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## Why separate report for $\mathbf{9 0 0} \mathbf{m V}$ output:

PMP9738 has same physical design and was tested at 1.0 Vout where off 12 Vin there is "fixed frequency" of about 300 kHz and variable on time. PMP10393 is the 600 mV version running always with fixed on time per phase of about 260 nsec (plus up to 30 nsec switch delay) and variable frequency down to the $220-250 \mathrm{kHz}$ range for 600 mV off 12 Vin . See its report showing satisfactory performance with this mode. Efficiency is actually improved with the reduced switching frequency. Even though there is no active current sharing, the fixed pulse width per phase actually improves thermal sharing for variations in on resistance of the power stages.

With the 900 mV application at 220 A , it was decided to test up to 240 A vs. the 200 A max previously.

At each load interval of 20A from zero to 120 A and at 139A, 180A, 220A and 240A, Vin was varied from below 11 V to over 13 V monitoring main switching pulses to verify no instabilities during transition between quasi constant frequency and fixed pulse width modes.

In most 12 Vin applications, extensive testing is not done at $11 \& 13$ Vin as operation and results are very similar. Here with 11 Vin having operation in quasi fixed frequency over almost the entire load range and 13 Vin having operation in fixed on time over the entire load range and 12 Vin having fixed on time at light loads and quasi fixed frequency at heavy loads, it was decided to look in more detail at all 3 inputs.

With the large load step \& dump test, 11 Vin would have quasi fixed frequency throughout the change, 13 Vin would have fixed on time throughout the change and 12 Vin would switch between the two modes. However, peak overshoots and undershoots were very similar for all 3 cases.

Efficiency at light loads was about $1 \%$ higher at 11 Vin than at 13 Vin. However, about 100 A loading the 3 curves ( $11 \mathrm{~V}, 12 \mathrm{~V}, 13 \mathrm{~V}$ ) converged with efficiency differences becoming less than $0.1 \%$ for loads above 195 A. Here, lower frequency at higher Vin cancelled higher switching losses per cycle at higher Vin.

PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B) Texas Instruments

Frequency and on time vs. Vin and load: scope with 8 nsec low pass filter
Fluke 87 meter used for measuring Vout for loads under 160A
Agilent 34401A voltage meter used for measuring Vout at loads 160A and above

| Vin in Volts | Vout | Iout | frequency | On time | Max temperature |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 12.04 | 0.9003 | 0 | 262k | 285n |  |
| 12.01 | 0.9002 | 20 | 271k | 278n |  |
| 12.05 | 0.9001 | 40 | 283k | 269n |  |
| 12.00 | 0.9000 | 60 | 288k | 268n |  |
| 12.00 | 0.8999 | 80 | 289k | 268n |  |
| 12.02 | 0.8998 | 100 | 291k | 268n |  |
| 12.04 | 0.8997 | 120 | 294k | 268n |  |
| 12.01 | 0.8996 | 138.6 | 298k | 268n |  |
| 12.00 | 0.8999 | 160 | 302k | $267 n$ | 46/ir1072 |
| 12.01 | 0.8998 | 180 | 305k | 267n | 50 |
| 12.01 | 0.8996 | 200 | 307k | 269n | 56/ir1073 |
| 12.01 | 0.8995 | 220 | 310k | 270n | 63/ir1074 |
| 12.01 | 0.8994 | 240 | 310k | 272n | 72/ir1075 |
|  |  |  |  |  |  |
| 11.00 | 0.9003 | 0 | 286k | 285n |  |
| 11.04 | 0.9002 | 20 | 294k | 280n |  |
| 11.00 | 0.9001 | 40 | 298k | 280n |  |
| 11.01 | 0.9000 | 60 | 300k | 281n |  |
| 11.02 | 0.9000 | 80 | 301k | 283n |  |
| 11.00 | 0.8998 | 100 | 302k | $285 n$ |  |
| 11.00 | 0.8997 | 120 | 304k | 286n |  |
| 11.05 | 0.8996 | 138.6 | 304k | 287n |  |
| 10.99 | 0.8996 | 180 | 307k | 291n | 52 |
| 10.99 | 0.8994 | 220 | 308k | 295n | 67/1r1080 |
| 10.99 | 0.8993 | 240 | 309k | 298k | 74/ir1077 |
|  |  |  |  |  |  |
| 13.01 | 0.9003 | 0 | 242k | 285n |  |
| 13.03 | 0.9002 | 20 | 250k | 279n |  |
| 13.01 | 0.9001 | 40 | 260k | 269n |  |
| 13.02 | 0.9000 | 60 | 266k | 268n |  |
| 13.01 | 0.8999 | 80 | 267k | 268n |  |
| 13.02 | 0.8999 | 100 | 269k | 268n |  |
| 13.01 | 0.8997 | 120 | 272k | 268n |  |
| 13.00 | 0.8996 | 138.6 | 276k | 268n |  |
| 13.00 | 0.8997 | 180 | 280k | 268n | 52 |
| 13.01 | 0.8994 | 220 | 287k | 268n | 66/ir1079 |
| 13.00 | 0.8993 | 240 | 289k | 268n | 75/ir1078 |
| Q |  |  |  |  |  |

