

# TLV183x-Q1 and TLV184x-Q1 Family of 40V, High-Speed Comparators

## 1 Features

- Qualified for automotive applications
- AEC-Q100 qualified with the following results:
  - Device temperature grade 1: -40°C to 125°C ambient operating temperature range
  - Device HBM ESD classification level 2
  - Device CDM ESD classification level C2B
- Wide supply range: 2.7V to 40V
- 65ns propagation delay
- Low supply current: 75µA per channel
- Rail-to-rail inputs
- Low input offset voltage: 500µV
- Power-on-reset (POR) provides a known startup condition
- Push-pull output option (TLV183x-Q1)
- Open-drain output option (TLV184x-Q1)
- Temperature range: -40°C to +125°C
- [Functional Safety Capable](#)
  - [Documentation available to aid functional safety system design](#)

comparators offer rail-to-rail inputs with push-pull and open-drain output options. These features coupled with 65ns propagation delay make this family well-suited for high speed current sensing and voltage protection applications.

All devices include a Power-On Reset (POR) feature that makes sure the output is in a known state until the minimum supply voltage has been reached. Once this voltage has been reached, the output responds to the inputs, thus preventing false outputs during system power-up and power-down.

The TLV183x-Q1 comparators have a push-pull output stage, which are designed for applications where symmetry between rising and falling output responses is desired. The TLV184x-Q1 comparators have an open-drain output stage, making them appropriate for level transition.

## 2 Applications

- [Telematics eCall](#)
- [Automotive head unit](#)
- [Instrument Cluster](#)
- [On-board \(OBC\) & wireless chargers](#)

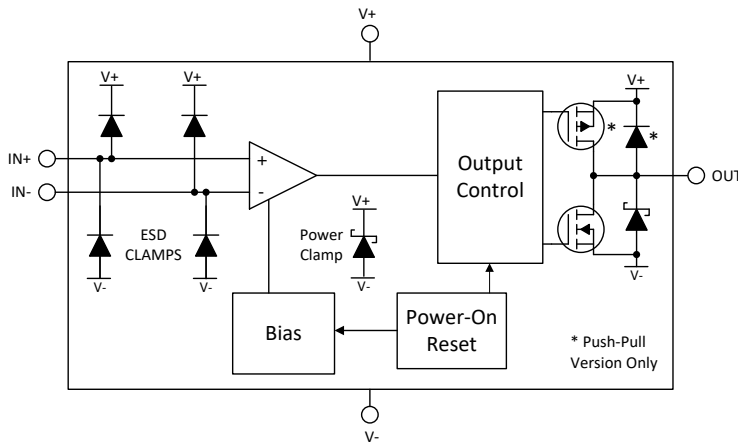
## 3 Description

The TLV183x-Q1 and TLV184x-Q1 are high-speed comparators with operating voltages up to 40V. The

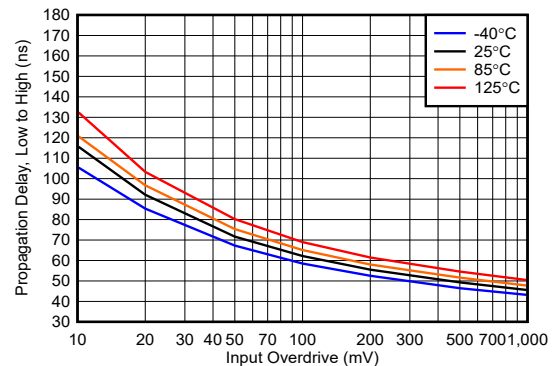
### Device Information

PART NUMBER	PACKAGE (1)	BODY SIZE (NOM) (2)
TLV1831-Q1, TLV1841-Q1	SC-70 (5)	2.00mm × 2.00mm
TLV1832-Q1, TLV1842-Q1	VSSOP (8)	3.00mm × 3.00mm
	TSSOP (8)	3.00mm × 4.40mm
	WSON (8) (Preview)	2.00mm × 2.00mm
TLV1834-Q1, TLV1844-Q1	SOT-23 (14) (Preview)	4.20mm × 2.00mm
	WQFN (16) (Preview)	3.00mm × 3.00mm

- (1) For all available packages, see the orderable addendum at the end of the data sheet.
- (2) The package size (length × width) is a nominal value and includes pins, where applicable.



**Functional Block Diagram**



**Propagation Delay, (Low to High) vs. Input Overdrive, 12V**

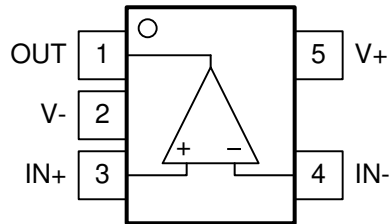


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## 4 Pin Configuration and Functions

### Pin Configuration: TLV1831-Q1 and TLV1841-Q1



**DBV, DCK Packages**  
**SOT-23-5, SC-70-5**  
**Top View**  
**(Standard "north west" pinout)**

**Table 4-1. Pin Functions: TLV1831-Q1 and TLV1841-Q1**

PIN		I/O	DESCRIPTION
NAME	NO.		
OUT	1	O	Output
V-	2	-	Negative supply voltage
IN+	3	I	Non-inverting (+) input
IN-	4	I	Inverting (-) input
V+	5	-	Positive supply voltage

### Pin Configurations: TLV1832-Q1 and TLV1842-Q1



**DKG, PW Packages**  
**8-Pin VSSOP, TSSOP**  
**Top View**



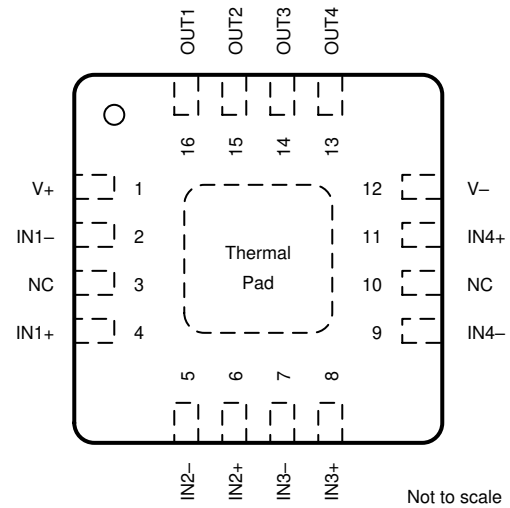
NOTE: Connect exposed thermal pad directly to V- pin.

**DSG Package**  
**8-Pad WSON With Exposed Thermal Pad,**  
**Top View**

**Table 4-2. Pin Functions: TLV1832-Q1 and TLV1842-Q1**

PIN		I/O	DESCRIPTION
NAME	NO.		
OUT1	1	O	Output pin of the comparator 1
IN1-	2	I	Inverting input pin of comparator 1
IN1+	3	I	Noninverting input pin of comparator 1
V-	4	—	Negative supply voltage
IN2+	5	I	Noninverting input pin of comparator 2
IN2-	6	I	Inverting input pin of comparator 2
OUT2	7	O	Output pin of the comparator 2
V+	8	—	Positive supply voltage

## Pin Configuration and Functions: TLV1834-Q1 and TLV1844-Q1



NOTE: Connect exposed thermal pad directly to V- pin.

### RTE Package, 16-Pad WQFN With Exposed Thermal Pad Top View

**Table 4-3. Pin Functions: TLV1834-Q1 and TLV1844-Q1**

PIN			I/O	DESCRIPTION
NAME	SOT-23	WQFN		
OUT2	1	15	O	Output pin of the comparator 2
OUT1	2	16	O	Output pin of the comparator 1
V+	3	1	-	Positive supply voltage
IN1-	4	2	I	Inverting input pin of the comparator 1
IN1+	5	4	I	Noninverting input pin of the comparator 1
IN2-	6	5	I	Inverting input pin of the comparator 2
IN2+	7	6	I	Noninverting input pin of the comparator 2
IN3-	8	7	I	Inverting input pin of the comparator 3
IN3+	9	8	I	Noninverting input pin of the comparator 3
IN4-	10	9	I	Inverting input pin of the comparator 4
IN4+	11	11	I	Noninverting input pin of the comparator 4
V-	12	12	-	Negative supply voltage
OUT4	13	13	O	Output pin of the comparator 4
OUT3	14	14	O	Output pin of the comparator 3
NC	-	3	-	No internal connection - leave floating or GND
NC	-	10	-	No internal connection - leave floating or GND
Thermal Pad	-	PAD	-	Connect directly to V- pin

## 5 Specifications

### 5.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

	MIN	MAX	UNIT
Supply voltage: $V_S = (V+) - (V-)$	-0.3	42	V
Input pins (IN+, IN-) from (V-) <sup>(2)</sup>	-0.3	(V+) + 0.3	V
Current into input pins (IN+, IN-)	-10	10	mA
Output (OUT) (Open-Drain) from (V-) <sup>(3)</sup>	-0.3	42	V
Output (OUT) (Push-Pull) from (V-)	-0.3	(V+) + 0.3	V
Output short circuit current <sup>(4)</sup>	-10	10	mA
Junction temperature, $T_J$		150	°C
Storage temperature, $T_{stg}$	-65	150	°C

- Operation outside the Absolute Maximum Ratings can cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- Input terminals are diode-clamped to (V-) and (V+). Input signals that can swing more than 0.3V beyond the supply rails must be current-limited to 10mA or less.
- Output (OUT) for open drain can be greater than (V+) and inputs (IN+, IN-) as long as the voltage is within the -0.3V to 42V range
- Continuous output short circuits at elevated supply voltages can result in excessive heating and exceeding the maximum allowed junction temperature, leading to eventual device destruction.

### 5.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM) per AEC Q100-002 <sup>(1)</sup>	±2000	V
		Charged-device model (CDM), per AEC Q100-0111	±1000	

- AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

### 5.3 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TLV183x/4x					UNIT
		DCK (SC-70)	DBV (SOT-23)	PW (TSSOP)	DSG (WSON)	DGK (VSSOP)	
		5 PINS	5 PINS	8 PINS	8 PINS	8 PINS	
$R_{qJA}$	Junction-to-ambient thermal resistance	216.4	183.6	157.6	110.3	151.5	°C/W
$R_{qJC(top)}$	Junction-to-case (top) thermal resistance	167.9	81.1	65.7	92.8	61.1	°C/W
$R_{qJB}$	Junction-to-board thermal resistance	98.1	50.4	96.5	71.0	86.1	°C/W
$\gamma_{JT}$	Junction-to-top characterization parameter	75.7	18.4	8.1	5.7	5.0	°C/W
$\gamma_{JB}$	Junction-to-board characterization parameter	97.1	50.0	95.2	70.8	84.8	°C/W
$R_{qJC(bot)}$	Junction-to-case (bottom) thermal resistance	-	-	-	62.0	-	°C/W

- For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) report.

