TI TECH DAYS



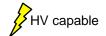
Mubina Toa and Peter Iliya

Current and Position Sensing



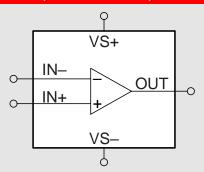
Agenda

- Current sensing architectures (5-7min)
- Error analysis (3 min)
- PSPICE simulation (9 min)
- Key current sensing applications (4 min)
- TI current sensing portfolio (4 min)

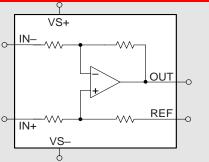


Current sensing architectures: types

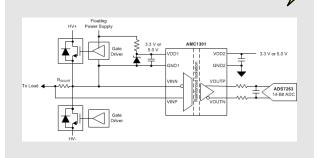
Operational amplifier



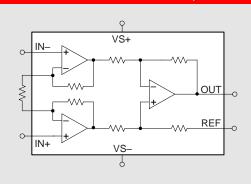
Difference amplifier



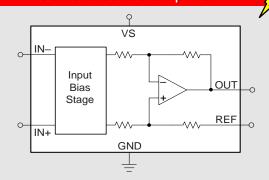
Isolated current sense



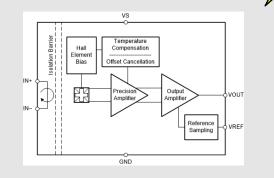
Instrumentation amplifier



Current sense amplifier



In-package Hall-effect current sensor





Current sensing architectures: pros and cons

Operational amplifier

Pros

- Large open-loop gain
- Often very low cost

Cons

- · Accuracy is set by external components
- . Low-side only: VCM ≈ GND
- With a single-ended input, PCB parasitics will create additional error

Instrumentation amplifier

Pros

- Large input impedance allows for measuring very small currents
- Change gain with external resistor

Cons

- Common-mode voltage must remain within supply voltage, VCM ≤ VS
- Usually used for low-side sensing, but can be used for high-side depending on common-mode voltage

Difference amplifier

Pros

 Can tolerate very large common-mode voltages (up to ±275V with ±15V supply)

Cons

- System impedance < than diff amp input impedances; Resistor network loads sys.
- Low gain requires additional amplifier stage to keep P_{DIS} in shunt reasonable
- Output must be managed to limit output dynamic range to protect downstream circuitry when supporting high V_{CM}

Current sense amplifier

Pros

- Unique floating input stage topology; V_{CM} can exceed and be independent of V_S
- Precision integrated gain network maximizes accuracy and minimizes drift
- Low offset enables use of low ohmic shunt resistors enabling higher current measurements & minimizing power loss

Cons

Typically only fixed gain

Isolated current sense

Pros

- Extends CM capability by galvanically isolating the input stage from the output
- Enables galvanic isolation even in low voltage (< 100V) apps w/ transients
- Low offset & integrated precision gain network on input enable high accuracy

Cons

Limited gain options limit shunt resistor options

In-package Hall-effect current sensor

Pros

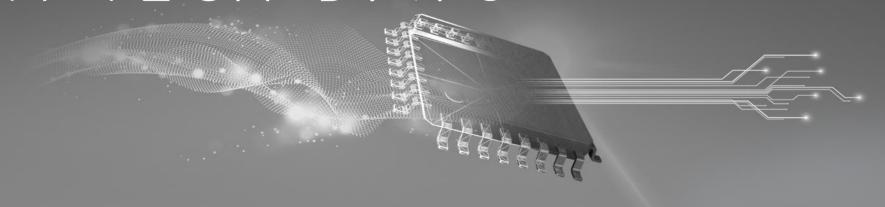
- Extends common mode capability by galvanically isolating the input stage from the output
- Enables galvanic isolation even in low voltage (< 100V) applications where transients exist that may require isolation

Cons

- Current limited to 30A at 25°C
- Sensitive to stray magnetic fields that can degrade measurement accuracy



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Error analysis (INA228)





