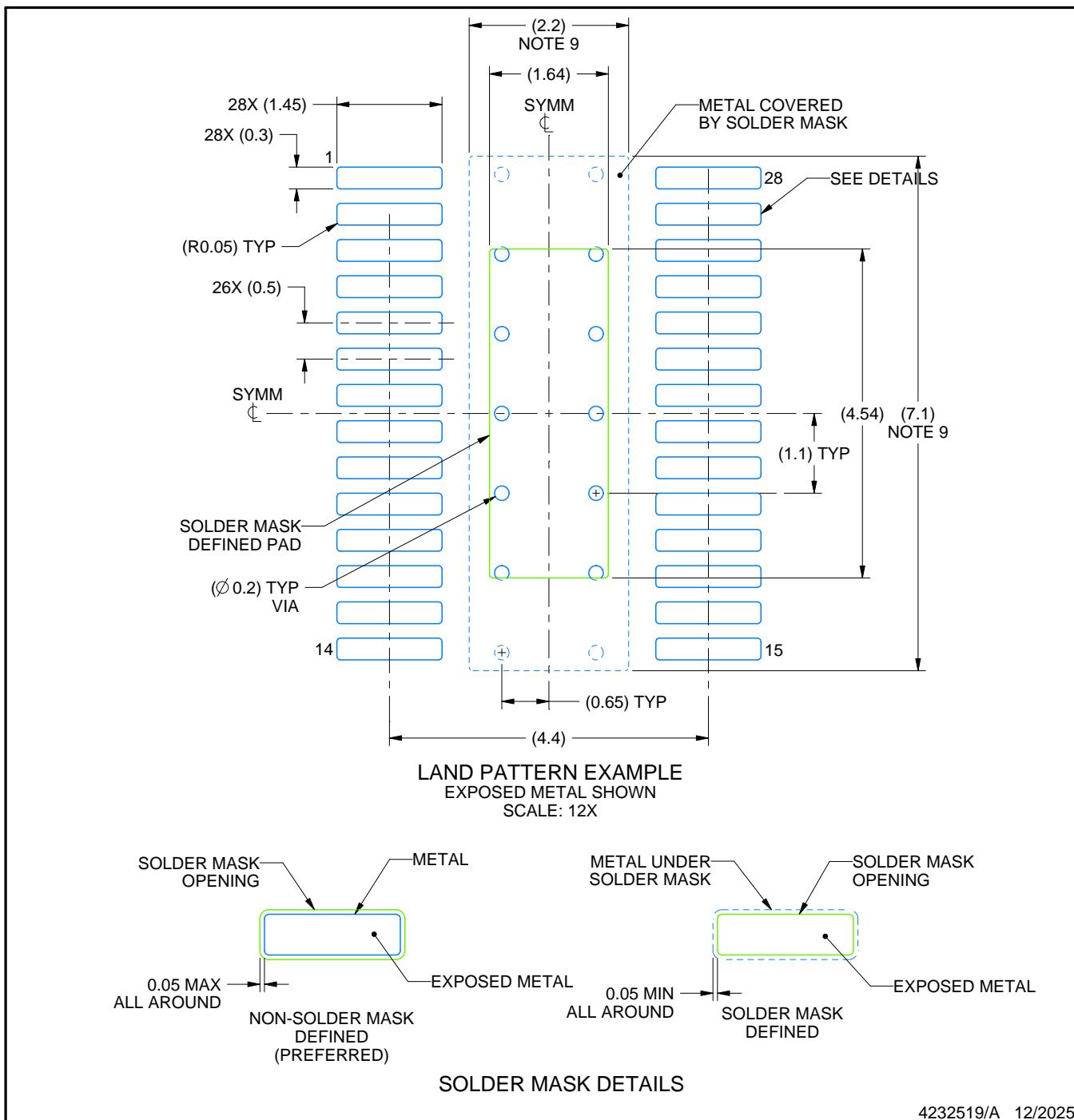
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. No JEDEC registration as of September 2020.
5. Features may differ or may not be present.

# EXAMPLE BOARD LAYOUT

DGQ0028C

PowerPAD™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



4232519/A 12/2025

NOTES: (continued)

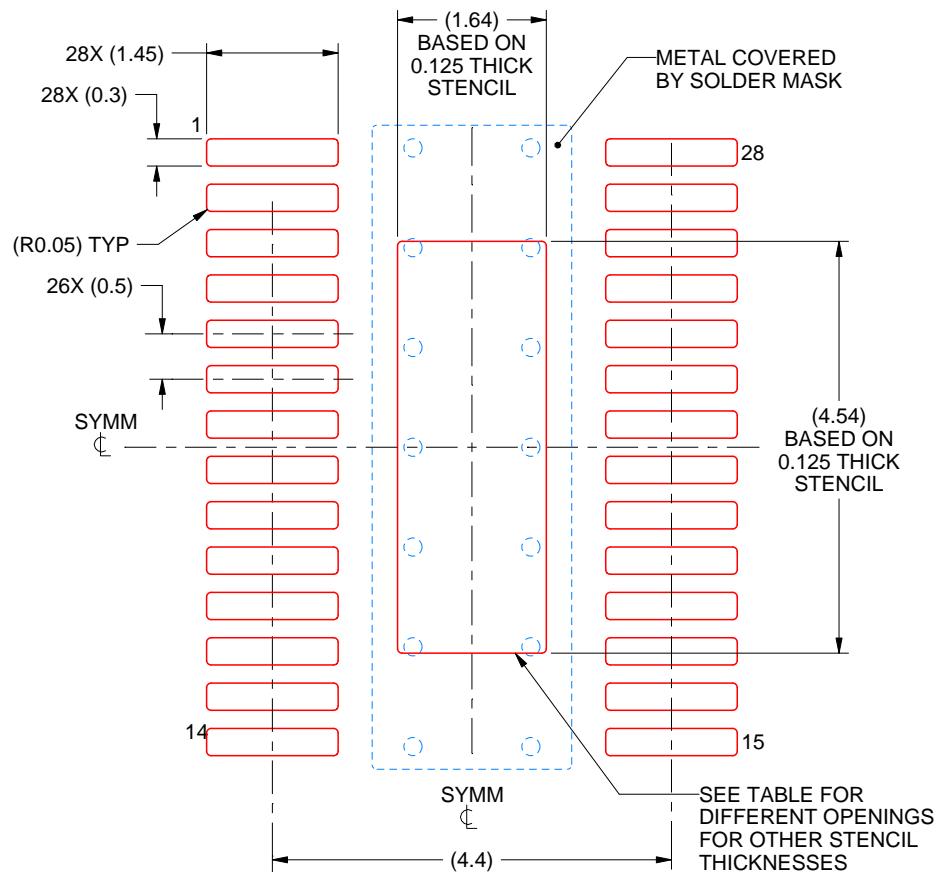
6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 ([www.ti.com/lit/slma002](http://www.ti.com/lit/slma002)) and SLMA004 ([www.ti.com/lit/slma004](http://www.ti.com/lit/slma004)).
9. Size of metal pad may vary due to creepage requirement.
10. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.

## EXAMPLE STENCIL DESIGN

**DGQ0028C**

## PowerPAD™ VSSOP - 1.1 mm max height

## SMALL OUTLINE PACKAGE



**SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE: 12X**

STENCIL THICKNESS	SOLDER STENCIL OPENING
0.1	1.83 X 5.08
0.125	1.64 X 4.54 (SHOWN)
0.15	1.50 X 4.14
0.175	1.39 X 3.84

4232519/A 12/2025

#### NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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