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## 1 Introduction

The LM27402 is a feature-rich, synchronous, single phase PWM DC/DC buck controller. A wide input voltage range of 3-V to 20-V, input voltage feedforward, and dual high current integrated N-channel MOSFET drivers make the LM27402 appropriate for high current intermediate bus system rails in point-of-load applications. A  $0.6\text{-V} \pm 1\%$  internal voltage reference enables high accuracy and low voltage capability at the output. Inductor DCR current sensing provides an accurate current limit detection method and promotes high output current and high system efficiency by eliminating resistive current sense elements.

This user's guide describes the steps taken in selecting the external components to build a fully functional DC/DC converter. This user's guide includes diagrams of the evaluation board layout and bill of materials. The evaluation board represents a typical application circuit and can be modified if different specifications are desired. Refer to the [LM27402 High Performance Synchronous Buck Controller with DCR Current Sensing](#) data sheet for additional design equations.

## 2 Evaluation Board

The LM27402 evaluation board represents a 20-A typical application circuit. The application circuit is optimized for an input voltage of 12 V. However, input voltage feedforward technology allows the evaluation board to operate up to 20 V while maintaining a stable output voltage of 1.5 V at 20 A. Temperature compensated inductor DCR current limit circuitry provides a steady current limit set point. Extra MOSFET and input/output capacitor footprints are included to accommodate higher currents if desired. An externally set soft-start time of 10 ms provides a controlled monotonic start-up. The LM27402 evaluation board also supports pre-biased start-up and provides a tracking connection for power supply sequencing. An external clock can be applied to change the switching frequency through an on board synchronization connection. PGOOD is externally pulled up to VDD and can be monitored via an on board terminal. Two extra terminals are included to provide a network analyzer connection for control loop stability analysis. The PCB measures 1.3 inch  $\times$  1.8 inch and includes input/output banana connectors for the input supply and load.

## 3 Evaluation Board Operating Specifications

- Input Voltage = 4.5 V to 20 V
- Output Voltage = 1.5 V
- Output Current = 0 A to 20 A

