

# Output Inductor Considerations in a Synchronous Buck Converter



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Inductors are an essential component of switching voltage regulators and synchronous buck converters, as shown in [Figure 1](#). In all switching regulators, the output inductor stores energy from the power input source when the MOSFETs switch on and releases the energy to the load (output).

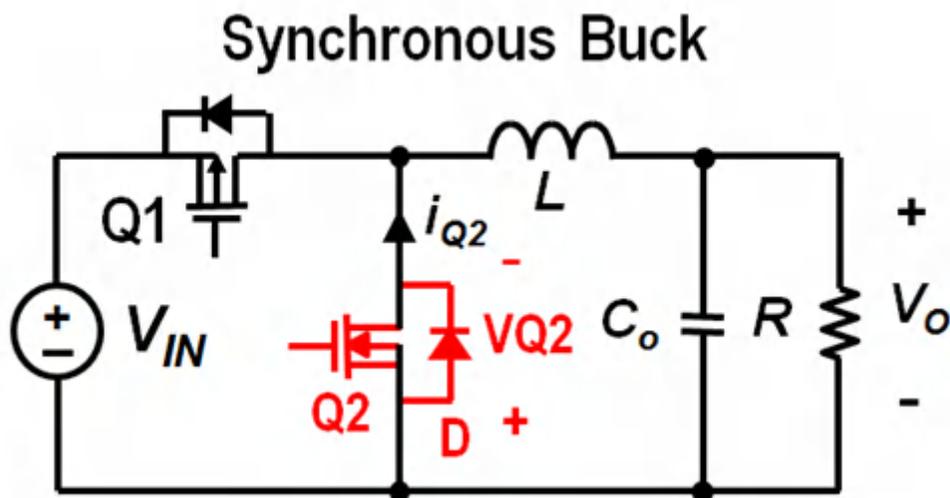


Figure 1. Synchronous Buck DC/DC Converter

You should select inductors to manage output capacitor size, load transients and output ripple current. There are benefits of both low and high inductance values.

The benefits of low inductance include:

- Lower DC resistance (DCR), which is inherent in the inductor wire, and which affects ripple and power loss.
- Higher saturation current, for higher output-current capability.
- Higher slew rate ( $di/dt$ ), which improves load transient response and reduces output capacitance for a given load transient.

The benefits of high inductance include:

- Lower ripple current, which in turn reduces:
  - AC losses (inductor skin effect).
  - MOSFET root-mean-square (RMS) current.
  - Output capacitor RMS current.
  - Output capacitance for an equivalent output ripple.
  - Continuous inductor current over a wider load range.

Equation 1 calculates the output inductor value:

$$L = \frac{V_{OUT}}{V_{IN(max)}} \times \frac{(V_{IN(max)} - V_{OUT})}{F_S \times I_{RIPPLE}} \quad (1)$$

where L is the output inductance,  $V_{OUT}$  is the target output voltage,  $V_{IN(max)}$  is the maximum input voltage,  $F_S$  is the buck converter switching frequency and  $I_{RIPPLE}$  is the target output ripple current.

I recommend sizing the ripple current for 10% to 30% of full load. Plugging values into Equation 1, Equation 2 shows the output inductance calculation result:

$$L = \frac{1.5}{13.2} \times \frac{(13.2 - 1.5)}{500 \times 10^3 \times 3} = 0.9 \mu H \quad (2)$$

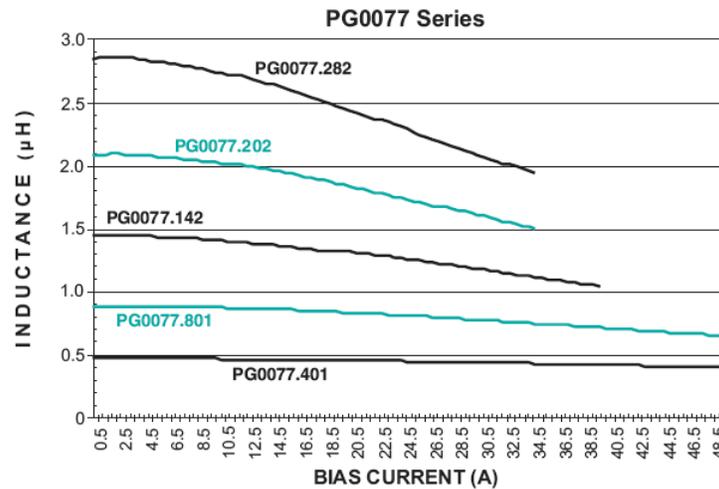
In this case, I selected the PG0077.801 inductor from Pulse Electronics. [Table 1](#) shows its relevant parameters.