Different types of error in current sensing circuits

- 1. Offset error e_{Offset} (%) $\approx e_{Vos} + e_{CMRR} + e_{PSRR}$
- 2. Gain error e_{Gain} (%) $\approx e_{Gain_error} + e_{Linearity} + e_{Shunt_tolerance}$
- 3. Application error $e_{Application}$ (%) $\approx e_{Bias_current} + e_{Other}$

Worst-case total error - more conservative

$$\varsigma_{Worst}(\%) \approx e_{Vos} + e_{CMRR} + e_{PSRR} + e_{Gain_error} + e_{Linearity} + e_{Shunt_tolerance} + e_{Bias_current} + e_{Other}$$

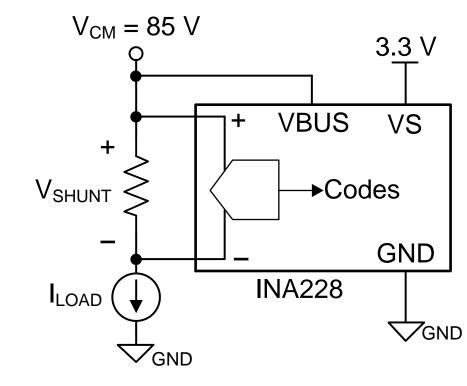
Root-sum-square (RSS) total error – more realistic

$$\zeta_{RSS}(\%) \approx \sqrt{e_{Vos}^2 + e_{CMRR}^2 + e_{PSRR}^2 + e_{Gain_error}^2 + e_{Linearity}^2 + e_{Shunt_tolerance}^2 + e_{Bias_current}^2 + e_{Other}^2}$$

INA228 error analysis

Conditions

- $V_{CM} = 85 \text{ V}$
- VS = 3.3 V
- $T_A = 25^{\circ}C \text{ to } 120^{\circ}C (\Delta 95^{\circ}C)$
- Load = 1 mA to 1 A
- $R_{SHUNT} = 100 \text{ m}\Omega$
 - $V_{SHUNT} = 100 \,\mu\text{V}$ to 163 mV
- LSB_V_{SHUNT} = 312 nV (ADCRANGE=0)
- ADC conversion time = 4.12 ms
- ADC number of averages = 512



Note: R_{SHUNT} has perfect 0% tolerance in this example

INA228 error analysis example

Determine the maximum offset for V_{SHUNT} measurement

$$V_{OSI} = \pm 2 \, uV$$

$$V_{OS_CMRR} = |V_{CM} - 48V| * 10^{\frac{-CMRR_{min}}{20dB}} = |85V - 48V| * 10^{\frac{-146}{20dB}} = \pm 1.85 \, \mu V$$

$$V_{OS_PSRR} = |VS - 3.3V| * PSRR_{min} = 0$$

$$V_{OS_drift} = |\Delta TA| * \frac{dV_{OS}}{dT} = |95^{\circ}C| * 0.01 \, \frac{\mu V}{^{\circ}C} = \pm 0.95 \, \mu V$$

$$V_{OS_Total} = V_{OSI} + V_{OS_{CMRR}} + V_{OS_PSRR} + V_{OS_drift} = \pm 4.8 \, \mu V$$

Determine the maximum ADC gain error for V_{SHUNT} measurement

$$G_{Error_25C} = \pm 0.1\% = \pm 0.001$$
 $G_{Error_drift} = |\Delta TA| * 20ppm = 95^{\circ}C * 20ppm * 10^{-6} = \pm 0.0019$
 $G_{Error_total} = G_{Error_25C} + G_{Error_drift} = \pm 0.0029$

INA228 error analysis example

Convert to digital codes and calculate total error at 1 mA load

$$G_{IDEAL} = \frac{1}{LSB_VSHUNT} = \frac{1}{312 \ nV} = 3,076,923 \frac{codes}{V}$$