### 5.4 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	MAX	UNIT
Supply voltage: $V_S = (V+) - (V-)$	2.7	40	V
Input voltage range from (V-)	-0.2	(V+) + 0.2	V
Output voltage for open drain	-0.2	40	V
Ambient temperature, $T_A$	-40	125	°C

## 5.5 Electrical Characteristics

For  $V_S$  (TOTAL SUPPLY VOLTAGE) =  $(V+) - (V-) = 12V$ ,  $V_{CM} = V_S/2$  at  $T_A = 25^\circ C$  (Unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>						
$V_{OS}$	Input offset voltage	$T_A = 25^\circ C$	-2.5	$\pm 0.3$	2.5	mV
		$T_A = -40^\circ C$ to $+125^\circ C$	-3.0		3.0	mV
$dV_{IO}/dT$	Input offset voltage drift	$T_A = -40^\circ C$ to $+125^\circ C$		$\pm 1.2$		$\mu V/^\circ C$
<b>POWER SUPPLY</b>						
$I_Q$	Quiescent current per comparator, TLV18x1 Only	No Load, Output High $T_A = 25^\circ C$ TLV1831, TLV1841		75	100	$\mu A$
		No Load, Output High $T_A = -40^\circ C$ to $+125^\circ C$ TLV1831, TLV1841			105	$\mu A$
		No Load, Output Low $T_A = 25^\circ C$ TLV1831, TLV1841		100	135	$\mu A$
		No Load, Output Low $T_A = -40^\circ C$ to $+125^\circ C$ TLV1831, TLV1841			140	$\mu A$
$I_Q$	Quiescent current per comparator	No Load, Output High $T_A = 25^\circ C$		75	95	$\mu A$
		No Load, Output High $T_A = -40^\circ C$ to $+125^\circ C$			100	$\mu A$
		No Load, Output Low $T_A = 25^\circ C$		95	130	$\mu A$
		No Load, Output Low $T_A = -40^\circ C$ to $+125^\circ C$			135	$\mu A$
$V_{POR}$			1.9			V
<b>INPUT BIAS CURRENT</b>						
$I_B$	Input bias current (1)			500		pA
$I_B$	Input bias current (1) (2)	$T_A = -40^\circ C$ to $+125^\circ C$	-5		5	nA
$I_{OS}$	Input offset current			10		pA
<b>INPUT CAPACITANCE</b>						
$C_{ID}$	Input Capacitance, Differential			5		pF
$C_{IC}$	Input Capacitance, Common Mode			5		pF
<b>INPUT COMMON MODE RANGE</b>						
$V_{CM-Range}$	Common-mode voltage range	$V_S = 2.7V$ to $40V$ $T_A = -40^\circ C$ to $+125^\circ C$	$(V-) - 0.2$		$(V+) + 0.2$	V
<b>OUTPUT</b>						
$V_{OL}$	Voltage swing from $(V-)$	$I_{SINK} = 4mA$ $T_A = -40^\circ C$ to $+125^\circ C$			400	mV
$V_{OH}$	Voltage swing from $(V+)$ (for Push-Pull only)	$I_{SOURCE} = 4mA$ $T_A = -40^\circ C$ to $+125^\circ C$			400	mV
$I_{LKG}$	Open-drain output leakage current	$V_{ID} = +0.1V$ , $V_{PULLUP} = (V+)$ $T_A = -40^\circ C$ to $+125^\circ C$		3	70	nA
$I_{OL}$	Short-circuit current	Sinking $T_A = -40^\circ C$ to $+125^\circ C$		30		mA
$I_{OH}$	Short-circuit current	Sourcing $T_A = -40^\circ C$ to $+125^\circ C$		30		mA

(1) Please see figure for  $I_{BIAS}$  vs  $V_{ID}$  performance curve

(2) This parameter is assured by design and/or characterization and is not tested in production.

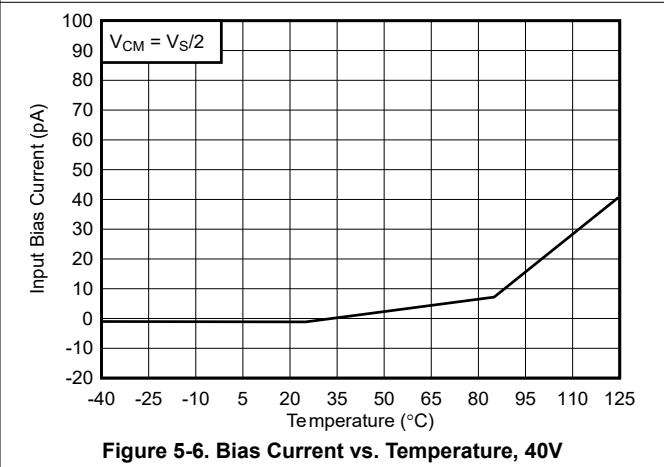
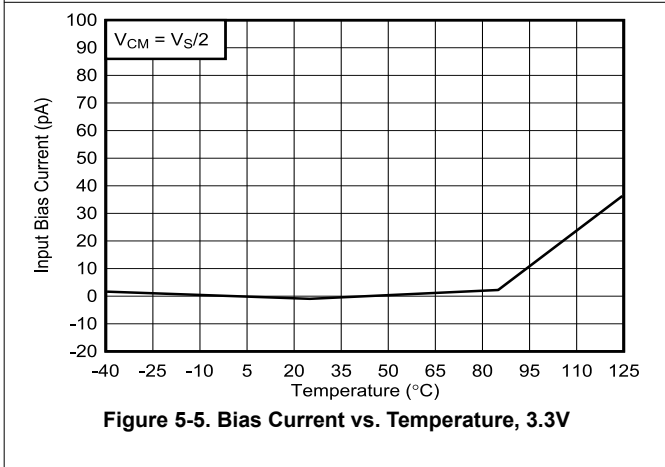
## 5.6 Switching Characteristics

For  $V_S$  (TOTAL SUPPLY VOLTAGE) =  $(V+) - (V-) = 12V$ ,  $V_{CM} = V_S/2$ ,  $C_L = 15pF$  at  $T_A = 25^\circ C$  (Unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>Output</b>						
$T_{PD-HL}$	Propagation delay time, high-to-low	$V_{OD} = 10mV$ , $V_{UD} = 100mV$ $V_{PU} = 5V$ and $R_{PU} = 10k$ (open-drain output only)		110		ns
$T_{PD-HL}$	Propagation delay time, high-to-low	$V_{OD} = 100mV$ , $V_{UD} = 100mV$ $V_{PU} = 5V$ and $R_{PU} = 10k$ (open-drain output only)		65		ns
$T_{PD-LH}$	Propagation delay time, low-to-high, push-pull output	$V_{OD} = 10mV$ , $V_{UD} = 100mV$		110		ns
$T_{PD-LH}$	Propagation delay time, low-to-high, push-pull output	$V_{OD} = 100mV$ , $V_{UD} = 100mV$		65		ns
$T_{RISE}$	Output Rise Time, 20% to 80%, push-pull output	$V_{OD} = 100mV$ , $V_{UD} = 100mV$		5		ns
$T_{FALL}$	Output Fall Time, 80% to 20%	$V_{OD} = 100mV$ , $V_{UD} = 100mV$		5		ns
$F_{TOGGLE}$	Toggle Frequency	$V_{ID} = 200mV$		7.5		MHz
<b>POWER ON TIME</b>						
$P_{ON}$	Power on-time			80		$\mu s$

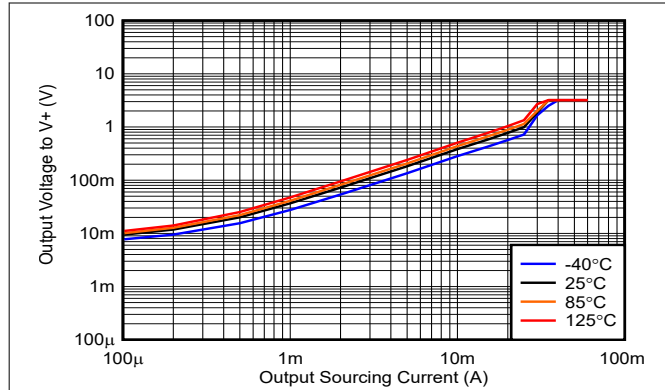
### 5.7 Typical Characteristics

At  $T_A = 25^\circ\text{C}$ ,  $V_S = 12\text{V}$ ,  $V_{CM} = V_S/2\text{V}$ ,  $C_L = 15\text{pF}$ , Input Overdrive = Input Underdrive =  $100\text{mV}$ ,  $R_{PU} = 10\text{k}\Omega$ , unless otherwise noted.

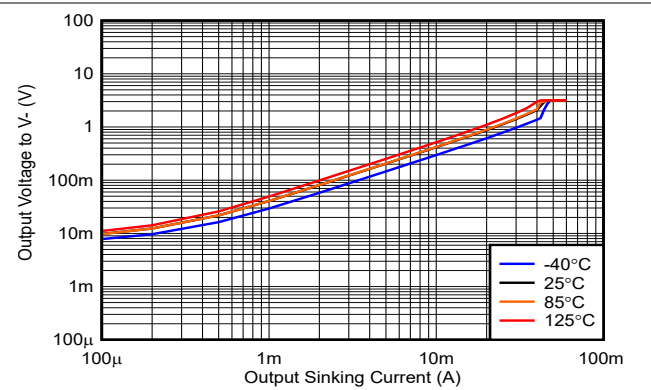


## 5.7 Typical Characteristics (continued)

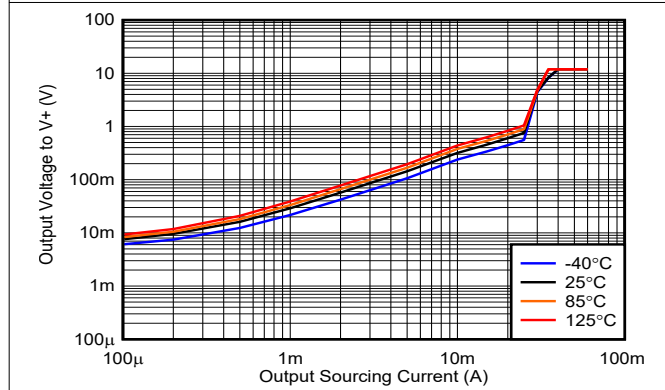
At  $T_A = 25^\circ\text{C}$ ,  $V_S = 12\text{V}$ ,  $V_{CM} = V_S/2\text{V}$ ,  $C_L = 15\text{pF}$ , Input Overdrive = Input Underdrive =  $100\text{mV}$ ,  $R_{PU} = 10\text{k}\Omega$ , unless otherwise noted.