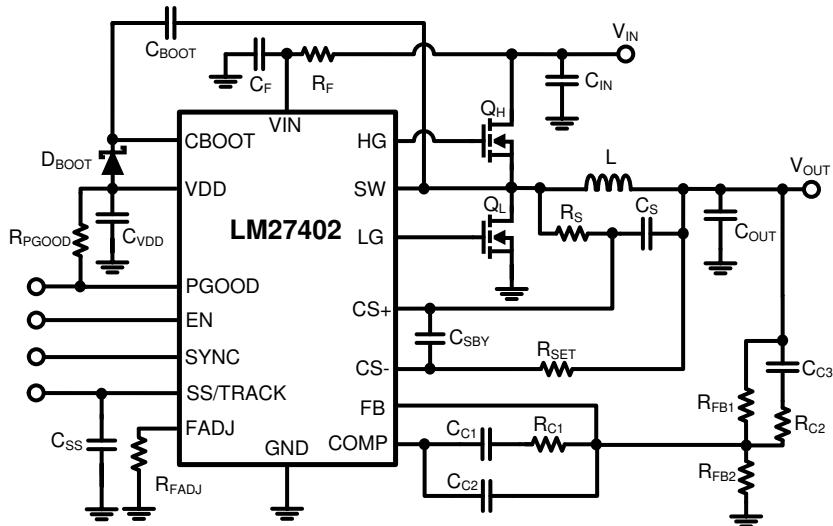


Figure 3-1. Simplified Application Schematic

## 4 Evaluation Board Schematic

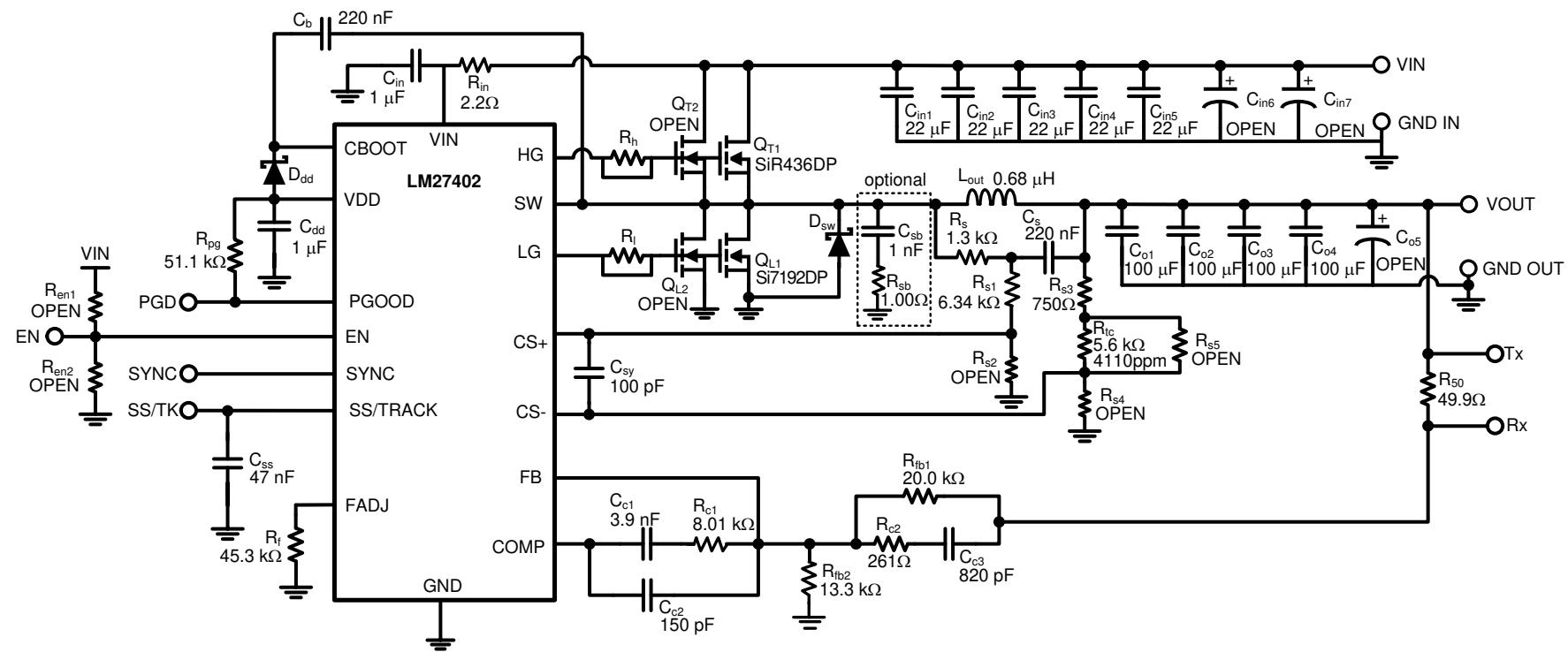


Figure 4-1.  $V_{IN} = 4.5$  V to 20 V,  $V_{OUT} = 1.5$  V,  $I_{OUT} = 20$  A

## 5 Connection Descriptions

PCB Silkscreen	Description
VIN	VIN is the input voltage terminal to the PCB and is equipped to handle a 1/4-inch banana jack or can be unbolted to accept a ring connector. The LM27402 will operate over the input voltage range of 3.0 V to 20 V. However, the evaluation board is optimized for an input voltage of 12 V and will operate from 4.5 V to 12 V. The absolute maximum voltage rating for this pin is 22 V.
GND IN	GND IN is the input ground terminal to the PCB and is equipped to handle a 1/4-inch banana jack or can be unbolted to accept a ring connector. There are two GND connections on the PCB. GND IN should be used for the input supply only.
VOUT	VOUT is the output voltage terminal of the PCB and is equipped to handle a 1/4-inch banana jack or can be unbolted to accept a ring connector. VOUT should be connected to the load through a low impedance line to minimize any line drop.
GND OUT	GND OUT is the output ground terminal of the PCB and is equipped to handle a 1/4-inch banana jack or can be unbolted to accept a ring connector. There are two GND connections on the PCB. GND OUT should be used for the output load only.
VDD	VDD is the output of the internal 4.5-V sub regulator.
PGD	PGOOD output. This connection allows the user to monitor PGOOD during fault conditions. PGOOD is pulled up to VDD and should not exceed 5.5 V under normal operating conditions and the absolute maximum voltage rating is 6 V.
EN	EN is connected to the EN pin of the LM27402. A voltage typically greater than 1.17 V will enable the IC. A hysteresis of 100 mV on EN provides noise immunity. The LM27402 will self enable by a 2- $\mu$ A internal current source to EN if no control signal is applied to EN. The enable threshold can be set with an optional external resistor divider from VIN. The EN pin should not exceed the voltage on VDD. The operating voltage for this pin should not exceed 5.5 V and the absolute maximum voltage rating is 6 V.
SS/TK	SS/TK provides access to the SS/TRACK pin of the LM27402. Connections to this terminal are not needed for most applications. The feedback pin of the LM27402 will track the voltage on the SS/TRACK pin if driven with an external voltage source that is less than the 0.6-V internal reference. The operating voltage for this pin should not exceed 5.5 V and the absolute maximum voltage rating on this pin is 6 V. The SS/TRACK pin should not exceed the voltage on VDD.
SYNC	SYNC connects to the SYNC pin of the LM27402. An external clock signal can be connected to the SYNC connection to set the switching frequency. If a SYNC signal is not present, the switching frequency will fall back to the frequency set by the FADJ resistor. The SYNC frequency must be greater than the frequency set by the FADJ resistor and can sync up to 400 kHz above the free running frequency. This pin should not exceed the voltage on VDD.
RX and TX	The RX and TX terminals provide the connections to measure the loop response with a network analyzer. RX refers to an applied reference signal and TX refers to the test voltage or in this case the output voltage. Between RX and TX exists a 50- $\Omega$ termination resistor.

## 6 Performance Characteristics

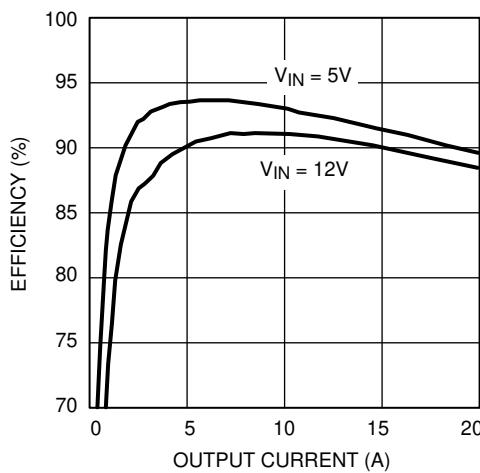


Figure 6-1. Efficiency vs Load

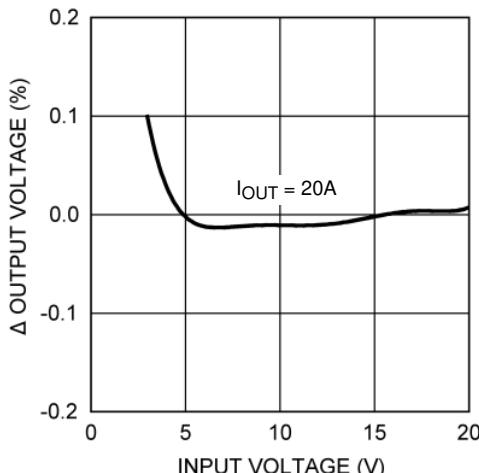


Figure 6-2. Line Regulation

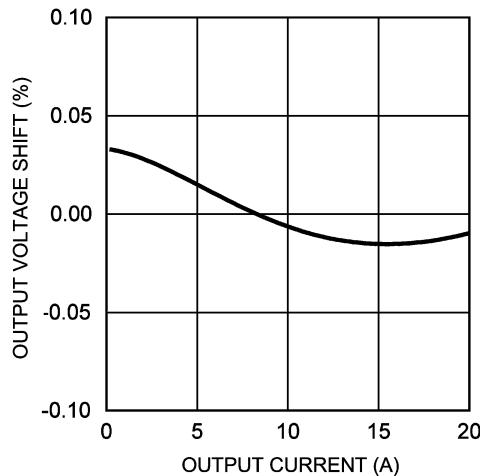


Figure 6-3. Load Regulation ( $V_{IN} = 12$  V)

