

GaN-based 4kW Bi-directional CLLLC Converter Reference Design



Description

The PMP23461 reference design is a 4kW, bidirectional, CLLLC converter. The design employs a full-bridge CLLLC converter with synchronous rectification. The CLLLC utilizes both frequency and phase modulation to regulate the output across the required regulation range. The design uses a single processing core inside a TMS320F28388D microcontroller to control CLLLC. Synchronous rectification is implemented by the same microcontroller with Rogowski coil current sensors. High density is achieved through the use of high-speed GaN switches (LMG3522). The CLLLC runs with a variable frequency from 250kHz to 800kHz.

Features

- 4kW, bidirectional, CLLLC converter
- Peak system efficiency of 96.5% with an open-frame power density of 2kW/L
- In-built frequency response analyzer (SFRA) for verification and design of control loops

Applications

- [Onboard charger](#)
- [Secondary voltage sense](#)
- [Secondary current sense](#)

Resources

[PMP23461](#)

Design Folder

[TLV365-Q1](#), [LMG3522R030-Q1](#)

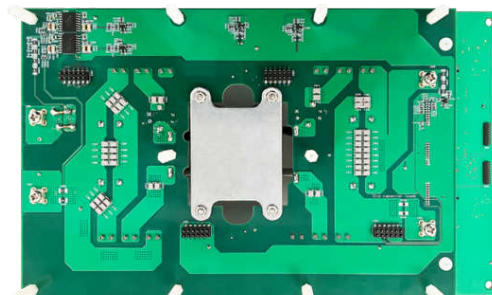
Product Folder

[TMS320F280039C-Q1](#), [TMS320F28388D](#)

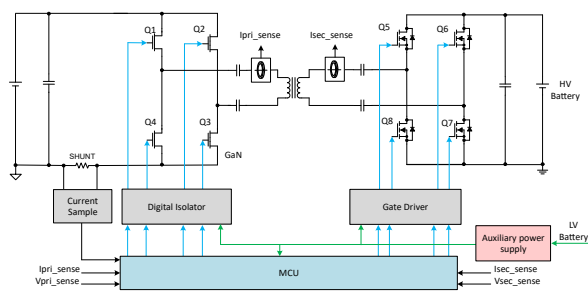
Product Folder



Top of Board



Bottom of Board



Block Diagram

1 Test Prerequisites

This chapter describes the functional parameters of CLLLC converters and the required test equipments.

1.1 Voltage and Current Requirements

Table 1-1. Voltage and Current Requirements

Parameter	MIN	TYP	MAX	UNITS
V_{in}	380	400	450	V
I_{in}			12	A
V_{out}	250	350	400	V
I_{out}	1		12	A
Switching Frequency	250	500	800	kHz

1.2 Required Equipment

- DC source: Chroma 62150H-1000
- DC source: GW Instek GPS-3303C
- DC load: Chroma 63208E-600-560
- Multimeter: Fluke 287C
- Oscilloscope: Tektronix DPO3054
- Electrical thermography: Fluke TiS55
- Vector Network Analyzer: OMICRON Bode100

1.3 Considerations

PMP23461 is a re-design of PMP22650/TIDM02013 CLLLC power stage. PMP23461 has four GaN daughter card, one Interposer, one MCU card and Main board. Using GaN daughter card enables customer quick replace failure switches. Most components of two reference design are the same, except for operational amplifier used in current sensing circuit.

The GaN card is [LMG3522EVM-042](#), you can apply for extra boards. There are three options for MCU card. You can use [F280039C EVM](#) or [F28P65X EVM](#) or [F28388D EVM](#).

For design guide, please refer to [TIDM-02013](#).

1.4 Dimensions

The board total dimensions are 250mm (length) × 160mm (width) × 50mm (height).