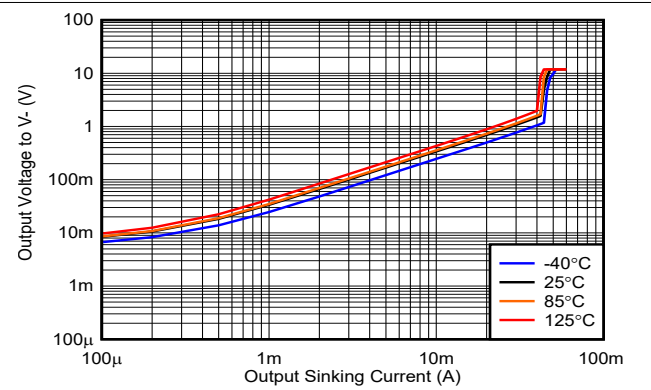
**Figure 5-7. Output Voltage vs. Sourcing Current, 3.3V, Push-Pull only**



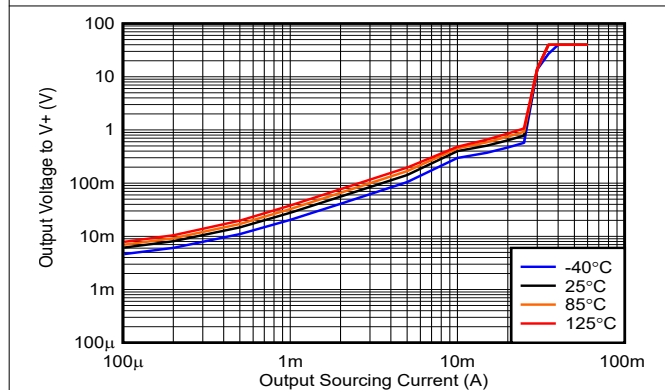
**Figure 5-8. Output Voltage vs. Sinking Current, 3.3V**



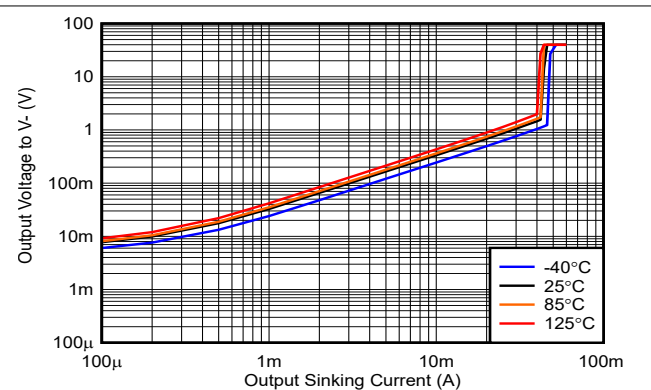
**Figure 5-9. Output Voltage vs. Sourcing Current, 12V, Push-Pull only**



**Figure 5-10. Output Voltage vs. Sinking Current, 12V**



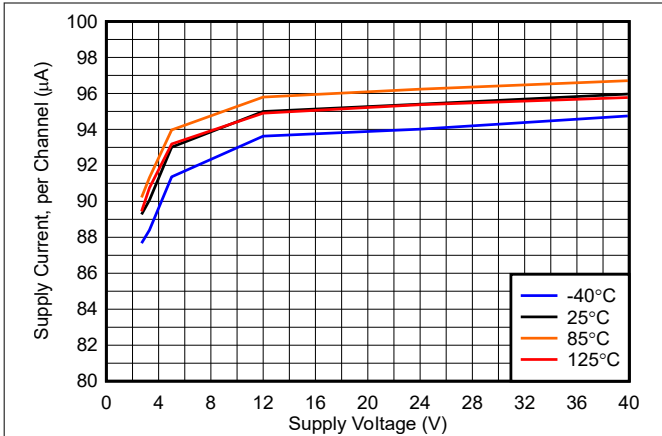
**Figure 5-11. Output Voltage vs. Sourcing Current, 40V, Push-Pull only**



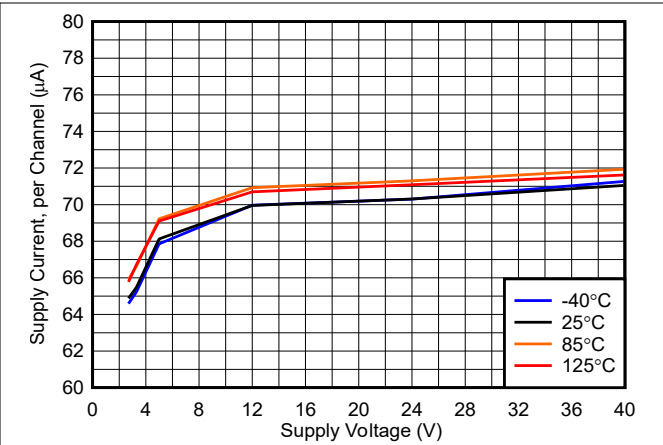
**Figure 5-12. Output Voltage vs. Sinking Current, 40V**

### 5.7 Typical Characteristics (continued)

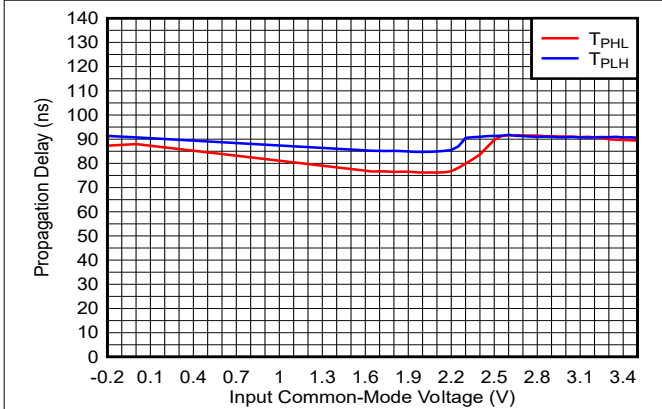
At  $T_A = 25^\circ\text{C}$ ,  $V_S = 12\text{V}$ ,  $V_{CM} = V_S/2\text{V}$ ,  $C_L = 15\text{pF}$ , Input Overdrive = Input Underdrive =  $100\text{mV}$ ,  $R_{PU} = 10\text{k}\Omega$ , unless otherwise noted.



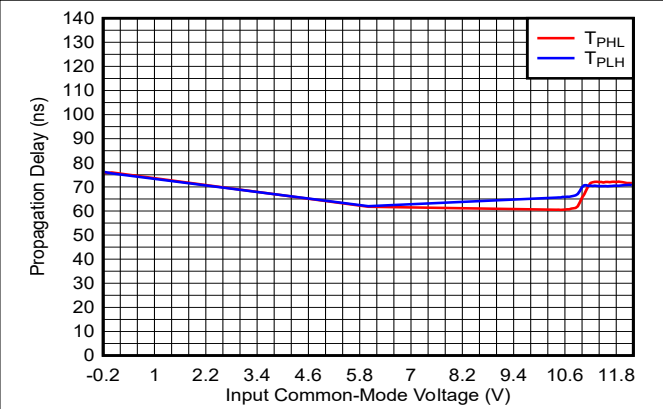
**Figure 5-13. Supply Current vs. Supply Voltage, Output Low, No Load**



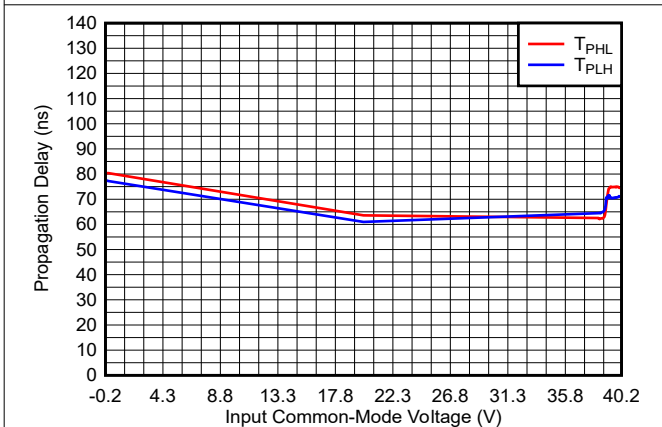
**Figure 5-14. Supply Current vs. Supply Voltage, Output High, No Load**



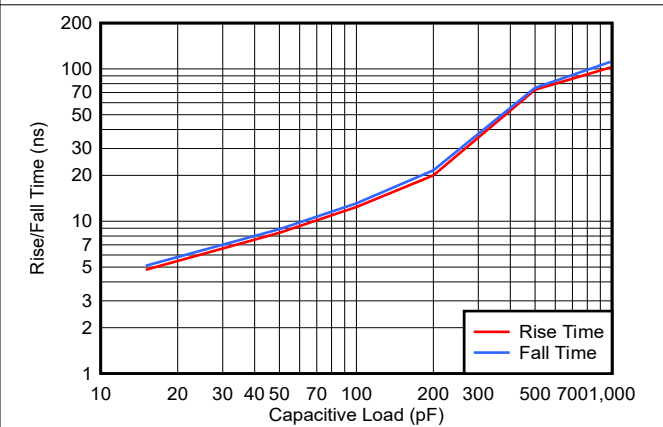
**Figure 5-15. Propagation Delay vs. Common-Mode, 3.3V**