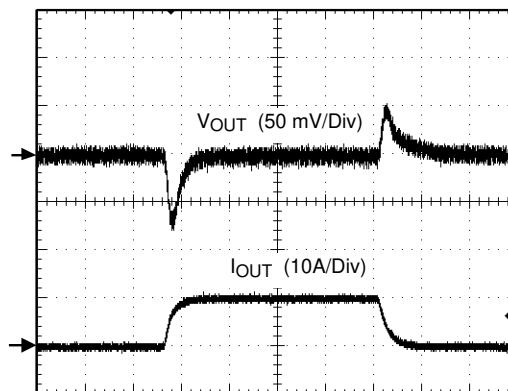


Figure 6-4. 0-A to 10-A Load Transient Response

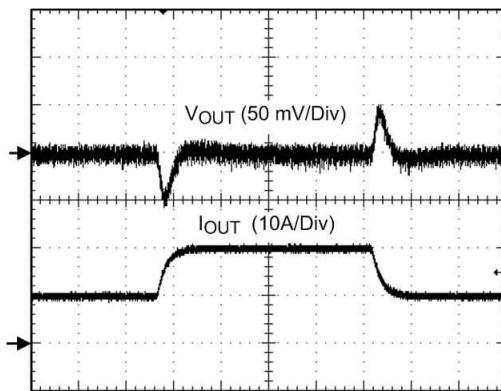


Figure 6-5. 10-A to 20-A Load Transient Response

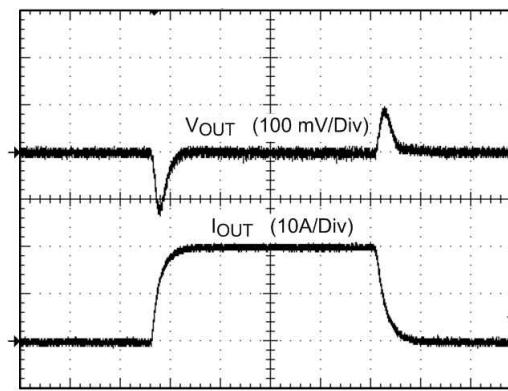


Figure 6-6. 0-A to 20-A Load Transient Response

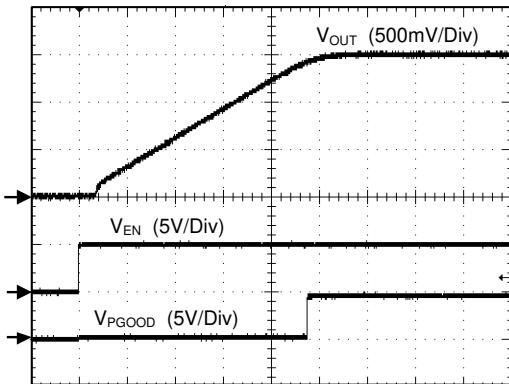


Figure 6-7. Start-Up Waveform (No Load)

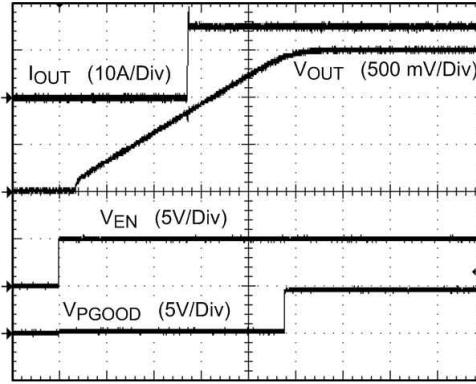


Figure 6-8. Start-Up Waveform (15-A Electronic Load)

## 7 LM27402 Evaluation Board

The LM27402 evaluation board is designed to support multiple applications and modifications and is optimized for a 4.5-V to 12-V input voltage range. The maximum steady state output current is set at 20 A and will typically current limit at 24 A. The PCB features bolt-on banana connections if heavy duty connectors are needed.

## 8 Setup Procedure

1. Set the input power supply voltage to 12 V. Adjust the input supply current limit level to 10 A to protect from any unanticipated shorts.
2. Turn the input power supply off. Connect the input supply positive terminal to the VIN terminal and the input supply ground terminal to the GND IN terminal.
3. Turn the output electronic load off. Connect the electronic load positive terminal to the VOUT terminal and the ground terminal to the GND OUT terminal of the LM27402 evaluation board.
4. Turn the input supply on. The part will self enable and the output voltage should be 1.5 V. Slowly increase the load current to 20 A. The input voltage can now be adjusted as well.

### CAUTION

If the input voltage is below 5 V, the internal LDO will be in a drop out state. The output of the LDO provides the driving voltage across the gates of the MOSFETs. If the voltage at VDD decreases enough, the efficiency can suffer if the MOSFETs are not fully enhanced in the on-state. The output should maintain regulation.

## 9 Evaluation Board Component Selection

This section describes the design process for the LM27402 evaluation board. Unless otherwise indicated, all formulae assume units of the following:

- Amps (A) for current
- Farads (F) for capacitance
- Henries (H) for inductance
- Volts (V) for voltage

The first equation to calculate for any buck converter is duty ratio:

$$D = \frac{V_{OUT}}{V_{IN}} \times \frac{1}{\eta} \quad (1)$$

Due to the resistive powertrain losses, the duty ratio will increase based on the overall efficiency,  $\eta$ . Setting  $\eta = 1$  yields an approximate result for D.

### 9.1 Input Filter, $R_{in}$ , $C_{in}$

An RC filter is added to prevent any switching noise from interfering with the internal analog circuitry connected to VIN. The RC filter can be seen in the evaluation board schematic as components  $R_{in}$  and  $C_{in}$ . There is a practical limit to the value of resistor  $R_{in}$  as the VIN pin of the LM27402 will draw large bias currents to switch the gate of each MOSFET. If  $R_{in}$  is too large, the resulting voltage drop can disrupt normal operation. For the evaluation board, a 2.2- $\Omega$  resistor in conjunction with a 1.0- $\mu$ F 25V X5R ceramic capacitor is used for the input RC filter.

### 9.2 Input Capacitors, $C_{in1}$ – $C_{in5}$

Input capacitors should be selected based on the required input voltage ripple and maximum RMS current rating. The required RMS current rating of the input capacitor for a buck regulator can be estimated by the following equation:

$$I_{CIN(RMS)} = I_{OUT} \sqrt{D(1 - D)} \quad (2)$$

From this equation, it follows that the maximum  $I_{CIN(RMS)}$  requirement will occur at a full 20-A load current with the system operating at 50% duty cycle. Under this condition, the maximum  $I_{CIN(RMS)}$  is given by:

$$I_{CIN(RMS)} = 20A \sqrt{0.5 \times 0.5} = 10A \quad (3)$$

The voltage ripple can be calculated by:

$$\Delta V_{IN} = \frac{I_{OUT} \times D \times (1 - D)}{C_{IN} \times f_{SW}} + \left( I_{OUT} + \frac{\Delta I_L}{2} \right) \times R_{ESR\_CIN} \quad (4)$$

Ceramic capacitors feature a very large  $I_{RMS}$  rating in a small footprint, making a ceramic capacitor ideal for this application. Five 22- $\mu$ F X5R 25-V ceramic capacitors were selected to provide the necessary input capacitance for the evaluation board. Neglecting the effects of ESR, at 12-V  $V_{IN}$  and 20-A  $I_{OUT}$  the selected input capacitors yield an input voltage ripple of:

$$\Delta V_{IN} = \frac{20A \times 0.125 \times (1 - 0.125)}{110 \mu F \times 300 kHz} = 66 mV \quad (5)$$

If desired, two extra capacitors can be added in the  $C_{in6}$  and  $C_{in7}$  footprints.