Target "quasi fixed frequency" is 300 kHz .
Even at "constant on time mode", actual on time at zero and 20 A loads increased due to slower turn off of power stages than turn on at light loads.
Hence, at 13 Vin always in "constant on time mode" with varying frequency;
At 11 Vin at "quasi fixed frequency" except to zero and 20 A loads;
At 12 Vin in "constant on time mode" at light to moderate loads.

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Full load GUI image:


Q
240A testing


PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B) Texas Instruments

Full load 13Vin


Q
Full load 11 Vin:


Qq

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Max 240A load output ripple on C19:
12 Vin (11 Vin very similar)


And now 13 Vin:


PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B) Texas Instruments

900 mV 300kHz settings: 11.0 VIN quasi constant frequency mode: frequency range $300-308 \mathrm{kHz}$ Vout measured at C19: All 6 phases on
Step load response from 60 A to 180 A (120 A step) in 7 usec: $\sim 30 \mathrm{mV}$ undeshoot

q
Load dump response from 196 A to 60 A (136 A step) in 5 usec: ~55 mV overshoot


PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B) Texas Instruments

900 mV 300kHz settings: 12.0 VIN
Constant on time mode at 60A \& quasi constant frequency at 180A:
frequency range $288-308 \mathrm{kHz} \quad$ Vout measured at C19: All 6 phases on
Step load response from 60 A to 180 A (120 A step) in 7 usec: $\sim 31 \mathrm{mV}$ undeshoot

q
Load dump response from 196 A to 60 A (136 A step) in 5 usec: ~56 mV overshoot


PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B) Texas Instruments

900 mV 300kHz settings: 13.0 VIN
Constant on time mode at $\sim 268-270 \mathrm{nsec}$ on times: frequency range $266-280 \mathrm{kHz}$
Vout measured at C19: All 6 phases on
Step load response from 60 A to 180 A (120 A step) in 7 usec: $\sim 32 \mathrm{mV}$ undeshoot

q
Load dump response from 196 A to 60 A (136 A step) in 5 usec: ~58 mV overshoot


Waveforms across resistors in dynamic load bank used to calculate step load current and speed: There are two resistor paths from Vout; R1 and R2 each 2mOhm and tied to Vout. Hence, the total load step is the sum of both. Here scope ground on Vout side of resistor. First R1 2mOhm: 120 mV in 7 usec or 60 A in 7 usec


And now R2(also 2mOhm): also 120 mV in 7 usec or 60 A in 7 usec


Load strings are in parallel driven by same FET Q1: Hence, combined: 120 A in 7 usec

Waveforms across resistors in dynamic load bank used to calculate load dump current and speed: There are two resistor paths from Vout; R1 and R2 each 2mOhm and tied to Vout. Hence, the total load dump is the sum of both. Here scope ground on Vout side of resistor. First R1 2 mOhm : 132 mV in 5 usec or 66 A in 5 usec
Voltage overshoot above Vout at end may be inductive: Hence, I will only count -132 mV to 0


And now R2(also 2 mOhm ): 140 mV in 5 usec or 70A in 5 usec
Voltage overshoot above Vout at end may be inductive: Hence, I will only count -140 mV to 0 .