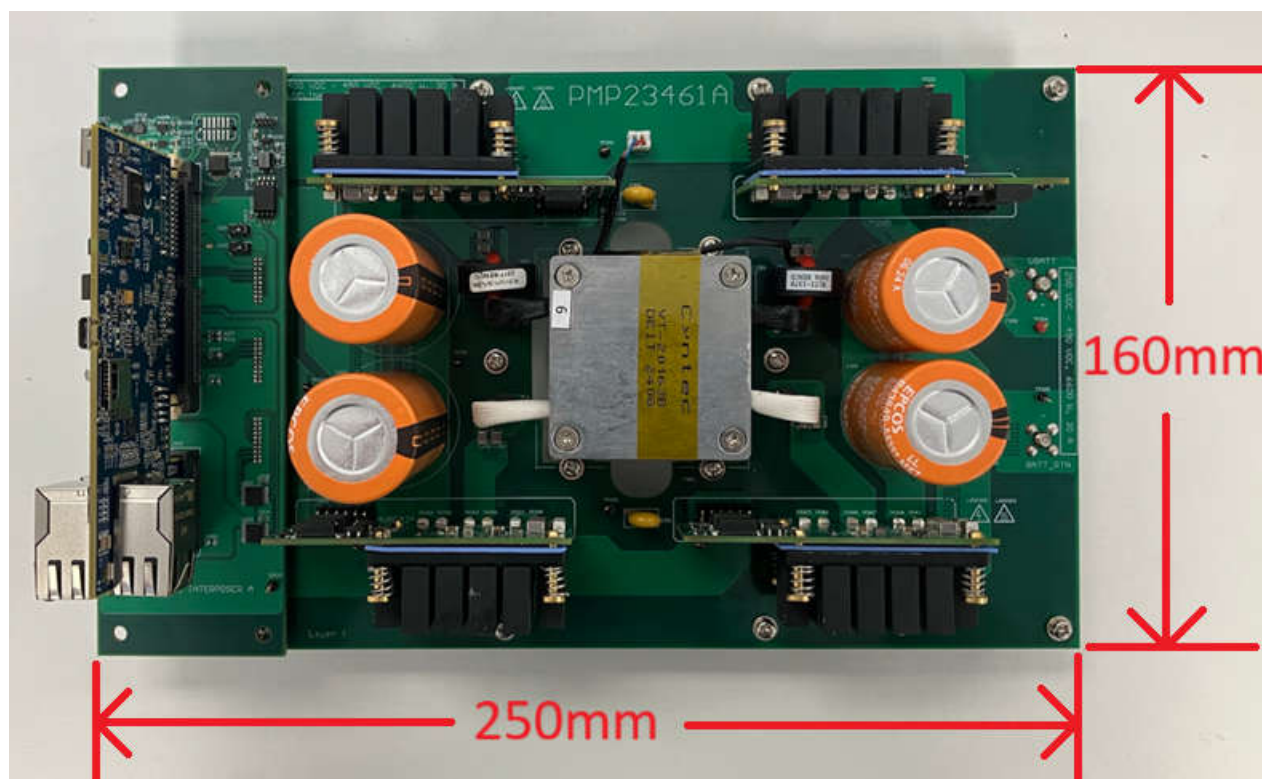


Figure 1-1. Dimensions

2 Testing and Results

2.1 Efficiency Graphs

Efficiency is shown in [Figure 2-1](#).