**Figure 5-16. Propagation Delay vs. Common-Mode, 12V**



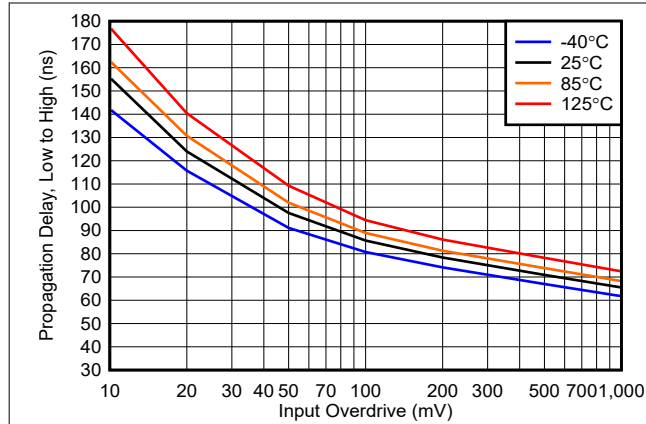
**Figure 5-17. Propagation Delay vs. Common-Mode, 40V**



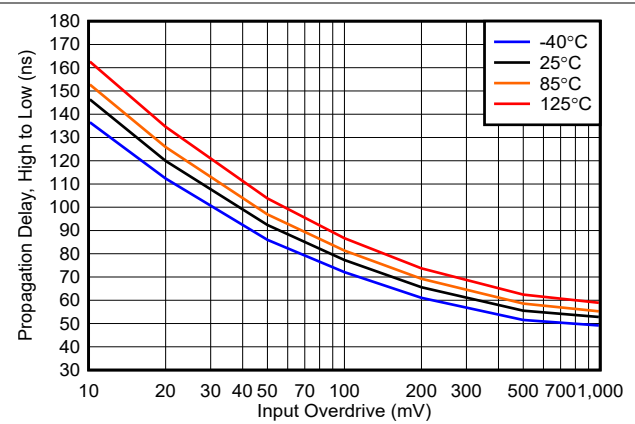
**Figure 5-18. Rise/Fall Time vs. Capacitive Load, 12V**

## 5.7 Typical Characteristics (continued)

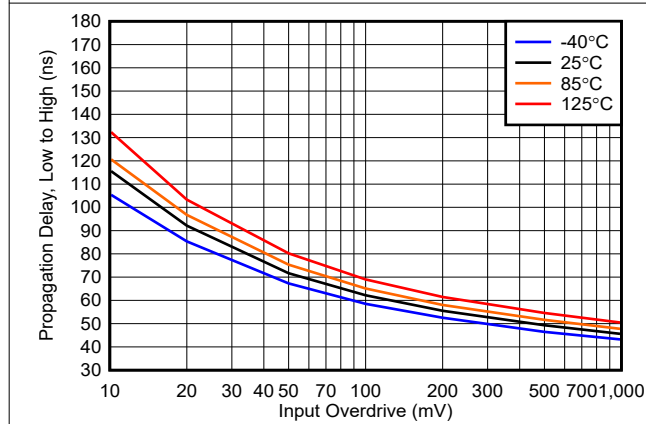
At  $T_A = 25^\circ\text{C}$ ,  $V_S = 12\text{V}$ ,  $V_{CM} = V_S/2\text{V}$ ,  $C_L = 15\text{pF}$ , Input Overdrive = Input Underdrive =  $100\text{mV}$ ,  $R_{PU} = 10\text{k}\Omega$ , unless otherwise noted.



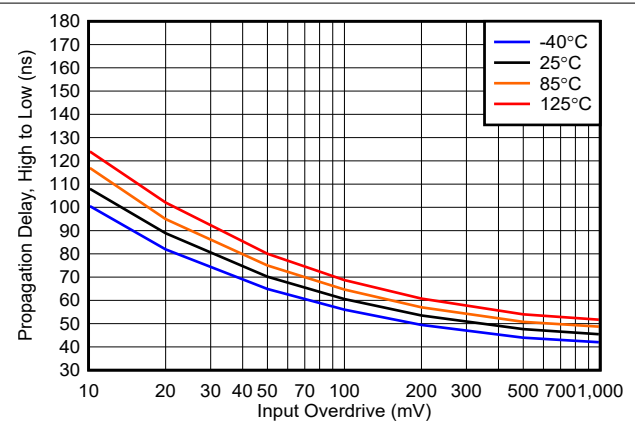
**Figure 5-19. Propagation Delay, (Low to High) vs. Input Overdrive, 3.3V**



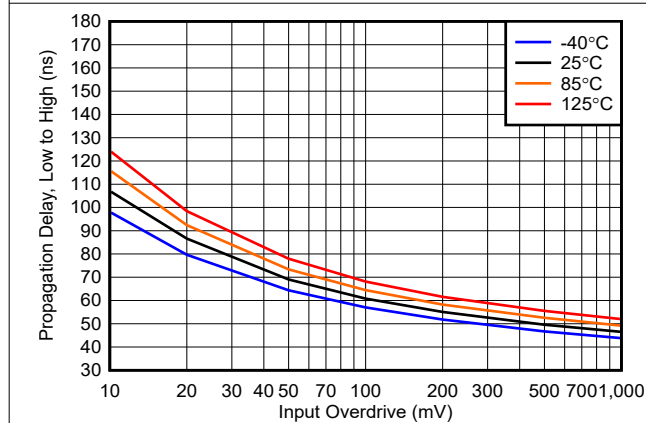
**Figure 5-20. Propagation Delay, (High to Low) vs. Input Overdrive, 3.3V**



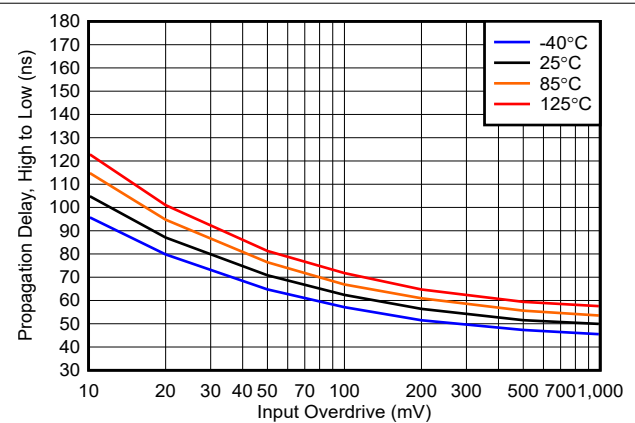
**Figure 5-21. Propagation Delay, (Low to High) vs. Input Overdrive, 12V**



**Figure 5-22. Propagation Delay, (High to Low) vs. Input Overdrive, 12V**



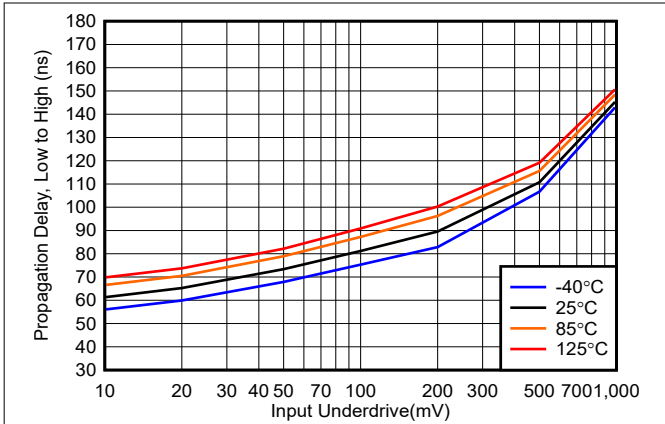
**Figure 5-23. Propagation Delay, (Low to High) vs. Input Overdrive, 40V**



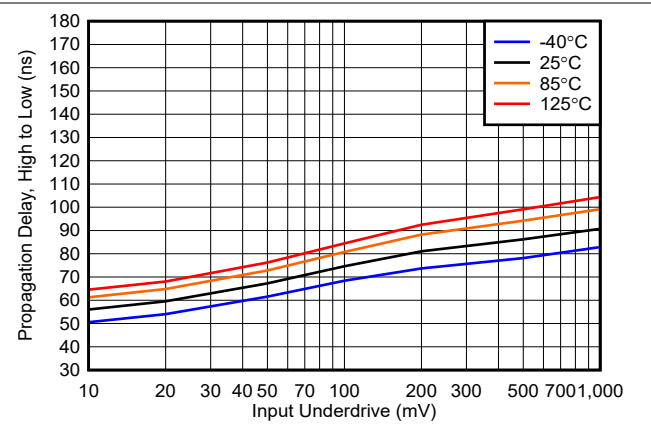
**Figure 5-24. Propagation Delay, (High to Low) vs. Input Overdrive, 40V**

### 5.7 Typical Characteristics (continued)

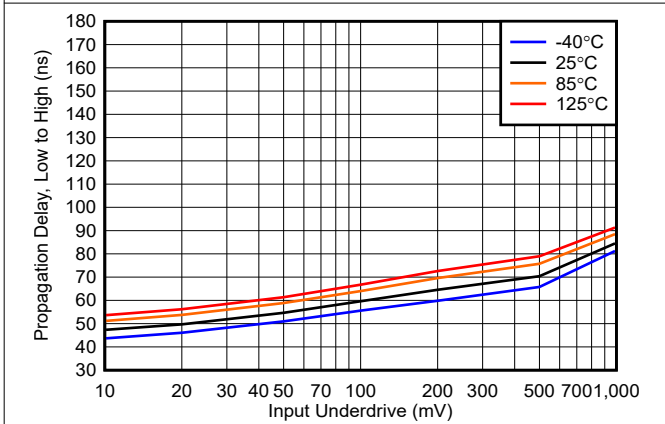
At  $T_A = 25^\circ\text{C}$ ,  $V_S = 12\text{V}$ ,  $V_{CM} = V_S/2\text{V}$ ,  $C_L = 15\text{pF}$ , Input Overdrive = Input Underdrive = 100mV,  $R_{PU} = 10\text{k}\Omega$ , unless otherwise noted.