Load strings are in parallel driven by same FET Q1: Hence, combined: 136 A in 5 usec

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Step load \& Dump waveforms:
R1


| Measure | P1:max(C1) | P2:min(C1) | P3:width( C 1 ) | P4:freq(C1) | P5:rise(C1) | P6:fall(C1) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| value | 15.3 mV | <-145.3 mV | -- | -- | $2.5720 \mu \mathrm{~s}$ | $5.5282 \mu \mathrm{~s}$ |  |  |
| status | $\Downarrow$ | $\Downarrow$ | A | 4 | $\Downarrow$ | - |  |  |
| C1 BwL DC1M |  |  |  |  |  | Timebase $-572 \mu \mathrm{~s}$ | Trigger | [C1]DC |
| $20.0 \mathrm{mV} / \mathrm{div}$ 60 mV offset |  |  |  |  |  | $\begin{array}{ll}  & 200 \mu \mathrm{~s} / \mathrm{div} \\ 8.00 \mathrm{MS} \\ 4.00 \mathrm{GS} / \mathrm{s} \end{array}$ | Stop Edge | $-67.8 \mathrm{mV}$ <br> Negative |

And now R2


| Measure | P1:max(C1) | P2:min (C1) | P3:width( C 1 ) | P4:freq(C1) | P5:rise(C1) | P6:fall(C1) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| value | 15.3 mV | $<-145.3 \mathrm{mV}$ | -- | -- | $1.8899 \mu \mathrm{~s}$ | $3.9466 \mu \mathrm{~s}$ |  |  |  |
| status | $\Downarrow$ | $\Downarrow$ | A | A | $\Downarrow$ |  | $\checkmark$ |  |  |
| C1 EwL DC1M |  |  |  |  |  | Timebase | $-572 \mu \mathrm{~s}$ | Trigger | [C1]DC |
| $\begin{aligned} & 20.0 \mathrm{mV} / \mathrm{div} \\ & 60 \mathrm{mV} \text { offset } \end{aligned}$ |  |  |  |  |  | 8.00 MS 4 | $\begin{aligned} & 200 \mu \mathrm{~s} / \mathrm{div} \\ & 4.00 \mathrm{GS} / \mathrm{s} \end{aligned}$ | Stop <br> Edge | $-67.8 \mathrm{mV}$ Negative |

PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B)
Texas Instruments

Efficiency data on Model t13 at 900 mV / 300kHz / 6 phases: 1-2 Meters per second airflow 21 degrees Celsius ambient: 12 Vin