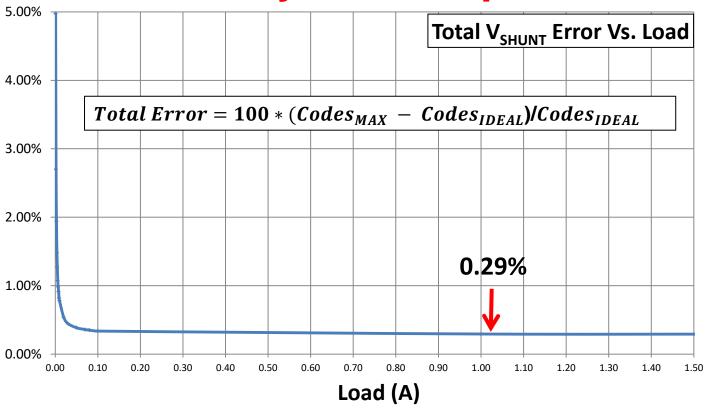
$$Codes_{IDEAL\ 1mA} = V_{SHUNT} * G_{IDEAL} = 1mA * 100m\Omega * 3,076,923 = 307.7\ codes$$

$$Codes_{MAX_1mA} = ROUND[(V_{SHUNT} + VOS) * G_{IDEAL} * (1 + G_{Error_total})] = 323 codes$$

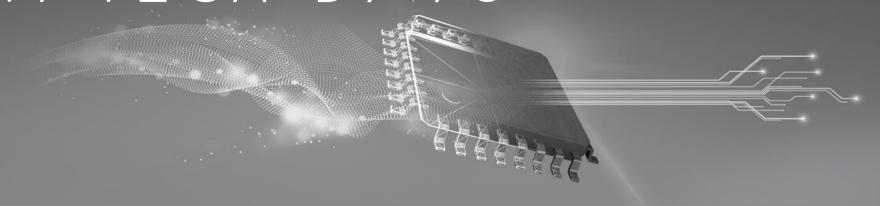
Total Error at
$$1mA = 100 * (Codes_{MAX \ 1mA} - Codes_{IDEAL \ 1mA})/Codes_{IDEAL \ 1mA} = 4.98\%$$



INA228 error analysis example



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PSPICE simulation with INA293



Simulation models for current sense amplifiers (CSA)

- SPICE models include the following behaviors from datasheet:
 - V_{OS}, gain error, and drift over temperature
 - Input bias and input offset currents
 - Noise density
 - Bandwidth, slew rate
 - Claw curve (Swing-to-rail Versus Output current)
 - AC and DC CMR
 - AC and DC PSR
 - Output impedance (Z_{OUT})
- Most models are behavioral based and not transistor based.
- Models work best for small-signal analyses.



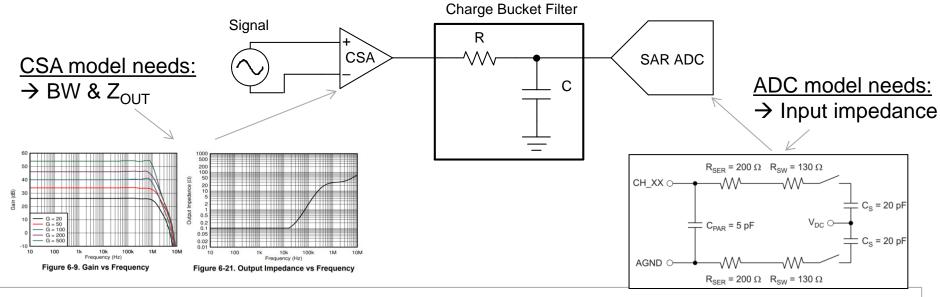
PSpice® for TI

- In addition to the free TINA-TI software, TI now offers a free simulation and design environment using PSPICE from Cadence.
- Includes mixed-signal simulation capability and a full library of pre-loaded models along with links to technical documentation.