### 9.3 Inductor, $L_{out}$

As per data sheet recommendations, the inductor value should initially be chosen to produce a peak to peak ripple current between 20% and 40% of the maximum operating output current. A 30% current ripple was chosen for the LM27402 evaluation board. The minimum inductance required is calculated by:

$$L_{MIN} = \frac{(V_{IN} - V_{OUT}) \times D}{\Delta I_L \times f_{SW}} = \frac{(12V - 1.5V) \times 0.125}{(0.3 \times 20A) \times 300 \text{ kHz}} = 0.73 \mu\text{H} \quad (6)$$

An actual inductor is selected based on a trade-off between physical size, efficiency, and current carrying capability. A Vishay IHLP5050 0.68- $\mu$ H inductor results in a peak to peak current ripple of 6.4 A and offers a balance between efficiency (2.34-m $\Omega$  DCR), size (12.9 mm  $\times$  13.2 mm), and saturation current rating (49-A  $I_{SAT}$ ).

### 9.4 Output Capacitor, $C_{o1}-C_{o4}$

The value of the output capacitor in a buck regulator influences the steady state voltage ripple as well as the output voltage response to a load transient. Given the peak-to-peak inductor current ripple ( $\Delta I_L$ ), the output voltage ripple can be approximated by:

$$\Delta V_{OUT} = \Delta I_L \times \sqrt{R_{ESR}^2 + \left( \frac{1}{8 \times f_{SW} \times C_{OUT}} \right)^2} \quad (7)$$

where

- $\Delta V_{OUT}$  (V) is the amount of peak-to-peak voltage ripple at the power supply output.
- $R_{ESR}$  ( $\Omega$ ) is the series resistance of the output capacitor.
- $f_{SW}$  (Hz) is the switching frequency.
- $C_{OUT}$  (F) is the output capacitance used in the design and is the sum of  $C_{o1}$  through  $C_{o4}$ .

For the evaluation board, four 100- $\mu$ F 6.3-V X5R ceramic capacitors were selected for the output capacitance to provide adequate transient and DC bias performance in a relatively small package. From the technical specifications of this capacitor, the ESR is approximately 3 m $\Omega$  and the effective in-circuit capacitance is approximately 60  $\mu$ F (reduced from 100  $\mu$ F due to the 1.5-V DC bias and worst case tolerance). With these values, the peak-to-peak voltage ripple when operating from a  $V_{IN}$  of 12 V is:

$$6.4A \times \sqrt{(0.75 \text{ m}\Omega)^2 + \left( \frac{1}{8 \times 300 \text{ kHz} \times 240 \text{ }\mu\text{F}} \right)^2} = 12 \text{ mV}_{pp} \quad (8)$$

### 9.5 Soft-Start Capacitor, $C_{ss}$

A soft-start capacitor can be used to control the start-up time of the LM27402. The start-up time is estimated by the following equation:

$$t_{ss} = \frac{0.6V \times C_{ss}}{I_{ss}} \quad (9)$$

$I_{ss}$  is nominally 3  $\mu$ A. For the evaluation board, the soft-start time has been designed to be approximately 10 ms, resulting in a  $C_{ss}$  capacitor value of 47 nF. The LM27402 defaults to a 1.28-ms start-up ramp time if  $C_{ss}$  is not used.

### 9.6 Internal LDO Bypass Capacitor, $C_{dd}$

The  $C_{dd}$  capacitor is necessary to bypass an internal 4.5-V subregulator. This capacitor should be sized equal to or greater than 1  $\mu$ F but less than 10  $\mu$ F. A value of 1  $\mu$ F is sufficient for most applications and is used in the LM27402 evaluation board.

### 9.7 Frequency Adjust Resistor, $R_f$

The LM27402 switching frequency can be adjusted from 200 kHz to 1.2 MHz using an external resistor labeled on the evaluation board as  $R_f$ . The frequency of the LM27402 evaluation board was selected to be 300 kHz.

A 300-kHz switching frequency enables the LM27402 to deliver high currents by reducing the MOSFET related losses while maintaining the ability to achieve satisfactory transient response. To find the value of resistance needed for a given frequency, use the following equation: ( $f_{SW}$  (kHz),  $R_f$  (k $\Omega$ )).

$$R_f = \frac{100}{\frac{f_{SW}}{100} - 1} = \frac{100}{\frac{300}{100} - 1} = 45 \text{ k}\Omega \quad (10)$$

A value of 45.7 k $\Omega$  was chosen for the  $R_f$  resistor on the LM27402 evaluation board.

### 9.8 Current Limit Circuitry, $R_s$ , $C_s$ , $R_{s1}$ , $R_{s5}$ , $R_{tc}$

The current limit circuitry included on the LM27402 evaluation board sets the current limit at 24 A. Components  $R_s$  and  $C_s$  connect directly under the inductor pads and create an RC filter. The time constant of  $R_s C_s$  should match the time constant of the inductance and DCR of the inductor:

$$R_s C_s = \frac{L}{R_{DCR}} \quad (11)$$

A typical range of capacitance used in the  $R_s C_s$  network is 100 nF to 1  $\mu$ F. A 220-nF capacitor was chosen for the  $C_s$  filter capacitor resulting in an  $R_s$  resistor of:

$$R_s = \frac{L_{out}}{C_s R_{DCR}} = \frac{0.68 \mu\text{H}}{220 \text{ nF} \times 2.34 \text{ m}\Omega} = 1.32 \text{ k}\Omega \quad (12)$$

A standard value resistor of 1.3 k $\Omega$  was selected for  $R_s$ . The current limit level is set through a resistor from CS- to the VOUT pad of the inductor. The LM27402 evaluation board is set to current limit at 24-A  $I_{OUT}$ . The maximum inductor current is  $I_{OUT} + \Delta I_L / 2 = 24 + 6.4 / 2 = 27.2$  A. The next equation describes the current limit resistor calculation:

$$R_{SET} = \frac{I_{LIMIT} R_{DCR}}{I_{CS}} = \frac{27.2 \text{ A} \times 2.34 \text{ m}\Omega}{10 \mu\text{A}} = 6.36 \text{ k}\Omega \quad (13)$$