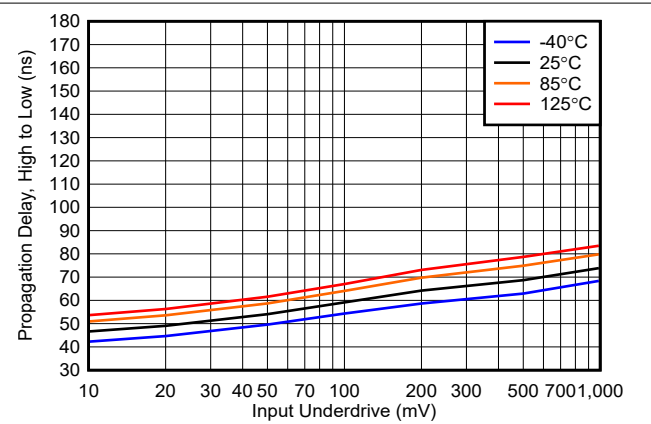
**Figure 5-25. Propagation Delay, (Low to High) vs. Input Underdrive, 3.3V**



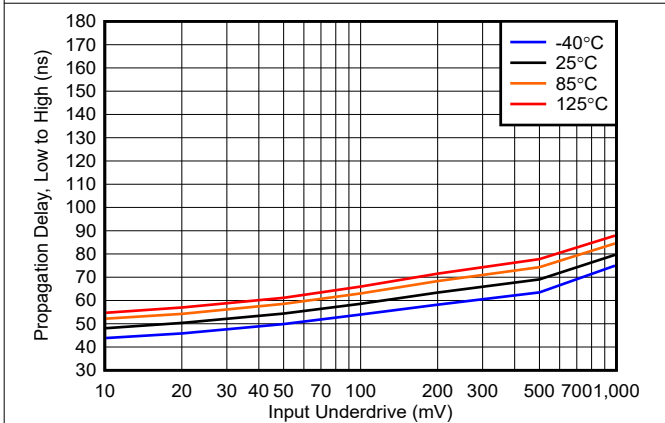
**Figure 5-26. Propagation Delay, (High to Low) vs. Input Underdrive, 3.3V**



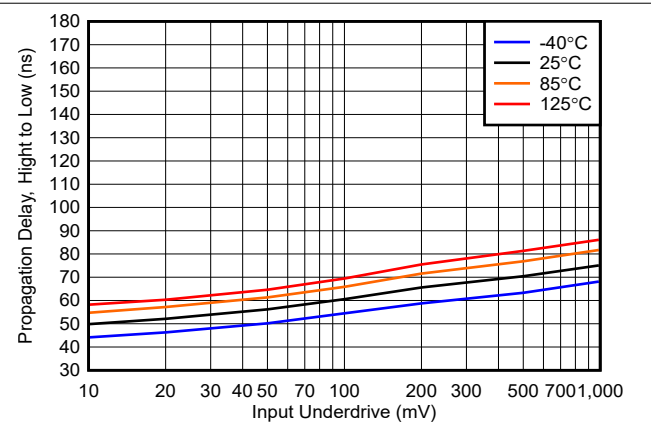
**Figure 5-27. Propagation Delay, (Low to High) vs. Input Underdrive, 12V**



**Figure 5-28. Propagation Delay, (High to Low) vs. Input Underdrive, 12V**



**Figure 5-29. Propagation Delay, (Low to High) vs. Input Underdrive, 40V**



**Figure 5-30. Propagation Delay, (High to Low) vs. Input Underdrive, 40V**

## 6 Detailed Description

### 6.1 Overview

The TLV183x-Q1 and TLV184x-Q1 devices are 40V high-speed comparators with push-pull and open-drain output options. Operating down to 2.7V while only consuming only 75µA per channel, the TLV183x-Q1 and TLV184x-Q1 are designed for voltage and current sensing applications in high voltage industrial and automotive systems. An internal power-on reset circuit makes sure that the output remains in a known state during power-up and power-down.

### 6.2 Functional Block Diagrams



Figure 6-1. Block Diagram

### 6.3 Feature Description

The TLV183x-Q1 (push-pull output) and TLV184x-Q1 (open-drain output) devices are high speed comparators with a typical propagation delay of 65ns and are capable of operating at voltages up to 40V. These comparators are well-suited for high-voltage systems where it is essential to have short-circuit current and over voltage protection for its internal components. These comparators also feature a rail-to-rail input stage capable of operating up to 200mV beyond the power supply rails combined with a maximum 2.5mV input offset and Power-on Reset (POR) for known start-up conditions.

### 6.4 Device Functional Modes

#### 6.4.1 Inputs

##### 6.4.1.1 Rail-to-Rail Input

The input voltage range extends from 200mV below ( $V^-$ ) to 200mV above ( $V^+$ ), maximizing input dynamic range. The input stage has ESD clamps to the ( $V^+$ ) supply line and therefore the input voltages must not exceed the supply voltages by more than 200mV. Do not apply signals to the rail to rail inputs with no supply voltage. To avoid damaging the inputs when exceeding the recommended input voltage range, an external resistor must be used to limit the current to less than 1mA.

Likewise, unlike high-speed amplifiers, the comparator inputs do not have clamping diodes between them. This allows for applications where the input differential voltage can match the supply voltage ( $V^+$ ). However, when the input differential voltage increases to 2V, bias current increases to the nA range occur. This is a result of internal circuitry intended to minimize propagation delay increases due to large input underdrive amplitudes.

#### 6.4.1.2 Unused Inputs

If a channel is not to be used, DO NOT tie the inputs together. Due to the high equivalent bandwidth and low offset voltage, tying the inputs directly together can cause high frequency oscillations as the device triggers on its own internal wideband noise. Instead, the inputs must be tied to any available voltage that resides within the specified input voltage range and provides a minimum of 50mV differential voltage. For example, one input can be grounded and the other input connected to a reference voltage, or even (V+).

#### 6.4.2 Outputs

##### 6.4.2.1 TLV183x-Q1 Push-Pull Output

The TLV183x-Q1 features a push-pull output stage capable of both sinking and sourcing current. This allows driving loads such as LED's and MOSFET gates, as well as eliminating the need for an external pull-up resistor. The push-pull output must never be connected to another output.

Directly shorting the output to the supply rails ((V+) when output "low" or (V-) when output "High") can result in thermal runaway and eventual device destruction at high (>12V) supply voltages. If output shorts are possible, a series current limiting resistor is recommended to limit the power dissipation.

Unused push-pull outputs must be left floating, and never tied to a supply, ground, or another output.

##### 6.4.2.2 TLV184x-Q1 Open-Drain Output

The TLV184x-Q1 features an open-drain (also commonly called open collector) sinking-only output stage enabling the output logic levels to be pulled up to an external voltage up to 40V, independent of the comparator supply voltage (V+). The open-drain output also allows logical OR'ing of multiple open drain outputs and logic level translation. TI recommends setting the pull-up resistor current to between 100uA and 1mA to optimize  $V_{OL}$  logic levels. Lower pull-up resistor values help increase the rising edge risetime, but at the expense of increasing  $V_{OL}$  and higher power dissipation. The risetime is dependent on the time constant of the total pull-up resistance and total load capacitance. Large value pull-up resistors (>1M $\Omega$ ) create an exponential rising edge due to the output RC time constant and increase the risetime.

Directly shorting the output to (V+) can result in thermal runaway and eventual device destruction at high (>12V) pull-up voltages. If output shorts are possible, a series current limiting resistor is recommended to limit the power dissipation.

Unused open drain outputs must be left floating, or can be tied to the (V-) pin if floating pins are not desired.

#### 6.4.3 ESD Protection

##### 6.4.3.1 Inputs

The rail-to-rail input does have an ESD clamp to (V+) and (V-) and therefore the input voltage must not exceed the supply voltages by more than 200mV. Do not apply signals to the rail to rail inputs with no supply voltage. To avoid damaging the inputs when exceeding the recommended input voltage range, an external resistor must be used to limit the current to less than 1mA.

Similarly, if the inputs are to be connected to a low impedance source, such as a power supply or buffered reference line, add a current-limiting resistor in series with the input to limit any transient currents if the clamps conduct. Limit the current to 1mA or less. This series resistance can be part of any resistive input dividers or networks.

##### 6.4.3.2 Outputs

The TLV183x-Q1 push-pull output ESD protection contains a conventional ESD clamp between the output and (V+), and a ESD clamp between the output and (V-). The output must not exceed the supply rails by more than 200mV.

The TLV184x-Q1 open-drain output ESD protection consists of an ESD clamping circuit to (V-) only to allow the output to be pulled above (V+) to a maximum of 40V. There is no ESD clamp diode between the output and (V+) on the open-drain output.

#### 6.4.4 Power-On Reset (POR)

The TLV183x-Q1 and TLV184x-Q1 devices have an internal Power-on-Reset (POR) circuit for known start-up or power-down conditions. While the power supply ( $V+$ ) is ramping up or ramping down, the POR circuitry is activated for up to  $80\mu\text{s}$  after the  $V_{\text{POR}}$  of  $1.9\text{V}$  is crossed. When the supply voltage is equal to or greater than the minimum supply voltage, and after the delay period, the comparator output reflects the state of the differential input ( $V_{\text{ID}}$ ).

For both TLV183x-Q1 and TLV184x-Q1 devices, the POR circuit keeps the output high impedance (Hi-Z) during the POR period ( $P_{\text{on}}$ ).