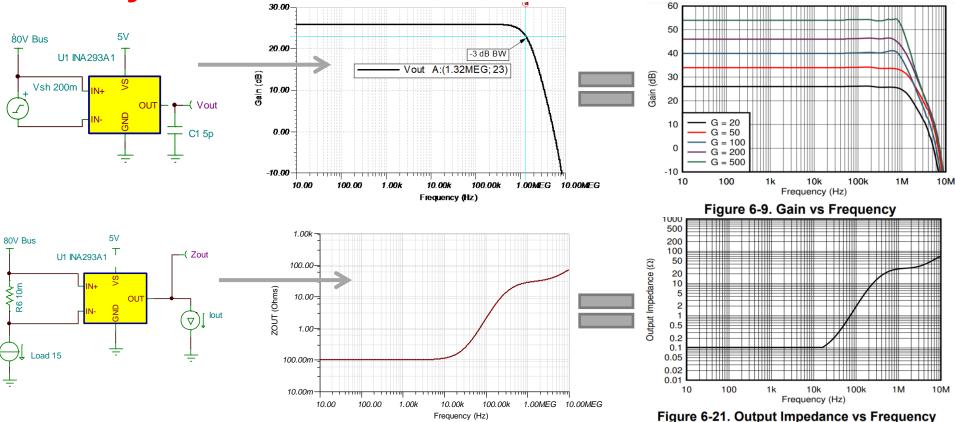
Simulation example - charge bucket filter for ADC

<u>Problem</u>: Solve for R and C to yield <1/2 LSB error with SAR ADC. <u>Advantages</u>:

- Reduce design time.
- Remove need for high-speed buffer amplifier.



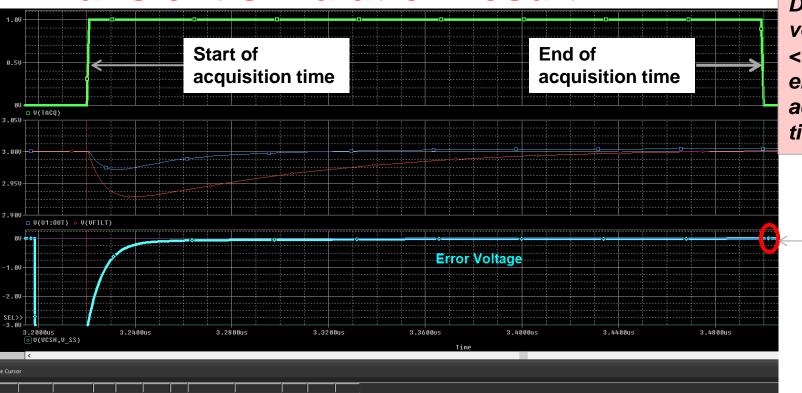
Verify INA293A1 model behavior



Charge Bucket Filter INA293 + ADS8528 with charge bucket Solve for R and C to yield <1/2 5.00000V LSB error. VON = 180V Bus VOFF = 0 S2 INA293A1 **S4** VON = 1 S VOFF = 0 8 80.0000V 1 100 R5 R4 3.00126V Shunt OUT 3.00126V 3.00126V 1.50063V 10m 3.00126V Error Voltage IN-C2 = 79.8500V 680p Load 15 C4 2.50000V 2.5Vdc GAIN = 1 C3 20p= R3 200 130 80V Bus 80.0000V Watch our training V SS 3.00126Vdc VON = 1videos for more VOFF = 0 5Vdc 80Vdc **S1** VON = 1 information. S VOFF = 0 Steady-state 12 bit SAR ADC tconv i Amplifier Settling and Charge Bucket Filter Design tacq = 280 nstconv = 1.33 usvoltage by Art Kay, Dale Li 1 LSB = $10V/2^12 = 2.44mV = 0V$ 0.5 LSB = 1.22 mV