| Vin in Volts | Iin Amperes | Vout | Iout | Efficiency \% | Losses in W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 11.999 | 0.225 | 0.901 | 0.000 | 0.000 | 2.694 |
| 11.999 | 0.601 | 0.901 | 4.989 | 62.326 | 2.716 |
| 11.999 | 0.979 | 0.900 | 9.988 | 76.551 | 2.755 |
| 11.999 | 1.360 | 0.901 | 14.990 | 82.747 | 2.815 |
| 11.999 | 1.742 | 0.900 | 19.990 | 86.118 | 2.902 |
| 11.999 | 2.130 | 0.900 | 24.991 | 88.049 | 3.054 |
| 11.999 | 2.527 | 0.900 | 29.991 | 89.072 | 3.313 |
| 11.999 | 2.934 | 0.900 | 34.993 | 89.515 | 3.691 |
| 11.999 | 3.347 | 0.900 | 39.994 | 89.660 | 4.153 |
| 11.999 | 3.751 | 0.900 | 44.996 | 90.017 | 4.493 |
| 11.999 | 4.163 | 0.900 | 49.999 | 90.126 | 4.932 |
| 11.999 | 4.564 | 0.900 | 55.002 | 90.430 | 5.241 |
| 11.999 | 4.964 | 0.900 | 60.007 | 90.713 | 5.531 |
| 11.999 | 5.362 | 0.900 | 65.012 | 90.967 | 5.812 |
| 11.999 | 5.769 | 0.900 | 70.018 | 91.064 | 6.185 |
| 11.999 | 6.162 | 0.900 | 75.026 | 91.359 | 6.389 |
| 11.999 | 6.571 | 0.900 | 80.031 | 91.384 | 6.793 |
| 11.999 | 6.982 | 0.900 | 85.040 | 91.384 | 7.218 |
| 11.999 | 7.395 | 0.900 | 90.050 | 91.358 | 7.668 |
| 11.999 | 7.810 | 0.900 | 95.060 | 91.317 | 8.137 |
| 11.999 | 8.227 | 0.900 | 100.071 | 91.256 | 8.632 |
| 11.999 | 8.646 | 0.900 | 105.082 | 91.176 | 9.154 |
| 11.999 | 9.067 | 0.900 | 110.096 | 91.089 | 9.696 |
| 11.999 | 9.491 | 0.900 | 115.113 | 90.982 | 10.270 |
| 11.999 | 9.916 | 0.900 | 120.128 | 90.872 | 10.862 |
| 11.999 | 9.904 | 0.900 | 120.000 | 90.881 | 10.837 |
| 11.999 | 10.330 | 0.900 | 124.983 | 90.749 | 11.466 |
| 11.999 | 10.760 | 0.900 | 129.982 | 90.613 | 12.120 |
| 11.999 | 11.192 | 0.900 | 134.984 | 90.462 | 12.810 |
| 11.999 | 11.626 | 0.900 | 139.985 | 90.308 | 13.521 |
| 11.999 | 12.063 | 0.900 | 144.986 | 90.143 | 14.268 |
| 11.999 | 12.502 | 0.900 | 149.986 | 89.976 | 15.038 |
| 11.999 | 12.944 | 0.900 | 154.990 | 89.801 | 15.841 |
| 11.999 | 13.389 | 0.900 | 159.992 | 89.616 | 16.682 |
| 11.999 | 13.836 | 0.900 | 164.993 | 89.428 | 17.551 |
| 11.999 | 14.286 | 0.900 | 169.998 | 89.240 | 18.444 |
| 11.999 | 14.738 | 0.900 | 175.001 | 89.044 | 19.375 |
| 11.999 | 15.192 | 0.900 | 180.008 | 88.851 | 20.325 |
| 11.999 | 15.648 | 0.900 | 185.012 | 88.654 | 21.304 |
| 11.999 | 16.108 | 0.900 | 190.020 | 88.454 | 22.317 |
| 11.999 | 16.570 | 0.900 | 195.027 | 88.252 | 23.358 |
| 11.999 | 17.035 | 0.900 | 200.034 | 88.044 | 24.439 |
| 11.999 | 17.503 | 0.900 | 205.043 | 87.828 | 25.564 |
| 11.999 | 17.975 | 0.900 | 210.053 | 87.612 | 26.719 |
| 11.999 | 18.451 | 0.900 | 215.063 | 87.384 | 27.930 |
| 11.999 | 18.929 | 0.900 | 220.076 | 87.161 | 29.161 |
| 11.999 | 19.410 | 0.899 | 225.088 | 86.931 | 30.438 |
| 11.999 | 19.894 | 0.899 | 230.103 | 86.701 | 31.745 |
| 11.999 | 20.383 | 0.899 | 235.120 | 86.465 | 33.103 |
| 11.999 | 20.874 | 0.899 | 240.135 | 86.226 | 34.501 |