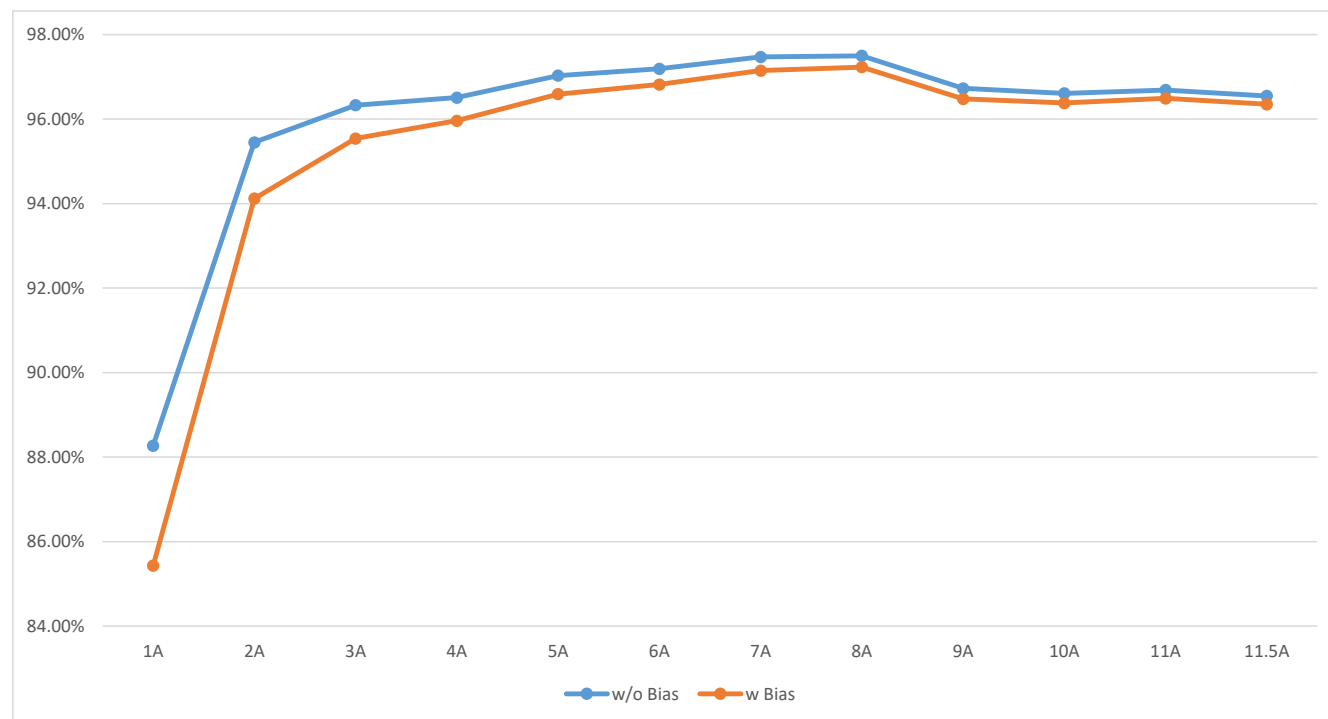


Figure 2-1. Efficiency Graph at 400V_{in}, 350V_{out}

2.2 Efficiency Data

Efficiency data is shown in [Table 2-1](#).

Table 2-1. Efficiency at 400V_{in}, 350V_{out}

V _{out} (350)/V	I _{out}	P _{out} /W	V _{in} /V	I _{in} /A	P _{in} /W	V _{bias} /V	I _{bias} /A	P _{bias} /W	Eff no bias/%	Eff with bias/%
353.07	1	353.07	399.99	1	399.99	5.1	2.61	13.311	88.27%	85.43%
353.137	2	706.274	399.95	1.85	739.9075	5.1	2.06	10.506	95.45%	94.12%
353.15	3	1059.45	399.93	2.75	1099.8075	5.1	1.78	9.078	96.33%	95.54%
353.19	4	1412.76	399.95	3.66	1463.817	5.1	1.65	8.415	96.51%	95.96%
353.16	5	1765.8	399.96	4.55	1819.818	5.1	1.64	8.364	97.03%	96.59%
353.1	6	2118.6	399.97	5.45	2179.8365	5.1	1.63	8.313	97.19%	96.82%
353.08	7	2471.56	399.96	6.34	2535.7464	5.1	1.62	8.262	97.47%	97.15%
352.93	8	2823.44	399.96	7.24	2895.7104	5.1	1.61	8.211	97.50%	97.23%
351.62	9	3164.58	399.95	8.18	3271.591	5.1	1.68	8.568	96.73%	96.48%
351.59	10	3515.9	399.94	9.1	3639.454	5.1	1.68	8.568	96.61%	96.38%
351.55	11	3867.05	399.93	10	3999.3	5.1	1.67	8.517	96.69%	96.49%
351.55	11.5	4042.825	399.93	10.47	4187.2671	5.1	1.67	8.517	96.55%	96.35%

2.3 Current Sense

Two Rogowski coils are added to monitor the current, one at primary resonant tank, one at secondary tank, as shown in [Block Diagram](#).

The output signal of Rogowski coil is a differential waveform of current, So we need add an integral circuit to restore the current signal. After that, using an amplifying circuit to adjust the amplitude of current signal, as [Figure 2-2](#) shows. R327 and C337 forms a basic integral circuit, then an inverting amplifier circuit using TLV365 provides a gain of 1.825 to the signal. Finally we can get the waveforms as [Figure 2-3](#), [Figure 2-4](#), and [Figure 2-5](#) shows.