Transient simulation result

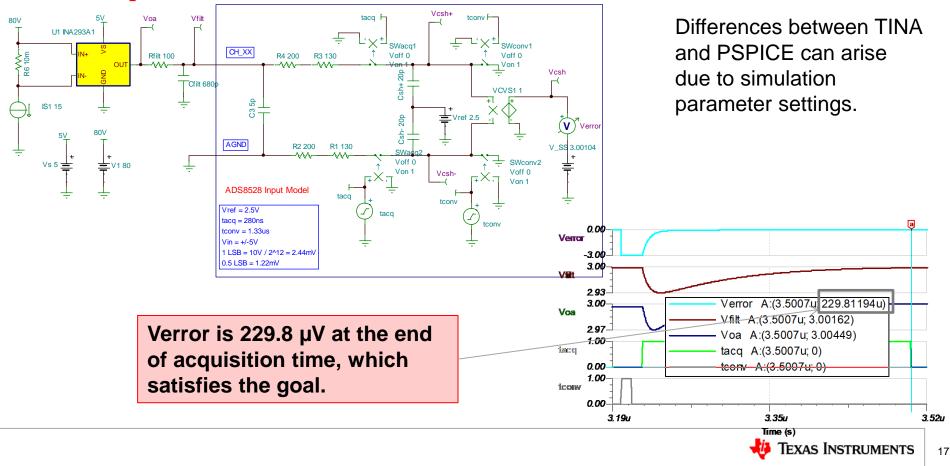
3.0010



Does the error voltage settle to < 1.22 mV at the end of the acquisition time?

150 μV. Yes, error voltage settles to < 0.5 LSB.

Comparison to TINA-TI



Current & power measurement use cases

Solutions customers seek



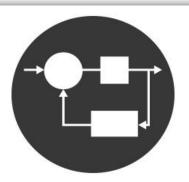
Real-time overcurrent protection (OCP)

Current-level detection exceeding a predetermined threshold as system fluctuations occur due to loads and transients



Current and power monitoring for system optimization

Modeling of system performance and energy to maximize efficiency and/or battery life

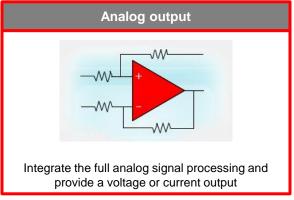


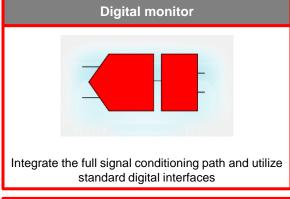
Current measurement for closed loop circuits

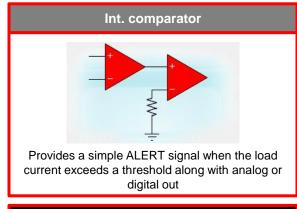
Infer diagnostic and/or operational system information from the current measurement

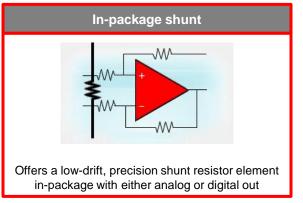


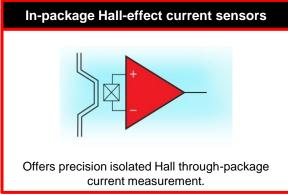
Current sensing portfolio

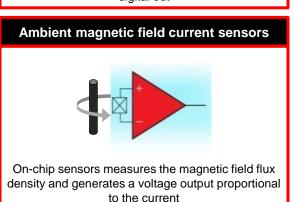












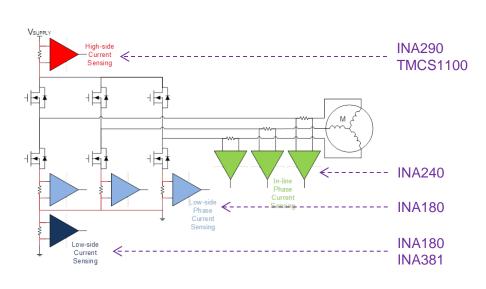


Current sensing use-cases in industrial

Analog current sense amplifier use-cases

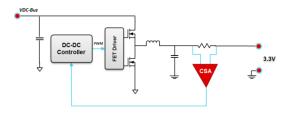
Brushless DC motor commutation

Uses up to three current sense amplifiers in low-side of high-side configurations for torque measurement.



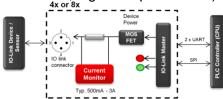
Power supplies

Current sensing in power supplies for accurate current measurement for control loops and quick over-current detection.