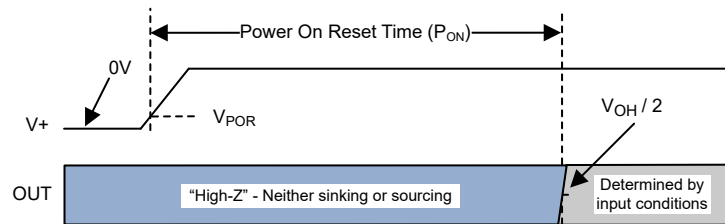


Figure 6-2. Power-On Reset Timing Diagram

## 7 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 7.1 Application Information

#### 7.1.1 Basic Comparator Definitions

##### 7.1.1.1 Operation

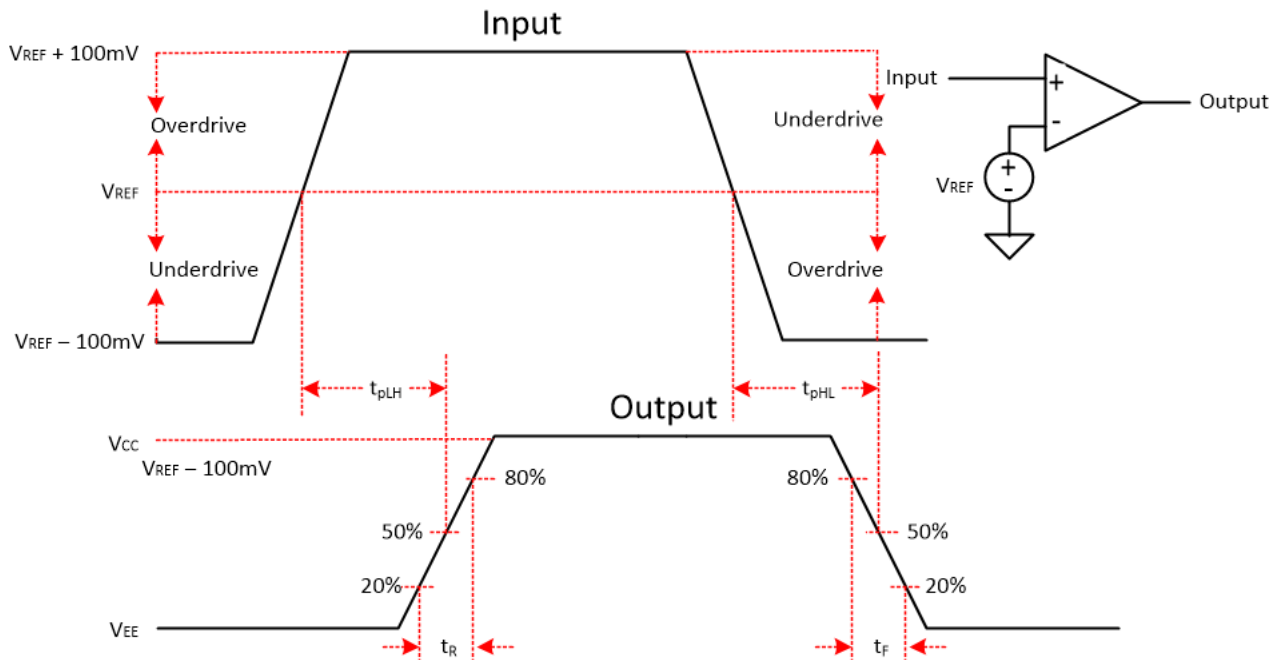
The basic comparator compares the input voltage ( $V_{IN}$ ) on one input to a reference voltage ( $V_{REF}$ ) on the other input. In the [Figure 7-1](#) example below, if  $V_{IN}$  is less than  $V_{REF}$ , the output voltage ( $V_O$ ) is logic low ( $V_{OL}$ ). If  $V_{IN}$  is greater than  $V_{REF}$ , the output voltage ( $V_O$ ) is at logic high ( $V_{OH}$ ). [Table 7-1](#) summarizes the output conditions. The output logic can be inverted by simply swapping the input pins.

**Table 7-1. Output Conditions**

Inputs Condition	Output
$IN+ > IN-$	HIGH ( $V_{OH}$ )
$IN+ = IN-$	Indeterminate (chatters - see <a href="#">Hysteresis</a> )
$IN+ < IN-$	LOW ( $V_{OL}$ )

##### 7.1.1.2 Propagation Delay

There is a delay between from when the input crosses the reference voltage and the output responds. This is called the Propagation Delay. Propagation delay can be different between high-to low and low-to-high input transitions. This is shown as  $t_{pLH}$  and  $t_{pHL}$  in [Figure 7-1](#) and is measured from the mid-point of the input to the midpoint of the output.



**Figure 7-1. Comparator Timing Diagram**

### 7.1.1.3 Overdrive Voltage

The overdrive voltage,  $V_{OD}$ , is the amount of input voltage beyond the reference voltage (and not the total input peak-to-peak voltage). The overdrive voltage is 100mV as shown in the [Figure 7-1](#) example. The overdrive voltage can influence the propagation delay ( $t_p$ ). The smaller the overdrive voltage, the longer the propagation delay, particularly when  $<100\text{mV}$ . If the fastest speeds are desired, TI recommends applying the highest amount of overdrive possible.

The risetime ( $t_r$ ) and falltime ( $t_f$ ) is the time from the 20% and 80% points of the output waveform.

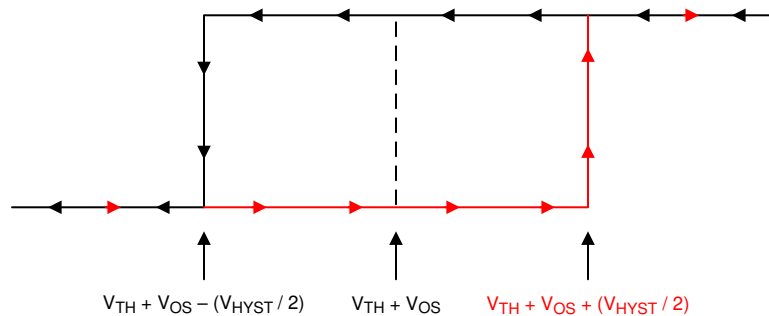
### 7.1.2 Hysteresis

The basic comparator configuration can produce a noisy "chatter" output if the applied differential input voltage is near the comparator's offset voltage. This usually occurs when the input signal is moving very slowly across the switching threshold of the comparator. This problem can be prevented by adding external hysteresis to the comparator.

External hysteresis can be applied in the form of a positive feedback loop that adjusts the trip point of the comparator depending on the current output state.

The hysteresis transfer curve is shown in [Figure 7-2](#). This curve is a function of three components:  $V_{TH}$ ,  $V_{OS}$ , and  $V_{HYST}$ :

- $V_{TH}$  is the actual set voltage or threshold trip voltage.
- $V_{OS}$  is the internal offset voltage between  $V_{IN+}$  and  $V_{IN-}$ . This voltage is added to  $V_{TH}$  to form the actual trip point at which the comparator must respond to change output states.
- $V_{HYST}$  is the hysteresis (or trip window) that is designed to reduce comparator sensitivity to noise.

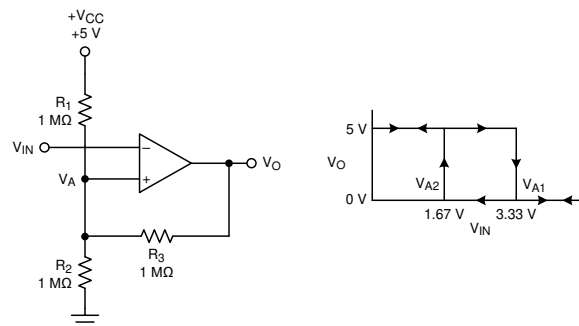


**Figure 7-2. Hysteresis Transfer Curve**

For more information, please see Application Note SBOA219 "[Comparator with and without hysteresis circuit](#)".

#### 7.1.2.1 Inverting Comparator With Hysteresis

The inverting comparator with hysteresis requires a three-resistor network that is referenced to the comparator supply voltage ( $V_{CC}$ ), as shown in [Figure 7-3](#).



**Figure 7-3. TLV183x-Q1 in an Inverting Configuration With Hysteresis**

The equivalent resistor networks when the output is high and low are shown in [Figure 7-3](#).



**Figure 7-4. Inverting Configuration Resistor Equivalent Networks**

When  $V_{IN}$  is less than  $V_A$ , the output voltage is high (for simplicity, assume  $V_O$  switches as high as  $V_{CC}$ ). The three network resistors can be represented as  $R1 \parallel R3$  in series with  $R2$ , as shown in [Figure 7-4](#).

[Equation 1](#) below defines the high-to-low trip voltage ( $V_{A1}$ ).

$$V_{A1} = V_{CC} \times \frac{R2}{(R1 \parallel R3) + R2} \quad (1)$$

When  $V_{IN}$  is greater than  $V_A$ , the output voltage is low. In this case, the three network resistors can be presented as  $R2 \parallel R3$  in series with  $R1$ , as shown in [Equation 2](#).

Use [Equation 2](#) to define the low to high trip voltage ( $V_{A2}$ ).

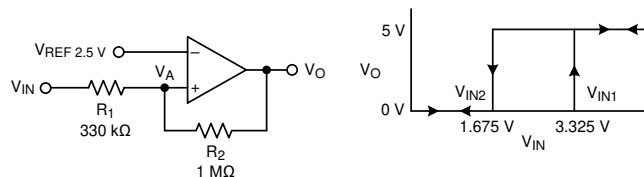
$$V_{A2} = V_{CC} \times \frac{R2 \parallel R3}{R1 + (R2 \parallel R3)} \quad (2)$$

[Equation 3](#) defines the total hysteresis provided by the network.

$$\Delta V_A = V_{A1} - V_{A2} \quad (3)$$

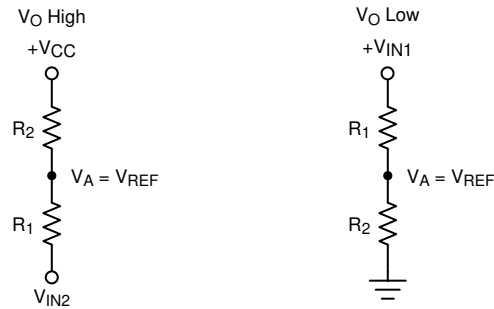
### 7.1.2.2 Non-Inverting Comparator With Hysteresis

A non-inverting comparator with hysteresis requires a two-resistor network and a voltage reference ( $V_{REF}$ ) at the inverting input, as shown in [Figure 7-5](#),



**Figure 7-5. TLV183x-Q1 in a Non-Inverting Configuration With Hysteresis**

The equivalent resistor networks when the output is high and low are shown in [Figure 7-6](#).