Copper resistance changes by about 3900 ppm/ $^{\circ}\text{C}$  and can cause a significant error in the current limit setpoint. The LM27402 evaluation board is equipped with a 5.6-k $\Omega$  positive temperature coefficient resistor ( $R_{tc}$ ) to compensate the effects of copper resistance and a 750- $\Omega$  resistor  $R_{s3}$  in series with  $R_{tc}$  to approximately provide the 6.36 k $\Omega$  needed for  $R_{SET}$ .  $R_{tc}$  was chosen to be a Vishay TFPT1206L5601F 5.6-k $\Omega$  resistor which has a temperature coefficient of 4110 ppm/ $^{\circ}\text{C}$ . An optional 6.34-k $\Omega$  resistor ( $R_{s1}$ ) was placed between CS+ and the  $R_s C_s$  filter to mirror the impedance of the CS- pin in addition to a 100-pF capacitor placed between CS+ and CS- near the IC to reduce the effects of noise.

The internal 10- $\mu$ A current source is powered from VIN. If the voltage between VIN and CS- is below 1 V, the current source will supply less than 10  $\mu$ A. If this happens, the common mode voltage of the current sense comparator inputs (CS+ and CS-) can be decreased to ensure 10  $\mu$ A of current. Extra resistor pads ( $R_{s1}$ ,  $R_{s2}$ ,  $R_{s4}$ ) are included in the LM27402 evaluation board to lower the common mode voltage. Please refer to the [AN-2060 LM27402 Current Limit Application Circuits](#) application report for design guidelines to adjust the common mode voltage of the current sense comparator.

### 9.9 Enable Resistors, $R_{en1}$ , $R_{en2}$

The LM27402 evaluation board is equipped with an enable connection tied directly to EN. Resistor footprints  $R_{en1}$  and  $R_{en2}$  provide an optional voltage divider network from VIN to GND to program the LM27402 to enable at a certain input voltage. The following equation will guide the user in choosing resistors values to create a resistor divider for EN:

$$R_{en1} = \frac{R_{en2}(V_{IN} - 1.17V)}{1.17V - I_{EN} \times R_{en2}} \quad (14)$$

## 9.10 Tracking

The LM27402 evaluation board is setup with a tracking connection (SS/TK). The SS/TK terminal is also the soft-start pin. If a voltage source is connected to the SS/TK connection of the board, the output can be controlled up to 1.5 V (voltage set by the feedback resistors). The LM27402 will stop tracking when the SS/TK voltage exceeds 0.6 V. Please refer to the data sheet for more details of the tracking function.

## 9.11 Compensation and Feedback, $R_{fb1}$ , $R_{c1}$ , $R_{c2}$ , $C_{c1}$ , $C_{c2}$ , $C_{c3}$

In order for the LM27402 to regulate, the feedback loop must be closed and compensated. The LM27402 employs voltage mode control to regulate the output voltage. Voltage mode control requires the LC complex double pole caused by  $L_{out}$  and  $C_{o1} - C_{o5}$  to be compensated to reduce the likelihood of oscillation. The evaluation board incorporates type III compensation which adds three poles and two zeros to the open loop transfer function. The evaluation board is conservatively compensated to grant the user the freedom to make small changes to the powertrain circuitry while maintaining adequate stability. Please refer to the [LM27402 High Performance Synchronous Buck Controller with DCR Current Sensing](#) data sheet for the type III compensator design equations. The compensation components include the following:

- $R_{fb1}$
- $R_{fb2}$
- $R_{c1}$
- $R_{c2}$
- $C_{c1}$
- $C_{c2}$
- $C_{c3}$

## 9.12 $R_{fb1}$ and $R_{fb2}$

The resistors labeled  $R_{fb1}$  and  $R_{fb2}$  create a voltage divider from  $V_{OUT}$  to FB and FB to GND that is used to set the nominal output voltage of the regulator. Nominally, the output of the LM27402 evaluation board is set to 1.5 V using resistor values of  $R_{fb1} = 20.0 \text{ k}\Omega$  and  $R_{fb2} = 13.3 \text{ k}\Omega$ . If a different output voltage is required, the value of  $R_{fb2}$  can be adjusted according to the equation:

$$R_{fb2} = \frac{R_{fb1}}{\left(\frac{V_{OUT}}{0.6} - 1\right)} \quad (15)$$

$R_{fb1}$  does not need to be changed from its value of 20.0 k $\Omega$ .