PLCs

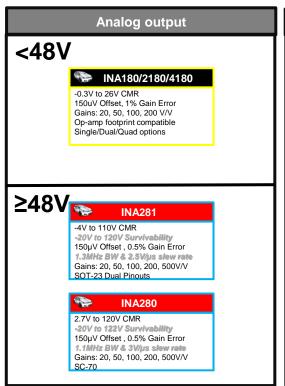
To avoid that a sensor could create problems for the system, each port monitors the current to ensure proper operation. (Stand-alone remote IO, digital output module)

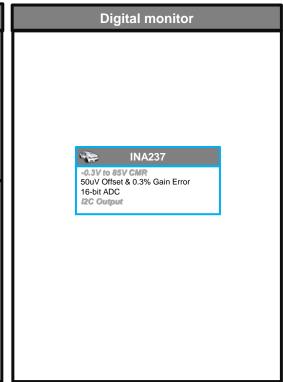




Low-cost hero devices









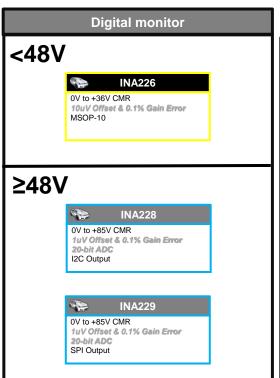


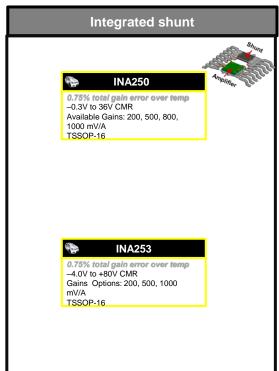
High performance hero devices



Q100 in Development









TMCS1100

Precision, bi-directional, galvanically isolated current sensor with external reference

Features

- 80 kHz signal bandwidth.
- 1% accuracy (-40 to 125°C).
- ±600 V working voltage, 3 kV dielectric isolation (IEC 60950-1).
- Operating voltage: 3.0 V to 5.5 V.
- 20 A max continuous DC/RMS current (thermally limited).
- Multiple sensitivities for wide linear measurement ranges:
 - TMCS1100A1: 50 mV/A –

TMCS1100A2: 100 mV/A

TMCS1100A3: 200 mV/A

-TMCS1100A4: 400 mV/A

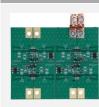
- 8-pin SOIC package.
- AEC-Q100 Grade 1 Option.

Applications

- Motor control
- PV string inverters
- Switching converters

- Overcurrent protection
- Power monitoring
- On-board charger PFC

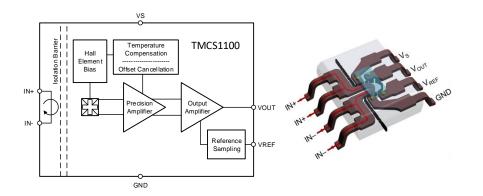
Tools & Resources



- TMCS1100EVM
- TINA—TI SPICE Model

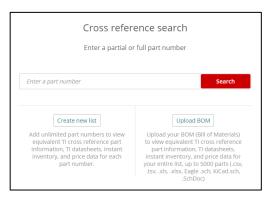
Benefits

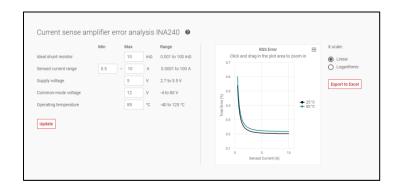
- Ability to measure an isolated ac or dc current.
- In-package sensing simplifies PCB and application design.
- Highest accuracy Hall current sensing device in the industry.
- Highest working voltage isolation (600 V) in 8-pin SOIC.
- Ability to precisely set the reference voltage (VREF) independent of Vcc enables higher accuracy.
- VREF can be shared with ADC for increased system accuracy.
- Fixed sensitivity eliminates ratiometry errors and improves supply noise rejection.



Key Resources







TI Precision Labs

Cross-reference search

Web-based error tool





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