**Table 1. PG0077.801 Inductor Parameters (Image Courtesy of Pulse Electronics)**

Electrical Specifications @ 25°C — Operating Temperature -40°C to +130°C <sup>1</sup>									
Part <sup>1,2</sup> Number	Inductance <sup>2</sup> @I <sub>rated</sub> (μH TYP)	I <sub>rated</sub> <sup>3</sup> (A)	DCR (mΩ)		Inductance @0A <sub>dc</sub> (μH ±20%)	Saturation <sup>4</sup> Current I <sub>sat</sub> (A)	Heating <sup>5</sup> Current I <sub>dc</sub> (A)	Core Loss <sup>6</sup> Factor	
			TYP	MAX				K1	K2
PG0077.401	0.38	35	0.75	0.80	0.45	48	35	13.77E-9	27.6
<b>PG0077.801</b>	<b>0.75</b>	<b>31</b>	<b>1.20</b>	<b>1.30</b>	<b>0.80</b>	<b>38</b>	<b>31</b>	<b>13.77E-9</b>	<b>39.4</b>
PG0077.142	1.32	26	2.00	2.10	1.40	28	26	13.77E-9	53.6
PG0077.202	1.90	21	2.80	2.90	2.00	24	21	13.77E-9	62.7
PG0077.282	2.65	17	4.10	4.20	2.80	20	17	13.77E-9	74.3
PG0084.351	0.28	28	1.30	1.80	0.35	40	28	9.18E-9	29.4
PG0084.651	0.52	21.5	2.30	2.80	0.65	32	21.5	9.18E-9	39.1
PG0084.112	0.88	19	3.60	4.20	1.10	24	19	9.18E-9	51.4

It is important to check the inductance vs. the load (bias) current, as inductance decreases with increasing current. Then you can determine what the actual inductance is at the target load current.

If you assume 15A of continuous output current, the actual inductance is 0.83mH, as shown in [Figure 2](#).



**Figure 2. Inductance vs. Current (Image Courtesy of Pulse Electronics)**

Once you know the actual inductance value, you can recalculate the ripple and RMS currents. Equation 3 recalculates ripple current:

$$\begin{aligned}
 I_{RIPPLE} &= \frac{V_{OUT}}{V_{IN(max)}} \times \frac{(V_{IN(max)} - V_{OUT})}{F_S \times L} \\
 &= \frac{1.5}{13.2} \times \frac{(13.2 - 1.5)}{500 \times 10^3 \times 0.83 \times 10^{-6}} \\
 &= 3.32A
 \end{aligned} \tag{3}$$

Equation 4 recalculates RMS current:

$$\begin{aligned}
 I_{L(RMS)} &= \sqrt{I_{OUT}^2 + \frac{\Delta I_{L(pp)}^2}{12}} \\
 &= \sqrt{15^2 + \frac{3.32^2}{12}} = 15.028A
 \end{aligned} \tag{4}$$

You can also calculate the inductor losses. Total inductor losses are winding losses and core losses, expressed by Equations 5 and 6:

$$P_{WINDING} = I_{L(RMS)}^2 \times R_L = 15.028^2 \times 1.3 \times 10^{-3} = 0.294W \tag{5}$$

$$P_{CORE} = K1 \times F_{SW}^{0.5539} \times (K2 \times \Delta I)^{2.2355} \tag{6}$$

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where  $K1 = 13.77 \times 10^{-9}$ ,  $K2 = 39.4$ ,  $F_{SW} = 500\text{kHz}$ ,  $DI = 3.32\text{A}$  (the calculated ripple current) and  $P_{CORE} = 0.983\text{W}$ .

In this example, the total inductor power loss is  $0.294\text{W} + 0.983\text{W} = 1.277\text{W}$ .

There are many inductor types to choose from, but most buck DC/DC converters typically use ferrite drum and iron powder toroid inductors. So when designing a buck converter, keep these inductor selection criteria in mind for a high-performance, stable and reliable design.

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