## 10 Bill of Materials

Designator	Type	Parameters	Part Number	Qty	Manufacturer
U <sub>1</sub>	Synchronous Buck Controller		LM27402S	1	Texas Instruments
C <sub>b</sub>	Capacitor	0.22 $\mu$ F, Ceramic, X7R, 25 V, 10%	GRM188R71E224KA88D	1	Murata
C <sub>c1</sub>	Capacitor	3900 pF, Ceramic, X7R, 50 V, 10%	GRM188R71H392KA01D	1	Murata
C <sub>c2</sub>	Capacitor	150 pF, Ceramic, C0G, 50 V, 5%	GRM1885C1H151JA01D	1	Murata
C <sub>c3</sub>	Capacitor	820 pF, Ceramic, C0G, 50 V, 5%	GRM1885C1H821JA01D	1	Murata
C <sub>dd</sub>	Capacitor	1 $\mu$ F, Ceramic, X5R, 25 V, 10%	GRM188R61E105KA12D	1	Murata
C <sub>in</sub>	Capacitor	1 $\mu$ F, Ceramic, X5R, 25 V, 10%	GRM188R61E105KA12D	1	Murata
C <sub>in1</sub> –C <sub>in5</sub>	Capacitor	22 $\mu$ F, Ceramic, X5R, 25 V, 10%	GRM32ER61E226KE15L	5	Murata
C <sub>o1</sub> –C <sub>o4</sub>	Capacitor	100 $\mu$ F, Ceramic, X5R, 6.3 V, 20%	C1210C107M9PACTU	4	Kemet
C <sub>s</sub>	Capacitor	0.22 $\mu$ F, Ceramic, X7R, 25 V, 10%	GRM188R71E224KA88D	1	Murata
C <sub>sb</sub>	Capacitor	1000 pF, Ceramic, X7R, 50 V, 10%	GRM188R71H102KA01D	1	Murata
C <sub>ss</sub>	Capacitor	47000 pF, Ceramic, X7R, 16 V, 10%	GRM188R71C473KA01D	1	Murata
C <sub>sy</sub>	Capacitor	100 pF, Ceramic, C0G/NP0, 50 V, 5%	GRM1885C1H101JA01D	1	Murata
D <sub>dd</sub>	Diode	Schottky Diode, Average I = 100 mA, Max Surge I = 750 mA	CMOSH-3	1	Central Semi
D <sub>sw</sub>	Diode	Schottky Diode, Average I = 3 A, Max Surge I = 80 A	CMSH3-40M	1	Central Semi
L <sub>out</sub>	Inductor	0.68 $\mu$ H, 2.34 m $\Omega$	IHLP5050CEERR68M06	1	Vishay
Q <sub>L1</sub>	N-CH MOSFET	30 V, 60 A, 43.5 nC, R <sub>DS(ON)</sub> at 4.5 V = 1.85 m $\Omega$	Si7192DP	1	Vishay
Q <sub>T1</sub>	N-CH MOSFET	25 V, 40 A, 13 nC, R <sub>DS(ON)</sub> at 4.5 V = 6.2 m $\Omega$	SiR436DP	1	Vishay
R <sub>50</sub>	Resistor	49.9 $\Omega$ , 1%, 0.1W	CRCW060349R9FKEA	1	Vishay
R <sub>c1</sub>	Resistor	8.06 k $\Omega$ , 1%, 0.1W	CRCW06038k06FKEA	1	Vishay
R <sub>c2</sub>	Resistor	261 $\Omega$ , 1%, 0.1W	CRCW0603261RFKEA	1	Vishay
R <sub>f</sub>	Resistor	45.3 k $\Omega$ , 1%, 0.1W	CRCW060345k3FKEA	1	Vishay
R <sub>fb1</sub>	Resistor	20.0 k $\Omega$ , 1%, 0.1W	CRCW060320k0FKEA	1	Vishay
R <sub>fb2</sub>	Resistor	13.3 k $\Omega$ , 1%, 0.1W	CRCW060313k3FKEA	1	Vishay
R <sub>in</sub>	Resistor	2.2 $\Omega$ , 5%, 0.1W	CRCW06032R20JNEA	1	Vishay
R <sub>pg</sub>	Resistor	51.1 k $\Omega$ , 1%, 0.1W	CRCW060351k1FKEA	1	Vishay
R <sub>s</sub>	Resistor	1.3 k $\Omega$ , 1%, 0.1W	CRCW06031k30FKEA	1	Vishay
R <sub>s1</sub>	Resistor	6.34 k $\Omega$ , 1%, 0.1W	CRCW06036k34FKEA	1	Vishay
R <sub>s3</sub>	Resistor	750 $\Omega$ , 1%, 0.1W	CRCW0603750RFKEA	1	Vishay
R <sub>sb</sub>	Resistor	1.0 $\Omega$ , 1%, 0.125W	CRCW08051R00FNEA	1	Vishay
R <sub>tc</sub>	Resistor	5.6 k $\Omega$ , 1%, 4110 ppm/ $^{\circ}$ C	TFPT1206L5601F	1	Vishay
GND IN, GND OUT, VOUT, VIN	Power Terminal		3267	4	Panoma
VDD, PGD, SS/Tk, SYNC, Rx, Tx	Turret Terminal		5002	6	Keystone