CH1: CLLLC_IPRIM_TANK signal

CH3: Primary resonant tank current

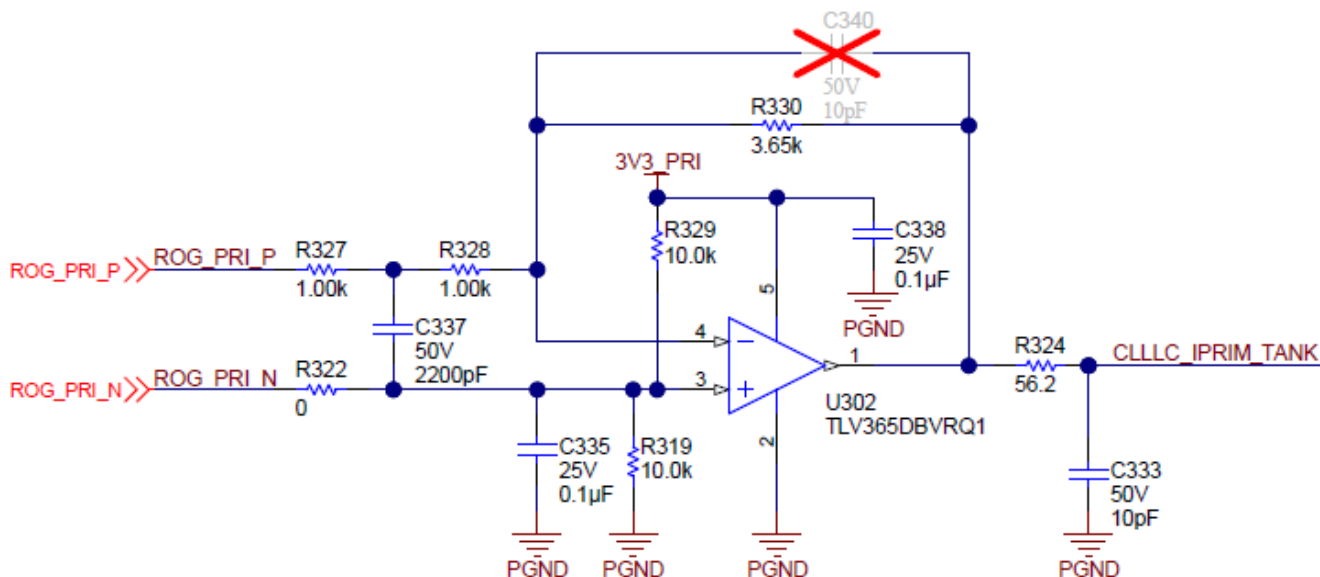


Figure 2-2. Current Sensing Circuit

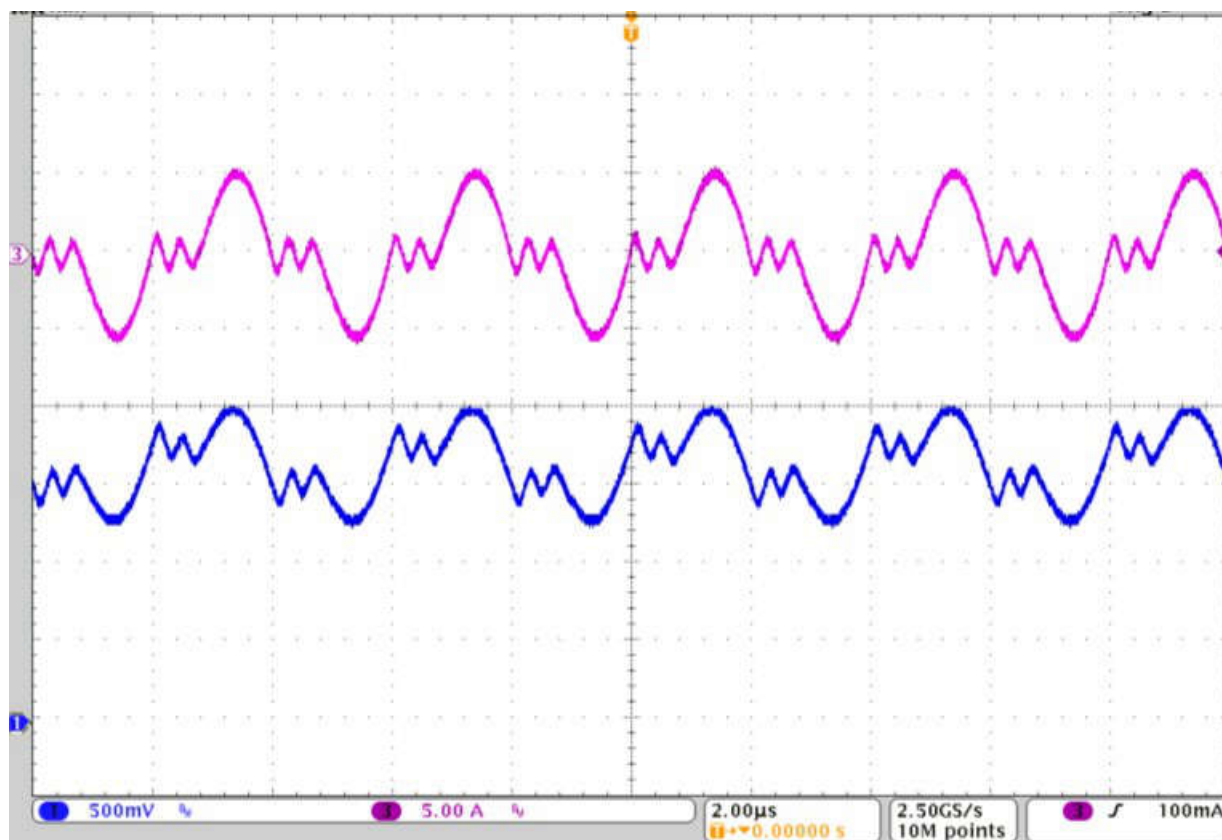


Figure 2-3. CLLLC_IPRIM_TANK Signal at 250kHz

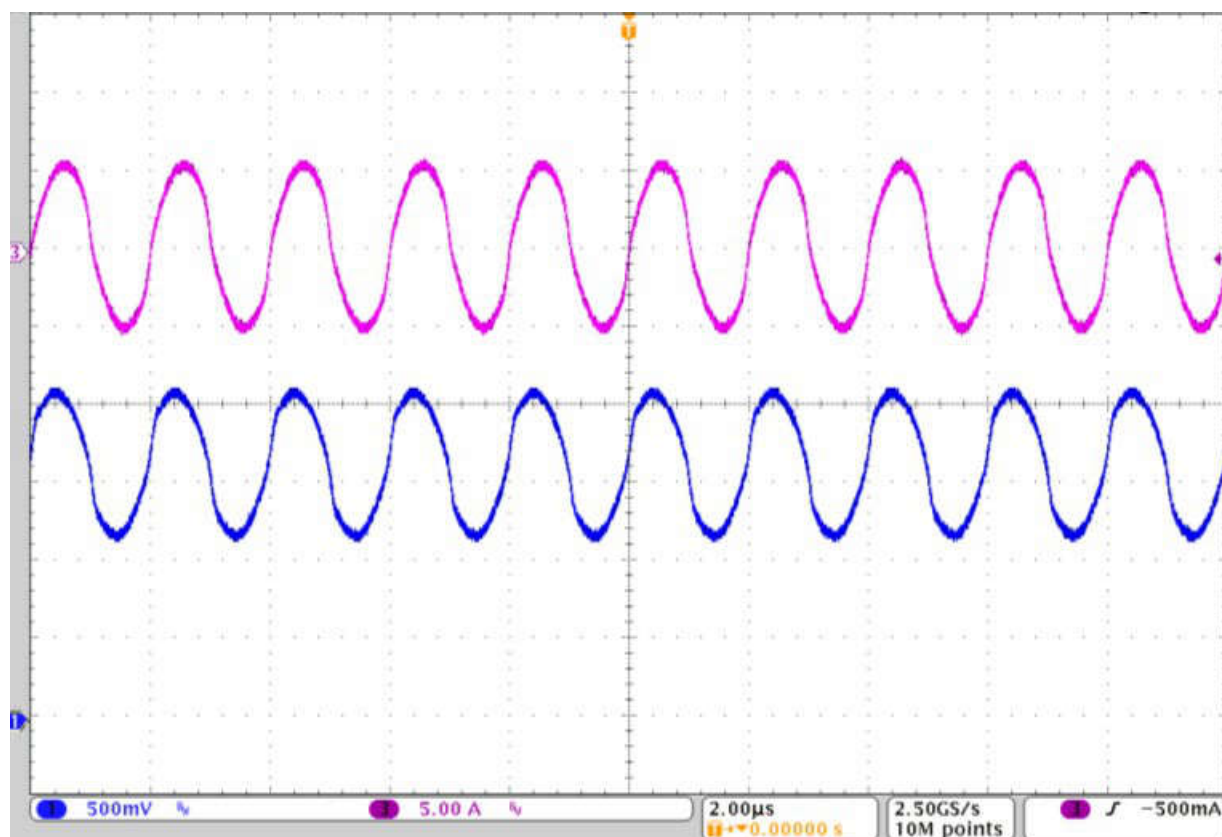