**Figure 7-6. Non-Inverting Configuration Resistor Networks**

When  $V_{IN}$  is less than  $V_{REF}$ , the output is low. For the output to switch from low to high,  $V_{IN}$  must rise above the  $V_{IN1}$  threshold. Use [Equation 4](#) to calculate  $V_{IN1}$ .

$$V_{IN1} = R1 \times \frac{V_{REF}}{R2} + V_{REF} \quad (4)$$

When  $V_{IN}$  is greater than  $V_{REF}$ , the output is high. For the comparator to switch back to a low state,  $V_{IN}$  must drop below  $V_{IN2}$ . Use [Equation 5](#) to calculate  $V_{IN2}$ .

$$V_{IN2} = \frac{V_{REF} (R1 + R2) - V_{CC} \times R1}{R2} \quad (5)$$

The hysteresis of this circuit is the difference between  $V_{IN1}$  and  $V_{IN2}$ , as shown in [Equation 6](#).

$$\Delta V_{IN} = V_{CC} \times \frac{R1}{R2} \quad (6)$$

For more information, please see Application Notes SNOA997 "[Inverting comparator with hysteresis circuit](#)" and SBOA313 "[Non-Inverting Comparator With Hysteresis Circuit](#)".

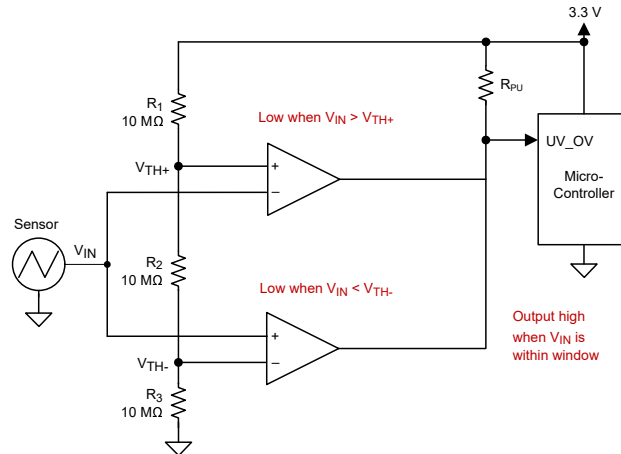
### 7.1.2.3 Inverting and Non-Inverting Hysteresis using Open-Drain Output

It is also possible to use an open drain output device, such as the TLV184x-Q1, but the output pull-up resistor must also be taken into account in the calculations. The pull-up resistor is seen in series with the feedback resistor when the output is high. Thus, the feedback resistor is actually seen as  $R2 + R_{PULLUP}$ . TI recommends that the pull-up resistor be at least 10 times less than the feedback resistor value.

## 7.2 Typical Applications

### 7.2.1 Window Comparator

Window comparators are commonly used to detect undervoltage and overvoltage conditions. [Figure 7-7](#) shows a simple window comparator circuit. Window comparators require open drain outputs (TLV184x-Q1 if the outputs are directly connected together).



**Figure 7-7. Window Comparator**

### 7.2.1.1 Design Requirements

For this design, follow these design requirements:

- Alert (logic low output) when an input signal is less than 1.1V
- Alert (logic low output) when an input signal is greater than 2.2V
- Alert signal is active low
- Operate from a 3.3V power supply

### 7.2.1.2 Detailed Design Procedure

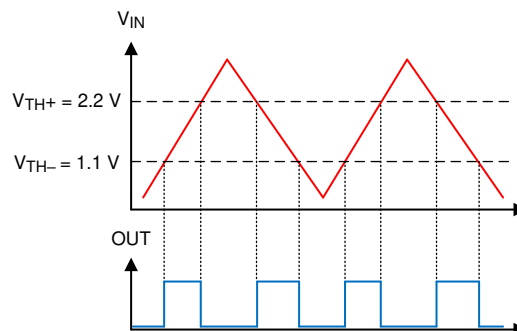
Configure the circuit as shown in [Figure 7-7](#). Connect  $V_+$  to a 3.3V power supply and  $V_{EE}$  to ground. Make  $R_1$ ,  $R_2$  and  $R_3$  each 10MΩ resistors. These three resistors are used to create the positive and negative thresholds for the window comparator ( $V_{TH+}$  and  $V_{TH-}$ ).

With each resistor being equal,  $V_{TH+}$  is 2.2V and  $V_{TH-}$  is 1.1V. Large resistor values such as 10MΩ are used to minimize power consumption. The resistor values can be recalculated to provide the desired trip point values.

The sensor output voltage is applied to the inverting and noninverting inputs of the two comparators. Using two open-drain output comparators allows the two comparator outputs to be Wire-OR'ed together.

The respective comparator outputs will be low when the sensor is less than 1.1V or greater than 2.2V. The respective comparator outputs will be high when the sensor is in the range of 1.1V to 2.2V (within the "window"), as shown in [Figure 7-8](#).

### 7.2.1.3 Application Curve

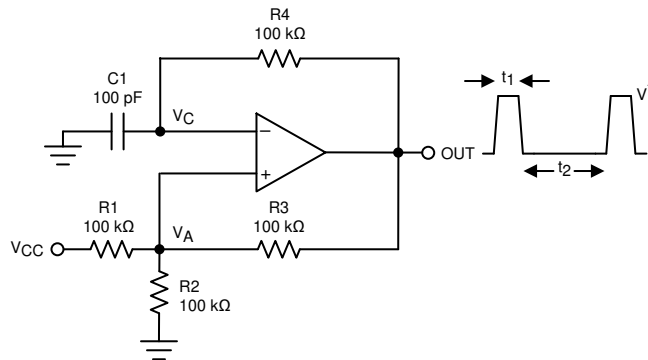


**Figure 7-8. Window Comparator Results**

For more information, please see Application note SBOA221 "[Window comparator circuit](#)".

## 7.2.2 Square Wave Oscillator

Square-wave oscillator can be used as low cost timing reference or system supervisory clock source. A push-pull output (TLV183x) is recommended for best symmetry.



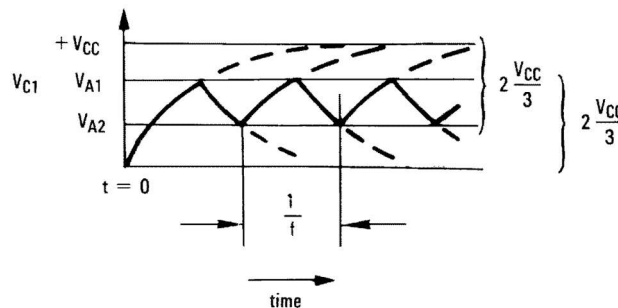
**Figure 7-9. Square-Wave Oscillator**

### 7.2.2.1 Design Requirements

The square-wave period is determined by the RC time constant of the capacitor C<sub>1</sub> and resistor R<sub>4</sub>. The maximum frequency is limited by propagation delay of the device and the capacitance load at the output. The low input bias current allows a lower capacitor value and larger resistor value combination for a given oscillator frequency, which can help to reduce BOM cost and board space. TI recommends that R<sub>4</sub> be over several kilo-ohms to minimize loading of the output.

### 7.2.2.2 Detailed Design Procedure

The oscillation frequency is determined by the resistor and capacitor values. The following calculation provides details of the steps.



**Figure 7-10. Square-Wave Oscillator Timing Thresholds**

First consider the output of Figure [Square-Wave Oscillator](#) as high, which indicates the inverted input V<sub>C</sub> is lower than the noninverting input (V<sub>A</sub>). This causes the C<sub>1</sub> to be charged through R<sub>4</sub>, and the voltage V<sub>C</sub> increases until it is equal to the noninverting input. The value of V<sub>A</sub> at the point is calculated below.

$$V_{A1} = \frac{V_{CC} \times R_2}{R_2 + R_1 + R_3} \quad (7)$$

if R<sub>1</sub> = R<sub>2</sub> = R<sub>3</sub>, then V<sub>A1</sub> = 2V<sub>CC</sub>/3

At this time the comparator output trips pulling down the output to the negative rail. The value of V<sub>A</sub> at this point is calculated below.

$$V_{A2} = \frac{V_{CC}(R_2 \parallel R_3)}{R_1 + R_2 \parallel R_3} \quad (8)$$

if  $R_1 = R_2 = R_3$ , then  $V_{A2} = V_{CC}/3$

The  $C_1$  now discharges through the  $R_4$ , and the voltage  $V_{CC}$  decreases until it reaches  $V_{A2}$ . At this point, the output switches back to the starting state. The oscillation period equals to the time duration for  $C_1$  from  $2V_{CC}/3$  to  $V_{CC}/3$  then back to  $2V_{CC}/3$ , which is given by  $R_4 C_1 \times \ln 2$  for each trip. Therefore, the total time duration is calculated as  $2 R_4 C_1 \times \ln 2$ .

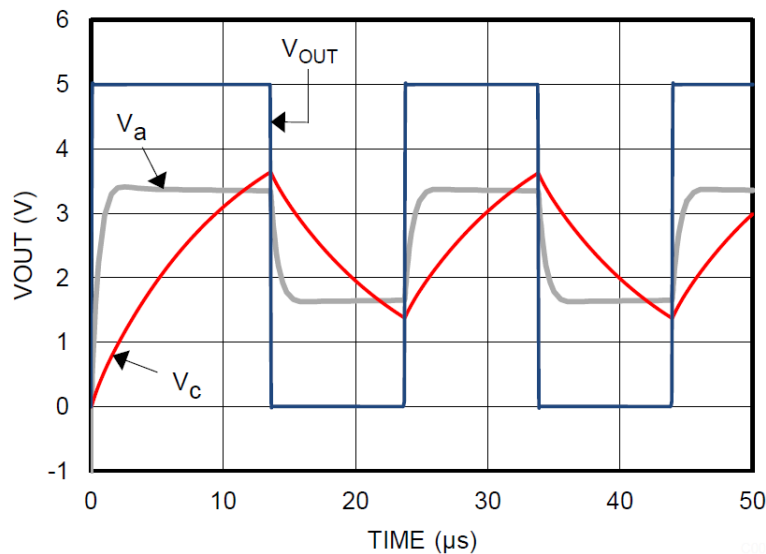
The oscillation frequency can be obtained below.

$$f = 1 / (2 R_4 \times C_1 \times \ln 2) \quad (9)$$

### 7.2.2.3 Application Performance Plots

The Square-Wave Oscillator Output Waveform shows the simulated results of an oscillator using the following component values:

- $R_1 = R_2 = R_3 = R_4 = 10k\Omega$
- $C_1 = 100pF, C_L = 20pF$
- $V+ = 5V, V- = GND$
- $C_{stray}$  (not shown) from  $V_A$  TO GND =  $10pF$



**Figure 7-11. Square-Wave Oscillator Output Waveform**

## 7.3 Power Supply Recommendations

Due to fast output edges, bypass capacitors are critical on the supply pin to prevent supply ringing and false triggers and oscillations. Bypass the supply directly at *each* device with a low ESR  $0.1\mu F$  ceramic bypass capacitor directly between the (V+) pin and ground pins. Narrow peak currents are drawn during the output transition time, particularly for the push-pull output device. These narrow pulses can cause un-bypassed supply lines and poor grounds to ring, possibly causing variation that can impact the input voltage range and create an inaccurate comparison or even oscillations.