## 11 PCB Component Placement

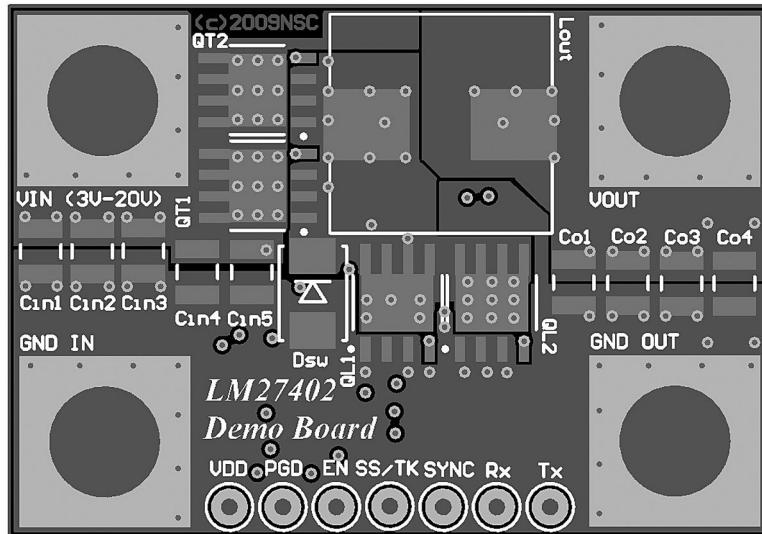


Figure 11-1. Top Layer

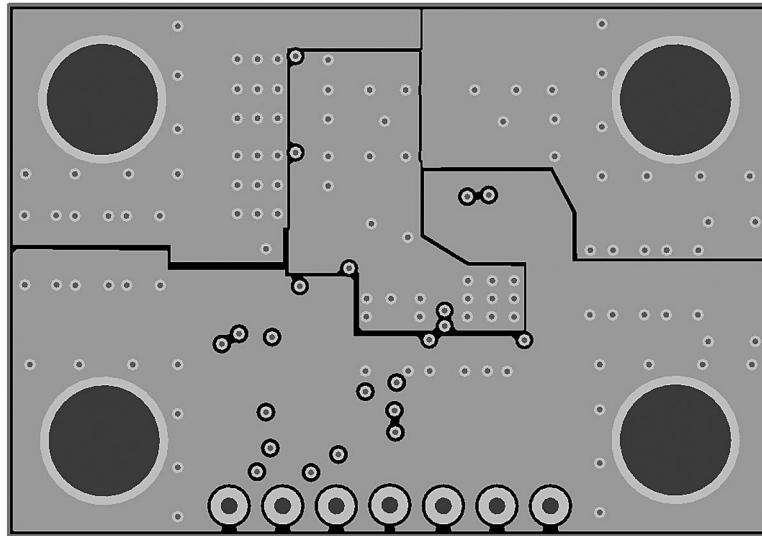


Figure 11-2. Mid Layer 1

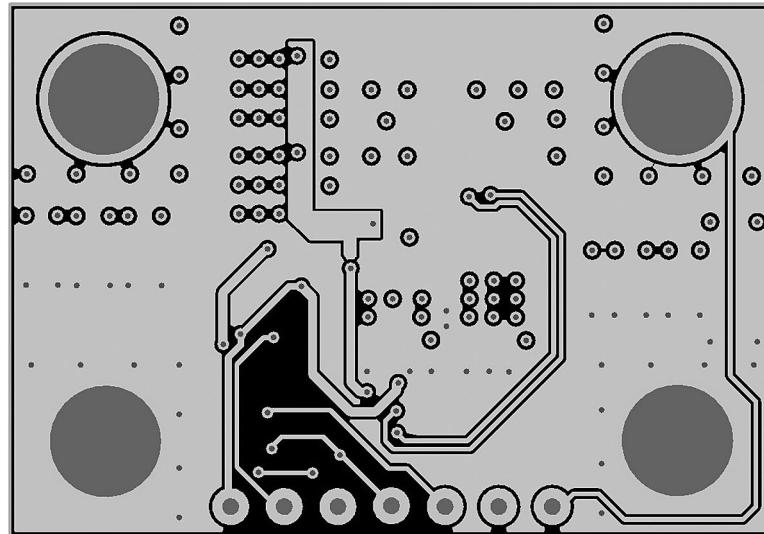


Figure 11-3. Mid Layer 2

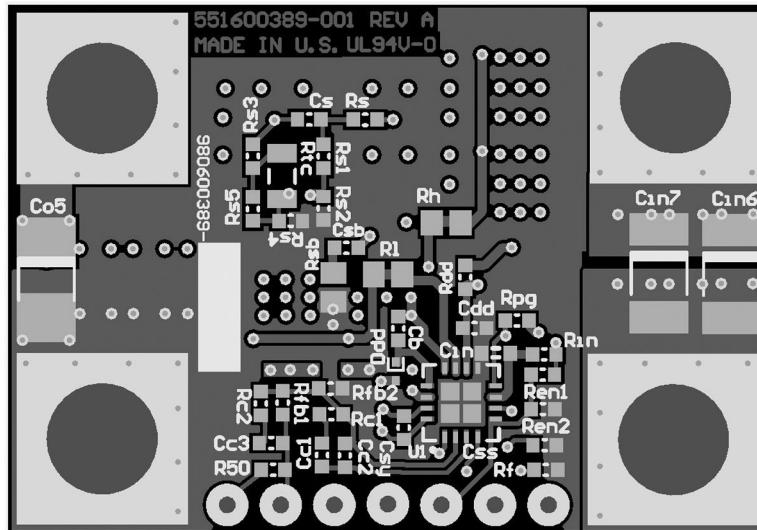


Figure 11-4. Bottom Layer (View From the Bottom)

## 12 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision B (May 2013) to Revision C (January 2022)	Page
• Updated the numbering format for tables, figures, and cross-references throughout the document. ....	2
• Updated the user's guide title.....	2

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  - 2.3 TI's sole liability shall be at its option to repair or replace EVMs that fail to conform to the warranty set forth above, or credit User's account for such EVM. TI's liability under this warranty shall be limited to EVMs that are returned during the warranty period to the address designated by TI and that are determined by TI not to conform to such warranty. If TI elects to repair or replace such EVM, TI shall have a reasonable time to repair such EVM or provide replacements. Repaired EVMs shall be warranted for the remainder of the original warranty period. Replaced EVMs shall be warranted for a new full ninety (90) day warranty period.

### **WARNING**

**Evaluation Kits are intended solely for use by technically qualified, professional electronics experts who are familiar with the dangers and application risks associated with handling electrical mechanical components, systems, and subsystems.**

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**NOTE:**

EXPOSURE TO ELECTROSTATIC DISCHARGE (ESD) MAY CAUSE DEGRADATION OR FAILURE OF THE EVALUATION KIT; TI RECOMMENDS STORAGE OF THE EVALUATION KIT IN A PROTECTIVE ESD BAG.

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### 3 Regulatory Notices:

#### 3.1 United States

##### 3.1.1 Notice applicable to EVMs not FCC-Approved:

**FCC NOTICE:** This kit is designed to allow product developers to evaluate electronic components, circuitry, or software associated with the kit to determine whether to incorporate such items in a finished product and software developers to write software applications for use with the end product. This kit is not a finished product and when assembled may not be resold or otherwise marketed unless all required FCC equipment authorizations are first obtained. Operation is subject to the condition that this product not cause harmful interference to licensed radio stations and that this product accept harmful interference. Unless the assembled kit is designed to operate under part 15, part 18 or part 95 of this chapter, the operator of the kit must operate under the authority of an FCC license holder or must secure an experimental authorization under part 5 of this chapter.

##### 3.1.2 For EVMs annotated as FCC – FEDERAL COMMUNICATIONS COMMISSION Part 15 Compliant:

#### CAUTION

This device complies with part 15 of the FCC Rules. Operation is subject to the following two conditions: (1) This device may not cause harmful interference, and (2) this device must accept any interference received, including interference that may cause undesired operation.

Changes or modifications not expressly approved by the party responsible for compliance could void the user's authority to operate the equipment.

#### FCC Interference Statement for Class A EVM devices

*NOTE: This equipment has been tested and found to comply with the limits for a Class A digital device, pursuant to part 15 of the FCC Rules. These limits are designed to provide reasonable protection against harmful interference when the equipment is operated in a commercial environment. This equipment generates, uses, and can radiate radio frequency energy and, if not installed and used in accordance with the instruction manual, may cause harmful interference to radio communications. Operation of this equipment in a residential area is likely to cause harmful interference in which case the user will be required to correct the interference at his own expense.*

#### FCC Interference Statement for Class B EVM devices

*NOTE: This equipment has been tested and found to comply with the limits for a Class B digital device, pursuant to part 15 of the FCC Rules. These limits are designed to provide reasonable protection against harmful interference in a residential installation. This equipment generates, uses and can radiate radio frequency energy and, if not installed and used in accordance with the instructions, may cause harmful interference to radio communications. However, there is no guarantee that interference will not occur in a particular installation. If this equipment does cause harmful interference to radio or television reception, which can be determined by turning the equipment off and on, the user is encouraged to try to correct the interference by one or more of the following measures:*

- Reorient or relocate the receiving antenna.
- Increase the separation between the equipment and receiver.
- Connect the equipment into an outlet on a circuit different from that to which the receiver is connected.
- Consult the dealer or an experienced radio/TV technician for help.