Q

## PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B)

## Texas Instruments

Efficiency data on Model t13 at 900 mV / 300kHz / 6 phases: 1-2 Meters per second airflow 21 degrees Celsius ambient: 13 Vin

| Vin in Volts | Iin Amperes | Vout | Iout | Efficiency \% | Losses in W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 13.004 | 0.223 | 0.901 | 0.000 | 0.002 | 2.896 |
| 13.004 | 0.570 | 0.900 | 4.992 | 60.649 | 2.916 |
| 13.004 | 0.919 | 0.900 | 9.992 | 75.283 | 2.954 |
| 13.004 | 1.270 | 0.900 | 14.993 | 81.762 | 3.011 |
| 13.004 | 1.622 | 0.900 | 19.993 | 85.344 | 3.092 |
| 13.004 | 1.978 | 0.900 | 24.993 | 87.505 | 3.213 |
| 13.004 | 2.340 | 0.900 | 29.993 | 88.759 | 3.420 |
| 13.004 | 2.710 | 0.900 | 34.996 | 89.404 | 3.734 |
| 13.004 | 3.089 | 0.900 | 39.997 | 89.655 | 4.156 |
| 13.004 | 3.471 | 0.900 | 44.998 | 89.759 | 4.622 |
| 13.004 | 3.845 | 0.900 | 50.002 | 90.042 | 4.979 |
| 13.004 | 4.217 | 0.900 | 55.004 | 90.302 | 5.318 |
| 13.004 | 4.596 | 0.900 | 60.010 | 90.397 | 5.739 |
| 13.004 | 4.966 | 0.900 | 65.013 | 90.636 | 6.047 |
| 13.004 | 5.335 | 0.900 | 70.020 | 90.867 | 6.336 |
| 13.004 | 5.705 | 0.900 | 75.028 | 91.050 | 6.639 |
| 13.004 | 6.075 | 0.900 | 80.032 | 91.199 | 6.953 |
| 13.004 | 6.454 | 0.900 | 85.040 | 91.213 | 7.375 |
| 13.004 | 6.835 | 0.900 | 90.050 | 91.206 | 7.816 |
| 13.004 | 7.218 | 0.900 | 95.060 | 91.172 | 8.286 |
| 13.004 | 7.602 | 0.900 | 100.071 | 91.123 | 8.776 |
| 13.004 | 7.988 | 0.900 | 105.081 | 91.054 | 9.292 |
| 13.004 | 8.376 | 0.900 | 110.096 | 90.978 | 9.827 |
| 13.004 | 8.767 | 0.900 | 115.113 | 90.884 | 10.393 |
| 13.004 | 9.159 | 0.900 | 120.126 | 90.779 | 10.983 |
| 13.004 | 9.149 | 0.900 | 120.000 | 90.785 | 10.964 |
| 13.004 | 9.541 | 0.900 | 124.983 | 90.664 | 11.584 |
| 13.004 | 9.938 | 0.900 | 129.984 | 90.530 | 12.238 |
| 13.004 | 10.335 | 0.900 | 134.985 | 90.389 | 12.917 |
| 13.004 | 10.736 | 0.900 | 139.986 | 90.245 | 13.619 |
| 13.004 | 11.138 | 0.900 | 144.988 | 90.086 | 14.360 |
| 13.004 | 11.543 | 0.900 | 149.987 | 89.921 | 15.130 |
| 13.004 | 11.950 | 0.900 | 154.990 | 89.755 | 15.921 |
| 13.004 | 12.360 | 0.900 | 159.992 | 89.582 | 16.745 |
| 13.004 | 12.771 | 0.900 | 164.993 | 89.399 | 17.605 |
| 13.004 | 13.186 | 0.900 | 169.999 | 89.213 | 18.497 |
| 13.004 | 13.602 | 0.900 | 175.000 | 89.024 | 19.415 |
| 13.004 | 14.021 | 0.900 | 180.007 | 88.833 | 20.360 |
| 13.004 | 14.443 | 0.900 | 185.012 | 88.636 | 21.344 |
| 13.004 | 14.867 | 0.900 | 190.020 | 88.434 | 22.360 |
| 13.004 | 15.293 | 0.900 | 195.029 | 88.230 | 23.408 |
| 13.004 | 15.723 | 0.900 | 200.033 | 88.022 | 24.490 |
| 13.004 | 16.155 | 0.900 | 205.043 | 87.810 | 25.609 |
| 13.004 | 16.590 | 0.900 | 210.053 | 87.593 | 26.765 |
| 13.004 | 17.028 | 0.900 | 215.064 | 87.374 | 27.957 |
| 13.004 | 17.468 | 0.900 | 220.076 | 87.155 | 29.177 |
| 13.004 | 17.911 | 0.900 | 225.088 | 86.933 | 30.435 |
| 13.004 | 18.357 | 0.899 | 230.102 | 86.703 | 31.743 |
| 13.004 | 18.807 | 0.899 | 235.119 | 86.471 | 33.087 |
| 13.004 | 19.261 | 0.899 | 240.133 | 86.232 | 34.483 |

PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B)
Texas Instruments
Efficiency data on Model t13 at 900 mV / 300kHz / 6 phases: 1-2 Meters per second airflow 21 degrees Celsius ambient: 11 Vin

| Vin in Volts | Iin Amperes | Vout | Iout | Efficiency \% | Losses in W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10.995 | 0.228 | 0.901 | 0.000 | 0.000 | 2.511 |
| 10.995 | 0.639 | 0.900 | 4.986 | 63.921 | 2.534 |
| 10.995 | 1.052 | 0.900 | 9.986 | 77.733 | 2.576 |
| 10.995 | 1.467 | 0.900 | 14.987 | 83.646 | 2.638 |
| 10.995 | 1.886 | 0.900 | 19.989 | 86.809 | 2.735 |
| 10.995 | 2.313 | 0.900 | 24.990 | 88.491 | 2.926 |
| 10.995 | 2.749 | 0.900 | 29.989 | 89.343 | 3.221 |
| 10.995 | 3.195 | 0.900 | 34.992 | 89.698 | 3.619 |
| 10.995 | 3.649 | 0.900 | 39.994 | 89.767 | 4.105 |
| 10.995 | 4.095 | 0.900 | 44.995 | 89.989 | 4.507 |
| 10.995 | 4.521 | 0.900 | 50.000 | 90.561 | 4.692 |
| 10.995 | 4.941 | 0.900 | 55.003 | 91.148 | 4.809 |
| 10.995 | 5.374 | 0.900 | 60.009 | 91.442 | 5.056 |
| 10.995 | 5.814 | 0.900 | 65.013 | 91.569 | 5.389 |
| 10.995 | 6.255 | 0.900 | 70.021 | 91.656 | 5.739 |
| 10.995 | 6.699 | 0.900 | 75.027 | 91.702 | 6.112 |
| 10.995 | 7.145 | 0.900 | 80.031 | 91.710 | 6.513 |
| 10.995 | 7.594 | 0.900 | 85.041 | 91.691 | 6.938 |
| 10.995 | 8.045 | 0.900 | 90.052 | 91.652 | 7.383 |
| 10.995 | 8.498 | 0.900 | 95.061 | 91.593 | 7.855 |
| 10.995 | 8.953 | 0.900 | 100.073 | 91.519 | 8.348 |
| 10.995 | 9.410 | 0.900 | 105.085 | 91.429 | 8.867 |
| 10.995 | 9.871 | 0.900 | 110.100 | 91.322 | 9.418 |
| 10.995 | 10.333 | 0.900 | 115.116 | 91.212 | 9.983 |
| 10.995 | 10.797 | 0.900 | 120.131 | 91.087 | 10.581 |
| 10.995 | 10.785 | 0.900 | 120.000 | 91.085 | 10.571 |
| 10.995 | 11.250 | 0.900 | 124.985 | 90.947 | 11.198 |
| 10.995 | 11.719 | 0.900 | 129.984 | 90.799 | 11.855 |
| 10.995 | 12.190 | 0.900 | 134.986 | 90.644 | 12.540 |
| 10.995 | 12.665 | 0.900 | 139.988 | 90.479 | 13.257 |
| 10.995 | 13.142 | 0.900 | 144.987 | 90.307 | 14.006 |
| 10.995 | 13.621 | 0.900 | 149.988 | 90.135 | 14.773 |