Figure 2-4. CLLLC_IPRIM_TANK Signal at 500kHz



Figure 2-5. CLLC_IPRIM_TANK Signal at 800kHz

2.4 Bode Plots

Bode plots are shown in Figure 2-6. The test condition is $400V_{in}$, $350V_{out}$, $11.5A I_{out}$, room temperature. As shown in Figure 2-6, the gain margin is $-15.79dB$. The phase margin is 101.93° with 635Hz bandwidth.

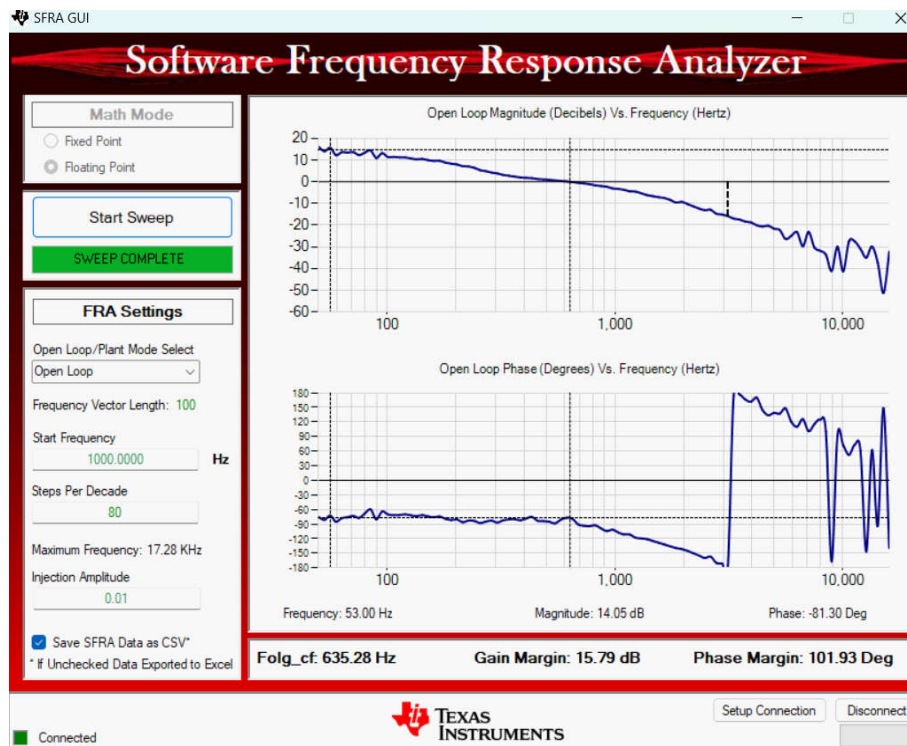


Figure 2-6. Bode Plot

3 Waveforms

3.1 Switching

Figure 3-1 shows CLLC operation at 11.5A (4kW) under the following parameters:

- Traces
 - CH1: GaN Primary Switch Node Drain Voltage
 - CH2: GaN Secondary Switch Node Drain Voltage
 - CH3: Transformer Primary Current
 - CH4: Transformer Secondary Current
- Conditions
 - $V_{IN} = 400V$
 - $V_{OUT} = 350V$
 - $I_{OUT} = 11.5A$

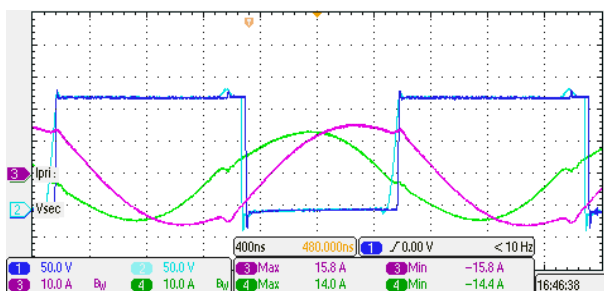


Figure 3-1. CLLLC Operation 11.5A (4kW)

Figure 3-2 shows CLLLC operation at 2A under the following parameters:

- Traces
 - C1: GaN Primary Switch Node Drain Voltage
 - C2: GaN Secondary Switch Node Drain Voltage
 - C3: Transformer Primary Current
 - C4: Transformer Secondary Current
- Conditions
 - $V_{IN} = 400V$
 - $V_{OUT} = 350V$
 - $I_{OUT} = 2A$

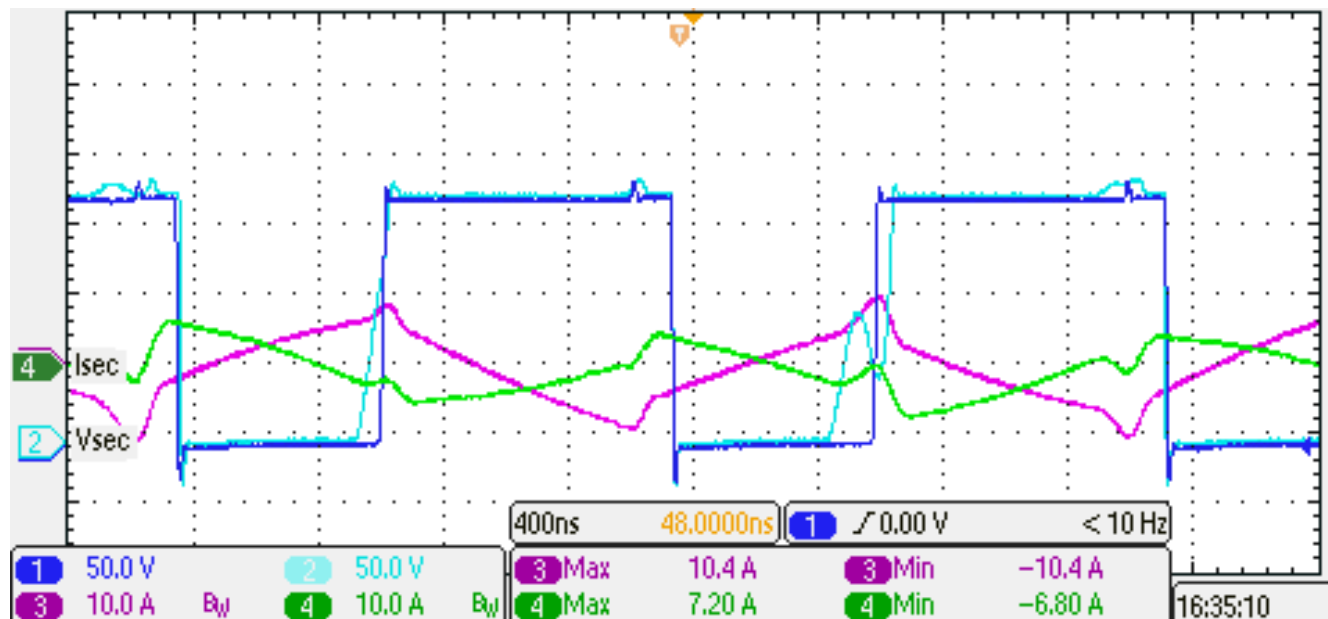


Figure 3-2. CLLLC Operation 2A

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Last updated 10/2025