The device can be powered from both "split" supplies ((V+) & (V-)), or "single" supplies ((V+) and GND), with GND applied to the (V-) pin. Input signals must stay within the recommended input range for either type. Note that with a "split" supply the output now swings "low" ( $V_{OL}$ ) to (V-) potential and not GND.

## 7.4 Layout

### 7.4.1 Layout Guidelines

For accurate comparator applications it is important to maintain a stable power supply with minimized noise and glitches. Output rise and fall times are in the tens of nanoseconds, and must be treated as high speed logic devices. The bypass capacitor must be as close to the supply pin as possible and connected to a solid ground plane, and preferably directly between the (V+) and GND pins.

Minimize coupling between outputs and inputs to prevent output oscillations. As shown in the figure below, it is "OK" to run input and output traces in parallel as long as there is a (V+) or GND trace between output to reduce coupling. A "better" way to reduce coupling is to have the traces ran further away from each other.

When series resistance is added to inputs, place the resistor close to the device. A low value (<100 ohms) resistor can also be added in series with the output to dampen any ringing or reflections on long, non-impedance controlled traces. For best edge shapes, controlled impedance traces with back-terminations must be used when routing long distances.

### 7.4.2 Layout Example

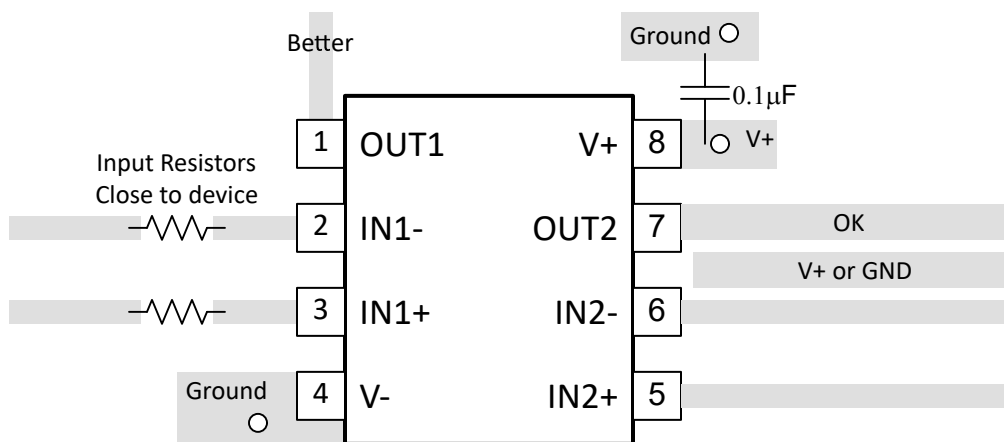


Figure 7-12. Dual Layout Example

## 8 Device and Documentation Support

### 8.1 Documentation Support

#### 8.1.1 Related Documentation

[Analog Engineers Circuit Cookbook: Amplifiers \(See Comparators section\) - SLYY137](#)

[Precision Design, Comparator with Hysteresis Reference Design— TIDU020](#)

[Window comparator circuit - SBOA221](#)

[Reference Design, Window Comparator Reference Design— TIPD178](#)

[Comparator with and without hysteresis circuit - SBOA219](#)

[Inverting comparator with hysteresis circuit - SNOA997](#)

[Non-Inverting Comparator With Hysteresis Circuit - SBOA313](#)

[A Quad of Independently Func Comparators - SNOA654](#)

### 8.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](http://ti.com). Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 8.3 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

### 8.4 Trademarks

TI E2E™ is a trademark of Texas Instruments.

All trademarks are the property of their respective owners.

### 8.5 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 8.6 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

## 9 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision * (September 2024) to Revision A (October 2024)	Page
• Updated quiescent current and input offset voltage specifications throughout document.....	1
• Release TLV1831_41_32_42-Q1 to production throughout datasheet.....	1

## 10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">TLV1831QDCKRQ1</a>	Active	Production	SC70 (DCK)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	1TO
<a href="#">TLV1832QDGRQ1</a>	Active	Production	VSSOP (DGK)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T32Q
TLV1832QDGRQ1.A	Active	Production	VSSOP (DGK)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	See TLV1832QDGRQ1	T32Q
<a href="#">TLV1832QPWRQ1</a>	Active	Production	TSSOP (PW)   8	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	TL32Q
TLV1832QPWRQ1.A	Active	Production	TSSOP (PW)   8	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	See TLV1832QPWRQ1	TL32Q
<a href="#">TLV1841QDCKRQ1</a>	Active	Production	SC70 (DCK)   5	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	1TQ
<a href="#">TLV1842QDGRQ1</a>	Active	Production	VSSOP (DGK)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T42Q
TLV1842QDGRQ1.A	Active	Production	VSSOP (DGK)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	See TLV1842QDGRQ1	T42Q
<a href="#">TLV1842QPWRQ1</a>	Active	Production	TSSOP (PW)   8	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T1842Q
TLV1842QPWRQ1.A	Active	Production	TSSOP (PW)   8	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	See TLV1842QPWRQ1	T1842Q

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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**OTHER QUALIFIED VERSIONS OF TLV1831-Q1, TLV1832-Q1, TLV1841-Q1, TLV1842-Q1 :**

- Catalog : [TLV1831](#), [TLV1832](#), [TLV1841](#), [TLV1842](#)

NOTE: Qualified Version Definitions:

- Catalog - TI's standard catalog product



# EXAMPLE BOARD LAYOUT

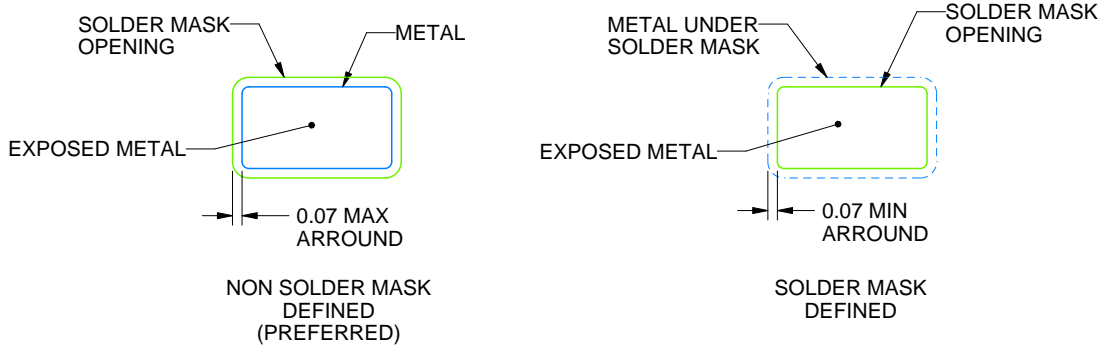
DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:18X



SOLDER MASK DETAILS

4214834/G 11/2024

NOTES: (continued)

- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 THICK STENCIL  
SCALE: 18X

4214834/G 11/2024

NOTES: (continued)

9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
10. Board assembly site may have different recommendations for stencil design.

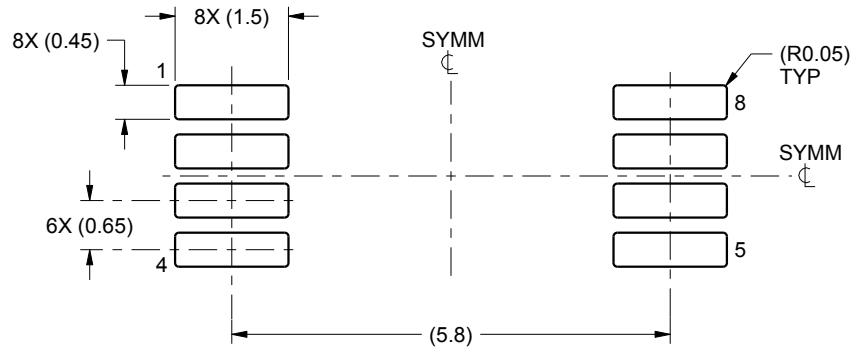


# EXAMPLE BOARD LAYOUT

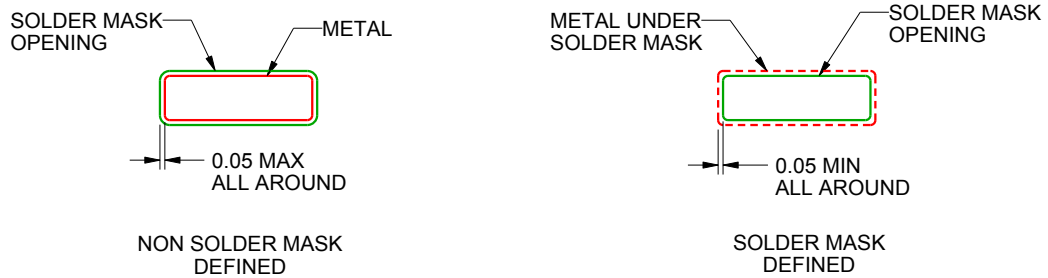
PW0008A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
SCALE:10X



SOLDER MASK DETAILS  
NOT TO SCALE

4221848/A 02/2015

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

PW0008A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:10X

4221848/A 02/2015

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

# DGK0008A



# PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



4214862/A 04/2023

**NOTES:**

PowerPAD is a trademark of Texas Instruments.

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

# EXAMPLE BOARD LAYOUT

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 15X



SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

# EXAMPLE STENCIL DESIGN

DGK0008A

<sup>TM</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
SCALE: 15X

4214862/A 04/2023

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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