#### 3.2 Canada

##### 3.2.1 For EVMs issued with an Industry Canada Certificate of Conformance to RSS-210 or RSS-247

#### Concerning EVMs Including Radio Transmitters:

This device complies with Industry Canada license-exempt RSSs. Operation is subject to the following two conditions:

(1) this device may not cause interference, and (2) this device must accept any interference, including interference that may cause undesired operation of the device.

#### Concernant les EVMs avec appareils radio:

Le présent appareil est conforme aux CNR d'Industrie Canada applicables aux appareils radio exempts de licence. L'exploitation est autorisée aux deux conditions suivantes: (1) l'appareil ne doit pas produire de brouillage, et (2) l'utilisateur de l'appareil doit accepter tout brouillage radioélectrique subi, même si le brouillage est susceptible d'en compromettre le fonctionnement.

#### Concerning EVMs Including Detachable Antennas:

Under Industry Canada regulations, this radio transmitter may only operate using an antenna of a type and maximum (or lesser) gain approved for the transmitter by Industry Canada. To reduce potential radio interference to other users, the antenna type and its gain should be so chosen that the equivalent isotropically radiated power (e.i.r.p.) is not more than that necessary for successful communication. This radio transmitter has been approved by Industry Canada to operate with the antenna types listed in the user guide with the maximum permissible gain and required antenna impedance for each antenna type indicated. Antenna types not included in this list, having a gain greater than the maximum gain indicated for that type, are strictly prohibited for use with this device.

#### Concernant les EVMs avec antennes détachables

Conformément à la réglementation d'Industrie Canada, le présent émetteur radio peut fonctionner avec une antenne d'un type et d'un gain maximal (ou inférieur) approuvé pour l'émetteur par Industrie Canada. Dans le but de réduire les risques de brouillage radioélectrique à l'intention des autres utilisateurs, il faut choisir le type d'antenne et son gain de sorte que la puissance isotope rayonnée équivalente (p.i.r.e.) ne dépasse pas l'intensité nécessaire à l'établissement d'une communication satisfaisante. Le présent émetteur radio a été approuvé par Industrie Canada pour fonctionner avec les types d'antenne énumérés dans le manuel d'usage et ayant un gain admissible maximal et l'impédance requise pour chaque type d'antenne. Les types d'antenne non inclus dans cette liste, ou dont le gain est supérieur au gain maximal indiqué, sont strictement interdits pour l'exploitation de l'émetteur

#### 3.3 Japan

3.3.1 *Notice for EVMs delivered in Japan:* Please see [http://www.tij.co.jp/lsds/ti\\_ja/general/eStore/notice\\_01.page](http://www.tij.co.jp/lsds/ti_ja/general/eStore/notice_01.page) 日本国内に輸入される評価用キット、ボードについては、次のところをご覧ください。  
[http://www.tij.co.jp/lsds/ti\\_ja/general/eStore/notice\\_01.page](http://www.tij.co.jp/lsds/ti_ja/general/eStore/notice_01.page)

3.3.2 *Notice for Users of EVMs Considered "Radio Frequency Products" in Japan:* EVMs entering Japan may not be certified by TI as conforming to Technical Regulations of Radio Law of Japan.

If User uses EVMs in Japan, not certified to Technical Regulations of Radio Law of Japan, User is required to follow the instructions set forth by Radio Law of Japan, which includes, but is not limited to, the instructions below with respect to EVMs (which for the avoidance of doubt are stated strictly for convenience and should be verified by User):

1. Use EVMs in a shielded room or any other test facility as defined in the notification #173 issued by Ministry of Internal Affairs and Communications on March 28, 2006, based on Sub-section 1.1 of Article 6 of the Ministry's Rule for Enforcement of Radio Law of Japan,
2. Use EVMs only after User obtains the license of Test Radio Station as provided in Radio Law of Japan with respect to EVMs, or
3. Use of EVMs only after User obtains the Technical Regulations Conformity Certification as provided in Radio Law of Japan with respect to EVMs. Also, do not transfer EVMs, unless User gives the same notice above to the transferee. Please note that if User does not follow the instructions above, User will be subject to penalties of Radio Law of Japan.

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#### 3.4 European Union

3.4.1 *For EVMs subject to EU Directive 2014/30/EU (Electromagnetic Compatibility Directive):*

This is a class A product intended for use in environments other than domestic environments that are connected to a low-voltage power-supply network that supplies buildings used for domestic purposes. In a domestic environment this product may cause radio interference in which case the user may be required to take adequate measures.

---

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4.1 EVMS ARE NOT FOR USE IN FUNCTIONAL SAFETY AND/OR SAFETY CRITICAL EVALUATIONS, INCLUDING BUT NOT LIMITED TO EVALUATIONS OF LIFE SUPPORT APPLICATIONS.

4.2 User must read and apply the user guide and other available documentation provided by TI regarding the EVM prior to handling or using the EVM, including without limitation any warning or restriction notices. The notices contain important safety information related to, for example, temperatures and voltages.

4.3 *Safety-Related Warnings and Restrictions:*

4.3.1 User shall operate the EVM within TI's recommended specifications and environmental considerations stated in the user guide, other available documentation provided by TI, and any other applicable requirements and employ reasonable and customary safeguards. Exceeding the specified performance ratings and specifications (including but not limited to input and output voltage, current, power, and environmental ranges) for the EVM may cause personal injury or death, or property damage. If there are questions concerning performance ratings and specifications, User should contact a TI field representative prior to connecting interface electronics including input power and intended loads. Any loads applied outside of the specified output range may also result in unintended and/or inaccurate operation and/or possible permanent damage to the EVM and/or interface electronics. Please consult the EVM user guide prior to connecting any load to the EVM output. If there is uncertainty as to the load specification, please contact a TI field representative. During normal operation, even with the inputs and outputs kept within the specified allowable ranges, some circuit components may have elevated case temperatures. These components include but are not limited to linear regulators, switching transistors, pass transistors, current sense resistors, and heat sinks, which can be identified using the information in the associated documentation. When working with the EVM, please be aware that the EVM may become very warm.

4.3.2 EVMs are intended solely for use by technically qualified, professional electronics experts who are familiar with the dangers and application risks associated with handling electrical mechanical components, systems, and subsystems. User assumes all responsibility and liability for proper and safe handling and use of the EVM by User or its employees, affiliates, contractors or designees. User assumes all responsibility and liability to ensure that any interfaces (electronic and/or mechanical) between the EVM and any human body are designed with suitable isolation and means to safely limit accessible leakage currents to minimize the risk of electrical shock hazard. User assumes all responsibility and liability for any improper or unsafe handling or use of the EVM by User or its employees, affiliates, contractors or designees.

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