| 10.995 | 14.104 | 0.900 | 154.991 | 89.949 | 15.585 |
| 10.995 | 14.589 | 0.900 | 159.993 | 89.761 | 16.423 |
| 10.995 | 15.077 | 0.900 | 164.994 | 89.566 | 17.296 |
| 10.995 | 15.568 | 0.900 | 169.999 | 89.371 | 18.193 |
| 10.995 | 16.062 | 0.900 | 175.002 | 89.168 | 19.128 |
| 10.995 | 16.558 | 0.900 | 180.008 | 88.968 | 20.084 |
| 10.995 | 17.058 | 0.900 | 185.014 | 88.757 | 21.086 |
| 10.995 | 17.561 | 0.900 | 190.020 | 88.547 | 22.114 |
| 10.995 | 18.067 | 0.900 | 195.029 | 88.330 | 23.180 |
| 10.995 | 18.576 | 0.900 | 200.034 | 88.114 | 24.275 |
| 10.995 | 19.088 | 0.900 | 205.044 | 87.894 | 25.405 |
| 10.994 | 19.605 | 0.900 | 210.055 | 87.669 | 26.579 |
| 10.994 | 20.123 | 0.900 | 215.065 | 87.443 | 27.782 |
| 10.994 | 20.646 | 0.899 | 220.076 | 87.210 | 29.033 |
| 10.994 | 21.172 | 0.899 | 225.089 | 86.975 | 30.319 |
| 10.994 | 21.702 | 0.899 | 230.103 | 86.738 | 31.644 |
| 10.994 | 22.236 | 0.899 | 235.119 | 86.500 | 33.003 |
| 10.994 | 22.774 | 0.899 | 240.135 | 86.254 | 34.417 |

PMP-11208 900 mV 220A 6 phases off 12Vin Test Report (TPS53661 / CSD95372B) Texas Instruments

Efficiency graph: All 3 Vin's and current range 20 to 240 A: on Model t13 at $900 \mathrm{mV} / 300 \mathrm{kHz} / 6$ phases:
1-2 Meters per second airflow 21 degrees Celsius ambient:
X axis is load current in A off 900 mV output and Y axis is efficiency in percent


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Thermal images: Ambient is 21 degrees Celsius with 1-2 Meters per second airflow: 12 Vin 900 mV out 160 A


Q
12Vin 900mV 200A

$$
\text { FFLIR Max } 56.1^{\circ} \mathrm{C}
$$


(6) $501512.14: 139 \rho 9=0.94$

Q

Thermal images: Ambient is 21 degrees Celsius with 1-2 Meters per second airflow: 12 Vin 900 mV out 220A
©FLIR Max $63.4^{\circ} \mathrm{C}$


65 5/15 $12223 \% 00$ pe=0.94
Q
13 Vin 900 mV out 220A


Q
11 Vin 900 mV out 220A


Thermal images: Ambient is 21 degrees Celsius with 1-2 Meters per second airflow: 12 Vin 900 mV out 240 A
©FLIR Max $72.1^{\circ} \mathrm{C}$


Q
13 Vin 900 mV out 240 A


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